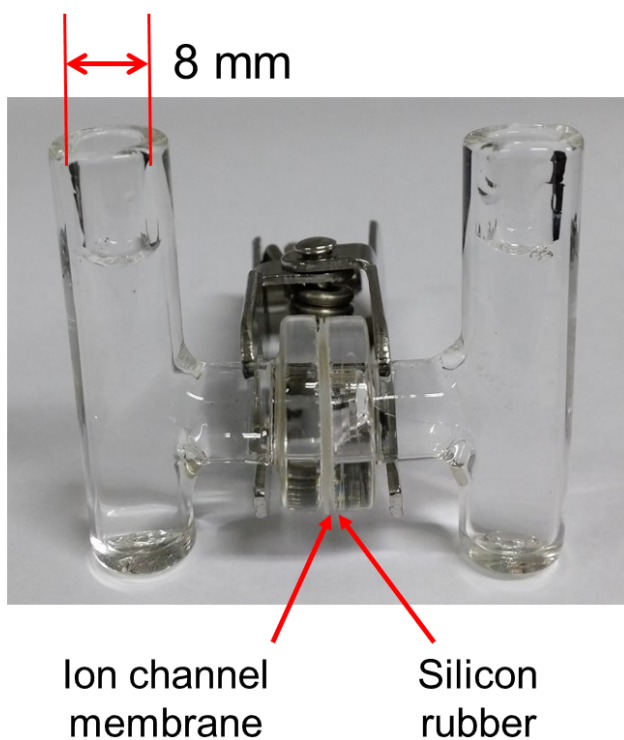


## Electronic Supplementary Information

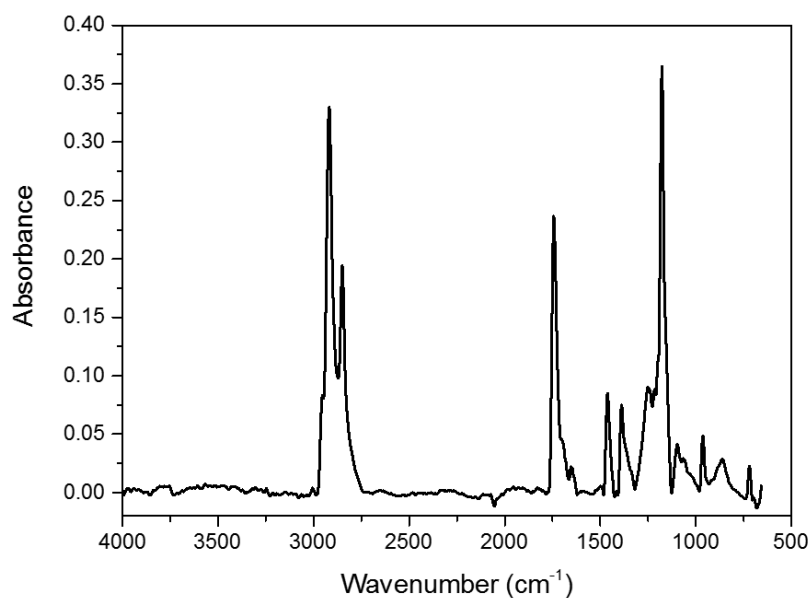
### Patchable, flexible heat-sensing hybrid ionic gate nanochannel modified with wax-composite

Kyoung-Yong Chun, Wook Choi, Sungchul Rho, Chang-Soo Han\*



**Fig. S1.** An experimental cell for the measurement of ionic current.

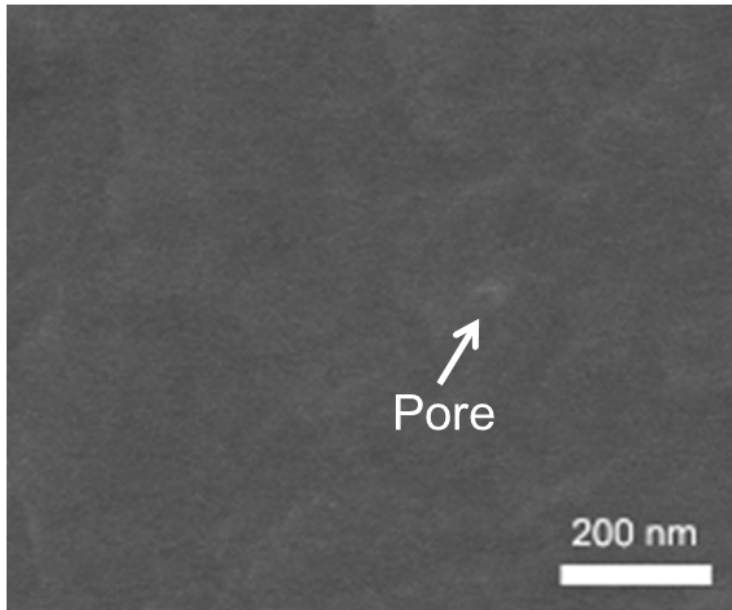
Long-chain hydrocarbons with C–H stretching vibrations of saturated hydrocarbons of wax are seen at 2918 and 2850  $\text{cm}^{-1}$ , carbonyl (C=O) stretching vibration from free carboxylic acid and from esters in region of 1740  $\text{cm}^{-1}$ ,  $-\text{CH}_3$  and C–H deformations at about 1460  $\text{cm}^{-1}$  and 1390  $\text{cm}^{-1}$ . Rocking and wagging of  $-\text{CH}_2-$  gives a clear peak at 720  $\text{cm}^{-1}$ .<sup>1</sup> The peaks at 2,850, 2,920, and 1,465  $\text{cm}^{-1}$  for stretching of  $-\text{CH}_3$  and  $-\text{CH}_2$  remain in mid ethylene–butylene (EB) block of SEBS are not observed or overlapped indicating that wax preferentially enter and swell EB segments.<sup>2,3</sup> Also, the doublet at 2924 and 2854  $\text{cm}^{-1}$  can be overlapped to asymmetric C–H stretching of methyl and methylene groups in SEBS.



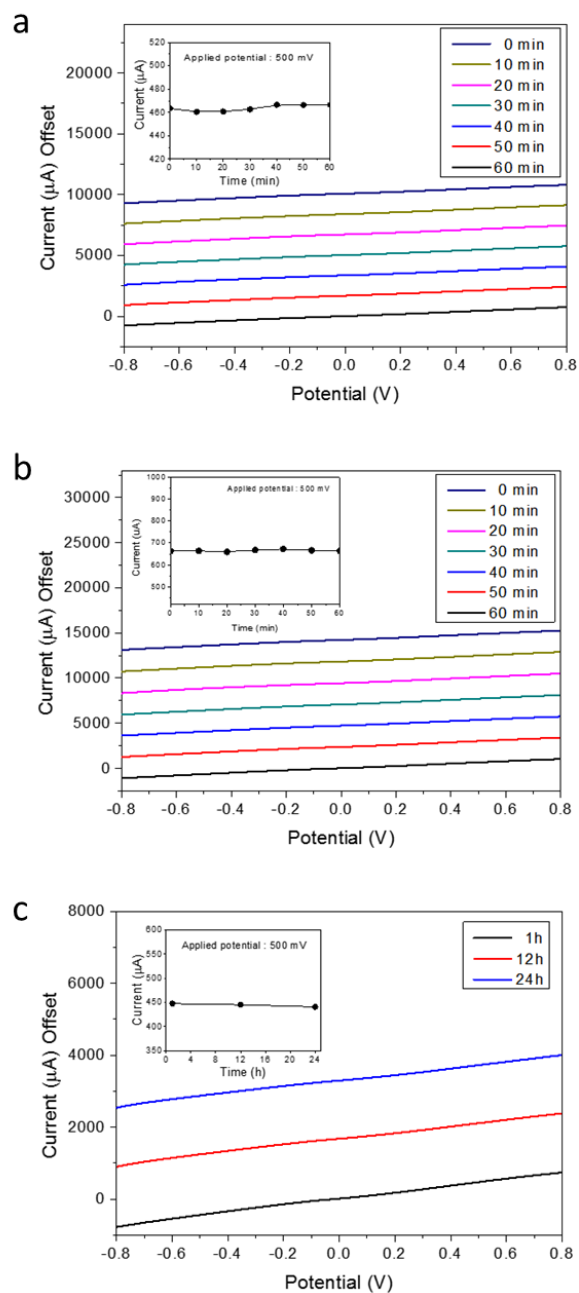
**Fig. S2.** Polarized infrared external reflectance spectra of wax-SEBS composite layers.

## References

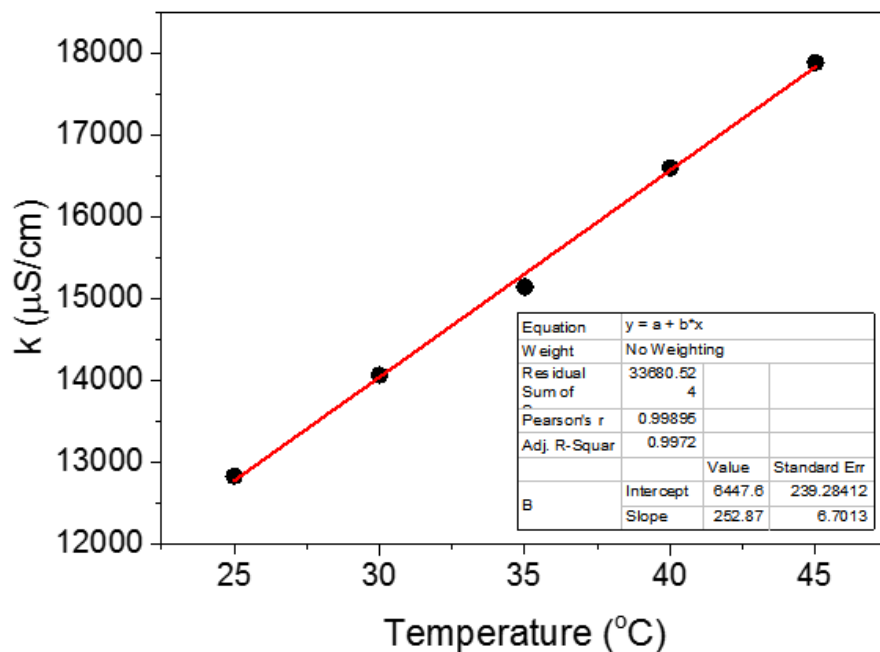
- [1] A. B. Paterakis, *J. the Am. Inst. for Conser.* **2003**, *42*, 313.
- [2] A. Ganguly, A. K. Bhowmick, *Nanoscale Res. Lett.* **2008**, *3*, 36.
- [3] S. Song, J. Feng, P. Wu, *Macromol. Rapid Commun.* **2011**, *32*, 1569.



**Fig. S3.** SEM image of a part of PCTE/wax-SEBS surface.



**Fig. S4. Time dependence of the ionic current vs. potential through the PCTE membrane.** (a) at 23 °C, (b) 41 °C (inset: ionic current vs. operation time). (c) Current flow vs. potential for longer time (1, 12, and 24h) at applied voltage of 500 mV.



**Fig. S5.** The plot from the recommended electrolytic conductivity ( $\kappa$ ) values for 0.1 mol aqueous potassium chloride solutions at temperatures from 25 to 45 °C.<sup>1</sup> All  $k$  values are given in units of  $\mu\text{S cm}^{-1}$ .

### Reference

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### The simulation of current change according to the temperature

Generally, the flowing current into the channel is expressed as followed equation.

$$i = \sigma \frac{A}{L} V \quad (1)$$

Where  $\sigma$  is proportional constant,  $A$  channel area,  $L$  channel length,  $V$  the voltage.

From equation (1),  $A$  and  $L$  is fixed. If  $V$  is constantly given, current  $i$  is dependent on  $A$ .

Therefore,

$$di = dA \quad (2)$$

However, if the volume expansion coefficient of wax is  $C$ ,

$$\frac{dV / V}{dT} = C \quad (3)$$

From (3), if the thermal expansion of wax composite is applicable to the geometry of Figure 2E

and

$$\frac{dV}{V} = CdT \quad (4)$$

where  $V$  is the volume of composite of wax-SEBS and  $T$  temperature.

As shown in Figure 2E, the volume of wax-SEBS in the height  $L$  can expressed as following. We just consider the volume expansion of wax composite in the x direction.

$$V = \pi(r_0^2 - r_i^2)L \quad (5)$$

Then,

$$dV = -2\pi r_i dr_i L \quad (6)$$

From (4) and (6), we get

$$dV = VCdT = \pi(r_0^2 - r_i^2)L \cdot C \cdot dT = -2\pi r_i dr_i L \quad (7)$$

and

$$-2r_i dr_i = C(r_0^2 - r_i^2)dT \quad (8)$$

Therefore, we get

$$\frac{-2r_i}{r_0^2 - r_i^2} dr_i = CdT \quad (9)$$

Channel area A is

$$A = \pi r_i^2 \quad (10)$$

This means

$$dA = 2\pi r_i dr_i \quad (11)$$

Also, from (1) and (2), the small change of current, is

$$di = \sigma \frac{V}{L} dA \quad (12)$$

From (11) and (12),

$$di = \sigma \frac{V}{L} 2\pi r_i dr_i \quad (13)$$

From (9),  $dr_i = \frac{r_0^2 - r_i^2}{-2r_i} CdT$  then substitute into (13) to get

$$di = -\pi\sigma \frac{V}{L} (r_0^2 - r_i^2) CdT \quad (14)$$

From (14),  $r_i$  can be expressed as the function of  $T$ . If equation (9) is integrated,  $r_i$  is obtained as  $f(T)$ ,

$$\int \frac{-2r_i}{r_0^2 - r_i^2} dr_i = \int CdT \quad (15)$$

In this experiment, the volume of mixture is expanded as increasing the temperature. Then,

$$\int \frac{-2r_i}{r_0^2 - r_i^2} dr_i = -\int CdT \quad (16)$$

The left side of the equation becomes

$$\int \frac{-2r_i}{r_0^2 - r_i^2} dr_i = \ln(r_i^2 - r_0^2) \quad (17)$$

The right side of the equation becomes

$$\int -CdT = -CT \quad (18)$$

From (17) and (18),

$$\ln(r_i^2 - r_0^2) = -CT + c_1 \quad (19)$$

and

$$r_i^2 - r_0^2 = e^{-CT+c_1} = c_2 e^{-CT} \quad (20)$$

Then,

$$r_i^2 = r_0^2 + c_2 e^{-CT} \quad (21)$$

Substitute (21) into (14) to get

$$di = -\pi\sigma \frac{V}{L} \left\{ r_0^2 - (r_0^2 + c_2 e^{-CT}) \right\} C dT$$

$$\pi\sigma \frac{V}{L} c_2 e^{-CT} C dT = c_3 e^{-CT} dT \quad (22)$$

If the temperature changes from  $T_0$  to  $T$ , the current change is obtained by integrating (22)

$$i \Big|_0 = -\frac{c_3}{C} e^{-CT} \Big|_0 \quad (23)$$

$$i - i_0 = c_4 (e^{-CT} - e^{-CT_0}) \quad (24)$$

Therefore,

$$i = i_0 + c_4 (e^{-CT} - e^{-CT_0}) \quad (25)$$

$$i = i_0 + c_5 (e^{-T} - e^{-T_0}) \quad (26)$$