

## Supplementary Information

### **Surface-modified piezoresistive nanocomposite flexible pressure sensors with high sensitivity and wide linearity**

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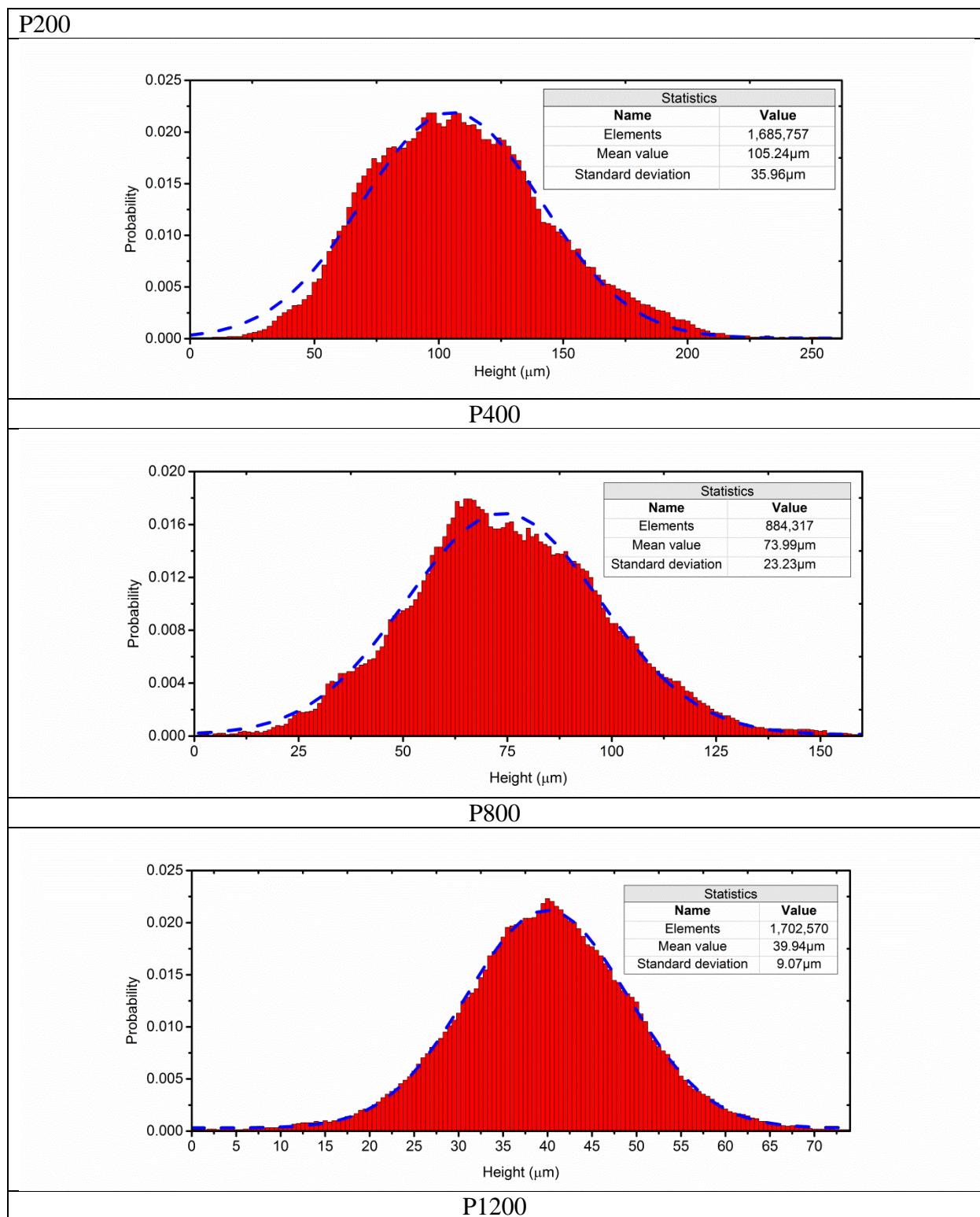
a Institute of Microelectronics, Tsinghua University, Beijing 100084, China. E-mail:  
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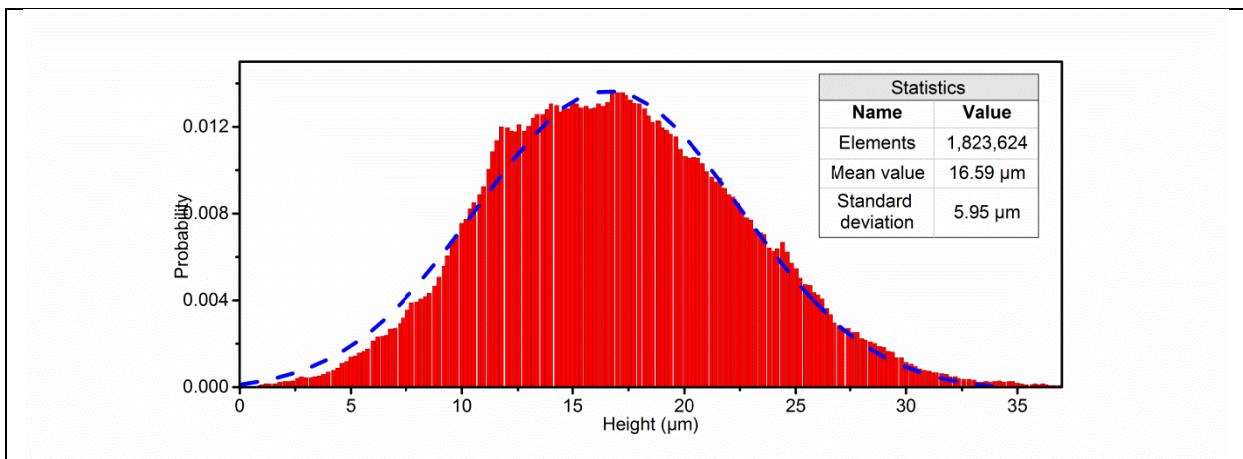
b Tsinghua National Laboratory for Information Science and Technology (TNList), Tsinghua University, Beijing 100084, China

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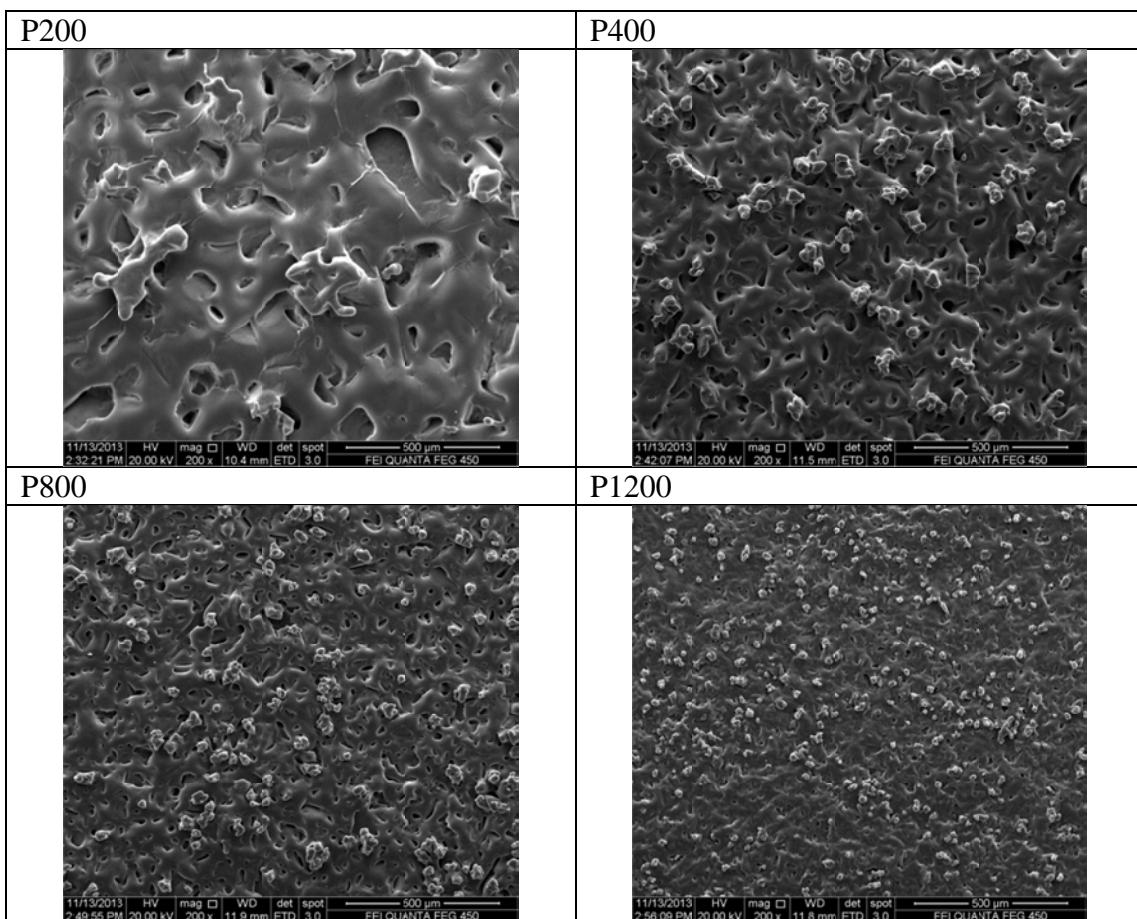
The surface measurement results of the samples with roughness grade P200 P400 P800 and P1200

a





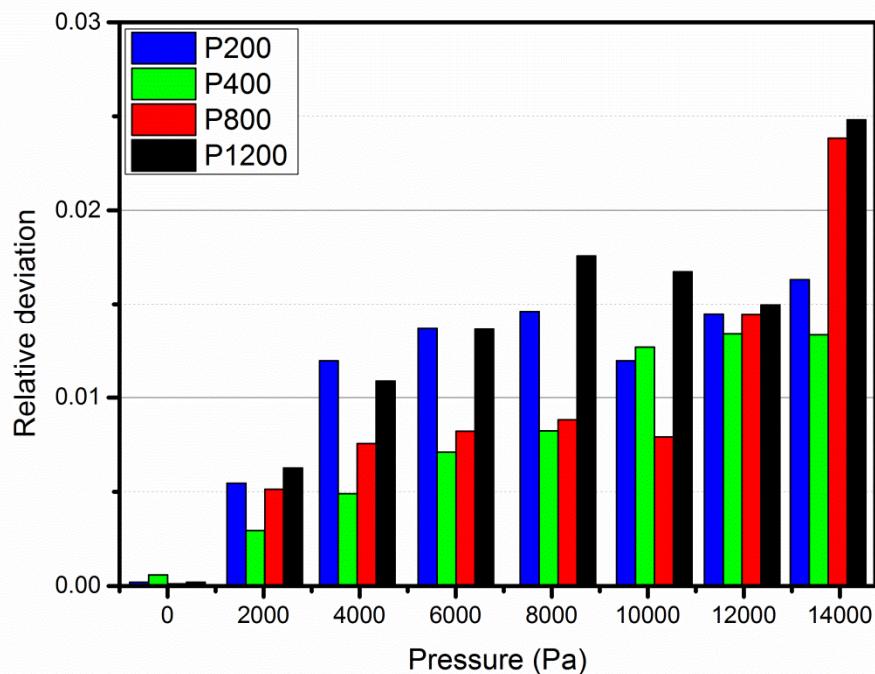
**b**



**Supplementary Figure S1** (a) The measured height distribution of the samples with mould grade P200, P400, P800 respectively; (b) The SEM photos of the corresponding samples.

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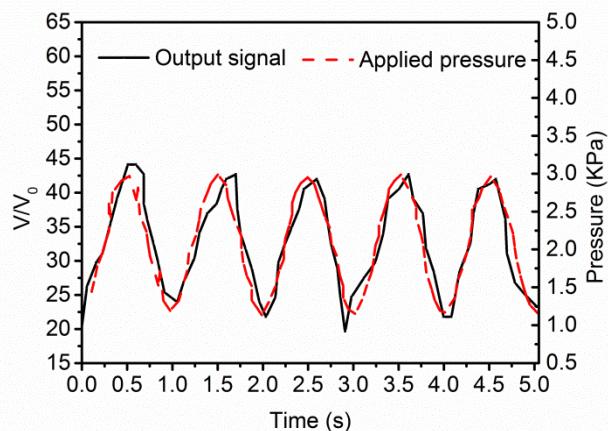
## Relative deviation of the four samples



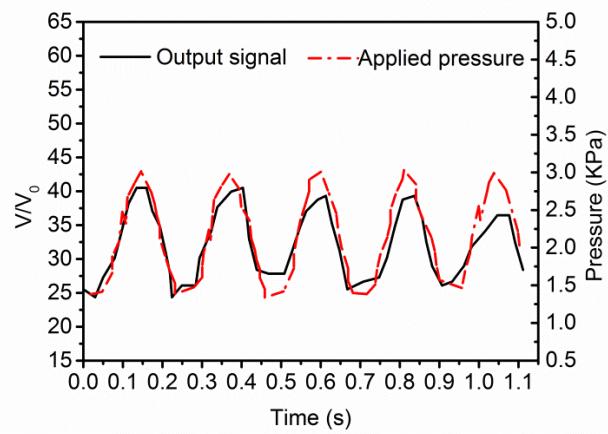
**Supplementary Figure S2** demonstrates the Relative deviation of four samples at different pressure levels, calculated by the division of the standard deviation by full scale measured value. The relative deviation can be worked out which are no more than 2.5% all along the working scale.

## Frequency response of the Device

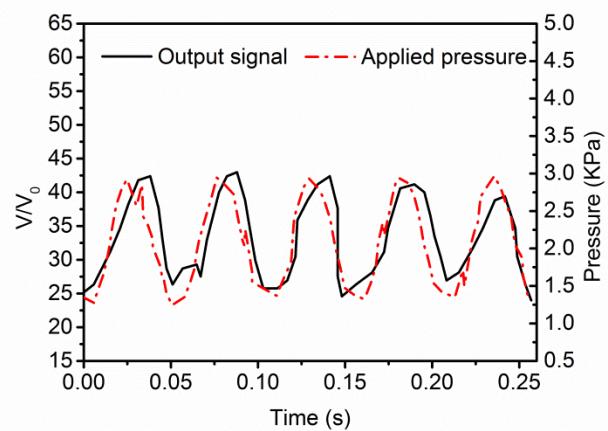
$f=1\text{Hz}$



$f=4.55\text{Hz}$



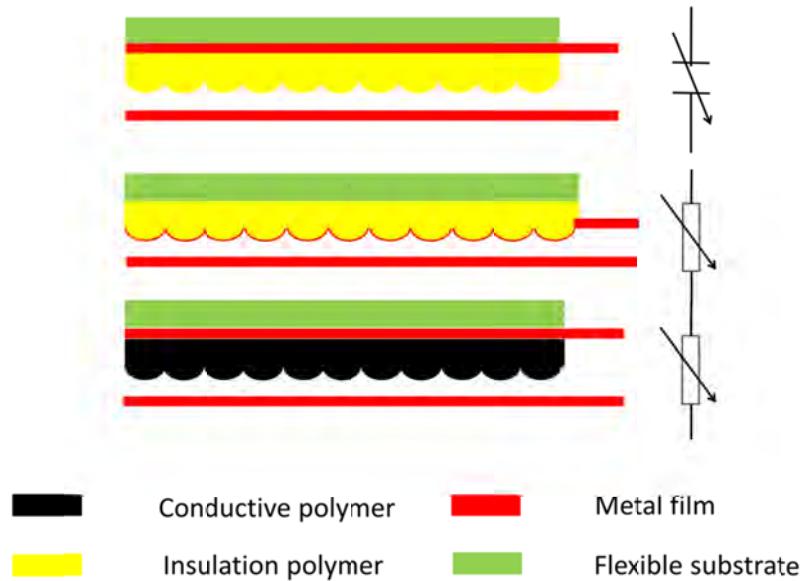
$f=19.2\text{Hz}$



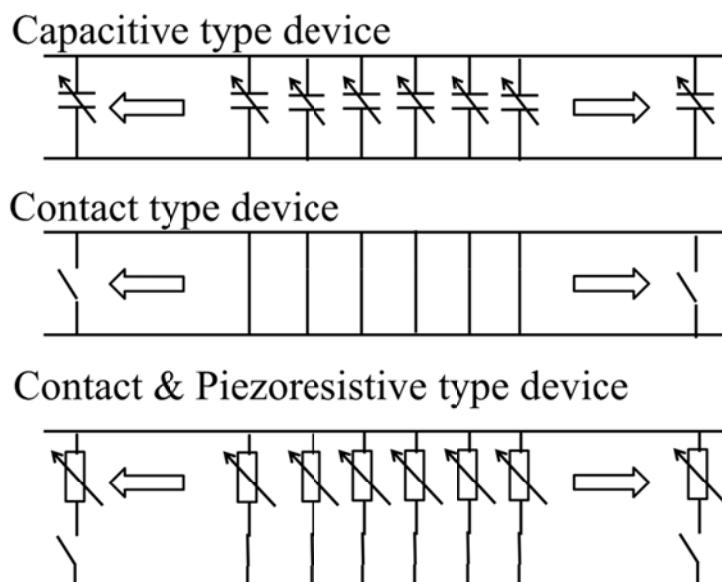
**Supplementary Figure S3** demonstrates the frequency response with the loading frequency 1Hz, 4.55Hz, 19.2 Hz respectively. The applied pressure wave and the response signals remain synchronous at low frequencies until the frequency reaches to almost 20Hz, an obvious delay of the output signals can be observed.

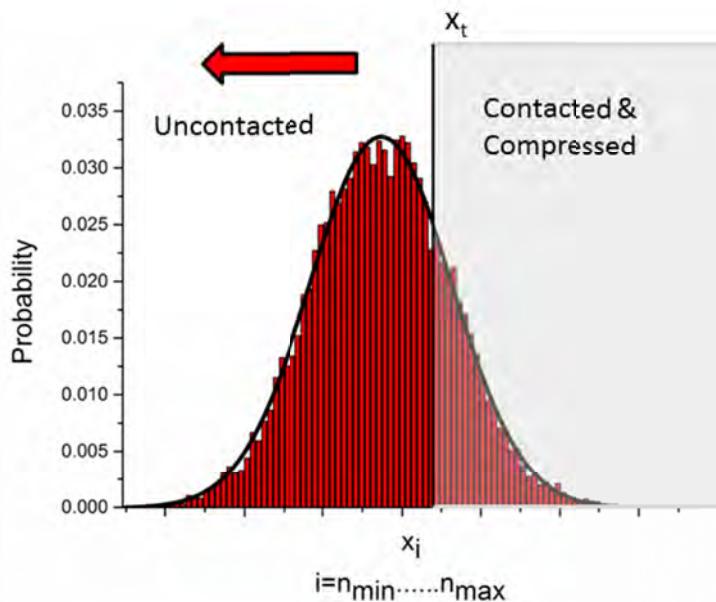
The equivalent circuit, physical image and equations used in the simulation

a



b



**c****d**

Capacitive type device

$$P(x_i) = S * \sum_{i=t}^{n_{\max}} [DF(x_i + \Delta x_i) - DF(x_i)] * p\left(\frac{x_i - x_t}{x_i}\right)$$

$$Ca(x_i) = S * \sum_{i=t}^{n_{\max}} [DF(x_i + \Delta x_i) - DF(x_i)] * \frac{\varepsilon_0 \varepsilon_p}{x_t}$$

$$+ S * \sum_{i=n_{\min}}^{t-1} [DF(x_i + \Delta x_i) - DF(x_i)] * \left[ \frac{1}{\frac{x_i}{\varepsilon_0 \varepsilon_p} + \frac{x_t - x_i}{\varepsilon_0}} \right]$$

Contact type device

$$P(x_i) = S * \sum_{i=t}^{n_{\max}} [DF(x_i + \Delta x_i) - DF(x_i)] * p\left(\frac{x_i - x_t}{x_i}\right)$$

$$Co(x_i) = S * \sum_{i=t}^{n_{\max}} [DF(x_i + \Delta x_i) - DF(x_i)]$$

Contact &amp; Piezoresistive type device

$$P(x_i) = S * \sum_{i=t}^{n_{\max}} [DF(x_i + \Delta x_i) - DF(x_i)] * p\left(\frac{x_i - x_t}{x_i}\right)$$

$$Cond(x_i) = S * \sum_{i=t}^{n_{\max}} [DF(x_i + \Delta x_i) - DF(x_i)] * \frac{1}{x_i} * cond\left(\frac{x_i - x_t}{x_i}\right)$$

**Supplementary Figure S5** (a) Three different working principles of the pressure sensor; (b) Equivalent circuits of three different working principles of the flexible pressure sensor; (c) Demonstration of a general physical picture (Take Gauss distribution as an example) when the micro structures are compressed to the height of  $x_t$ , all the portions with the height higher

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than  $x_t$  are compressed to the height of  $x_t$  with different strain degree depending on their original height, other portions remain original state; (d) The numerical models of these three different working principles.

The meanings of the symbols in these equations are listed below:

DF-Distribution functions of the micro-structured profile;

P-Pressure applied on the device

Ca-Capacitance of the device

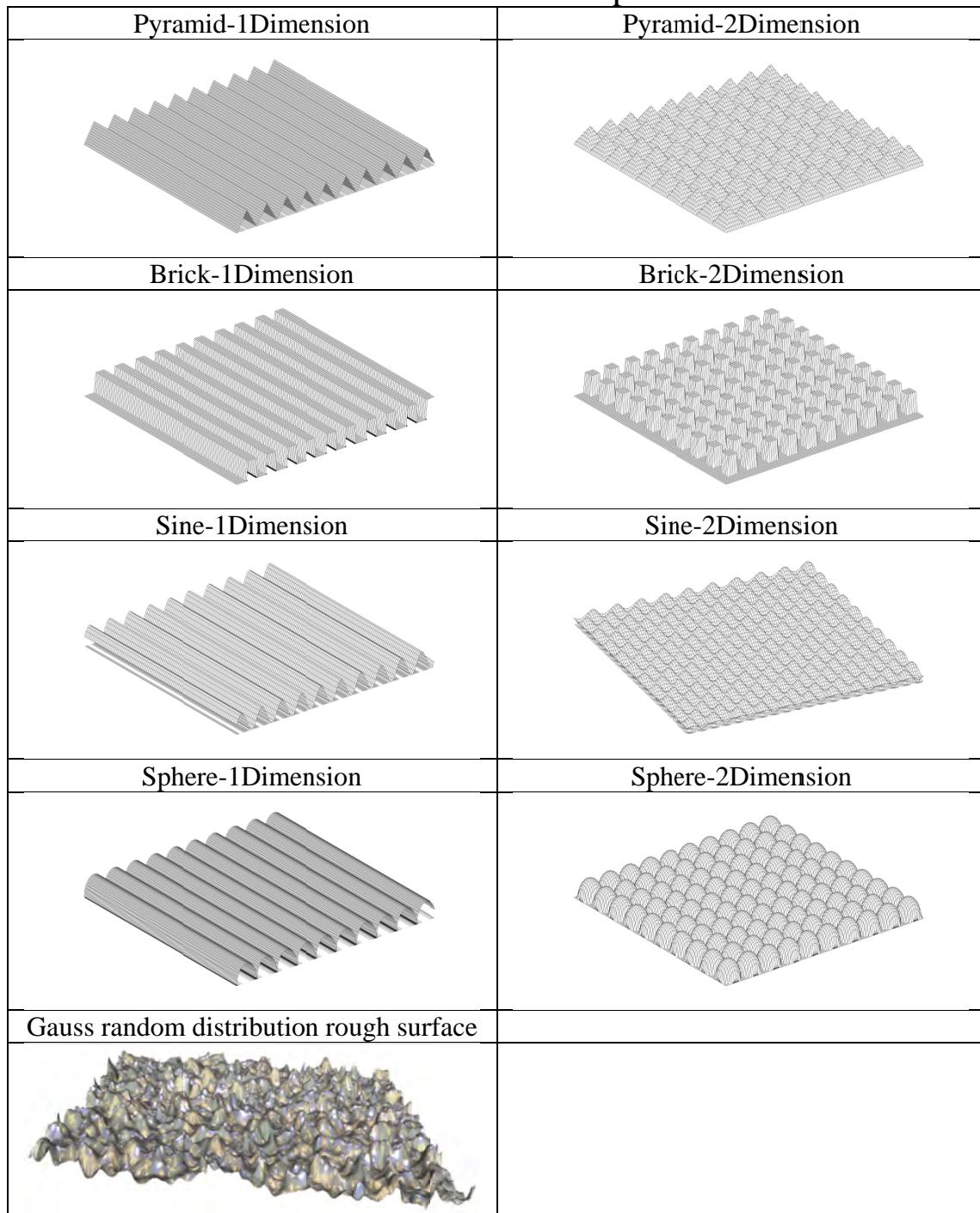
Co-Contact ration of the device

Cond-Conductivity of the device

p-bulk polymer materials' strain-stress property

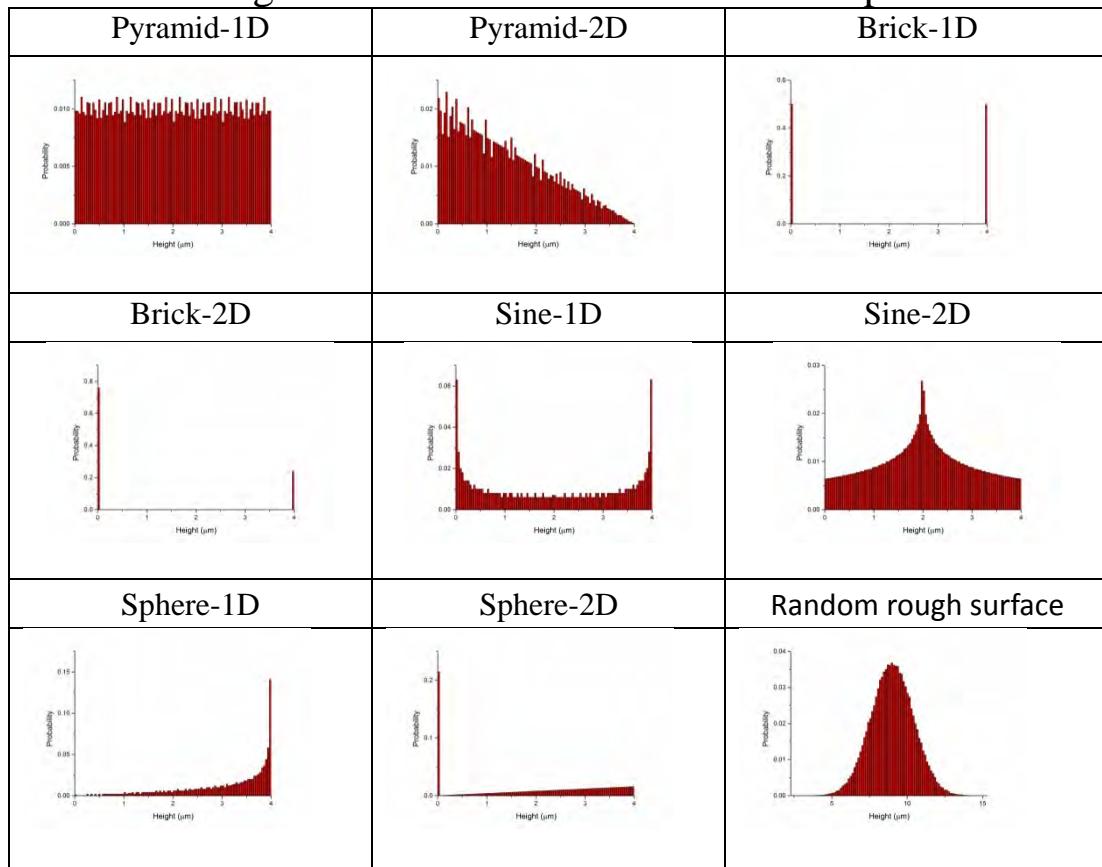
cond- bulk conductive polymer materials' piezoresistive property

## Demonstrations of 9 different profile models



**Supplementary Figure S6** Demonstrations of 9 different profile models. The Pyramid & Sphere structures have no gaps between them. The Sine wave-like surface profile obeys the Sinusoidal function. The two Brick structures' profile has the duty cycle of 1:1.

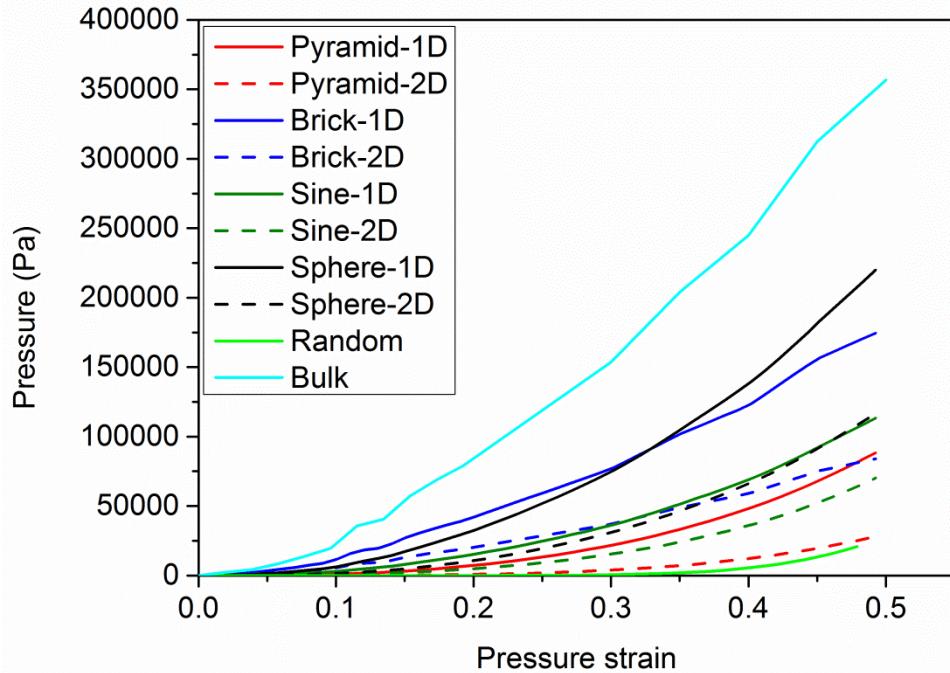
## The height distribution of different surface profiles



**Supplementary Figure S7** The height distribution of different surface profiles

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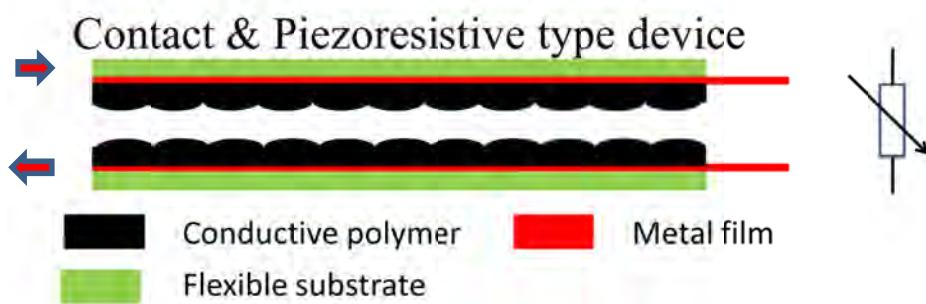
## The elastic responds of the different surface profiles



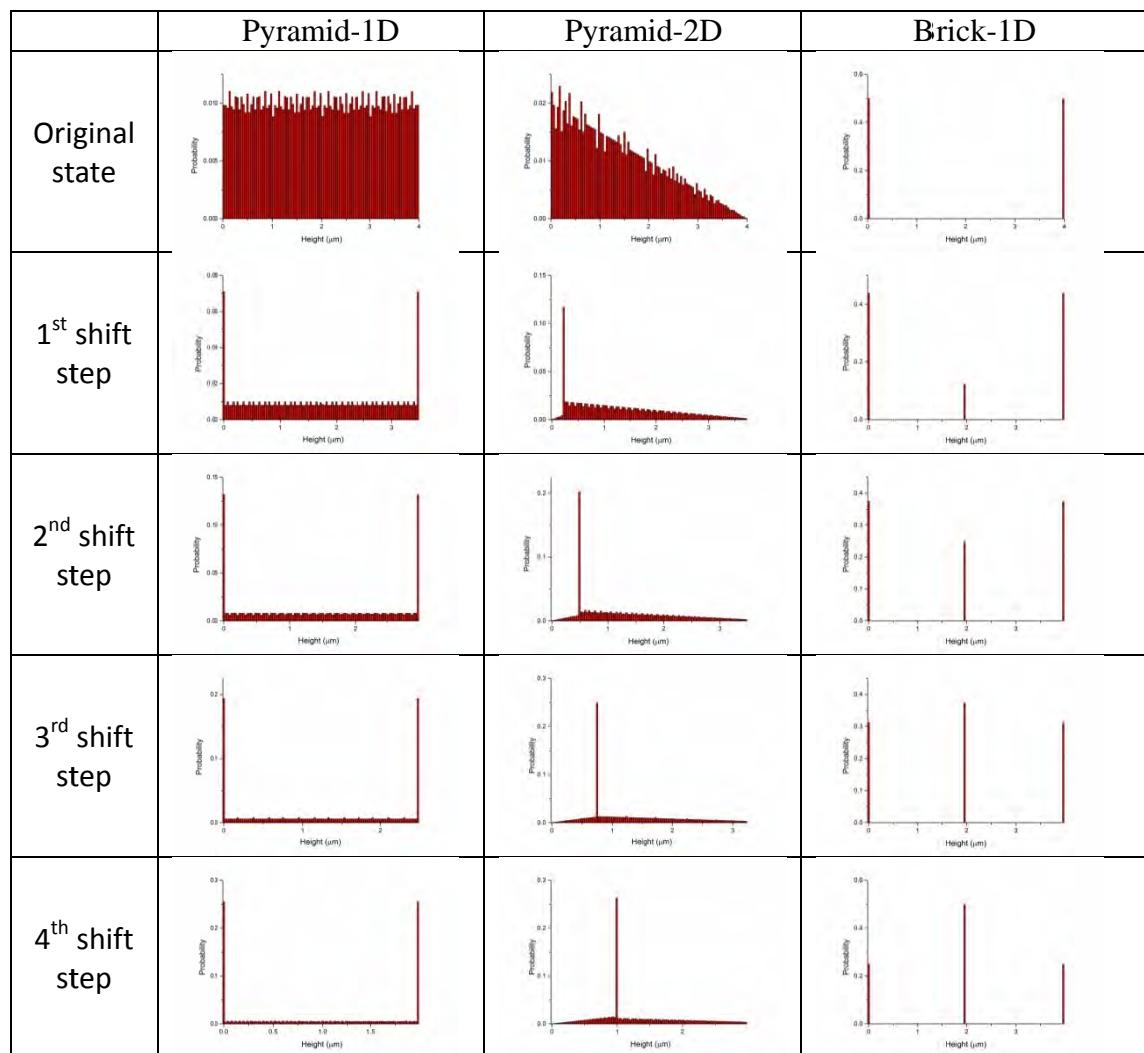
**Supplementary Figure S8** The elastic responds of the different surface profiles

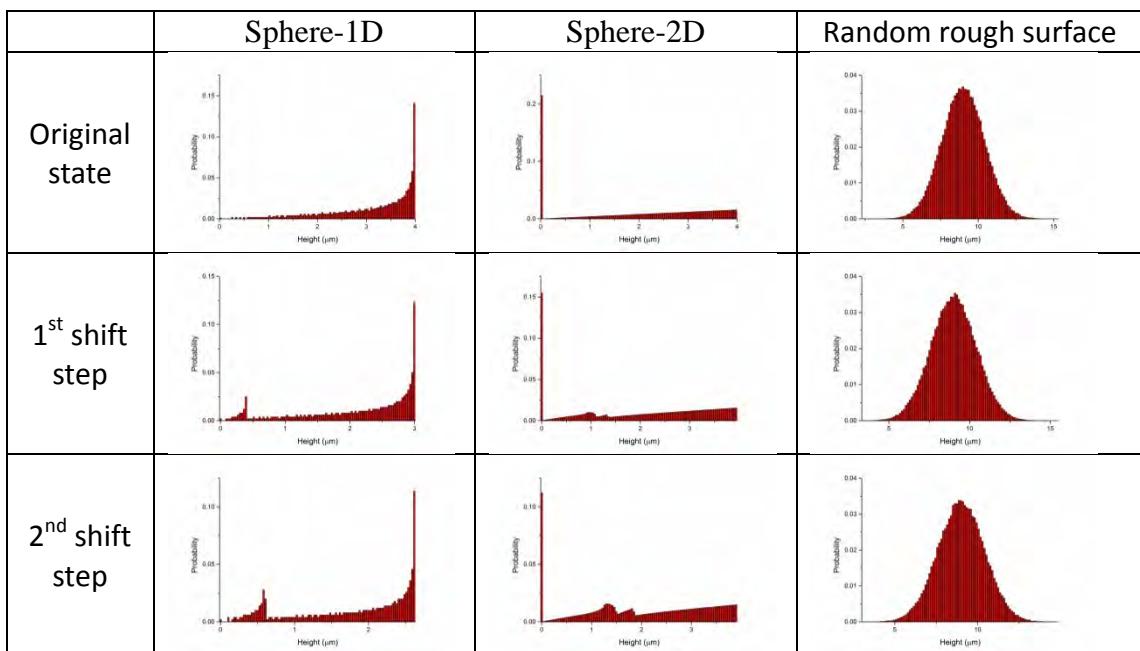
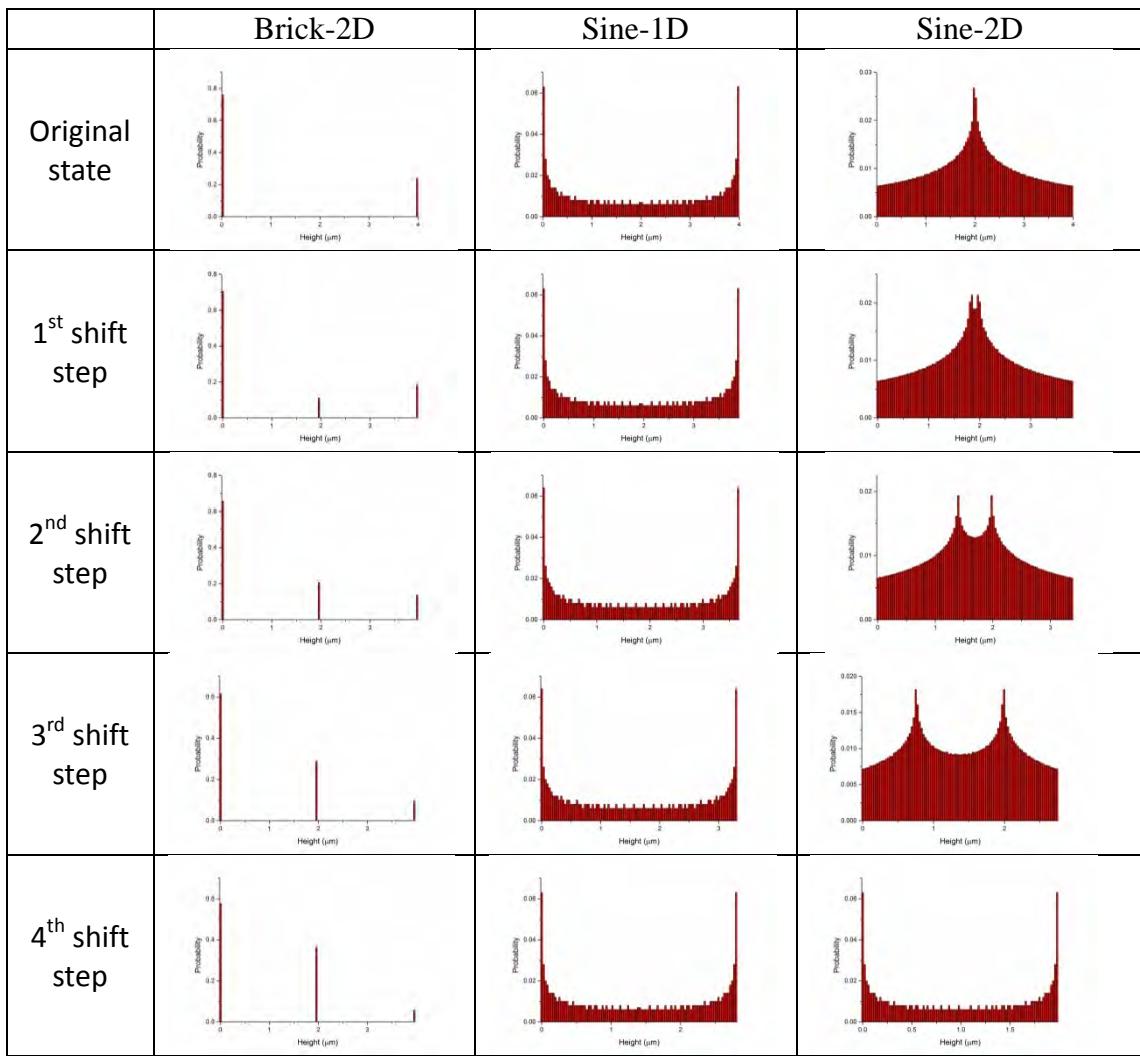
## Two layer device structures and their height distributions at different sliding steps

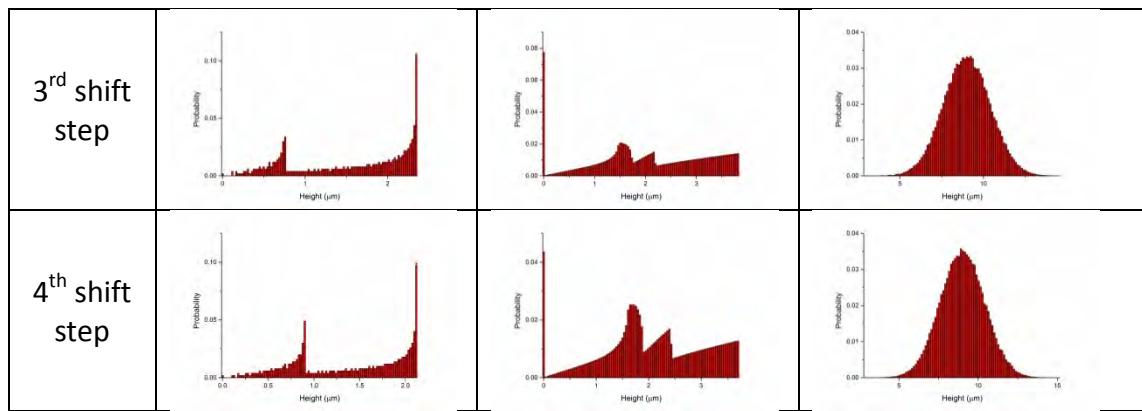
**a**



**b**

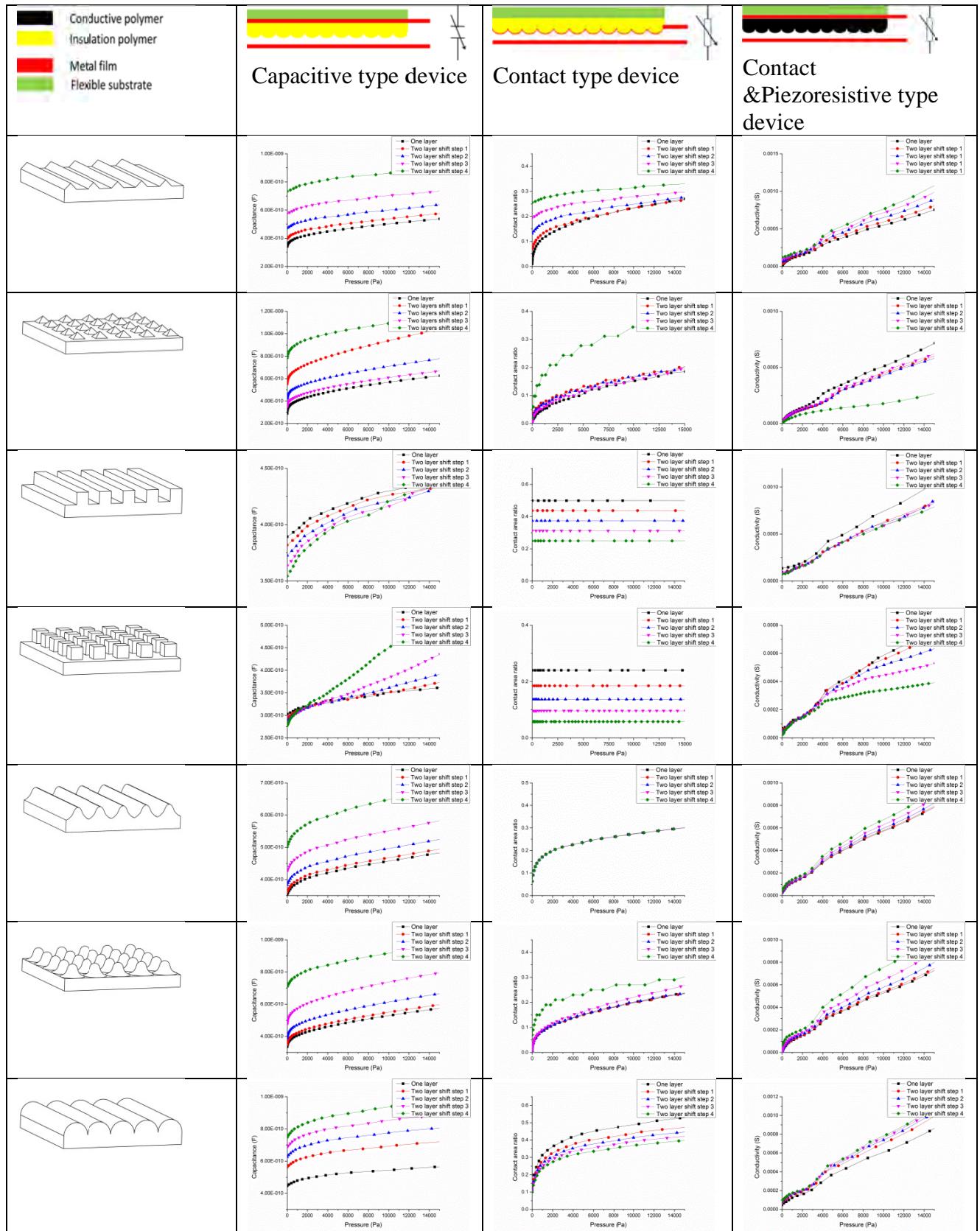


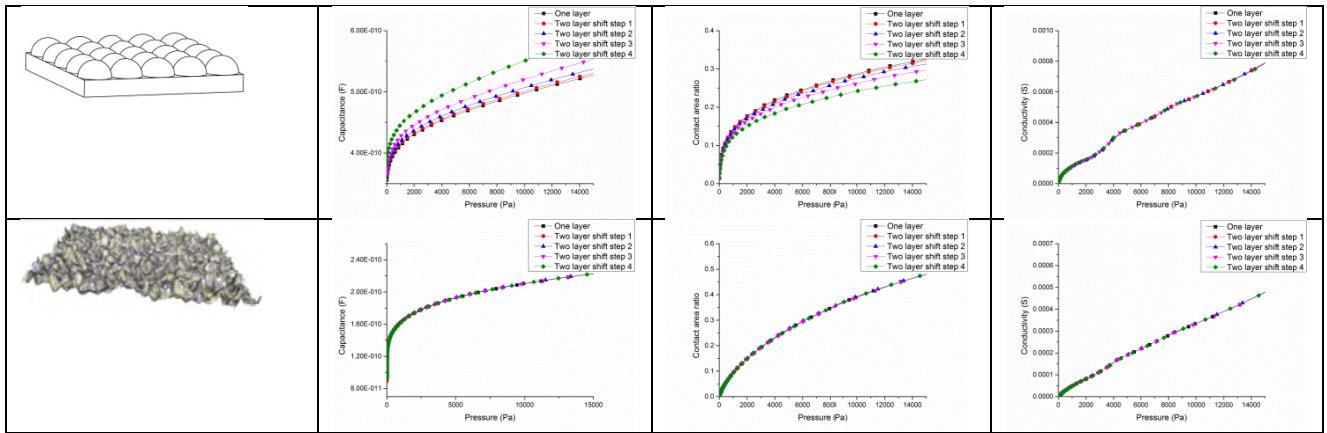




**Supplementary Figure S9** (a) Two layer device structures under the condition of lateral sliding; (b)The height distribution of different surface profiles in their original state and side sliding steps of two contact surfaces

# Stability performance comparison between different surface profiles and working principles

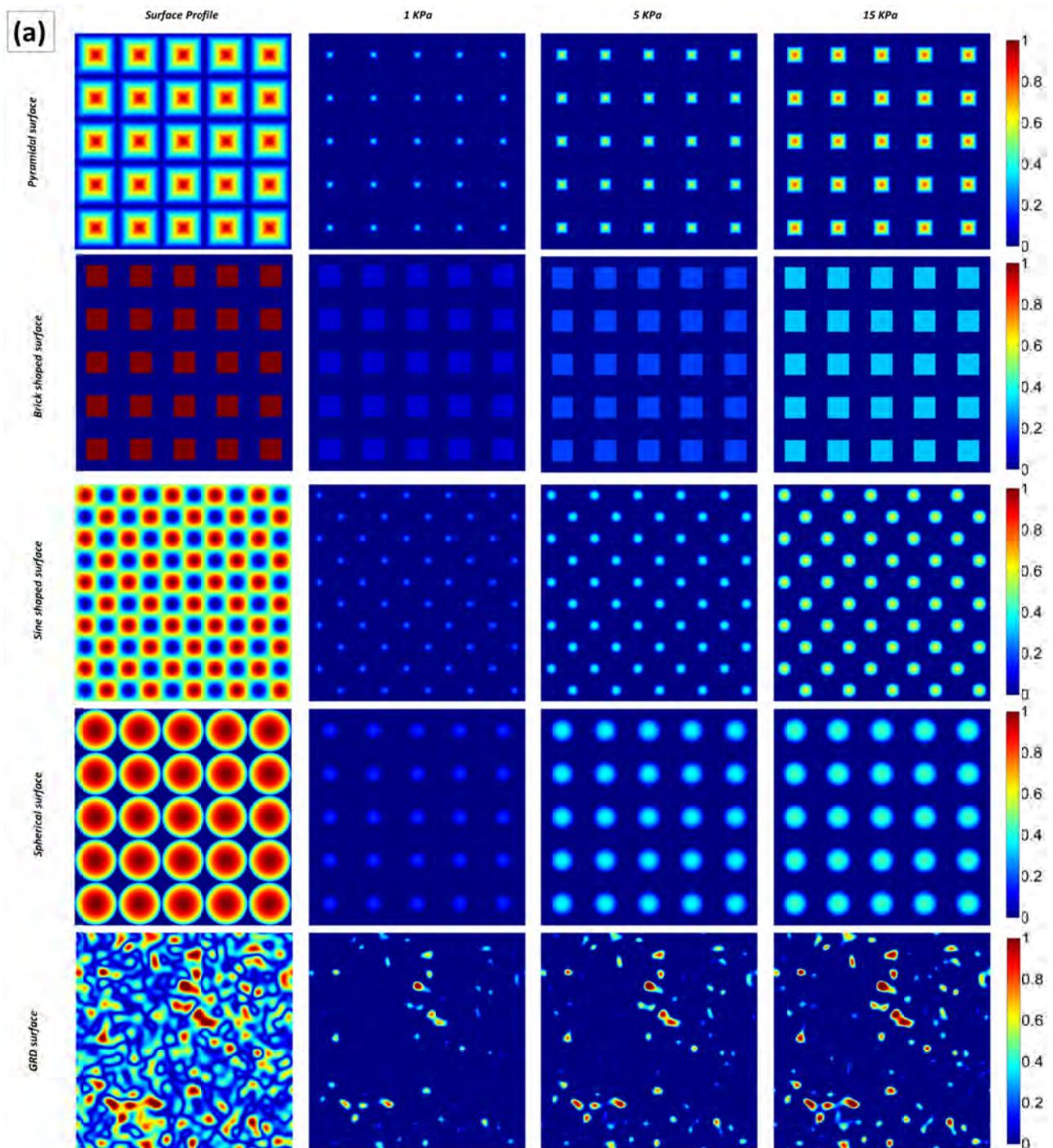


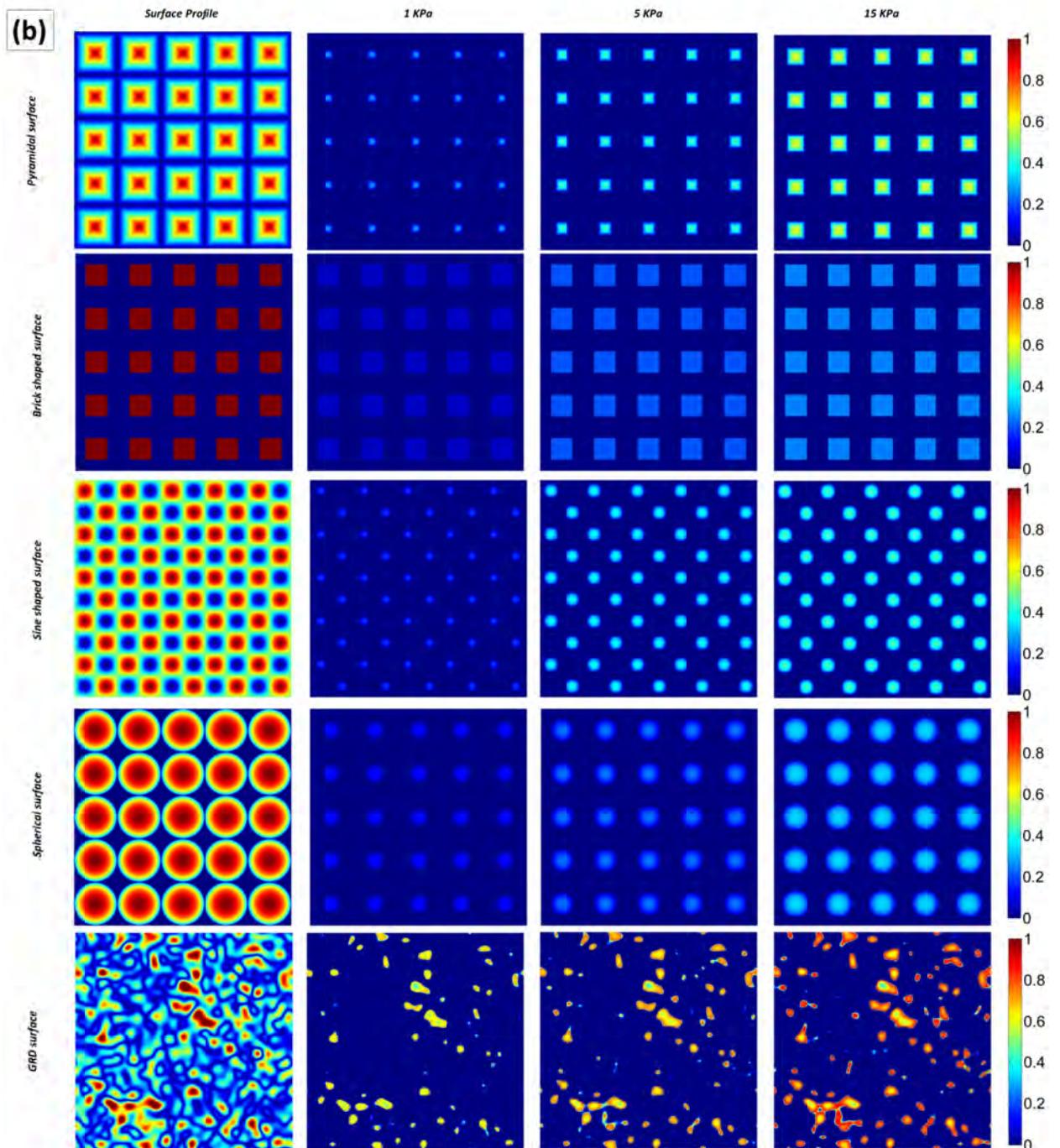


**Supplementary Figure S10** To investigate whether the two layer face to face structure have a stable performance when tangential shifts between two surface take place, numerical simulation is carried out at 4 shift steps with interval of  $\lambda/4$  along the cross-section direction for 1D profile and diagonal direction for 2D profile. There are also calculated initial performance data for comparison. 9 different surface profiles and 3 working principles are included in this simulation.

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The comparison between different profiles with pressure mappings and conductance mappings

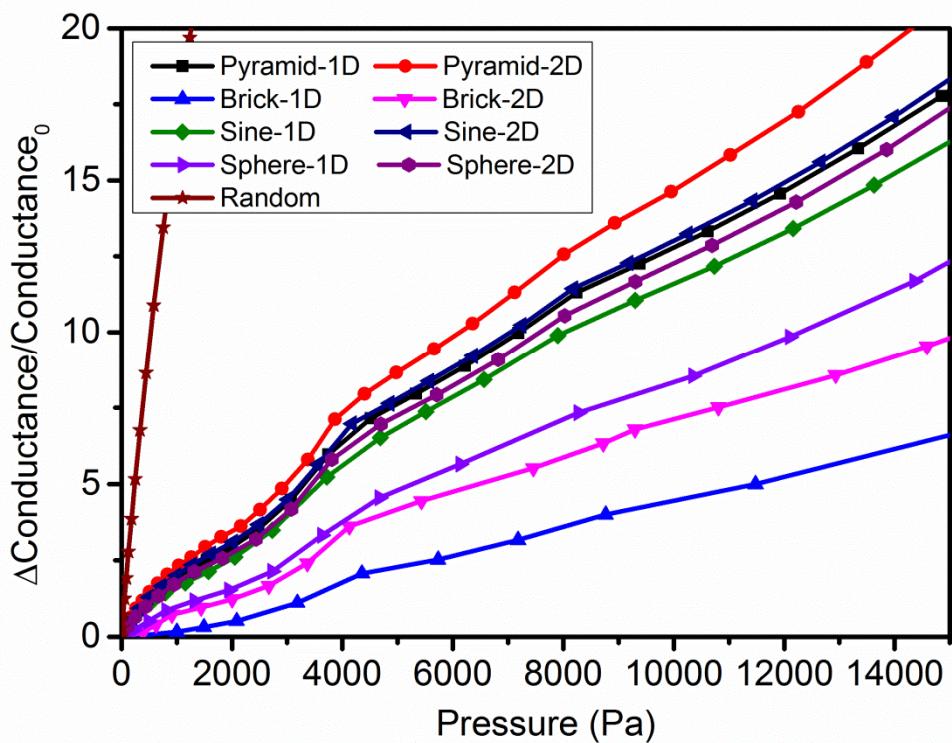
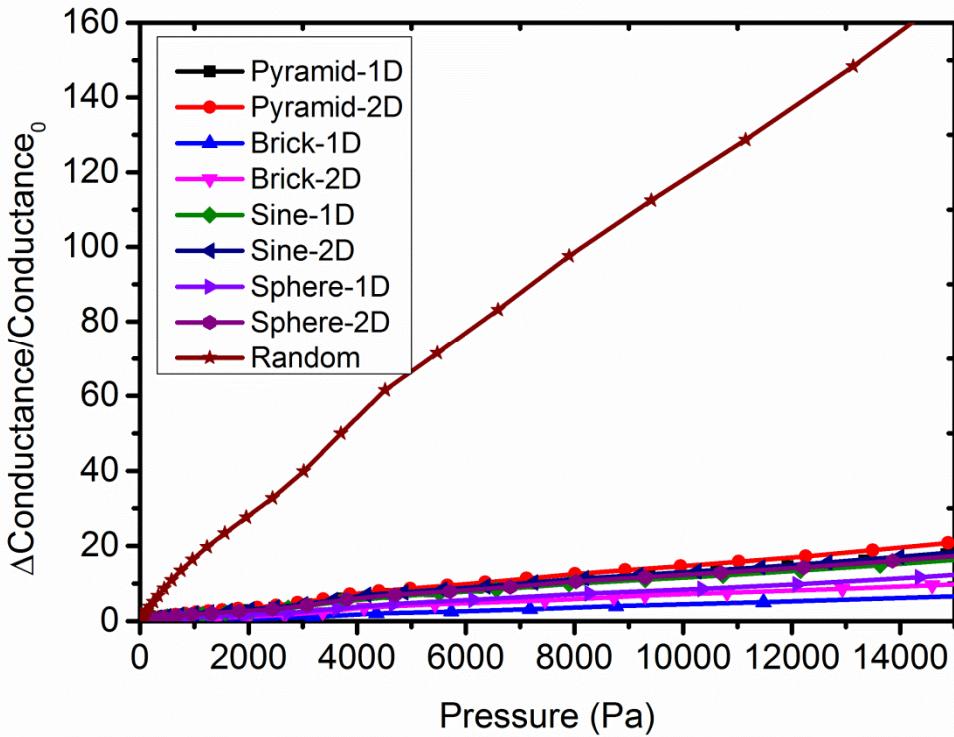




**Supplementary Figure S11** The comparison between different profiles with (a) pressure mappings and (b) conductance mappings at different pressure levels.

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## The simulated performance comparison between surface profiles



**Supplementary Figure S12** The simulated performance comparison between surface profiles  
(a)Overall plot (b)Magnified plot.