Supplementary information to

# General interpretation and theory of apparent height in dynamic atomic force microscopy

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# A. Equation of motion

In AM AFM the equation of motion can be written as

$$\frac{k}{\omega_0^2} \mathcal{B}(t) + \frac{k}{Q\omega_0} \mathcal{B}(t) + kz = F_0 \cos(\omega t) + F_{ts}$$
(S1)

where higher flexural modes of oscillation are ignored, z is the instantaneous tip position, k is the spring constant, Q is the Q factor due to dissipation with the medium,  $\omega_0$  is the angular natural frequency, the effective mass is m=k/( $\omega_0$ )<sup>2</sup>,  $\omega$  is the angular drive frequency and F<sub>0</sub> is the magnitude of the driving force (typically  $\omega = \omega_0$ ).

# **B.** Tip displacement

The general response z can be written as a Fourier series as

$$z(t) = z_0 + A\cos(\omega t - \phi) + O(\varepsilon)$$
(S2)

where  $z_0$  is the mean cantilever deflection.

#### C. Transfer function

By neglecting higher harmonics  $O(\varepsilon)$  and by first multiplying (1) by z(t) and its derivative  $\dot{z}(t)$  and by then integrating over a cycle one arrives to the transfer function<sup>1-3</sup>

$$A_{r} = \frac{\frac{1}{Q}}{\sqrt{\left(-2\frac{V}{kA}\right)^{2} + \left(\frac{1}{Q} + \frac{E_{ts}}{\pi kA^{2}}\right)^{2}}}$$
(S3)

where  $A_r = A/A_0$  is the normalized amplitude,  $A_0$  is the free oscillation amplitude, V stands for Virial (V= $\langle F_{ts} \times z \rangle$ ) and  $E_{ts}$  stands for the energy dissipated per cycle in the interaction. From (S3) it follows that V and  $E_{ts}$  control  $A_r$ . The terms  $E_{ts}$  and V are defined as

$$E_{ts}(z_c) = \oint F_{ts} z \, dt \approx \frac{\pi k A(z_c) A_0}{Q} \left[ \sin \phi(z_c) - \frac{A(z_c)}{A_0} \right]$$
(S4)

$$V_{sur}(z_c) = \frac{1}{T} = \oint F_{ts} z dt \approx -\frac{kA(z_c)A_0}{2Q} \cos\phi(z_c)$$
(S5)

where  $z_c$  is the cantilever separation.

# D. The virial

In the absence of the sample the virial of (5) gives (accounting for  $z_0$  and the fundamental frequency)

$$V_{sur}(z_c) \approx \frac{R_t H_{sur}}{6A} \left[ \left(\frac{z_c}{A}\right)^2 - 1 \right]^{-3/2} \left[ 1 - \frac{z_c z_0}{A^2} \right]$$
(S6)

where  $R_t$  is the radius of the tip and  $H_{sur}$  is the Hamaker of the tip-surface system. Then, from (S5) and (S6)<sup>1</sup>

$$z_c \approx A \left( D \left[ 1 - \frac{z_c z_0}{A^2} \right]^{2/3} + 1 \right)^{1/2}$$
 (S7)

where

$$D = \sqrt[3]{\frac{\left(\frac{QR_{tip}H}{3kA_0^3}\right)^2}{\left(A_r^4 - A_r^6\right)}}$$
(S8)

The resulting net virial from (9) accounting from the net interaction in the presence of the sample, i.e.  $V_{sur-sam}(z^*_{c}, h) = V_{sur}(z^*_{c}, h) + V_{sam}(z^*_{c})$ , is

$$V_{sur-sam}(z_{c}^{*},h) = \frac{R_{t}H_{sur}}{6A} \left[ \left(\frac{z_{c}^{*}+h}{A}\right)^{2} - 1 \right]^{-3/2} \left[ 1 - \frac{(z_{c}^{*}+h)z_{0}}{A^{2}} \right] + \frac{R^{*}H_{sam}}{6A} \left[ \left(\frac{z_{c}^{*}}{A}\right)^{2} - 1 \right]^{-3/2} \left[ 1 - \frac{z_{c}^{*}z_{0}}{A^{2}} \right]$$
(S9)

where  $V_{sur}(z_c^*, h)$  accounts for the tip-supporting surface interaction and  $V_{sam}(z_c^*)$  for the tipsample interaction in the presence of the sample.

The result is that (S7) and (S9) are the expressions that together with the main constraint in (4) give place to the two separations that can be employed to compute the error in apparent height when the mean deflection cannot be neglected, for example in liquid environments and/or where samples or surfaces are very compliant<sup>4</sup>.

# Reference

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