## Supplementary Information for

## Designed synthesis of Zr-based ceria-zirconia-neodymia composite with highly thermal stability and its enhanced catalytic performance for Rh-only three-way catalyst

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Table S1. BET surface area for several advanced ceria-zirconia mixed oxides with different preparation methods and thermal treatment.

Structure	Preparation method	Thermal treatment	Surface area (m <sup>2</sup> ·g <sup>-1</sup> )	Reference
	Co-precipitation combined	600 °C/3 h in air	92	
$Ce_{0.15}Zr_{0.85}O_2$	with mechanical mixing of N235	1000 °C/5 h in air	31	This work
$Ce_{0.15}Zr_{0.85}O_2$		600 °C/3 h in air	71	
$Ce_{0.18}Zr_{0.82}O_2$	Co-precipitation	1000 °C/5 h in air	13	This work
		700 °C/5 h in air	92	
Ce <sub>0.65</sub> Zr <sub>0.35</sub> O <sub>2</sub>	Continuous hydrothermal synthesis in supercritical water	1000 °C/6 h in H <sub>2</sub> and 1000 °C/6 h in O <sub>2</sub>	20	Reference [2]
	Co-precipitation method	500 °C in air	97	
$\mathrm{Ce}_{0.2}\mathrm{Zr}_{0.8}\mathrm{O}_2$	combined with supercritical drying technology	1100 °C/4 h in air	28	Reference [20]
Ce <sub>0.68</sub> Zr <sub>0.32</sub> O <sub>2</sub>	CTAB-assisted precipitation technique	900 °C/2 h in air	40	Reference [30]

Ce-Zr-Pr-O <sub>2</sub>	Conventional co-precipitation	500 °C/4 h in air	100	Deference [10]
(Ce/Zr=1/8)	method	1100 °C/4 h in air	10	Kelelence [19]
Ceo (77to oc Oc	Co-precipitation and	600 °C/4 h in air	55	Reference [15]
CC0.67Z10.33C2	supercritical drying method	1100 °C/4 h in air	8	Kererenee [15]
$CeZr_2O_x$	Homogeneous precipitation method	500 °C/3 h in air	107	Reference [5]

Sample	Crystal form	Crystallite size (Å)	Weight (%)	a = b(Å)	c (Å)	V (Å <sup>3</sup> )	R <sub>wp</sub> (%)
CZ-70	c-Ce <sub>0.6</sub> Zr <sub>0.4</sub> O <sub>2</sub>	29	-	5.307	5.307	149.468	-
CZ/N235-70	c-Ce <sub>0.6</sub> Zr <sub>0.4</sub> O <sub>2</sub>	33	-	5.308	5.308	149.552	-
CZ-600	t-Ce <sub>0.15</sub> Zr <sub>0.85</sub> O <sub>2</sub>	81	100	3.644	5.209	69.169	8.45
CZ/N235-600	t-Ce <sub>0.15</sub> Zr <sub>0.85</sub> O <sub>2</sub>	69	100	3.648	5.219	69.454	7.80
CZ-1000	t-Ce <sub>0.18</sub> Zr <sub>0.82</sub> O <sub>2</sub>	154	94.6	3.686	5.213	70.827	6.76
	<i>t</i> -ZrO <sub>2</sub>		5.4	3.653	5.202	69.418	
CZ/N235-1000	t-Ce <sub>0.15</sub> Zr <sub>0.85</sub> O <sub>2</sub>	125	100	3.649	5.228	69.612	8.26

Table S2. Structural parameters of samples calcined at different temperatures.

	Temperature of	Total H <sub>2</sub> consumption	Reduction ratio
Sample	reduction peak (°C)	$(\mu mol \cdot g^{-1})$	(%) <sup>a</sup>
CZ-600	583	405	70.43
CZ/N235-600	563	422	73.39
CZ-1000	699	334	58.09
CZ/N235-1000	585	380	66.09

Table S3. The reduction peak temperatures and quantitative analysis results of  $H_2$ -TPR for the samples.

a: The ratio between experimental total  $H_2$  consumption and the theoretical  $H_2$  consumption which is calculated assuming that all Ce species are in oxidized state (Ce<sup>4+</sup>) before  $H_2$ -TPR test and can be totally reduced to Ce<sup>3+</sup>.

Table S4. The quantitative analysis results of OSC for the samples and the surface atomic ratios of Zr/Ce and  $Ce^{3+}$  in Ce (%) derived from XPS analyses.

Sample	OSC (µmol·g <sup>-1</sup> )	OSC (mol O <sub>2</sub> /mol CeO <sub>2</sub> )	Oxidation ratio (%) <sup>b</sup>	Zr/Ce	Ce <sup>3+</sup> in Ce (%)
CZ-600	132	0.1148	45.92	5.64	16.92
CZ/N235-600	143	0.1243	49.72	5.62	23.80
CZ-1000	74	0.0643	25.72	6.29	11.70
CZ/N235-1000	138	0.1200	48.00	5.69	21.77

b: The ratio between experimental OSC (expressed as mol  $O_2$ /mol Ce $O_2$ ) and the theoretical OSC value (0.25 mol  $O_2$ /mol Ce $O_2$ ).

Table S5. The OSC for the samples pretreated in  $H_2$  flowing at 950 °C for 1 h.

Sample	OSC		
Sumple	$(\mu mol \cdot g^{-1})$		
CZ-600	218		
CZ/N235-600	260		
CZ-1000	173		
CZ/N235-1000	245		

Catalyst	NO	СО	$C_3H_8$
Catalyst	<i>T</i> <sub>50%</sub> (°C)	<i>T</i> <sub>50%</sub> (°C)	<i>T</i> <sub>50%</sub> (°C)
Rh/CZ-f	204	205	347
Rh/CZ/N235-f	168	171	278
Rh/CZ-a	278	280	-
Rh/CZ/N235-a	229	235	-

Table S6. Light-off temperatures ( $T_{50\%}$ ) of NO, CO and  $C_3H_8$  over catalysts.



Figure S1. TG/DTG/DSC curves of CZ/N235-70.

Figure S1 shows the TG/DTG/DSC curves of the CZ/N235-70. A weight loss of 34.9 % is calculated from TG characterization between room temperature and 1000 °C. It can be found that DTG curve displays two mass loss stages, corresponding with peaks located at about 136.9 and 311.0 °C, respectively. The peak observed at 136.9 °C could be attributed to the loss of water. While a stronger plateau at approximately 311.0 °C is probably assigned to the decomposition of carbonates, hydroxides and organics, which is coincident with the endothermic peak found in DSC profile. The other endothermic peak centered at about 510.6 °C is not associated with weight loss, suggesting the phase transformation of materials.



Figure S2. XRD diffraction patterns of dried precipitates, fresh samples and aged samples.



Figure S3. The illustrative crystallographic structure of cubic  $Ce_{0.6}Zr_{0.4}O_2$ .



Figure S4. Multiples of crystal growth for the fresh and aged samples based on the corresponding crystallite size for dried materials.



Figure S5. Raman spectra of dried precipitates, fresh samples and aged samples.



Figure S6. The statistics of particle distribution of CZ/N235-600 (a) and CZ-600 (b).



Figure S7. FTIR spectra of samples treated at different temperatures.



Figure S8. H<sub>2</sub>-TPR profiles of the sample calcinated at 600 and 1000 °C.



Figure S9. H<sub>2</sub>-TPR profiles of the fresh and aged catalysts.



Figure S10. OSC values of the fresh and aged catalysts.



Figure S11. Rh dispersions of the fresh and aged catalysts.



Figure S12. Rh 3d XPS spectra of the fresh and aged catalysts.

The spectra of Rh  $(3d_{5/2}, 3d_{3/2})$  for fresh and aged catalysts are shown in Figure S12. For fresh catalysts, faint peaks attributed to Rh<sup>0</sup> are detected in a fashion at approximately 307 eV, demonstrating the presence of slight metallic Rh. Prominent peaks at about 308 eV (Rh  $3d_{5/2}$ ) could be observed, which is in accordance with the literature data for Rh<sub>2</sub>O<sub>3</sub>.<sup>1, 2</sup> Upon aging treatment, the peaks of Rh  $3d_{5/2}$  are shifted to higher binding energies, especially Rh/CZ-a, indicating the formation of more RhO<sub>2</sub> on the surface of Rh/CZ-a.<sup>3</sup> According to the references,<sup>3-5</sup> the presence of RhO<sub>2</sub>, which is hard to reduce to the active state, will result in deteriorated catalytic property for the aged catalysts. So Rh/CZ/N235-a may have a superior catalytic performance due to its lower amount of RhO<sub>2</sub>.

## References

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