

SUPPORTING INFORMATION

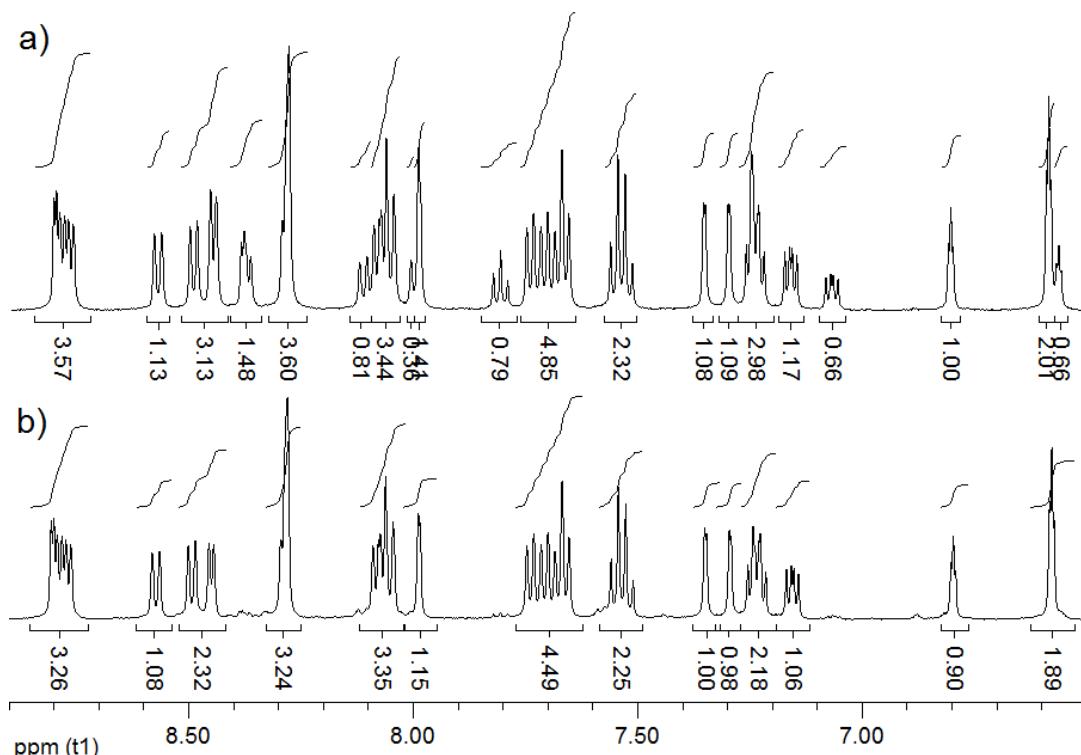


Figure S1. ^1H -NMR spectra of (a) *mer*/*fac* mixture of $[\text{Ru}(\text{Q1Pz})_3]^{2+}$ and (b) *mer*- $[\text{Ru}(\text{Q1Pz})_3]^{2+}$ isolated product after light illumination.

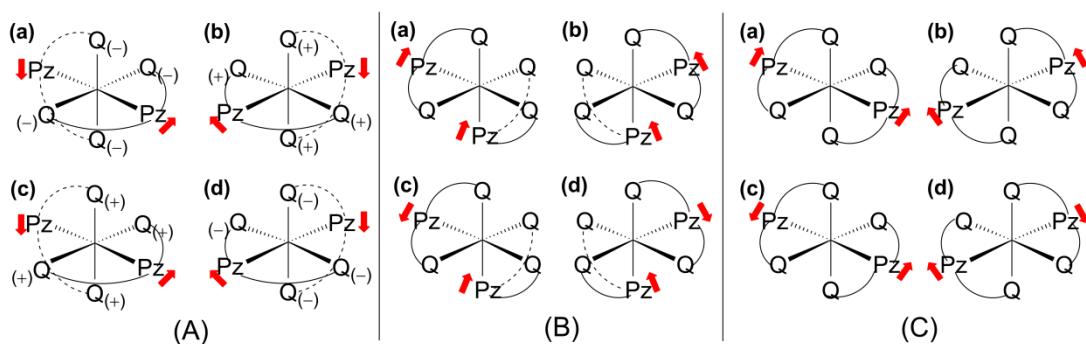


Figure S2. Illustrations of different stereoisomers for which optimized total energies have been calculated (A, left) *meridional*, (B, centre) *cis-facial* and (C, right) *trans-facial* isomers. The red arrow indicates the plane and direction of the polarity of the pyrazole group. In (A) the subscript (+) and (-) indicate the sign of the dihedral angle between the *trans*-quinolines as defined in Figure S2 and the stereochemical labels for each isomer is (a) C-S_a, (b) A-R_a, (c) C-R_a and (d) A-S_a respectively. No stereochemical labels have been assigned to the *fac* isomers.

Table S1. Calculated total energy (eV) of each calculated isomer of $[\text{Ru}(\text{DQPz})_2]^{2+}$, referenced to the lowest energy isomer of each complex. Isomers shown in Figure S2.

	<i>mer</i> -	<i>trans-fac</i> -	<i>cis-fac</i> -
(a)	0	0	0
(b)	0	0.000001	0.01
(c)	0.002	0.01	0.003
(d)	0.002	0.006	0.003

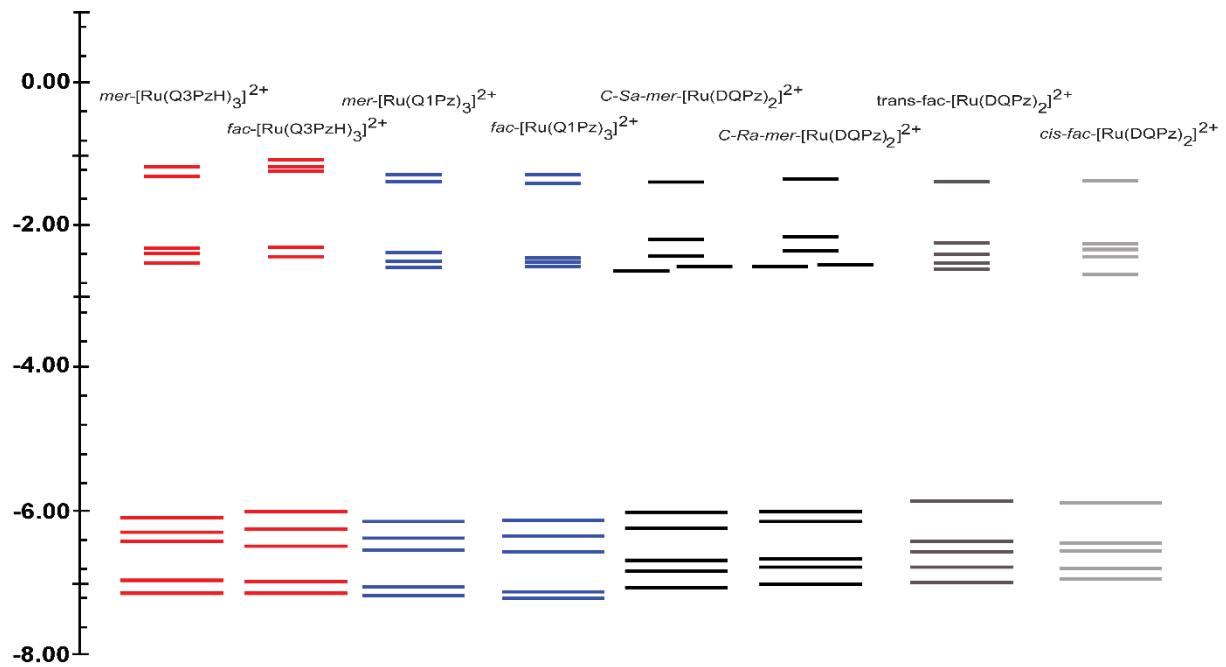


Figure S3: The first 5 HOMO and LUMOs of representative calculated complex isomers.

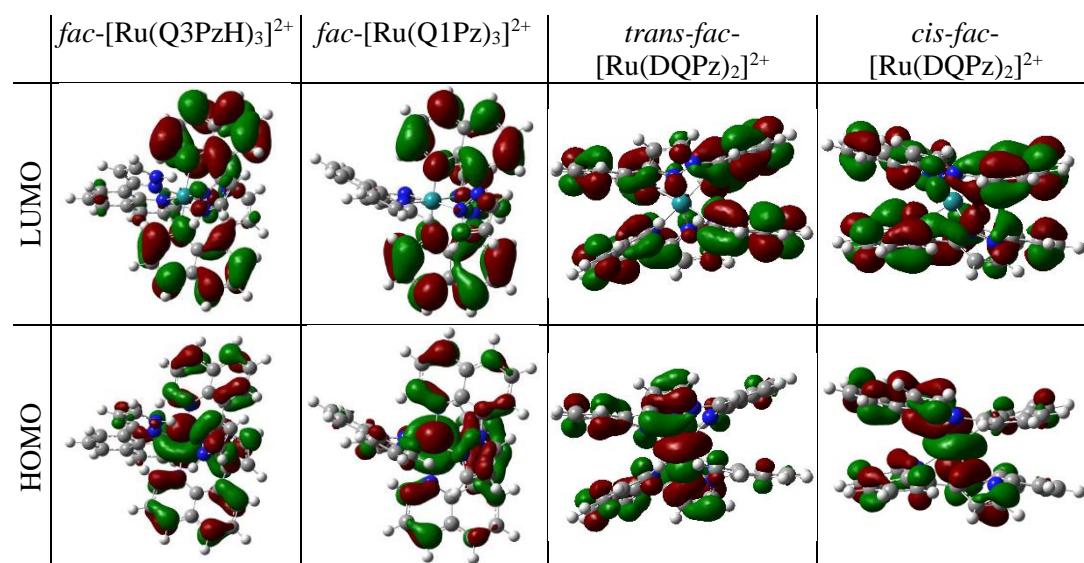


Figure S4. Frontier molecular orbitals of the *fac*-isomers of three complexes.

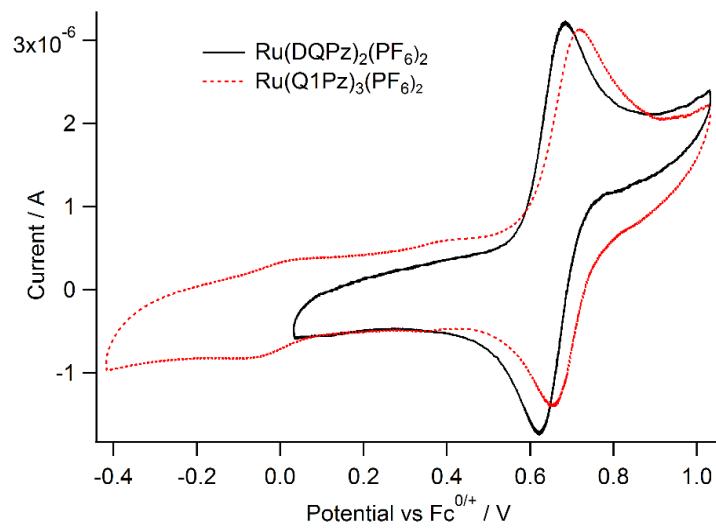


Figure S5. Cyclic voltammetry for the oxidations of *mer-/fac-[Ru(Q1Pz)₃]²⁺* and *mer-[Ru(DQPz)₂]²⁺*.

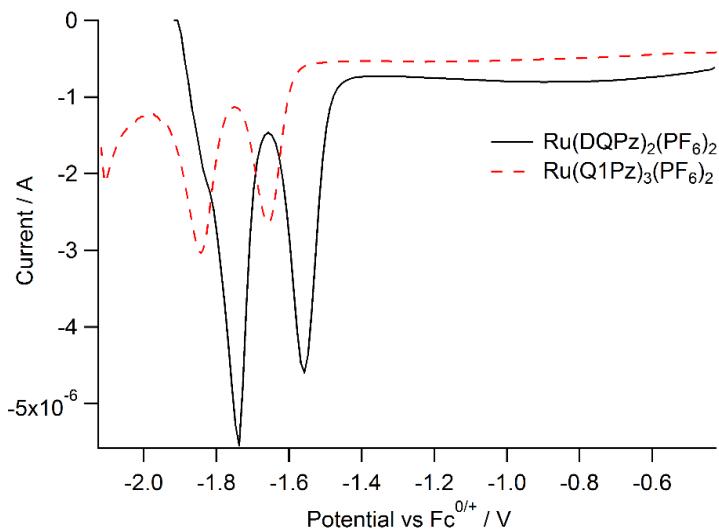


Figure S6. Differential pulse voltammetry for the reductions of *mer-/fac-[Ru(Q1Pz)₃]²⁺* and *mer-[Ru(DQPz)₂]²⁺*.

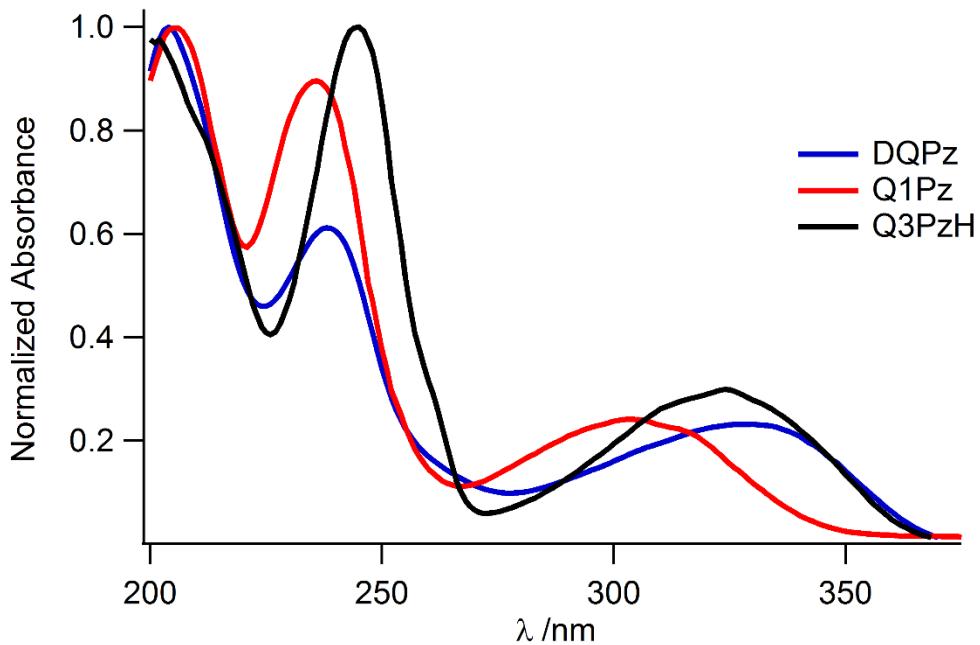


Figure S7. Electronic absorption spectra of ligands Q3PzH, Q1Pz and DQPz in neat acetonitrile.

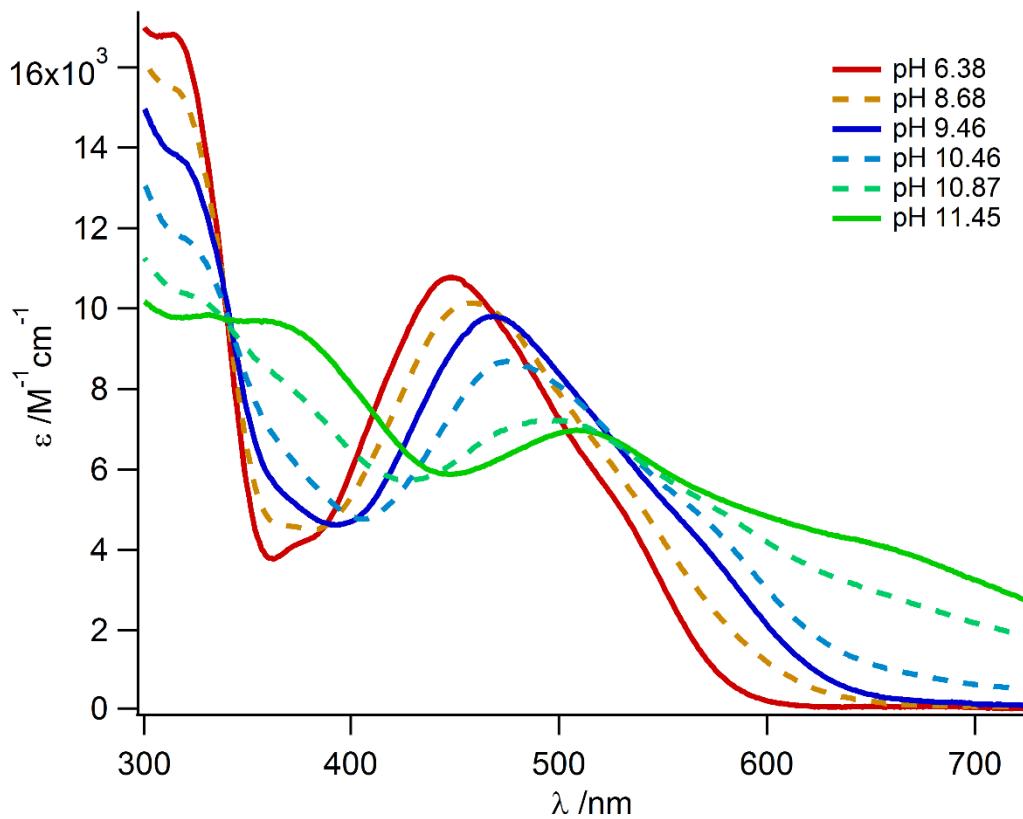


Figure S8. UV-Vis absorption spectra of *mer*-[Ru(Q3PzH)₃]²⁺ in H₂O at different measured pH (set by HCl and NaOH).

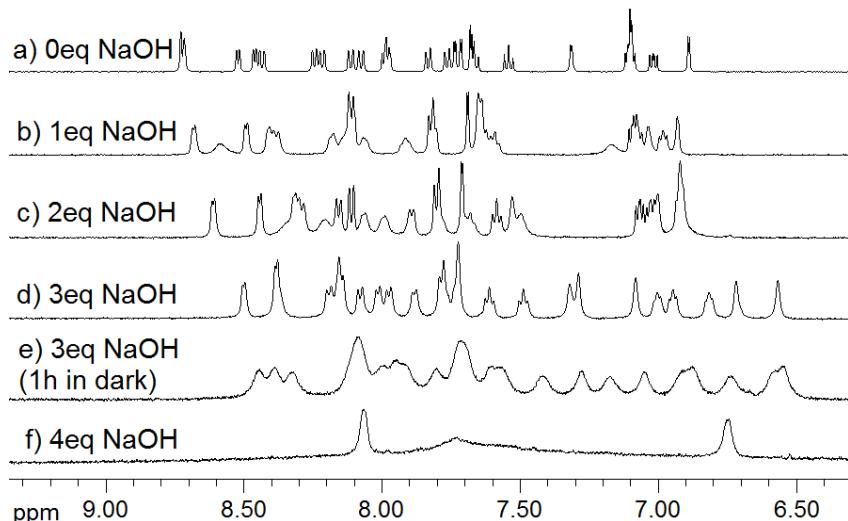


Figure S9. ^1H -NMR spectra of $[\text{Ru}(\text{Q3PzH})_3]^{2+}$ in CD_3CN titrated with $\text{NaOH}(\text{aq})$. Number of equivalents: (a) 0, (b) 1.0, (c) 2.0, (d) 3.0, (e) 3.0 after 1 h at room temperature in the dark and (f) 4.0 (*i.e.* +1 equivalent to sample in e).

Table S2: Electro-spray ionization high resolution mass spectrometry on *mer*- $[\text{Ru}(\text{Q3PzH})_3]^{2+}$, *mer*- $[\text{Ru}(\text{Q1Pz})_3]^{2+}$ and *mer*- $[\text{Ru}(\text{DQPz})_2]^{2+}$ after 5 h light with 10 equivalences of triflic acid^a

Complex	Species after 5h of irradiation ^b	m/z	Rel. int. (%)	Species without irradiation	m/z	Rel. int. (%)
<i>mer</i> - $[\text{Ru}(\text{Q3PzH})_3]^{2+}$	$[\text{L}+\text{H}^+]^+$	196.08724	100	$[\text{L}+\text{H}^+]^+$	196.08693	20
	$[\text{M}]^{2+}$	343.57125	57	$[\text{M}]^{2+}$	343.57159	100
	$[\text{M}-\text{L}+\text{CD}_3\text{CN}]^{2+}$	266.54442	9			
<i>mer</i> - $[\text{Ru}(\text{Q1Pz})_3]^{2+}$	$[\text{L}+\text{H}^+]^+$	196.08657	100	$[\text{L}+\text{H}^+]^+$	196.08657	10
	$[\text{M}]^{2+}$	343.57063	20	$[\text{M}]^{2+}$	343.57063	100
	$[\text{M}-\text{L}]^{2+}$	246.03088	9	$[\text{M}^{2+}\text{PF}_6]^+$	832.10831	10
	$[\text{M}-\text{L}+\text{CD}_3\text{CN}]^{2+}$	266.54426	9	$[\text{M}^{2+}-\text{L}+\text{DMSO}+\text{Cl}^-]^+$	605.04637	5 ^c
	$[\text{M}-\text{L}+\text{2CD}_3\text{CN}]^{2+}$	290.07610	5			
	$[\text{M}-\text{L}+\text{2CD}_3\text{CN}]^{2+}$					
<i>mer</i> - $[\text{Ru}(\text{DQPz})_2]^{2+}$	$[\text{M}]^{2+}$	373.07371	100	$[\text{M}]^{2+}$	373.07377	100

^a The sample with $[\text{Ru}(\text{DQPz})_2]^{2+}$ had 20 equivalences triflic acid. ^b L represents the respective ligand. ^c A minor contamination from the synthesis.

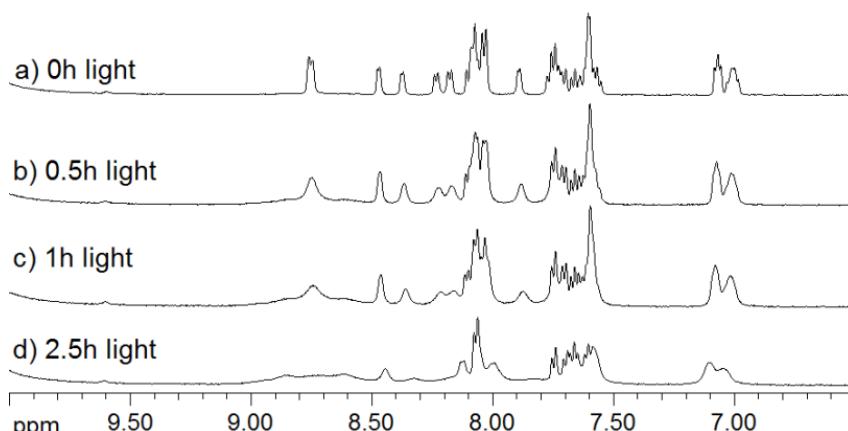


Figure S10. ^1H -NMR spectra of $[\text{Ru}(\text{DQPz})_2]^{2+}$ with 20 equiv. triflic acid after exposure to visible light for (a) 0 h after keeping the sample in the dark for 2 h, (b) 0.5 h, (c) 1 h and (d) 2.5 h.

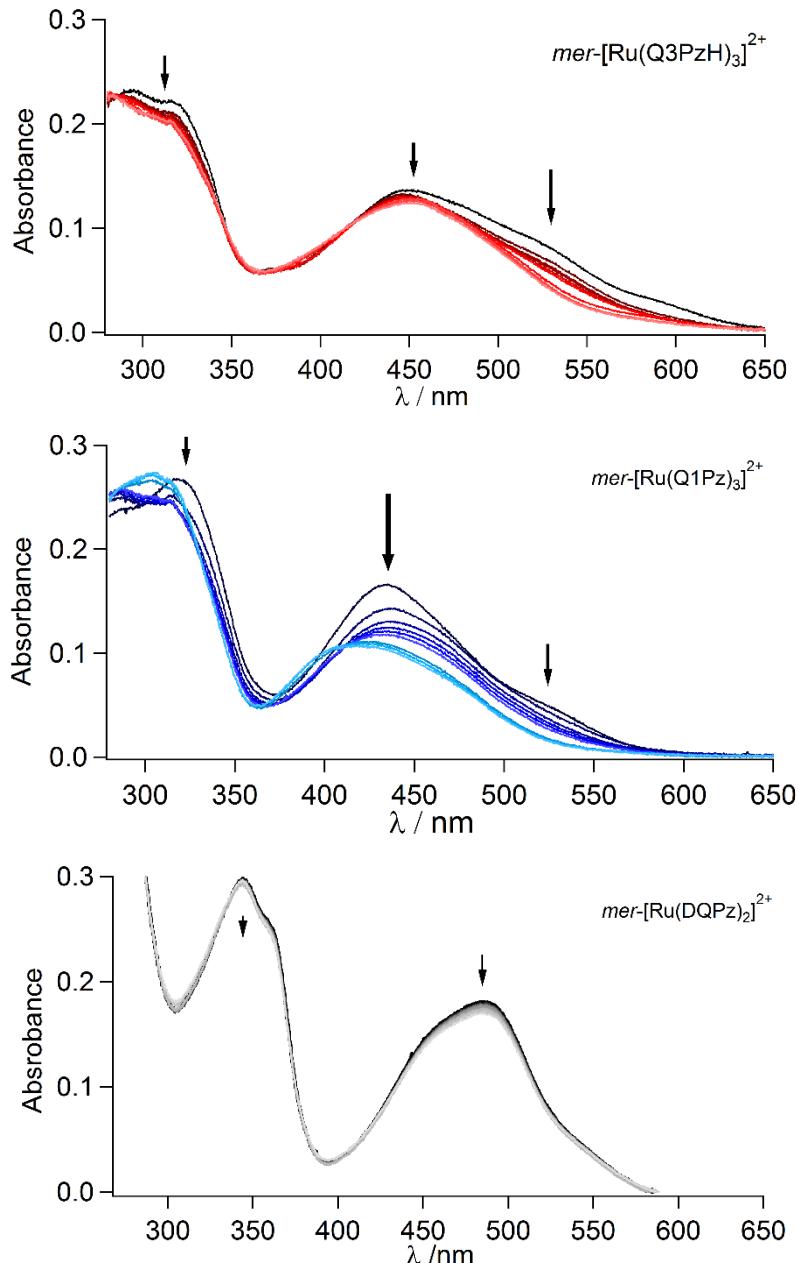


Figure S11. Absorption changes with continuous broad band visible light irradiation for (Top) $mer\text{-}[Ru(Q3PzH)_3]^{2+}$, (Middle) $mer\text{-}[Ru(Q1Pz)_3]^{2+}$ and (Bottom) $mer\text{-}[Ru(DQPz)_2]^{2+}$ in neat acetonitrile (without triflic acid).

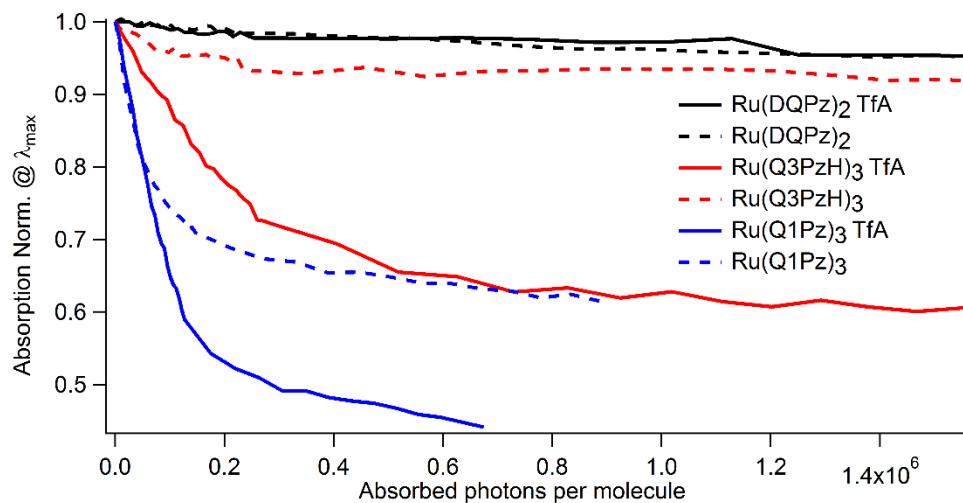


Figure S12: Kinetic traces following the changes in UV/vis absorption at specified wavelengths as a function of photons absorbed per molecule in the light experiment for *mer*-[Ru(Q3PzH)₃]²⁺ (a) and *mer*-[Ru(Q1Pz)₃]²⁺ (b). Solid lines are for experiments without acid and dashed lines are with 10 equiv. triflic acid.

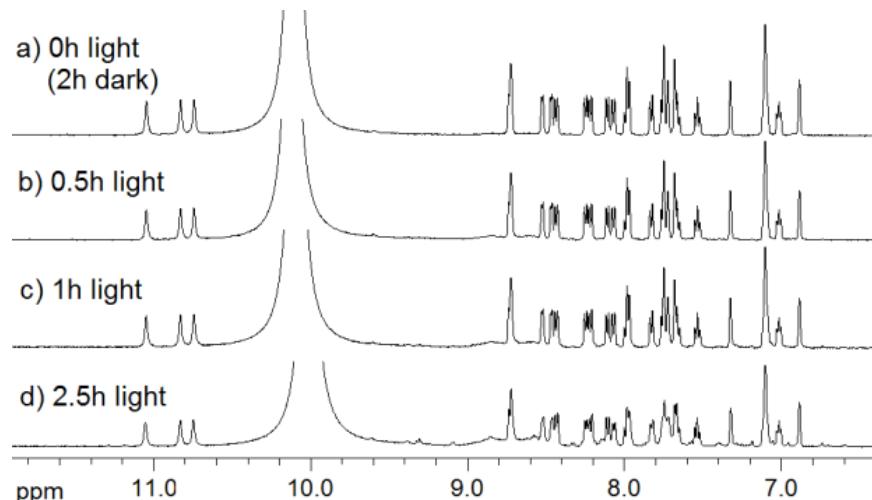


Figure S13. ¹H-NMR spectra of *mer*-[Ru(Q3PzH)₃]²⁺ with 10 equiv. triflic acid after exposure to visible light for (a) 0 h after keeping the sample in the dark for 2 h, (b) 0.5 h, (c) 1 h and (d) 2.5 h.

TDDFT calculated transitions for *fac*-[Ru(Q3PzH)₃]²⁺ (**Table S3**), *fac*-[Ru(Q3PzH)₂(Q3Pz)]⁺ (**Table S4**), *fac*-[Ru(Q3PzH)(Q3Pz)₂] (**Table S5**), *fac*-[Ru(Q3Pz)₃]⁻ (**Table S6**), *mer*-[Ru(Q3PzH)₃]²⁺ (**Table S7**), *mer*-[Ru(Q3PzH)₂(Q3Pz_a)]⁺ (**Table S8**), *mer*-[Ru(Q3PzH)₂(Q3Pz_b)]⁺ (**Table S9**), *mer*-[Ru(Q3PzH)₂(Q3Pz_c)]⁺ (**Table S10**), *mer*-[Ru(Q3PzH_a)(Q3Pz)₂] (**Table S11**), *mer*-[Ru(Q3PzH_b)(Q3Pz)₂] (**Table S12**), *mer*-[Ru(Q3PzH_c)(Q3Pz)₂] (**Table S13**), *mer*-[Ru(Q3Pz)₃] (**Table S14**), *fac*-[Ru(Q1Pz)₃]²⁺ (**Table S15**), *mer*-[Ru(Q1Pz)₃]²⁺ (**Table S16**), *cis-fac*-[Ru(DQPz)₂]²⁺ (**Table S17**), *trans-fac*-[Ru(DQPz)₂]²⁺ (**Table S18**), *C-R_a-mer*-[Ru(DQPz)₂]²⁺ (**Table S19**), *C-S_a-mer*-[Ru(DQPz)₂]²⁺ (**Table S20**).

Table S3. TDDFT calculated transitions for *fac*-[Ru(Q3PzH)₃]²⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.6983	459.48	0.0199	160	→	161	0.17523
				160	→	162	0.67352
2	2.7374	452.93	0.0831	160	→	161	0.64617
				160	→	162	-0.17321
				160	→	163	-0.18627
3	2.8519	434.74	0.0508	159	→	161	-0.40809
				159	→	163	0.15969
				160	→	161	0.17516
				160	→	163	0.49971
4	2.8972	427.94	0.0486	158	→	162	0.1094
				159	→	161	0.12853
				159	→	162	0.64844
				159	→	163	-0.14987
				160	→	163	0.11858
5	2.9109	425.93	0.0202	158	→	162	-0.11042
				159	→	161	0.52244
				159	→	163	0.34499
				160	→	161	0.10375
				160	→	163	0.25514
6	2.9773	416.43	0.0037	158	→	162	0.26407
				159	→	161	-0.14231
				159	→	162	0.15287
				159	→	163	0.53776
				160	→	163	-0.26483
7	3.1097	398.71	0.0091	158	→	161	0.66699
				158	→	162	0.14543
				158	→	163	0.1162
8	3.1911	388.53	0.0511	158	→	162	-0.1647
				158	→	163	0.65001
				160	→	163	-0.12731
9	3.204	386.96	0.0782	158	→	161	-0.141
				158	→	162	0.57048
				158	→	163	0.17836
				159	→	162	-0.19346
				159	→	163	-0.13544
				160	→	163	0.16151

10	3.6411	340.51	0.0031	160	→	164	0.25414
				160	→	165	0.42522
				160	→	169	-0.1187
				160	→	173	0.13151
				160	→	174	0.3236
				160	→	175	0.11661
11	3.7505	330.58	0.0009	158	→	174	0.11408
				158	→	175	-0.13734
				159	→	165	0.10576
				159	→	174	0.17126
				160	→	164	0.21208
				160	→	165	-0.15849
				160	→	166	-0.15704
				160	→	167	0.18701
				160	→	168	0.17487
				160	→	170	0.13123
				160	→	171	-0.17011
				160	→	175	0.28627
				160	→	177	-0.10436
12	3.8268	323.99	0.0056	158	→	165	-0.12856
				158	→	174	-0.23017
				159	→	165	-0.15858
				159	→	167	0.15902
				159	→	168	0.11082
				159	→	170	0.16253
				159	→	171	-0.20701
				159	→	172	-0.10561
				159	→	174	-0.10271
				159	→	175	0.33503
				159	→	177	-0.12639
				160	→	165	-0.20335
13	3.8579	321.38	0.0916	157	→	161	0.55978
				157	→	162	0.31005
				157	→	163	-0.18636
14	3.8809	319.48	0.0392	157	→	161	-0.23442
				157	→	163	-0.15171
				159	→	164	-0.19617
				159	→	165	-0.16474
				159	→	174	-0.15728
				160	→	164	0.34514
				160	→	165	-0.30778
				160	→	166	0.12518
15	3.9145	316.73	0.0396	155	→	161	-0.11339
				156	→	161	-0.1072
				156	→	162	-0.1276
				157	→	161	-0.21489

				157	\rightarrow	162	0.3641
				157	\rightarrow	163	-0.32516
				158	\rightarrow	174	-0.10053
				160	\rightarrow	165	0.23033
				160	\rightarrow	166	-0.16443
				160	\rightarrow	174	-0.12727
16	3.9314	315.37	0.0274	156	\rightarrow	161	0.1104
				157	\rightarrow	161	0.14147
				157	\rightarrow	162	-0.12065
				157	\rightarrow	163	0.18319
				158	\rightarrow	165	-0.13173
				158	\rightarrow	174	-0.19866
				160	\rightarrow	164	0.40802
				160	\rightarrow	165	0.12283
				160	\rightarrow	166	-0.20789
				160	\rightarrow	174	-0.19134
				160	\rightarrow	175	-0.12927
17	3.976	311.83	0.0841	156	\rightarrow	161	-0.2279
				156	\rightarrow	162	0.48988
				157	\rightarrow	162	-0.23466
				157	\rightarrow	163	-0.29073
				160	\rightarrow	166	-0.16052
18	4.0056	309.53	0.0061	155	\rightarrow	161	-0.13729
				156	\rightarrow	161	-0.19019
				156	\rightarrow	162	-0.13447
				157	\rightarrow	161	0.1255
				157	\rightarrow	162	-0.20193
				157	\rightarrow	163	-0.15954
				158	\rightarrow	175	-0.10934
				160	\rightarrow	165	0.14585
				160	\rightarrow	166	0.41167
				160	\rightarrow	167	0.1127
				160	\rightarrow	174	-0.13138
19	4.0151	308.79	0.0312	155	\rightarrow	161	0.13785
				155	\rightarrow	162	-0.11103
				156	\rightarrow	161	0.10149
				156	\rightarrow	162	0.36399
				157	\rightarrow	162	0.32086
				157	\rightarrow	163	0.15814
				159	\rightarrow	165	0.15823
				160	\rightarrow	166	0.26397
20	4.0378	307.06	0.0135	155	\rightarrow	161	0.13237
				155	\rightarrow	162	0.1783
				156	\rightarrow	161	0.34454
				157	\rightarrow	162	-0.13267
				157	\rightarrow	163	-0.31156

				159	\rightarrow	164	0.2407
				159	\rightarrow	165	0.1361
				160	\rightarrow	164	0.12934
				160	\rightarrow	166	0.11469
				160	\rightarrow	168	-0.20421
21	4.0558	305.7	0.0199	155	\rightarrow	162	-0.11113
				156	\rightarrow	161	-0.33911
				157	\rightarrow	163	0.18733
				159	\rightarrow	164	0.3427
				159	\rightarrow	166	0.18063
				159	\rightarrow	167	0.1009
				160	\rightarrow	164	0.19604
				160	\rightarrow	167	-0.17145
				160	\rightarrow	168	-0.21008
22	4.079	303.96	0.0627	155	\rightarrow	161	-0.14086
				155	\rightarrow	162	-0.19981
				155	\rightarrow	163	0.12889
				156	\rightarrow	162	-0.13618
				156	\rightarrow	163	0.25809
				158	\rightarrow	164	0.1142
				159	\rightarrow	164	-0.13831
				159	\rightarrow	165	0.3889
				159	\rightarrow	166	-0.16342
				160	\rightarrow	167	-0.1659
				160	\rightarrow	168	-0.10449
23	4.1003	302.38	0.0026	155	\rightarrow	161	-0.17088
				155	\rightarrow	162	-0.21043
				155	\rightarrow	163	0.12239
				156	\rightarrow	161	0.29021
				156	\rightarrow	163	0.38397
				159	\rightarrow	164	0.18943
				159	\rightarrow	165	-0.2438
24	4.1704	297.3	0.0036	155	\rightarrow	161	0.10124
				158	\rightarrow	174	-0.10702
				158	\rightarrow	175	0.11395
				159	\rightarrow	164	0.21173
				159	\rightarrow	165	0.28163
				159	\rightarrow	166	0.11742
				159	\rightarrow	167	-0.12366
				159	\rightarrow	168	-0.12819
				160	\rightarrow	167	0.28815
				160	\rightarrow	168	0.28257
25	4.1837	296.35	0.0026	155	\rightarrow	161	0.52792
				155	\rightarrow	162	-0.14209
				155	\rightarrow	163	0.11758
				156	\rightarrow	162	-0.14159

				156	\rightarrow	163	0.13402
				157	\rightarrow	163	-0.11285
				160	\rightarrow	167	0.16531
				160	\rightarrow	168	-0.18066
26	4.1986	295.3	0.003	155	\rightarrow	161	-0.16664
				155	\rightarrow	162	0.376
				156	\rightarrow	163	0.21797
				158	\rightarrow	164	-0.18992
				158	\rightarrow	166	-0.10206
				159	\rightarrow	166	-0.13027
				159	\rightarrow	167	-0.14206
				160	\rightarrow	166	-0.11345
				160	\rightarrow	167	0.21163
				160	\rightarrow	168	-0.23553
27	4.2084	294.61	0.0087	158	\rightarrow	164	-0.14729
				159	\rightarrow	164	-0.30996
				159	\rightarrow	166	0.48837
				159	\rightarrow	167	0.11396
				159	\rightarrow	168	-0.12371
				160	\rightarrow	167	0.11281
				160	\rightarrow	168	-0.19032
				160	\rightarrow	169	-0.11165
28	4.2162	294.06	0.0061	155	\rightarrow	161	0.17653
				155	\rightarrow	162	0.37936
				156	\rightarrow	161	-0.10705
				156	\rightarrow	163	0.32357
				158	\rightarrow	164	0.11045
				159	\rightarrow	164	-0.10482
				159	\rightarrow	166	0.13472
				160	\rightarrow	167	-0.22499
				160	\rightarrow	168	0.22313
29	4.2349	292.77	0.005	155	\rightarrow	162	0.13709
				155	\rightarrow	163	0.12587
				156	\rightarrow	163	-0.13925
				158	\rightarrow	164	0.39103
				158	\rightarrow	165	-0.19848
				158	\rightarrow	166	0.17984
				158	\rightarrow	167	0.22155
				160	\rightarrow	167	0.20031
				160	\rightarrow	168	-0.1968
30	4.2719	290.23	0.0061	154	\rightarrow	163	-0.11454
				155	\rightarrow	163	0.46345
				156	\rightarrow	162	0.1054
				156	\rightarrow	163	-0.19056
				158	\rightarrow	164	-0.14418
				158	\rightarrow	166	-0.14576

					159	\rightarrow	164	-0.11956
					160	\rightarrow	169	0.2925
31	4.2834	289.45	0.0038		154	\rightarrow	163	-0.11864
					155	\rightarrow	163	-0.26989
					158	\rightarrow	164	0.11894
					158	\rightarrow	165	0.29495
					159	\rightarrow	166	0.14438
					159	\rightarrow	174	-0.10191
					160	\rightarrow	169	0.40259
32	4.3006	288.3	0.0256		154	\rightarrow	163	0.1103
					155	\rightarrow	163	0.23458
					158	\rightarrow	164	0.15348
					158	\rightarrow	165	0.45484
					158	\rightarrow	174	-0.12514
					160	\rightarrow	169	-0.24443
					160	\rightarrow	174	-0.1764
33	4.351	284.96	0.0076		152	\rightarrow	162	0.11852
					153	\rightarrow	162	-0.20498
					158	\rightarrow	164	-0.12408
					158	\rightarrow	166	0.2153
					158	\rightarrow	167	-0.12429
					158	\rightarrow	168	-0.10787
					159	\rightarrow	165	0.10365
					159	\rightarrow	166	-0.13843
					159	\rightarrow	167	0.47681
					160	\rightarrow	167	0.13386
34	4.379	283.14	0.0015		158	\rightarrow	164	-0.18907
					158	\rightarrow	166	0.36363
					158	\rightarrow	167	0.17972
					158	\rightarrow	168	-0.10085
					159	\rightarrow	166	0.10908
					159	\rightarrow	168	0.30683
					159	\rightarrow	169	0.10671
					159	\rightarrow	174	-0.16087
35	4.4284	279.98	0.0055		155	\rightarrow	163	0.13641
					158	\rightarrow	166	0.32654
					158	\rightarrow	168	-0.16455
					158	\rightarrow	171	0.12527
					158	\rightarrow	175	-0.20549
					159	\rightarrow	167	-0.22003
					159	\rightarrow	168	-0.2403
					159	\rightarrow	171	-0.11175
					159	\rightarrow	175	0.11995
					160	\rightarrow	171	0.10398
					160	\rightarrow	175	-0.12215
36	4.4569	278.19	0.0042		158	\rightarrow	164	0.10324

				159	\rightarrow	168	0.40369
				159	\rightarrow	173	0.10401
				159	\rightarrow	174	0.29574
				160	\rightarrow	167	0.12111
				160	\rightarrow	170	-0.13629
				160	\rightarrow	171	0.16147
				160	\rightarrow	174	0.14495
				160	\rightarrow	175	-0.17873
37	4.4758	277.01	0.0208	154	\rightarrow	161	-0.14022
				158	\rightarrow	164	-0.23547
				158	\rightarrow	165	0.12128
				158	\rightarrow	166	0.10784
				158	\rightarrow	167	0.33327
				158	\rightarrow	168	0.23507
				159	\rightarrow	165	-0.11486
				159	\rightarrow	166	-0.15166
				159	\rightarrow	168	-0.23216
				159	\rightarrow	174	0.21592
				160	\rightarrow	169	0.10818
38	4.5354	273.37	0.0477	152	\rightarrow	163	0.10392
				153	\rightarrow	162	-0.17245
				154	\rightarrow	161	-0.21861
				158	\rightarrow	167	-0.24636
				158	\rightarrow	168	0.27239
				158	\rightarrow	169	0.15737
				158	\rightarrow	174	-0.14364
				159	\rightarrow	167	-0.11553
				159	\rightarrow	169	0.29712
				160	\rightarrow	174	0.10908
39	4.5646	271.62	0.0031	153	\rightarrow	162	0.15228
				158	\rightarrow	166	-0.11339
				158	\rightarrow	167	0.18992
				158	\rightarrow	168	-0.21124
				158	\rightarrow	175	-0.11297
				159	\rightarrow	165	0.12537
				159	\rightarrow	167	0.15842
				159	\rightarrow	169	0.49597
40	4.6115	268.86	0.064	152	\rightarrow	161	-0.1763
				153	\rightarrow	161	-0.14889
				154	\rightarrow	161	0.11008
				154	\rightarrow	162	-0.14978
				154	\rightarrow	163	0.28567
				157	\rightarrow	164	0.24948
				157	\rightarrow	166	-0.17256
				158	\rightarrow	168	-0.10606
				158	\rightarrow	169	0.1784

				159	\rightarrow	169	-0.14636
				160	\rightarrow	169	0.3043
41	4.6195	268.39	0.0683	154	\rightarrow	161	0.35652
				156	\rightarrow	164	0.11758
				157	\rightarrow	165	0.17038
				157	\rightarrow	169	0.11222
				158	\rightarrow	164	-0.11672
				158	\rightarrow	165	0.11221
				158	\rightarrow	166	0.17
				158	\rightarrow	168	0.14234
				158	\rightarrow	174	-0.2139
				158	\rightarrow	175	-0.12063
				159	\rightarrow	175	-0.1027
				160	\rightarrow	166	-0.11559
				160	\rightarrow	168	-0.13222
				160	\rightarrow	174	0.12952
42	4.6401	267.2	0.0149	154	\rightarrow	161	0.17199
				158	\rightarrow	164	-0.10943
				158	\rightarrow	166	0.10237
				158	\rightarrow	168	0.244
				158	\rightarrow	173	0.11391
				158	\rightarrow	174	0.24856
				158	\rightarrow	175	0.15888
				159	\rightarrow	169	0.28339
				159	\rightarrow	174	0.14382
				159	\rightarrow	175	0.17705
				160	\rightarrow	174	-0.15433
				160	\rightarrow	175	-0.1199
43	4.7575	260.61	0.0125	153	\rightarrow	162	0.21373
				156	\rightarrow	164	-0.14821
				156	\rightarrow	166	-0.12984
				158	\rightarrow	165	-0.12297
				158	\rightarrow	168	0.36013
				158	\rightarrow	170	-0.10391
				158	\rightarrow	171	0.14358
				158	\rightarrow	175	-0.18015
				159	\rightarrow	167	0.1758
				159	\rightarrow	174	-0.15694
44	4.8021	258.19	0.0448	152	\rightarrow	162	-0.1357
				153	\rightarrow	162	0.15807
				154	\rightarrow	162	0.17806
				156	\rightarrow	164	-0.1353
				156	\rightarrow	166	-0.12071
				158	\rightarrow	166	0.16686
				158	\rightarrow	167	-0.20591
				158	\rightarrow	169	0.44112

					158	\rightarrow	175	0.1388
45	4.812	257.66	0.0122		153	\rightarrow	162	-0.14696
					154	\rightarrow	162	0.22492
					158	\rightarrow	166	-0.11204
					158	\rightarrow	167	0.2854
					158	\rightarrow	169	0.35878
					158	\rightarrow	170	-0.10182
					158	\rightarrow	171	0.13685
					158	\rightarrow	174	0.11114
					158	\rightarrow	175	-0.15606
					159	\rightarrow	168	0.12853
					159	\rightarrow	174	-0.1511
46	4.8197	257.24	0.0034		152	\rightarrow	161	-0.19928
					153	\rightarrow	161	-0.26985
					154	\rightarrow	161	-0.13131
					154	\rightarrow	162	0.50624
					158	\rightarrow	169	-0.24558
47	4.8604	255.09	0.0074		152	\rightarrow	162	-0.2383
					152	\rightarrow	163	0.27951
					153	\rightarrow	162	-0.23724
					153	\rightarrow	163	0.31269
					154	\rightarrow	161	0.36117
					157	\rightarrow	165	-0.19226
48	4.8714	254.51	0.0023		152	\rightarrow	161	0.20579
					153	\rightarrow	161	0.33356
					154	\rightarrow	162	0.28895
					154	\rightarrow	163	0.49969
49	4.9373	251.12	0.0038		152	\rightarrow	161	0.48452
					152	\rightarrow	162	0.11836
					153	\rightarrow	161	-0.45667
					154	\rightarrow	163	0.11961
50	4.988	248.56	0.0027		152	\rightarrow	162	0.50188
					152	\rightarrow	163	0.21814
					153	\rightarrow	162	0.29585
					153	\rightarrow	163	0.22934
					157	\rightarrow	165	-0.16826

Table S4. TDDFT calculated transitions for *fac*-[Ru(Q3PzH)₂(Q3Pz)]⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.3545	526.58	0.0783	160	\rightarrow	161	0.63228
				160	\rightarrow	162	-0.26438
				160	\rightarrow	163	0.10197
2	2.3638	524.51	0.0205	160	\rightarrow	161	0.24693
				160	\rightarrow	162	0.64027
				160	\rightarrow	163	0.1308
3	2.5132	493.34	0.0344	158	\rightarrow	163	0.14216

				160	\rightarrow	161	-0.11369
				160	\rightarrow	163	0.6489
4	2.5762	481.28	0.0039	159	\rightarrow	161	0.68966
				159	\rightarrow	163	-0.10882
5	2.7164	456.43	0.0406	157	\rightarrow	161	-0.20092
				158	\rightarrow	161	0.52985
				158	\rightarrow	162	-0.10788
				159	\rightarrow	162	-0.37521
6	2.742	452.16	0.0218	157	\rightarrow	161	-0.12984
				158	\rightarrow	161	0.35111
				158	\rightarrow	162	0.25273
				159	\rightarrow	162	0.43168
				159	\rightarrow	163	0.29316
7	2.7997	442.85	0.0005	157	\rightarrow	162	0.13722
				158	\rightarrow	162	-0.38361
				159	\rightarrow	163	0.54783
8	2.9018	427.27	0.0989	157	\rightarrow	162	-0.11536
				157	\rightarrow	163	0.11601
				158	\rightarrow	161	-0.11059
				158	\rightarrow	162	0.4116
				158	\rightarrow	163	-0.28505
				159	\rightarrow	162	-0.34943
				159	\rightarrow	163	0.24963
9	3.0133	411.45	0.0714	157	\rightarrow	163	-0.20172
				158	\rightarrow	162	0.20743
				158	\rightarrow	163	0.57107
				159	\rightarrow	162	-0.13441
				160	\rightarrow	163	-0.16034
10	3.2224	384.76	0.0572	157	\rightarrow	161	0.49846
				157	\rightarrow	162	0.31295
				157	\rightarrow	163	0.27575
				158	\rightarrow	161	0.18685
				158	\rightarrow	162	0.13029
				158	\rightarrow	163	0.1316
11	3.2457	381.99	0.0012	157	\rightarrow	161	-0.35819
				157	\rightarrow	162	0.56178
				158	\rightarrow	161	-0.12546
				158	\rightarrow	162	0.16375
12	3.3368	371.57	0.0091	157	\rightarrow	161	-0.22488
				157	\rightarrow	162	-0.1726
				157	\rightarrow	163	0.59163
				158	\rightarrow	163	0.20643
13	3.3905	365.68	0.0085	160	\rightarrow	164	0.5194
				160	\rightarrow	165	-0.38558
				160	\rightarrow	166	0.1424
				160	\rightarrow	167	0.10682

14	3.5669	347.6	0.005	160	→	164	0.42812
				160	→	165	0.524
				160	→	166	-0.12329
15	3.661	338.66	0.0274	159	→	164	-0.19503
				159	→	166	-0.11207
				160	→	165	0.17103
				160	→	166	0.5236
				160	→	167	-0.1476
				160	→	168	0.10362
				160	→	169	-0.10916
				160	→	173	-0.15415
				160	→	176	0.10666
16	3.7932	326.86	0.0058	158	→	164	-0.18581
				158	→	165	0.13144
				159	→	164	0.39426
				159	→	165	-0.10007
				159	→	173	0.10096
				159	→	175	0.13944
				159	→	177	-0.11118
				160	→	166	0.24809
				160	→	168	0.16381
				160	→	173	0.15078
				160	→	175	0.15021
				160	→	177	-0.10857
17	3.805	325.85	0.0047	158	→	165	-0.10082
				159	→	164	-0.28612
				160	→	164	-0.11853
				160	→	166	-0.17986
				160	→	167	0.15206
				160	→	168	0.41382
				160	→	169	0.14578
				160	→	175	0.1827
				160	→	177	-0.15246
18	3.8442	322.52	0.0046	157	→	173	0.11291
				158	→	164	0.14104
				158	→	165	-0.14508
				158	→	166	0.14212
				158	→	173	-0.16508
				159	→	164	0.11351
				159	→	166	0.11212
				159	→	173	-0.19141
				160	→	165	0.11861
				160	→	166	0.1917
				160	→	167	0.41587
19	3.8605	321.16	0.0138	156	→	161	0.11427
				158	→	165	-0.12088

				159	\rightarrow	164	0.25815
				159	\rightarrow	165	0.4106
				159	\rightarrow	166	0.12026
				159	\rightarrow	167	-0.12389
				160	\rightarrow	167	-0.29937
				160	\rightarrow	168	0.13614
20	3.8708	320.3	0.0065	155	\rightarrow	161	-0.1169
				157	\rightarrow	173	-0.13814
				158	\rightarrow	164	0.14241
				158	\rightarrow	173	0.17077
				159	\rightarrow	164	0.18178
				159	\rightarrow	165	0.13922
				159	\rightarrow	169	0.11354
				159	\rightarrow	173	0.22669
				159	\rightarrow	176	-0.12111
				160	\rightarrow	167	0.30252
				160	\rightarrow	173	-0.15085
				160	\rightarrow	176	0.12424
21	3.8871	318.96	0.0325	155	\rightarrow	161	0.19721
				156	\rightarrow	161	0.37677
				158	\rightarrow	164	-0.20319
				159	\rightarrow	164	-0.17312
				159	\rightarrow	165	0.26742
				159	\rightarrow	166	0.113
				160	\rightarrow	167	0.1707
22	3.9104	317.06	0.0875	156	\rightarrow	161	0.47908
				156	\rightarrow	162	-0.36655
				158	\rightarrow	164	0.12107
				159	\rightarrow	165	-0.2195
				160	\rightarrow	167	-0.11531
23	3.9316	315.35	0.0582	155	\rightarrow	161	0.531
				156	\rightarrow	162	0.30312
				158	\rightarrow	164	0.18048
				159	\rightarrow	165	-0.15966
				160	\rightarrow	168	-0.12174
24	3.9537	313.59	0.0617	155	\rightarrow	161	-0.33187
				156	\rightarrow	161	0.29609
				156	\rightarrow	162	0.47413
				159	\rightarrow	165	-0.11706
25	3.956	313.41	0.0031	155	\rightarrow	161	0.10851
				158	\rightarrow	164	-0.26325
				159	\rightarrow	164	0.17866
				159	\rightarrow	165	-0.17487
				159	\rightarrow	168	-0.12504
				159	\rightarrow	173	-0.10225
				159	\rightarrow	175	-0.15864

				159	\rightarrow	177	0.1281
				160	\rightarrow	166	-0.10096
				160	\rightarrow	167	0.10634
				160	\rightarrow	168	0.27024
				160	\rightarrow	169	-0.17808
				160	\rightarrow	173	-0.23079
				160	\rightarrow	175	-0.13711
26	3.9836	311.24	0.0163	156	\rightarrow	161	0.10358
				157	\rightarrow	164	-0.10093
				158	\rightarrow	164	0.3595
				158	\rightarrow	165	0.28435
				158	\rightarrow	168	0.10547
				159	\rightarrow	166	-0.14754
				159	\rightarrow	173	-0.10299
				160	\rightarrow	168	0.26462
				160	\rightarrow	175	-0.10695
				160	\rightarrow	176	-0.10497
				160	\rightarrow	177	0.10757
27	4.0057	309.52	0.0069	157	\rightarrow	165	-0.15643
				158	\rightarrow	165	0.48049
				158	\rightarrow	167	-0.12349
				158	\rightarrow	173	-0.14062
				158	\rightarrow	176	0.10925
				159	\rightarrow	166	0.15434
				160	\rightarrow	173	-0.11295
				160	\rightarrow	175	0.1096
				160	\rightarrow	176	0.13691
				160	\rightarrow	177	-0.11972
28	4.0679	304.79	0.0278	158	\rightarrow	173	0.12479
				159	\rightarrow	164	-0.11758
				159	\rightarrow	165	-0.20552
				159	\rightarrow	166	0.49382
				159	\rightarrow	168	0.15202
				160	\rightarrow	168	0.17113
				160	\rightarrow	169	-0.14863
29	4.1057	301.98	0.0038	155	\rightarrow	162	-0.15196
				155	\rightarrow	163	-0.25573
				156	\rightarrow	163	0.15478
				157	\rightarrow	168	-0.11661
				158	\rightarrow	164	-0.10037
				158	\rightarrow	166	0.47093
				158	\rightarrow	167	-0.18394
				158	\rightarrow	168	0.16345
30	4.1341	299.91	0.0139	155	\rightarrow	162	0.32601
				155	\rightarrow	163	0.3728
				156	\rightarrow	163	-0.30147

				158	\rightarrow	164	-0.12773
				158	\rightarrow	166	0.25377
				158	\rightarrow	168	0.10654
				159	\rightarrow	166	-0.11284
31	4.1512	298.67	0.0204	154	\rightarrow	163	-0.12748
				155	\rightarrow	162	0.17728
				155	\rightarrow	163	0.21356
				156	\rightarrow	163	0.35216
				158	\rightarrow	168	0.10534
				159	\rightarrow	166	0.15412
				159	\rightarrow	167	0.2125
				159	\rightarrow	168	-0.25522
				160	\rightarrow	169	0.2103
32	4.1755	296.93	0.0088	151	\rightarrow	162	-0.11248
				155	\rightarrow	162	-0.11144
				156	\rightarrow	163	-0.3527
				159	\rightarrow	165	0.12261
				159	\rightarrow	166	0.15701
				159	\rightarrow	167	0.4269
				159	\rightarrow	168	-0.25005
33	4.2072	294.7	0.0016	154	\rightarrow	162	0.20023
				155	\rightarrow	162	0.46582
				155	\rightarrow	163	-0.27648
				156	\rightarrow	163	0.15576
				159	\rightarrow	167	0.15283
				160	\rightarrow	169	-0.20994
34	4.2244	293.5	0.0325	155	\rightarrow	162	-0.18617
				155	\rightarrow	163	0.35568
				156	\rightarrow	163	0.24449
				158	\rightarrow	166	0.102
				159	\rightarrow	167	0.19456
				159	\rightarrow	168	0.10996
				160	\rightarrow	169	-0.32749
35	4.2679	290.51	0.0049	152	\rightarrow	163	-0.13325
				157	\rightarrow	164	0.15722
				157	\rightarrow	165	0.15077
				157	\rightarrow	166	-0.16338
				158	\rightarrow	167	0.34554
				158	\rightarrow	168	0.27916
				159	\rightarrow	167	0.22742
				159	\rightarrow	168	0.25575
36	4.2861	289.27	0.0065	154	\rightarrow	161	0.11867
				157	\rightarrow	164	-0.11237
				157	\rightarrow	165	-0.11393
				158	\rightarrow	167	-0.19846
				158	\rightarrow	168	-0.11519

					159	\rightarrow	167	0.29251
					159	\rightarrow	168	0.38055
					160	\rightarrow	169	0.27526
					160	\rightarrow	173	-0.10078
37	4.2987	288.42	0.0047		157	\rightarrow	167	0.12432
					157	\rightarrow	168	-0.14136
					158	\rightarrow	165	-0.14232
					158	\rightarrow	166	-0.29452
					158	\rightarrow	167	-0.32256
					158	\rightarrow	168	0.40068
					159	\rightarrow	166	-0.10092
					160	\rightarrow	169	-0.11959
38	4.3343	286.05	0.0038		154	\rightarrow	161	0.60524
					154	\rightarrow	162	-0.24156
					155	\rightarrow	162	0.16199
39	4.3672	283.9	0.0026		154	\rightarrow	161	0.27003
					154	\rightarrow	162	0.57206
					155	\rightarrow	162	-0.15646
					156	\rightarrow	163	0.10907
					157	\rightarrow	164	0.12336
40	4.3886	282.52	0.0046		154	\rightarrow	162	-0.12869
					157	\rightarrow	164	0.52335
					157	\rightarrow	165	0.13079
					157	\rightarrow	167	0.17267
					158	\rightarrow	164	0.20856
					158	\rightarrow	167	-0.23626

Table S5. TDDFT calculated transitions for *fac*-[Ru(Q3PzH)(Q3Pz)₂].

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	1.9402	639.03	0.0046	160	\rightarrow	161	0.64529
				160	\rightarrow	162	-0.25531
2	2.0912	592.88	0.0716	160	\rightarrow	161	0.27445
				160	\rightarrow	162	0.60922
				160	\rightarrow	163	0.20157
3	2.2749	545.02	0.0871	159	\rightarrow	161	-0.16369
				159	\rightarrow	162	0.1151
				159	\rightarrow	163	0.19381
				160	\rightarrow	162	-0.21516
				160	\rightarrow	163	0.59334
4	2.4691	502.13	0.0046	158	\rightarrow	161	0.53299
				158	\rightarrow	162	-0.17201
				158	\rightarrow	163	-0.11339
				159	\rightarrow	161	-0.25017
				159	\rightarrow	162	-0.29858
				159	\rightarrow	163	0.10816
5	2.4856	498.81	0.0142	158	\rightarrow	161	0.39239

				159	→	161	0.28986
				159	→	162	0.46926
				159	→	163	-0.13587
6	2.5626	483.82	0.061	158	→	161	0.13891
				158	→	162	0.52468
				159	→	161	-0.37705
				159	→	162	0.19029
				159	→	163	-0.1051
7	2.5816	480.27	0.0707	158	→	161	0.14075
				158	→	162	0.31347
				158	→	163	0.18759
				159	→	161	0.33533
				159	→	162	-0.12133
8	2.6364	470.28	0.0152	159	→	163	0.45585
				158	→	162	-0.19993
				158	→	163	0.65475
				158	→	162	-0.18115
				159	→	161	-0.22496
9	2.7411	452.32	0.0561	159	→	162	0.32409
				159	→	163	0.43109
				160	→	163	-0.27658
				157	→	161	0.69552
				157	→	162	0.58825
10	3.0971	400.32	0.0075	157	→	163	0.34543
				160	→	164	0.68664
				160	→	165	0.66984
				156	→	161	0.37494
				156	→	162	0.48525
11	3.1574	392.68	0.0649	157	→	162	-0.12055
				157	→	163	0.2766
				160	→	166	-0.1176
				156	→	161	-0.19035
				156	→	162	-0.21288
12	3.2099	386.25	0.0182	157	→	162	-0.32899
				157	→	163	0.53186
				156	→	161	0.15432
				160	→	166	0.6587
				156	→	161	0.53863
13	3.2446	382.12	0.0032	156	→	162	-0.44192
				156	→	163	0.69445
				159	→	164	0.64204
				159	→	166	0.13188
				159	→	167	0.15867
14	3.3196	373.49	0.0606	158	→	164	0.14943
				159	→	164	-0.12424
				159	→	165	0.12389
				158	→	164	0.12389
				159	→	165	0.12389
15	3.3525	369.82	0.0078	156	→	161	-0.19035
				156	→	162	-0.21288
				157	→	162	-0.32899
				157	→	163	0.53186
				156	→	161	-0.19035
16	3.444	360	0.0099	156	→	161	0.15432
				160	→	166	0.6587
				156	→	161	0.53863
				156	→	162	-0.44192
				156	→	163	0.69445
17	3.4633	357.99	0.0052	156	→	161	0.53863
				156	→	162	-0.44192
				156	→	163	0.69445
				159	→	164	0.64204
				159	→	166	0.13188
18	3.4707	357.23	0.0211	156	→	163	0.15867
				159	→	167	0.15867
				159	→	168	0.15867
				159	→	169	0.15867
				159	→	170	0.15867
19	3.5671	347.57	0.0004	158	→	164	0.14943
				159	→	164	-0.12424
				159	→	165	0.12389
				159	→	166	0.12389
				159	→	167	0.12389
20	3.6097	343.47	0.0235	158	→	164	0.14943
				159	→	164	-0.12424
				159	→	165	0.12389
				159	→	166	0.12389
				159	→	167	0.12389

				160	\rightarrow	167	0.615
				160	\rightarrow	168	-0.11486
21	3.6631	338.46	0.0086	159	\rightarrow	165	0.17163
				160	\rightarrow	165	0.13311
				160	\rightarrow	168	0.44195
				160	\rightarrow	169	0.3382
				160	\rightarrow	174	0.11588
				160	\rightarrow	176	-0.23121
22	3.7396	331.54	0.0011	158	\rightarrow	164	-0.25136
				159	\rightarrow	165	0.56384
				160	\rightarrow	167	-0.13298
				160	\rightarrow	168	-0.18351
23	3.7645	329.35	0.0401	158	\rightarrow	164	0.58791
				158	\rightarrow	167	0.13956
				159	\rightarrow	165	0.11898
				160	\rightarrow	167	-0.21959
				160	\rightarrow	168	-0.16056
24	3.819	324.65	0.0024	158	\rightarrow	165	0.59889
				158	\rightarrow	169	-0.10934
				158	\rightarrow	175	0.12515
				160	\rightarrow	169	-0.22057
25	3.8345	323.34	0.0161	158	\rightarrow	164	-0.14446
				158	\rightarrow	165	0.2433
				159	\rightarrow	165	-0.27432
				160	\rightarrow	168	-0.25939
				160	\rightarrow	169	0.41161
				160	\rightarrow	175	-0.18197
26	3.8508	321.97	0.0969	155	\rightarrow	161	0.63629
				155	\rightarrow	162	-0.14711
				159	\rightarrow	166	-0.15253
				159	\rightarrow	167	-0.12305
27	3.8924	318.53	0.0182	155	\rightarrow	161	0.20993
				159	\rightarrow	164	-0.16302
				159	\rightarrow	166	0.5703
				159	\rightarrow	167	0.27222
28	3.9636	312.81	0.0038	154	\rightarrow	161	-0.10886
				155	\rightarrow	162	-0.20138
				158	\rightarrow	165	-0.11463
				158	\rightarrow	166	0.32769
				158	\rightarrow	169	-0.12617
				158	\rightarrow	175	0.17524
				159	\rightarrow	167	-0.10776
				159	\rightarrow	176	-0.11139
				160	\rightarrow	168	-0.22176
				160	\rightarrow	169	0.11669
				160	\rightarrow	175	0.20172

				160	\rightarrow	176	-0.16495
29	3.9744	311.96	0.0064	155	\rightarrow	162	-0.14649
				158	\rightarrow	165	-0.15671
				158	\rightarrow	166	0.26789
				158	\rightarrow	169	-0.12434
				158	\rightarrow	175	0.12291
				159	\rightarrow	166	-0.14561
				159	\rightarrow	167	0.32052
				159	\rightarrow	168	-0.15977
				159	\rightarrow	175	-0.11994
				159	\rightarrow	176	0.17239
				160	\rightarrow	168	0.15296
				160	\rightarrow	175	-0.1127
				160	\rightarrow	176	0.11601
30	3.9931	310.5	0.0054	154	\rightarrow	161	0.40598
				155	\rightarrow	161	0.1211
				155	\rightarrow	162	0.35382
				155	\rightarrow	163	0.12967
				158	\rightarrow	166	0.29926
				158	\rightarrow	167	0.1548
31	4.0182	308.56	0.008	154	\rightarrow	161	0.27553
				158	\rightarrow	166	-0.13709
				158	\rightarrow	167	-0.21105
				158	\rightarrow	175	0.11194
				159	\rightarrow	166	-0.19556
				159	\rightarrow	167	0.29353
				159	\rightarrow	168	0.10927
				159	\rightarrow	169	0.163
				159	\rightarrow	175	-0.14081
				159	\rightarrow	176	-0.10566
				160	\rightarrow	169	0.18277
				160	\rightarrow	175	0.14263
32	4.0231	308.18	0.003	154	\rightarrow	161	0.4472
				154	\rightarrow	162	-0.18881
				154	\rightarrow	163	-0.12423
				155	\rightarrow	162	-0.40607
				159	\rightarrow	167	-0.1674
33	4.0491	306.2	0.0041	155	\rightarrow	162	-0.10503
				158	\rightarrow	165	0.13133
				158	\rightarrow	166	0.20259
				158	\rightarrow	167	0.25324
				158	\rightarrow	168	0.13579
				158	\rightarrow	169	0.19238
				158	\rightarrow	175	-0.22746
				158	\rightarrow	176	-0.1561
				159	\rightarrow	165	0.10039

				159	→	167	0.123
				159	→	168	0.17388
				159	→	169	0.16355
				159	→	176	-0.14992
				160	→	168	0.11694
				160	→	176	0.15659
34	4.0915	303.03	0.0042	154	→	162	0.33997
				154	→	163	0.11069
				155	→	162	-0.27191
				155	→	163	0.29723
				159	→	167	0.22577
				159	→	169	-0.12948
				159	→	175	0.15235
				160	→	168	-0.12571
				160	→	176	-0.16688
35	4.1082	301.8	0.0004	154	→	162	-0.24518
				155	→	163	-0.27925
				158	→	166	-0.14785
				158	→	167	0.30009
				158	→	175	-0.13111
				159	→	166	-0.11435
				159	→	167	0.19411
				159	→	169	-0.11099
				159	→	175	0.18062
				160	→	169	-0.12989
				160	→	176	-0.15905
36	4.1573	298.23	0.0072	154	→	162	0.18499
				158	→	166	-0.31781
				158	→	167	0.44716
				158	→	168	-0.10965
				158	→	175	0.17843
				159	→	169	0.11225
				159	→	175	-0.14176
37	4.1937	295.64	0.0027	153	→	161	0.11951
				153	→	162	0.17432
				154	→	162	0.40239
				154	→	163	-0.27925
				155	→	163	-0.38389
				157	→	164	0.12092
38	4.225	293.45	0.0007	153	→	163	0.13193
				154	→	163	0.12781
				157	→	164	0.41048
				157	→	165	-0.2989
				157	→	166	-0.24017
				158	→	168	-0.10928
				159	→	168	0.19424

39	4.2631	290.83	0.0044	154	→	162	0.11931
				154	→	163	0.12956
				155	→	163	-0.15574
				157	→	164	-0.19894
				158	→	168	-0.28527
				159	→	168	0.4046
				160	→	169	-0.10211
				160	→	171	-0.10306
				160	→	175	-0.21343
40	4.3051	287.99	0.0036	153	→	163	0.10213
				154	→	163	0.50613
				155	→	163	-0.29372
				156	→	165	-0.11622
				159	→	168	-0.25592
				159	→	169	0.10842

Table S6. TDDFT calculated transitions for *fac*-[Ru(Q3Pz)₃]⁻.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	1.9016	651.98	0.0087	160	→	162	0.69055
2	1.9295	642.58	0.0578	160	→	161	0.66462
				160	→	163	0.18093
3	2.1123	586.95	0.0546	158	→	162	0.12946
				158	→	163	-0.11111
				159	→	161	0.478
				159	→	162	-0.10123
				160	→	161	0.18884
				160	→	163	-0.41893
4	2.1537	575.67	0.0048	158	→	161	-0.12106
				159	→	161	0.21652
				159	→	162	0.47191
				159	→	163	-0.44071
5	2.1846	567.53	0.0435	158	→	162	-0.21594
				158	→	163	0.1778
				159	→	161	0.43178
				159	→	162	-0.26191
				160	→	161	-0.10282
				160	→	163	0.37818
6	2.2314	555.62	0.0006	158	→	161	-0.11708
				158	→	162	-0.20073
				159	→	162	0.37985
				159	→	163	0.52618
7	2.2699	546.21	0.0122	158	→	161	0.6073
				158	→	163	-0.2948
				159	→	162	0.12975
8	2.3861	519.61	0.1233	158	→	161	0.28431

				158	\rightarrow	163	0.58686
				160	\rightarrow	163	-0.20784
9	2.5923	478.27	0.0756	158	\rightarrow	162	0.58413
				159	\rightarrow	161	0.12138
				159	\rightarrow	162	0.14428
				160	\rightarrow	163	0.28266
10	3.0508	406.4	0.0478	155	\rightarrow	161	-0.17166
				157	\rightarrow	161	0.58304
				157	\rightarrow	162	-0.20629
				160	\rightarrow	164	-0.23432
11	3.0523	406.2	0.0046	157	\rightarrow	161	0.2169
				160	\rightarrow	164	0.64514
12	3.1479	393.87	0.0689	155	\rightarrow	162	-0.11096
				156	\rightarrow	161	0.34023
				157	\rightarrow	161	-0.12183
				157	\rightarrow	162	-0.32179
				157	\rightarrow	163	0.4742
13	3.1594	392.43	0.0544	155	\rightarrow	161	0.26088
				155	\rightarrow	163	0.13152
				156	\rightarrow	161	0.39259
				156	\rightarrow	162	-0.22838
				156	\rightarrow	163	0.23189
				157	\rightarrow	161	0.17982
				157	\rightarrow	162	0.14163
				157	\rightarrow	163	-0.12543
				160	\rightarrow	165	0.25207
				160	\rightarrow	166	-0.10539
14	3.1834	389.47	0.0469	155	\rightarrow	162	0.10888
				156	\rightarrow	161	-0.19821
				156	\rightarrow	163	-0.10235
				157	\rightarrow	163	0.16755
				160	\rightarrow	165	0.59925
				160	\rightarrow	166	-0.1273
15	3.1907	388.58	0.0574	155	\rightarrow	161	0.30092
				155	\rightarrow	162	0.35663
				155	\rightarrow	163	-0.10769
				156	\rightarrow	161	-0.1112
				156	\rightarrow	162	-0.13481
				157	\rightarrow	161	0.10382
				157	\rightarrow	162	0.22653
				157	\rightarrow	163	0.35516
				160	\rightarrow	165	-0.15244
				160	\rightarrow	166	0.10936
16	3.2402	382.65	0.0064	155	\rightarrow	161	-0.32717
				155	\rightarrow	162	0.20369
				155	\rightarrow	163	0.15271

					156	→	161	0.28728
					156	→	162	0.31252
					157	→	162	0.34633
17	3.2518	381.28	0.0188	155	→	161	0.35563	
				155	→	163	-0.20204	
				156	→	162	0.53447	
18	3.2904	376.81	0.0018	157	→	162	-0.10593	
				160	→	165	0.16899	
				160	→	166	0.64254	
19	3.3352	371.74	0.0076	155	→	162	0.50845	
				156	→	161	0.10911	
				157	→	161	-0.11743	
				157	→	162	-0.36471	
				157	→	163	-0.21392	
20	3.3612	368.87	0.0029	158	→	164	-0.11735	
				159	→	164	0.67607	
21	3.3972	364.96	0.0056	155	→	163	0.55642	
				156	→	161	-0.22132	
				156	→	162	0.13871	
				156	→	163	0.25219	
				157	→	163	0.17275	
22	3.3997	364.69	0.0037	155	→	161	-0.20833	
				155	→	162	0.14627	
				155	→	163	-0.25144	
				156	→	163	0.57938	
				157	→	161	-0.10573	
23	3.4532	359.04	0.0003	158	→	164	0.64294	
				158	→	165	-0.10729	
				159	→	164	0.11212	
				159	→	165	-0.1357	
				159	→	166	-0.1028	
24	3.4937	354.88	0.0016	158	→	164	0.12722	
				159	→	165	0.67762	
25	3.5681	347.48	0.0091	158	→	165	0.64823	
				160	→	169	0.16206	
26	3.6025	344.16	0.0042	158	→	165	-0.17139	
				159	→	166	0.543	
				160	→	167	-0.17074	
				160	→	169	0.29871	
				160	→	175	0.11205	
27	3.6306	341.5	0.0038	158	→	164	-0.15633	
				158	→	165	-0.11615	
				158	→	166	0.16738	
				159	→	166	-0.32504	
				160	→	168	-0.12748	
				160	→	169	0.44842	

					160	\rightarrow	174	-0.15438
					160	\rightarrow	175	0.11929
28	3.6829	336.65	0.0084		160	\rightarrow	167	0.31472
					160	\rightarrow	168	0.54851
					160	\rightarrow	169	0.15382
					160	\rightarrow	175	0.13867
29	3.6927	335.76	0.0118		158	\rightarrow	166	0.64486
					159	\rightarrow	166	0.12706
					160	\rightarrow	169	-0.12179
30	3.7273	332.64	0.0551		154	\rightarrow	162	0.10159
					159	\rightarrow	166	0.12185
					159	\rightarrow	169	-0.14458
					160	\rightarrow	167	0.50926
					160	\rightarrow	168	-0.35641
					160	\rightarrow	169	0.11034
31	3.8092	325.49	0.0017		158	\rightarrow	174	-0.1562
					159	\rightarrow	166	-0.1392
					159	\rightarrow	167	0.22769
					159	\rightarrow	168	0.17591
					159	\rightarrow	169	-0.3138
					159	\rightarrow	174	0.34214
					160	\rightarrow	167	-0.19797
					160	\rightarrow	175	0.14591
32	3.9102	317.08	0.0141		154	\rightarrow	161	0.59652
					154	\rightarrow	162	-0.12935
					154	\rightarrow	163	0.16388
					159	\rightarrow	167	0.1317
					159	\rightarrow	169	-0.12715
33	3.9357	315.02	0.0144		154	\rightarrow	161	0.24183
					158	\rightarrow	167	-0.23938
					158	\rightarrow	169	0.23605
					158	\rightarrow	174	-0.17341
					159	\rightarrow	168	0.29633
					159	\rightarrow	169	0.18901
					159	\rightarrow	175	0.18115
					160	\rightarrow	169	0.15973
					160	\rightarrow	174	0.19267
34	3.949	313.96	0.0158		154	\rightarrow	162	-0.10566
					159	\rightarrow	167	0.59343
					159	\rightarrow	168	-0.14132
					159	\rightarrow	169	0.20577
35	3.9741	311.98	0.0133		154	\rightarrow	162	0.34982
					154	\rightarrow	163	-0.13138
					158	\rightarrow	167	0.24757
					158	\rightarrow	174	0.16639
					158	\rightarrow	175	0.20649

					159	→	168	0.18169
					160	→	169	-0.10251
					160	→	175	0.24757
36	3.9818	311.38	0.0029		154	→	162	-0.20918
					154	→	163	0.19829
					158	→	168	0.25906
					158	→	169	0.21486
					158	→	175	0.23669
					159	→	167	-0.13464
					159	→	168	-0.23019
					160	→	175	0.27647
37	4.0183	308.55	0.0067		154	→	162	0.47517
					158	→	167	-0.3102
					159	→	168	-0.2873
					160	→	167	-0.11208
38	4.0557	305.7	0.0067		154	→	162	0.11696
					158	→	167	0.44847
					158	→	168	-0.17522
					158	→	169	0.26688
					158	→	174	-0.15574
					159	→	168	-0.23425
39	4.0727	304.43	0.0064		152	→	161	0.14162
					153	→	161	-0.19791
					154	→	162	0.11823
					154	→	163	0.54883
					158	→	167	0.10213
					159	→	168	0.22743
					160	→	175	-0.10413
40	4.1041	302.1	0.0073		148	→	163	0.12528
					155	→	164	-0.1023
					155	→	165	-0.11287
					157	→	164	0.55468
					157	→	165	0.23259
					159	→	168	-0.11502

Table S7. TDDFT calculated transitions for *mer*-[Ru(Q3PzH)₃]²⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.731	453.99	0.1438	159	→	161	0.14756
				160	→	161	0.66451
				160	→	162	0.14543
2	2.8101	441.21	0.0175	159	→	161	-0.1347
				160	→	161	-0.12092
				160	→	162	0.66208
				160	→	163	0.13349
3	2.8521	434.72	0.0561	159	→	161	0.64847
				160	→	161	-0.16601

				160	\rightarrow	162	0.12942
				160	\rightarrow	163	-0.15037
4	2.9389	421.87	0.0303	158	\rightarrow	161	-0.29867
				159	\rightarrow	161	0.1245
				159	\rightarrow	162	-0.26671
				159	\rightarrow	163	0.27546
				160	\rightarrow	163	0.47159
5	2.9549	419.59	0.0096	158	\rightarrow	161	0.53195
				158	\rightarrow	162	0.14898
				159	\rightarrow	162	-0.41028
6	2.9876	415	0.03	158	\rightarrow	161	0.153
				159	\rightarrow	162	0.17915
				159	\rightarrow	163	0.62369
				160	\rightarrow	163	-0.16043
7	3.0211	410.4	0.0034	158	\rightarrow	161	0.27513
				158	\rightarrow	162	-0.3027
				158	\rightarrow	163	-0.22086
				159	\rightarrow	162	0.35481
				159	\rightarrow	163	-0.12157
				160	\rightarrow	163	0.34007
8	3.0962	400.43	0.0155	158	\rightarrow	162	-0.37113
				158	\rightarrow	163	0.56929
9	3.2321	383.61	0.105	158	\rightarrow	162	0.46789
				158	\rightarrow	163	0.30806
				159	\rightarrow	162	0.2873
				160	\rightarrow	163	0.24396
10	3.5989	344.51	0.0016	158	\rightarrow	172	0.15121
				158	\rightarrow	174	0.12216
				159	\rightarrow	175	-0.10007
				160	\rightarrow	164	0.14697
				160	\rightarrow	165	-0.26368
				160	\rightarrow	166	0.18571
				160	\rightarrow	168	0.19788
				160	\rightarrow	170	-0.11003
				160	\rightarrow	171	-0.15001
				160	\rightarrow	172	0.27206
				160	\rightarrow	173	-0.1548
				160	\rightarrow	174	0.2213
11	3.7469	330.9	0.0046	157	\rightarrow	161	0.29799
				158	\rightarrow	172	-0.13332
				158	\rightarrow	174	-0.10889
				159	\rightarrow	165	0.18962
				159	\rightarrow	168	-0.10191
				159	\rightarrow	172	-0.20676
				159	\rightarrow	173	0.15912
				159	\rightarrow	174	-0.16129

				159	→	175	-0.12962
				160	→	164	-0.14224
				160	→	165	-0.14136
				160	→	175	0.18755
12	3.7635	329.44	0.0014	157	→	161	0.61624
				159	→	172	0.10317
13	3.7929	326.88	0.0016	158	→	172	-0.12215
				160	→	164	0.592
				160	→	165	0.16475
				160	→	166	0.1066
14	3.8964	318.2	0.0537	156	→	161	-0.2411
				157	→	162	-0.12267
				157	→	163	0.25336
				158	→	171	0.15746
				158	→	172	-0.11623
				158	→	175	0.19144
				159	→	171	-0.11498
				159	→	175	-0.1809
				160	→	164	-0.12317
				160	→	171	-0.16847
				160	→	172	0.11313
				160	→	175	-0.23647
15	3.8989	318	0.1532	155	→	161	0.11994
				156	→	161	-0.30244
				157	→	162	-0.23348
				157	→	163	0.40818
				158	→	175	-0.11877
				159	→	175	0.12752
				160	→	164	0.15475
				160	→	171	0.10834
				160	→	175	0.12169
16	3.9306	315.43	0.0298	156	→	161	0.13949
				156	→	162	0.10276
				157	→	162	-0.10613
				158	→	171	-0.11029
				158	→	172	0.1692
				158	→	174	0.13436
				159	→	164	-0.11201
				159	→	165	0.15542
				159	→	172	-0.12069
				160	→	165	0.4495
				160	→	169	0.10594
17	3.9451	314.27	0.0094	156	→	161	0.50031
				156	→	162	0.14841
				157	→	162	-0.35486
				157	→	163	0.14705

				160	\rightarrow	165	-0.14582
18	3.9877	310.92	0.0215	155	\rightarrow	161	0.1239
				156	\rightarrow	161	0.2357
				156	\rightarrow	162	-0.21529
				157	\rightarrow	162	0.45182
				157	\rightarrow	163	0.40739
19	4.0153	308.78	0.0403	155	\rightarrow	162	0.19343
				156	\rightarrow	162	0.52007
				157	\rightarrow	162	0.25583
				159	\rightarrow	164	0.205
				160	\rightarrow	166	-0.1737
20	4.0243	308.09	0.0344	156	\rightarrow	162	0.26391
				159	\rightarrow	164	-0.38547
				160	\rightarrow	166	0.38661
				160	\rightarrow	168	0.13893
21	4.058	305.53	0.0211	159	\rightarrow	164	0.45275
				159	\rightarrow	165	0.14787
				159	\rightarrow	166	0.11176
				159	\rightarrow	175	0.12493
				160	\rightarrow	166	0.40053
22	4.1149	301.31	0.0075	155	\rightarrow	161	0.61142
				156	\rightarrow	163	0.20125
				157	\rightarrow	163	-0.23146
23	4.124	300.64	0.0135	156	\rightarrow	163	0.40883
				158	\rightarrow	164	0.21713
				158	\rightarrow	165	-0.16258
				159	\rightarrow	164	0.12314
				159	\rightarrow	165	-0.20227
				159	\rightarrow	166	-0.31141
				159	\rightarrow	168	-0.10515
24	4.1395	299.52	0.0129	155	\rightarrow	161	-0.16281
				156	\rightarrow	163	0.45448
				158	\rightarrow	164	-0.40282
				158	\rightarrow	167	-0.11004
				159	\rightarrow	166	0.1522
25	4.1513	298.66	0.0146	156	\rightarrow	163	0.2141
				158	\rightarrow	164	0.36564
				158	\rightarrow	165	0.13279
				158	\rightarrow	166	0.13753
				159	\rightarrow	165	0.28811
				159	\rightarrow	166	0.24262
				160	\rightarrow	165	-0.10434
				160	\rightarrow	167	-0.24856
26	4.1681	297.46	0.008	152	\rightarrow	161	-0.12405
				153	\rightarrow	161	0.12898
				153	\rightarrow	163	-0.10089

				158	\rightarrow	164	0.26219
				158	\rightarrow	165	0.15455
				159	\rightarrow	166	0.13428
				160	\rightarrow	164	-0.11617
				160	\rightarrow	165	0.1933
				160	\rightarrow	167	0.44131
				160	\rightarrow	168	0.1273
27	4.1907	295.86	0.0029	154	\rightarrow	161	-0.1093
				158	\rightarrow	166	-0.10404
				159	\rightarrow	175	0.10391
				160	\rightarrow	165	0.10145
				160	\rightarrow	166	-0.16703
				160	\rightarrow	167	-0.21909
				160	\rightarrow	168	0.5262
				160	\rightarrow	169	-0.16031
28	4.2436	292.17	0.0117	155	\rightarrow	163	-0.10854
				158	\rightarrow	165	0.304
				158	\rightarrow	166	0.38821
				158	\rightarrow	168	0.1341
				159	\rightarrow	166	-0.25463
				159	\rightarrow	168	-0.19829
				160	\rightarrow	168	0.16358
				160	\rightarrow	175	-0.13054
29	4.2556	291.35	0.0151	155	\rightarrow	163	0.29751
				158	\rightarrow	165	0.24698
				159	\rightarrow	165	-0.23431
				159	\rightarrow	175	-0.11872
				160	\rightarrow	165	0.15546
				160	\rightarrow	166	0.14225
				160	\rightarrow	167	-0.22816
				160	\rightarrow	168	-0.12905
				160	\rightarrow	169	-0.21316
30	4.2849	289.35	0	155	\rightarrow	162	0.50782
				155	\rightarrow	163	-0.32133
				156	\rightarrow	162	-0.14449
				159	\rightarrow	165	-0.12917
				160	\rightarrow	169	-0.17488
31	4.2938	288.75	0.0016	155	\rightarrow	162	-0.24519
				155	\rightarrow	163	-0.17862
				158	\rightarrow	165	-0.17543
				158	\rightarrow	166	0.27511
				158	\rightarrow	169	-0.10227
				159	\rightarrow	165	-0.27349
				159	\rightarrow	166	0.26777
				159	\rightarrow	172	-0.13616
32	4.3144	287.37	0.0015	155	\rightarrow	162	0.14996

				155	→	163	0.233
				158	→	168	0.10191
				159	→	165	-0.19139
				159	→	166	0.12157
				159	→	167	-0.21329
				159	→	168	0.15487
				159	→	172	-0.10695
				160	→	168	0.15239
				160	→	169	0.37641
33	4.3411	285.61	0.0044	154	→	162	-0.11338
				155	→	162	0.28834
				155	→	163	0.38492
				158	→	165	-0.18975
				158	→	166	0.11085
				159	→	166	0.10079
				159	→	167	0.25872
				159	→	168	-0.18416
34	4.3775	283.23	0.0125	155	→	163	0.12064
				158	→	165	-0.18694
				158	→	166	0.24013
				159	→	165	0.12659
				159	→	166	-0.19008
				159	→	167	-0.17543
				159	→	168	0.41578
				160	→	167	0.10275
				160	→	169	-0.23866
				160	→	172	-0.12912
35	4.4289	279.94	0.0209	154	→	162	-0.12431
				158	→	167	0.30484
				158	→	168	-0.29076
				159	→	167	-0.23655
				159	→	168	-0.14405
				159	→	171	-0.1159
				159	→	172	0.17216
				159	→	174	0.11395
				160	→	169	0.12176
				160	→	171	0.1063
				160	→	175	0.18292
36	4.4353	279.54	0.0051	158	→	166	0.14948
				158	→	172	-0.12903
				158	→	173	0.11312
				158	→	175	-0.10619
				159	→	166	-0.10877
				159	→	167	0.36758
				159	→	168	0.25503
				160	→	165	0.10424

				160	\rightarrow	169	0.19647
				160	\rightarrow	172	0.14218
				160	\rightarrow	173	-0.112
				160	\rightarrow	175	0.15938
37	4.4675	277.53	0.002	158	\rightarrow	167	0.17233
				158	\rightarrow	172	-0.12488
				159	\rightarrow	166	-0.10341
				159	\rightarrow	167	-0.18207
				159	\rightarrow	169	-0.14085
				159	\rightarrow	171	0.22117
				159	\rightarrow	172	-0.13132
				159	\rightarrow	173	-0.11482
				159	\rightarrow	175	0.28701
				159	\rightarrow	177	-0.10229
				160	\rightarrow	168	-0.11671
				160	\rightarrow	171	-0.17627
				160	\rightarrow	172	0.20124
				160	\rightarrow	174	0.15158
38	4.4958	275.78	0.0018	152	\rightarrow	162	-0.10516
				154	\rightarrow	162	0.12387
				158	\rightarrow	166	0.18436
				158	\rightarrow	167	0.10215
				158	\rightarrow	169	0.14964
				159	\rightarrow	168	-0.14272
				159	\rightarrow	169	0.45984
				159	\rightarrow	172	0.10303
				159	\rightarrow	175	0.10672
39	4.533	273.51	0.0074	158	\rightarrow	164	-0.12208
				158	\rightarrow	165	0.20801
				158	\rightarrow	166	-0.14696
				158	\rightarrow	167	0.43486
				158	\rightarrow	168	0.33264
				158	\rightarrow	169	-0.13248
				159	\rightarrow	167	0.16246
				159	\rightarrow	168	0.11414
40	4.5554	272.17	0.0074	154	\rightarrow	161	-0.15306
				154	\rightarrow	163	-0.10706
				158	\rightarrow	168	-0.31695
				158	\rightarrow	169	-0.26569
				159	\rightarrow	165	-0.11163
				159	\rightarrow	168	0.14359
				159	\rightarrow	169	0.36773
				160	\rightarrow	169	0.10574

Table S8. TDDFT calculated transitions for *mer*-[Ru(Q3PzH)₂(Q3Pz_a)]⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.2748	545.03	0.006	160	→	161	-0.47304
				160	→	162	0.51488
2	2.3697	523.21	0.159	160	→	161	0.51265
				160	→	162	0.46974
3	2.5739	481.69	0.0596	158	→	163	0.13777
				159	→	161	-0.24679
				159	→	162	0.16661
				160	→	163	0.60843
4	2.6251	472.29	0.0055	159	→	161	0.50873
				159	→	162	0.45972
5	2.7364	453.09	0.0228	158	→	161	0.28151
				158	→	162	-0.24477
				159	→	161	0.27756
				159	→	162	-0.233
				159	→	163	0.43362
				160	→	163	0.11066
				158	→	161	-0.37515
				158	→	162	0.44251
6	2.7621	448.88	0.0028	159	→	161	0.15254
				159	→	162	-0.13629
				159	→	163	0.27499
				160	→	163	0.16344
				158	→	161	0.49121
				158	→	162	0.45083
7	2.7963	443.39	0.0722	158	→	163	-0.1389
				159	→	162	0.10698
				158	→	163	-0.28397
				159	→	161	-0.23532
8	2.8518	434.75	0.0659	159	→	162	0.36211
				159	→	163	0.43444
				160	→	163	-0.1311
				157	→	163	-0.10602
				158	→	163	0.57797
9	3.0302	409.16	0.0239	159	→	161	-0.11682
				159	→	162	0.1626
				159	→	163	0.13198
				160	→	163	-0.20321
				157	→	161	0.59474
10	3.2474	381.79	0.0177	157	→	162	0.32942
				157	→	161	-0.285
11	3.3979	364.89	0.0162	157	→	162	0.56611
				157	→	163	-0.20397
				160	→	165	-0.11212
				157	→	161	-0.10765
12	3.4304	361.43	0.0122	157	→	162	0.2048

				157	\rightarrow	163	0.12451
				160	\rightarrow	164	-0.21238
				160	\rightarrow	165	0.4631
				160	\rightarrow	166	-0.18561
				160	\rightarrow	167	0.19861
				160	\rightarrow	169	0.1458
				160	\rightarrow	173	0.15081
13	3.4836	355.91	0.0351	157	\rightarrow	161	-0.15648
				157	\rightarrow	163	0.58993
				160	\rightarrow	164	0.26709
				160	\rightarrow	165	-0.14101
14	3.5384	350.39	0.0108	157	\rightarrow	163	-0.24832
				160	\rightarrow	164	0.55484
				160	\rightarrow	165	0.10224
				160	\rightarrow	166	-0.14573
				160	\rightarrow	167	0.12267
				160	\rightarrow	169	0.1032
				160	\rightarrow	173	0.11868
15	3.6187	342.62	0.0021	160	\rightarrow	164	0.13165
				160	\rightarrow	165	0.35371
				160	\rightarrow	166	0.5398
				160	\rightarrow	169	-0.14963
16	3.709	334.28	0.0035	159	\rightarrow	164	0.21081
				159	\rightarrow	165	0.24819
				159	\rightarrow	166	-0.11324
				159	\rightarrow	167	0.20202
				159	\rightarrow	169	0.19208
				159	\rightarrow	173	0.2953
				159	\rightarrow	175	0.11028
				160	\rightarrow	164	0.12444
				160	\rightarrow	165	0.17458
				160	\rightarrow	166	-0.14618
				160	\rightarrow	167	-0.14984
				160	\rightarrow	177	0.12117
17	3.7739	328.53	0.0016	158	\rightarrow	165	-0.11951
				158	\rightarrow	169	-0.103
				158	\rightarrow	173	-0.11539
				159	\rightarrow	164	0.22555
				159	\rightarrow	173	0.10346
				160	\rightarrow	164	-0.10591
				160	\rightarrow	165	-0.25361
				160	\rightarrow	166	0.21613
				160	\rightarrow	167	0.36517
				160	\rightarrow	169	0.13868
				160	\rightarrow	173	0.14699
18	3.798	326.45	0.001	158	\rightarrow	165	0.12413

				159	\rightarrow	164	0.5377
				159	\rightarrow	165	-0.15812
				159	\rightarrow	166	0.16311
				159	\rightarrow	168	0.14049
				160	\rightarrow	166	-0.13251
19	3.8377	323.06	0.0206	155	\rightarrow	161	-0.10409
				158	\rightarrow	165	-0.11302
				160	\rightarrow	164	-0.11237
				160	\rightarrow	167	-0.32574
				160	\rightarrow	168	0.50248
20	3.8842	319.2	0.0817	155	\rightarrow	161	-0.18446
				155	\rightarrow	162	0.25958
				156	\rightarrow	162	0.19844
				158	\rightarrow	164	0.1083
				159	\rightarrow	164	-0.18106
				160	\rightarrow	166	-0.15061
				160	\rightarrow	167	0.29865
				160	\rightarrow	168	0.27091
				160	\rightarrow	169	-0.19553
				160	\rightarrow	173	-0.13049
21	3.894	318.4	0.031	155	\rightarrow	161	-0.21767
				155	\rightarrow	162	0.43464
				156	\rightarrow	161	-0.30058
				156	\rightarrow	162	0.1207
				158	\rightarrow	164	-0.10491
				160	\rightarrow	167	-0.15197
				160	\rightarrow	168	-0.26242
22	3.9164	316.58	0.089	155	\rightarrow	161	-0.18539
				156	\rightarrow	161	0.43782
				156	\rightarrow	162	0.44317
				158	\rightarrow	164	-0.12408
23	3.972	312.15	0.0184	156	\rightarrow	162	0.14142
				158	\rightarrow	164	0.24427
				158	\rightarrow	167	0.10296
				158	\rightarrow	173	0.11959
				159	\rightarrow	165	0.43801
				159	\rightarrow	166	0.21125
				159	\rightarrow	167	0.1078
				160	\rightarrow	169	0.1312
				160	\rightarrow	177	-0.10818
24	3.9923	310.56	0.0117	155	\rightarrow	161	0.51787
				155	\rightarrow	162	0.39698
				156	\rightarrow	161	0.21424
25	4.0153	308.78	0.0155	158	\rightarrow	164	-0.26054
				158	\rightarrow	165	-0.25612
				158	\rightarrow	167	-0.19783

				158	\rightarrow	169	-0.1007
				158	\rightarrow	173	-0.10647
				159	\rightarrow	165	0.24786
				159	\rightarrow	166	0.32863
				160	\rightarrow	169	-0.22603
26	4.0249	308.04	0.0068	155	\rightarrow	161	0.27248
				155	\rightarrow	162	-0.182
				156	\rightarrow	161	-0.3091
				156	\rightarrow	162	0.40241
				158	\rightarrow	164	0.14088
				158	\rightarrow	165	-0.23099
27	4.0432	306.65	0.0202	155	\rightarrow	161	-0.10048
				155	\rightarrow	162	0.12843
				156	\rightarrow	161	0.20345
				156	\rightarrow	162	-0.17009
				158	\rightarrow	164	0.37564
				158	\rightarrow	165	-0.32953
				159	\rightarrow	165	-0.17819
				160	\rightarrow	168	-0.16176
28	4.0789	303.96	0.0057	159	\rightarrow	164	-0.17169
				159	\rightarrow	165	-0.24725
				159	\rightarrow	166	0.41785
				159	\rightarrow	167	0.29604
				159	\rightarrow	168	0.21849
				159	\rightarrow	173	0.11554
				160	\rightarrow	169	0.11705
29	4.0901	303.13	0.0032	158	\rightarrow	164	0.14494
				158	\rightarrow	166	-0.15645
				158	\rightarrow	176	-0.16025
				158	\rightarrow	177	0.25571
				159	\rightarrow	166	0.12462
				160	\rightarrow	171	0.11242
				160	\rightarrow	172	0.13414
				160	\rightarrow	174	-0.14097
				160	\rightarrow	176	-0.18463
				160	\rightarrow	177	0.36003
30	4.1422	299.32	0.0091	156	\rightarrow	163	0.10487
				158	\rightarrow	164	0.22056
				158	\rightarrow	165	0.24521
				158	\rightarrow	166	0.43834
				158	\rightarrow	169	-0.10456
				158	\rightarrow	173	-0.1162
				159	\rightarrow	166	0.10698
				159	\rightarrow	167	-0.11979
				159	\rightarrow	168	-0.20225
31	4.2031	294.98	0.0057	154	\rightarrow	161	0.18485

				154	\rightarrow	162	0.10291
				155	\rightarrow	163	0.10166
				156	\rightarrow	163	0.59023
				159	\rightarrow	166	-0.10673
				159	\rightarrow	167	0.10183
				159	\rightarrow	168	0.1255
32	4.2148	294.17	0.0112	154	\rightarrow	161	-0.14101
				155	\rightarrow	163	0.20703
				156	\rightarrow	163	-0.13366
				158	\rightarrow	166	0.3156
				159	\rightarrow	166	-0.25259
				159	\rightarrow	167	0.25936
				159	\rightarrow	168	0.18428
				159	\rightarrow	169	-0.1563
				159	\rightarrow	173	-0.16405
33	4.2281	293.24	0.0052	155	\rightarrow	163	0.20232
				156	\rightarrow	163	-0.14807
				158	\rightarrow	164	0.23015
				158	\rightarrow	165	0.20086
				158	\rightarrow	166	-0.16435
				158	\rightarrow	167	-0.14235
				158	\rightarrow	168	-0.19706
				158	\rightarrow	169	-0.11199
				158	\rightarrow	173	-0.14759
				159	\rightarrow	167	-0.12175
				159	\rightarrow	168	0.35977
				160	\rightarrow	169	-0.14361
34	4.2448	292.09	0.0107	154	\rightarrow	161	0.28675
				154	\rightarrow	162	0.19235
				155	\rightarrow	163	-0.30972
				156	\rightarrow	163	-0.16347
				158	\rightarrow	165	0.11188
				158	\rightarrow	167	-0.1096
				159	\rightarrow	167	0.32019
				159	\rightarrow	168	-0.10617
				160	\rightarrow	169	-0.20426
35	4.2619	290.91	0.0139	155	\rightarrow	163	0.45214
				158	\rightarrow	165	0.11858
				158	\rightarrow	166	-0.1767
				159	\rightarrow	167	0.20087
				159	\rightarrow	168	-0.359
36	4.2705	290.32	0.0031	154	\rightarrow	161	0.395
				154	\rightarrow	162	0.25719
				155	\rightarrow	163	0.26678
				156	\rightarrow	163	-0.16768
				158	\rightarrow	165	-0.17564

					158	\rightarrow	167	0.30154
					159	\rightarrow	167	-0.11205
37	4.2998	288.35	0.0214		154	\rightarrow	161	-0.20413
					154	\rightarrow	162	-0.12708
					155	\rightarrow	163	-0.12095
					157	\rightarrow	166	-0.10348
					158	\rightarrow	165	-0.11139
					158	\rightarrow	166	-0.10935
					158	\rightarrow	167	0.45305
					158	\rightarrow	168	-0.1079
					160	\rightarrow	169	-0.23863
					160	\rightarrow	173	0.13958
38	4.3395	285.71	0.0044		154	\rightarrow	162	0.1345
					158	\rightarrow	168	0.54405
					159	\rightarrow	167	-0.15117
					159	\rightarrow	168	0.11272
					160	\rightarrow	169	-0.20638
					160	\rightarrow	173	0.14541
39	4.3878	282.56	0.0001		152	\rightarrow	161	-0.13567
					152	\rightarrow	163	-0.11559
					154	\rightarrow	161	-0.21581
					154	\rightarrow	162	0.31773
					154	\rightarrow	163	-0.17781
					157	\rightarrow	164	-0.1022
					157	\rightarrow	166	0.19295
					158	\rightarrow	168	-0.22686
					158	\rightarrow	169	0.17262
					159	\rightarrow	169	0.16109
					160	\rightarrow	169	-0.10683
					160	\rightarrow	173	0.11673
40	4.4199	280.51	0.0024		152	\rightarrow	161	0.15126
					152	\rightarrow	163	0.12548
					154	\rightarrow	161	-0.27996
					154	\rightarrow	162	0.42748
					157	\rightarrow	164	0.13008
					157	\rightarrow	165	-0.14223
					157	\rightarrow	166	-0.25188
					158	\rightarrow	169	-0.10756
					160	\rightarrow	173	-0.13683

Table S9. TDDFT calculated transitions for *mer*-[Ru(Q3PzH)₂(Q3Pz_b)]⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.3575	525.92	0.0222	160	\rightarrow	161	0.58029
				160	\rightarrow	162	0.38308
2	2.423	511.61	0.101	159	\rightarrow	161	0.13462
				160	\rightarrow	161	-0.36945

				160	\rightarrow	162	0.57483
3	2.596	477.58	0.0493	159	\rightarrow	161	0.52499
				159	\rightarrow	162	0.14472
				160	\rightarrow	163	0.41073
4	2.641	469.44	0.0069	158	\rightarrow	161	0.21044
				159	\rightarrow	161	0.10604
				159	\rightarrow	162	0.53668
				159	\rightarrow	163	0.22473
				160	\rightarrow	163	-0.27168
5	2.647	468.24	0.0302	158	\rightarrow	162	0.1514
				159	\rightarrow	161	0.40195
				159	\rightarrow	162	-0.33789
				160	\rightarrow	161	0.10894
				160	\rightarrow	163	-0.40044
6	2.769	447.75	0.0533	157	\rightarrow	161	0.17373
				157	\rightarrow	162	-0.1019
				158	\rightarrow	161	0.55628
				158	\rightarrow	162	-0.25706
				159	\rightarrow	162	-0.13406
				159	\rightarrow	163	-0.19035
7	2.79	444.3	0.0101	158	\rightarrow	162	-0.1993
				158	\rightarrow	163	-0.25582
				159	\rightarrow	162	-0.14409
				159	\rightarrow	163	0.57984
				160	\rightarrow	163	0.11066
8	2.889	429.06	0.0786	157	\rightarrow	162	0.13519
				157	\rightarrow	163	-0.11762
				158	\rightarrow	161	0.2118
				158	\rightarrow	162	0.54224
				158	\rightarrow	163	-0.27724
				159	\rightarrow	161	-0.12053
9	3.022	410.22	0.0536	157	\rightarrow	161	0.22941
				157	\rightarrow	162	-0.12454
				157	\rightarrow	163	0.19274
				158	\rightarrow	161	0.13525
				158	\rightarrow	162	0.15528
				158	\rightarrow	163	0.48362
				159	\rightarrow	163	0.18181
10	3.08	402.48	0.0046	160	\rightarrow	163	0.21852
				157	\rightarrow	161	0.57163
				157	\rightarrow	162	-0.21935
				158	\rightarrow	161	-0.25349
				158	\rightarrow	163	-0.16517
11	3.155	392.93	0.011	159	\rightarrow	163	-0.10328
				157	\rightarrow	161	0.26215
				157	\rightarrow	162	0.601

				158	\rightarrow	162	-0.17177
12	3.285	377.41	0.0707	157	\rightarrow	162	0.13685
				157	\rightarrow	163	0.64251
				158	\rightarrow	163	-0.21074
13	3.429	361.51	0.0116	160	\rightarrow	164	0.45728
				160	\rightarrow	165	-0.18542
				160	\rightarrow	166	0.2852
				160	\rightarrow	167	0.15382
				160	\rightarrow	168	-0.1801
				160	\rightarrow	169	-0.11781
				160	\rightarrow	173	-0.20334
14	3.593	344.99	0.001	159	\rightarrow	164	-0.20451
				159	\rightarrow	166	-0.1564
				159	\rightarrow	167	-0.10382
				159	\rightarrow	173	0.13874
				160	\rightarrow	164	0.32558
				160	\rightarrow	165	0.46135
				160	\rightarrow	168	0.15609
15	3.614	343.02	0.001	158	\rightarrow	173	-0.10254
				160	\rightarrow	164	-0.33909
				160	\rightarrow	165	0.3464
				160	\rightarrow	166	0.3857
				160	\rightarrow	169	-0.14233
				160	\rightarrow	173	-0.14937
16	3.701	334.95	0.0028	157	\rightarrow	173	0.1416
				158	\rightarrow	164	-0.27037
				158	\rightarrow	166	-0.21926
				158	\rightarrow	167	-0.12987
				158	\rightarrow	168	0.12487
				158	\rightarrow	169	0.1411
				158	\rightarrow	173	0.30213
				160	\rightarrow	166	0.24329
17	3.775	328.4	0.0131	158	\rightarrow	165	-0.10149
				159	\rightarrow	164	0.36526
				159	\rightarrow	166	0.1637
				159	\rightarrow	173	-0.20222
				160	\rightarrow	164	0.15439
				160	\rightarrow	165	0.26949
				160	\rightarrow	166	-0.28079
18	3.837	323.08	0.0032	159	\rightarrow	164	0.31477
				159	\rightarrow	165	0.26196
				159	\rightarrow	177	-0.11268
				160	\rightarrow	166	0.25179
				160	\rightarrow	167	-0.30085
				160	\rightarrow	168	0.21902
19	3.85	321.99	0.0315	158	\rightarrow	164	-0.12352

				159	→	164	0.12663
				159	→	165	0.36807
				159	→	168	0.15599
				159	→	173	0.17942
				160	→	166	-0.15635
				160	→	167	0.12864
				160	→	168	-0.26719
				160	→	173	-0.1799
				160	→	176	0.12938
				160	→	177	-0.12635
20	3.866	320.69	0.0078	159	→	164	0.20184
				159	→	166	-0.15599
				159	→	177	-0.11446
				160	→	167	0.52995
				160	→	168	0.11529
				160	→	173	0.13158
21	3.902	317.71	0.0703	155	→	161	-0.10911
				156	→	161	0.5494
				156	→	162	-0.30877
				159	→	164	0.15514
22	3.915	316.68	0.0206	156	→	161	0.13879
				159	→	164	-0.29086
				159	→	165	0.44212
				159	→	166	0.23089
				159	→	173	-0.16521
				160	→	176	-0.10154
				160	→	177	0.13292
23	3.944	314.3	0.0066	156	→	161	0.12956
				159	→	176	-0.10273
				159	→	177	0.13254
				160	→	165	-0.14164
				160	→	167	0.11486
				160	→	168	0.48342
				160	→	169	-0.11692
				160	→	173	-0.21231
				160	→	176	0.11777
24	3.966	312.58	0.0223	157	→	164	0.15842
				157	→	165	0.10255
				158	→	164	0.51576
				158	→	165	0.19411
				158	→	173	0.15671
				159	→	164	0.13447
				159	→	165	0.10462
25	4.004	309.64	0.0774	155	→	161	0.23474
				155	→	162	0.17021
				156	→	161	0.31491

				156	\rightarrow	162	0.52808
26	4.023	308.17	0.0027	157	\rightarrow	165	0.182
				158	\rightarrow	164	-0.19867
				158	\rightarrow	165	0.5609
				158	\rightarrow	166	0.14221
				158	\rightarrow	168	0.13049
				158	\rightarrow	173	-0.10708
27	4.066	304.9	0.0254	154	\rightarrow	161	-0.19114
				155	\rightarrow	161	0.45264
				155	\rightarrow	162	0.11048
				156	\rightarrow	162	-0.18206
				158	\rightarrow	166	0.12321
				159	\rightarrow	166	0.29107
				160	\rightarrow	167	0.12447
				160	\rightarrow	169	0.11045
28	4.093	302.89	0.0044	154	\rightarrow	162	0.12129
				155	\rightarrow	161	-0.2362
				155	\rightarrow	162	-0.35588
				156	\rightarrow	162	0.17462
				159	\rightarrow	166	0.35691
				159	\rightarrow	167	-0.15301
				159	\rightarrow	168	0.12828
				160	\rightarrow	169	0.10908
				160	\rightarrow	177	-0.11159
29	4.124	300.64	0.0214	154	\rightarrow	161	0.29087
				154	\rightarrow	162	-0.22205
				155	\rightarrow	161	-0.21064
				155	\rightarrow	162	0.42187
				156	\rightarrow	163	0.1677
				159	\rightarrow	166	0.18187
				159	\rightarrow	167	-0.11997
30	4.147	298.96	0.004	155	\rightarrow	161	-0.12033
				155	\rightarrow	162	0.14893
				156	\rightarrow	163	-0.2702
				158	\rightarrow	166	-0.22872
				158	\rightarrow	173	-0.1493
				159	\rightarrow	165	-0.16457
				159	\rightarrow	166	0.14246
				159	\rightarrow	167	0.298
				159	\rightarrow	168	0.23669
31	4.148	298.88	0.0215	154	\rightarrow	161	0.1302
				154	\rightarrow	162	-0.14595
				154	\rightarrow	163	0.10583
				155	\rightarrow	162	-0.20053
				156	\rightarrow	163	0.41141
				158	\rightarrow	166	-0.2063

				158	\rightarrow	167	-0.10961
				159	\rightarrow	167	0.28897
				160	\rightarrow	169	0.14395
32	4.183	296.38	0.0098	154	\rightarrow	161	-0.22322
				154	\rightarrow	162	0.10924
				154	\rightarrow	163	0.11749
				155	\rightarrow	161	-0.17104
				155	\rightarrow	162	0.13036
				158	\rightarrow	166	0.14376
				159	\rightarrow	167	0.27148
				159	\rightarrow	168	-0.21674
				159	\rightarrow	173	-0.10042
				160	\rightarrow	169	0.30645
				160	\rightarrow	177	-0.12441
33	4.199	295.27	0.0111	158	\rightarrow	166	0.42151
				158	\rightarrow	173	0.16322
				159	\rightarrow	165	-0.11562
				159	\rightarrow	167	0.31569
				159	\rightarrow	168	0.22476
				160	\rightarrow	169	-0.13123
34	4.21	294.49	0.0055	154	\rightarrow	161	0.41009
				154	\rightarrow	162	-0.14385
				155	\rightarrow	161	0.19657
				155	\rightarrow	162	-0.16657
				156	\rightarrow	163	-0.35828
				160	\rightarrow	169	0.18504
35	4.237	292.59	0.0285	157	\rightarrow	164	0.33096
				157	\rightarrow	165	-0.16795
				157	\rightarrow	166	-0.20836
				158	\rightarrow	165	0.12157
				158	\rightarrow	167	-0.30525
				158	\rightarrow	168	-0.10375
				159	\rightarrow	168	-0.28702
				160	\rightarrow	169	-0.13644
36	4.246	291.94	0.0108	153	\rightarrow	161	-0.16141
				157	\rightarrow	164	0.28049
				157	\rightarrow	165	-0.13358
				158	\rightarrow	167	-0.14883
				159	\rightarrow	166	-0.17604
				159	\rightarrow	168	0.30147
				159	\rightarrow	169	-0.12279
				159	\rightarrow	173	-0.1138
				159	\rightarrow	177	0.11233
				160	\rightarrow	169	0.24552
37	4.278	289.81	0.0168	154	\rightarrow	161	0.20656
				154	\rightarrow	162	0.30489

					154	\rightarrow	163	0.10215
					155	\rightarrow	163	-0.15934
					157	\rightarrow	164	0.25492
					157	\rightarrow	165	-0.15796
					157	\rightarrow	167	0.11193
					158	\rightarrow	164	-0.10698
					158	\rightarrow	166	-0.19152
					158	\rightarrow	167	0.30768
					159	\rightarrow	167	0.13082
38	4.292	288.87	0.0043		154	\rightarrow	161	0.19809
					154	\rightarrow	162	0.43015
					156	\rightarrow	162	-0.10199
					157	\rightarrow	164	-0.14756
					157	\rightarrow	167	-0.11361
					158	\rightarrow	164	0.14958
					158	\rightarrow	166	0.11824
					158	\rightarrow	167	-0.32201
					158	\rightarrow	168	0.16638
39	4.307	287.83	0.0012		153	\rightarrow	161	-0.21483
					153	\rightarrow	162	0.13286
					154	\rightarrow	162	-0.2371
					154	\rightarrow	163	0.13479
					155	\rightarrow	163	-0.23414
					157	\rightarrow	166	0.20648
					158	\rightarrow	168	0.33101
					159	\rightarrow	168	-0.15825
					160	\rightarrow	169	-0.13343
40	4.34	285.68	0.0093		153	\rightarrow	161	-0.22126
					153	\rightarrow	162	0.14855
					154	\rightarrow	163	-0.21488
					155	\rightarrow	163	0.48819
					156	\rightarrow	163	0.17753
					157	\rightarrow	166	0.11212
					158	\rightarrow	167	0.12289
					158	\rightarrow	168	0.14736
					159	\rightarrow	169	0.10226

Table S10. TDDFT calculated transitions for *mer*-[Ru(Q3PzH)₂(Q3Pz_c)]⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.276	544.74	0.1307	159	\rightarrow	161	0.10663
				160	\rightarrow	161	0.69365
2	2.389	518.84	0.0062	160	\rightarrow	162	0.64174
				160	\rightarrow	163	-0.27341
3	2.527	490.51	0.025	159	\rightarrow	163	0.2383
				160	\rightarrow	162	0.24128
				160	\rightarrow	163	0.59157

4	2.564	483.55	0.0658	158	→	161	0.17809
				159	→	161	0.66104
5	2.681	462.42	0.0548	158	→	162	0.18888
				158	→	163	0.10337
				159	→	162	0.57084
				159	→	163	0.27341
				160	→	163	-0.13199
6	2.749	450.94	0.0464	157	→	161	-0.10554
				158	→	161	0.67003
				159	→	161	-0.16173
7	2.858	433.78	0.0292	157	→	162	-0.12041
				158	→	162	0.59851
				158	→	163	0.25316
				159	→	162	-0.21021
8	2.907	426.39	0.0146	158	→	162	-0.26312
				158	→	163	0.47378
				159	→	162	-0.20928
				159	→	163	0.371
9	3.048	406.75	0.0622	157	→	163	0.11197
				158	→	162	0.1236
				158	→	163	-0.40848
				159	→	162	-0.22252
				159	→	163	0.43684
				160	→	163	-0.12626
10	3.291	376.73	0.0037	157	→	161	0.68495
11	3.359	369.07	0.0012	160	→	164	-0.3205
				160	→	165	0.42304
				160	→	168	-0.28165
				160	→	173	0.20612
12	3.375	367.3	0.0417	157	→	162	0.66227
				158	→	162	0.10226
				159	→	162	-0.10938
13	3.432	361.25	0.0083	160	→	164	0.55949
				160	→	165	0.35912
				160	→	167	0.16477
14	3.572	347.04	0.0114	157	→	163	0.60802
				159	→	163	-0.11724
				159	→	165	-0.12641
				159	→	168	0.10956
				159	→	173	-0.14884
15	3.616	342.84	0.0068	157	→	162	0.11566
				157	→	163	0.28854
				159	→	164	-0.24034
				159	→	165	0.27503
				159	→	168	-0.2629
				159	→	173	0.29646

				159	\rightarrow	176	-0.11578
16	3.674	337.43	0.003	160	\rightarrow	164	-0.147
				160	\rightarrow	166	0.64715
				160	\rightarrow	167	0.16243
17	3.732	332.15	0.0046	158	\rightarrow	165	-0.1148
				158	\rightarrow	173	-0.10716
				160	\rightarrow	164	-0.20203
				160	\rightarrow	165	0.28439
				160	\rightarrow	166	-0.14977
				160	\rightarrow	167	0.34209
				160	\rightarrow	168	0.30284
				160	\rightarrow	169	0.11205
				160	\rightarrow	173	-0.19661
18	3.767	329.08	0.0081	155	\rightarrow	161	-0.12037
				156	\rightarrow	161	0.54512
				160	\rightarrow	165	-0.1296
				160	\rightarrow	166	-0.11061
				160	\rightarrow	167	0.33466
				160	\rightarrow	168	-0.10351
19	3.777	328.21	0.0091	156	\rightarrow	161	-0.3912
				160	\rightarrow	165	-0.22638
				160	\rightarrow	167	0.41785
				160	\rightarrow	168	-0.2111
				160	\rightarrow	173	0.10004
20	3.821	324.45	0.0035	158	\rightarrow	165	0.12628
				159	\rightarrow	164	0.56698
				159	\rightarrow	165	0.28905
				159	\rightarrow	167	0.13156
21	3.873	320.1	0.1504	155	\rightarrow	161	0.64809
				156	\rightarrow	162	0.13691
				156	\rightarrow	163	0.13036
				160	\rightarrow	167	0.10055
22	3.919	316.37	0.0252	158	\rightarrow	164	0.3512
				158	\rightarrow	165	-0.202
				158	\rightarrow	168	0.19491
				158	\rightarrow	173	-0.21789
				159	\rightarrow	166	0.22359
				160	\rightarrow	168	-0.28602
				160	\rightarrow	177	-0.11719
23	3.965	312.69	0.0042	153	\rightarrow	162	-0.1163
				158	\rightarrow	164	-0.12071
				159	\rightarrow	166	0.60233
				160	\rightarrow	168	0.1188
24	3.993	310.46	0.0325	158	\rightarrow	164	0.43386
				158	\rightarrow	165	0.3348
				158	\rightarrow	167	0.18793

				159	\rightarrow	164	-0.11666
				160	\rightarrow	168	0.19785
				160	\rightarrow	169	-0.16338
25	4.03	307.62	0.0219	155	\rightarrow	161	-0.19443
				156	\rightarrow	162	0.57138
				156	\rightarrow	163	0.3202
26	4.035	307.22	0.0147	155	\rightarrow	162	-0.15942
				159	\rightarrow	164	-0.20977
				159	\rightarrow	165	0.47057
				159	\rightarrow	167	0.11464
				159	\rightarrow	168	0.18329
				159	\rightarrow	169	0.10797
				159	\rightarrow	173	-0.21562
				160	\rightarrow	169	0.11634
27	4.063	305.12	0.0186	158	\rightarrow	164	0.1535
				158	\rightarrow	165	0.17419
				158	\rightarrow	166	0.12697
				158	\rightarrow	177	-0.16145
				159	\rightarrow	165	-0.11607
				160	\rightarrow	168	-0.13498
				160	\rightarrow	169	0.40349
				160	\rightarrow	173	-0.18153
				160	\rightarrow	177	0.21671
28	4.102	302.23	0.0054	155	\rightarrow	162	0.58269
				155	\rightarrow	163	0.16772
				156	\rightarrow	163	-0.2348
				159	\rightarrow	167	0.10995
29	4.134	299.9	0.0075	156	\rightarrow	163	0.17198
				158	\rightarrow	164	-0.15348
				158	\rightarrow	165	0.12938
				159	\rightarrow	165	-0.12701
				159	\rightarrow	167	0.51888
				160	\rightarrow	169	0.10752
				160	\rightarrow	177	-0.14661
30	4.143	299.25	0.0047	155	\rightarrow	162	-0.12623
				156	\rightarrow	162	0.19609
				156	\rightarrow	163	-0.25286
				158	\rightarrow	164	-0.16287
				158	\rightarrow	165	0.28331
				159	\rightarrow	167	-0.19709
				160	\rightarrow	168	-0.13932
				160	\rightarrow	171	0.10039
				160	\rightarrow	173	-0.15278
				160	\rightarrow	174	0.11828
				160	\rightarrow	177	-0.28211
31	4.158	298.13	0.0167	155	\rightarrow	162	0.15598

				156	\rightarrow	162	-0.29233
				156	\rightarrow	163	0.45236
				158	\rightarrow	165	0.12491
				159	\rightarrow	167	-0.24358
				160	\rightarrow	173	-0.12247
				160	\rightarrow	177	-0.10698
32	4.196	295.44	0.0034	154	\rightarrow	162	0.11611
				155	\rightarrow	163	0.55562
				158	\rightarrow	177	0.12653
				160	\rightarrow	169	0.21637
				160	\rightarrow	173	0.15535
33	4.226	293.38	0.0036	155	\rightarrow	163	-0.13823
				158	\rightarrow	164	-0.16469
				158	\rightarrow	166	0.48525
				158	\rightarrow	167	0.22285
				160	\rightarrow	168	0.10628
				160	\rightarrow	169	0.19405
				160	\rightarrow	171	-0.11135
				160	\rightarrow	173	0.19432
34	4.253	291.52	0.0183	155	\rightarrow	162	-0.17648
				155	\rightarrow	163	0.31634
				158	\rightarrow	166	0.30897
				158	\rightarrow	177	-0.17685
				159	\rightarrow	167	0.11805
				159	\rightarrow	168	0.10309
				159	\rightarrow	169	-0.10923
				160	\rightarrow	169	-0.31505
				160	\rightarrow	173	-0.13594
35	4.289	289.02	0.0027	154	\rightarrow	161	0.14428
				158	\rightarrow	164	-0.14842
				158	\rightarrow	166	-0.23434
				158	\rightarrow	167	0.51947
				158	\rightarrow	177	-0.11136
				159	\rightarrow	168	-0.18675
36	4.319	287.06	0.0047	154	\rightarrow	161	0.64398
				158	\rightarrow	167	-0.10566
				158	\rightarrow	168	-0.12374
37	4.334	286.04	0.0294	154	\rightarrow	161	0.11118
				158	\rightarrow	166	-0.16974
				158	\rightarrow	167	0.15422
				158	\rightarrow	168	0.13488
				159	\rightarrow	168	0.47773
				159	\rightarrow	169	-0.21321
				159	\rightarrow	171	-0.11043
				159	\rightarrow	173	0.19597
38	4.355	284.68	0.0018	154	\rightarrow	161	0.12668

				158	\rightarrow	165	0.32705
				158	\rightarrow	167	-0.21762
				158	\rightarrow	168	0.42463
				158	\rightarrow	173	-0.1543
				160	\rightarrow	177	0.15837
39	4.486	276.35	0.0294	154	\rightarrow	162	0.48121
				157	\rightarrow	164	0.22336
				157	\rightarrow	166	-0.27809
				159	\rightarrow	166	-0.10723
				159	\rightarrow	169	-0.25565
40	4.497	275.69	0.0015	153	\rightarrow	162	0.22465
				154	\rightarrow	162	0.1439
				154	\rightarrow	163	0.19286
				157	\rightarrow	164	-0.25953
				157	\rightarrow	166	0.34674
				159	\rightarrow	168	-0.12256
				159	\rightarrow	169	-0.23379
				159	\rightarrow	173	-0.14631

Table S11. TDDFT calculated transitions for *mer*-[Ru(Q3PzH_a)(Q3Pz)₂].

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.1731	570.54	0.1431	158	\rightarrow	161	0.11888
				159	\rightarrow	161	-0.13505
				160	\rightarrow	161	0.67142
2	2.237	554.24	0.0128	159	\rightarrow	161	0.6819
				160	\rightarrow	161	0.12848
				160	\rightarrow	161	0.10009
3	2.2592	548.79	0.0147	160	\rightarrow	162	0.66423
				160	\rightarrow	163	-0.17972
				158	\rightarrow	163	-0.13715
				159	\rightarrow	162	0.46506
4	2.4017	516.24	0.0293	159	\rightarrow	163	0.27377
				160	\rightarrow	162	-0.10361
				160	\rightarrow	163	-0.39946
				159	\rightarrow	163	0.61474
5	2.4152	513.34	0.0174	160	\rightarrow	162	0.13837
				160	\rightarrow	163	0.25506
				158	\rightarrow	162	-0.17541
6	2.4848	498.97	0.0022	158	\rightarrow	163	0.25218
				159	\rightarrow	162	0.46391
				159	\rightarrow	163	-0.1074
				160	\rightarrow	163	0.37897
				158	\rightarrow	161	0.66643
7	2.5488	486.45	0.077	158	\rightarrow	163	-0.12213
				160	\rightarrow	161	-0.1177

8	2.7291	454.31	0.0566	158	→	162	0.56765
				158	→	163	0.34473
				159	→	162	0.10379
				160	→	163	-0.1047
9	2.9005	427.46	0.0792	157	→	161	-0.10591
				158	→	162	-0.33369
				158	→	163	0.4907
				159	→	162	-0.18189
				160	→	163	-0.23057
10	3.0734	403.41	0.0139	157	→	161	0.68263
11	3.1926	388.35	0.0127	156	→	161	0.6842
				157	→	161	-0.10974
12	3.279	378.11	0.0582	157	→	162	0.61006
				157	→	163	0.32249
13	3.309	374.69	0.0339	156	→	162	0.35017
				160	→	164	0.45205
				160	→	165	0.27158
				160	→	166	-0.11926
				160	→	167	0.18747
14	3.3178	373.7	0.0384	156	→	162	0.57001
				157	→	163	0.11098
				160	→	164	-0.31118
				160	→	165	-0.125
				160	→	166	0.11124
				160	→	167	-0.11135
15	3.3668	368.26	0.0242	156	→	162	-0.13991
				157	→	162	-0.34121
				157	→	163	0.55874
				160	→	164	-0.11856
				160	→	165	0.13033
16	3.4027	364.37	0.0063	157	→	163	-0.19662
				160	→	164	-0.35547
				160	→	165	0.49572
				160	→	169	0.15947
17	3.4655	357.77	0.0094	156	→	163	0.64693
				157	→	163	-0.1158
				158	→	163	0.1251
				159	→	164	-0.1032
18	3.5336	350.88	0.0101	156	→	163	0.12542
				159	→	164	0.45269
				159	→	165	0.16616
				160	→	164	-0.11725
				160	→	166	-0.41774
				160	→	167	0.11932
19	3.5548	348.78	0.003	159	→	164	0.4941
				160	→	164	0.15263

				160	\rightarrow	166	0.42475
				160	\rightarrow	167	-0.1649
20	3.6343	341.15	0.0057	156	\rightarrow	163	0.10001
				159	\rightarrow	164	-0.12391
				159	\rightarrow	165	0.51311
				159	\rightarrow	169	0.12039
				160	\rightarrow	165	-0.16432
				160	\rightarrow	166	0.24182
				160	\rightarrow	167	0.1073
				160	\rightarrow	169	0.12035
21	3.6471	339.95	0.0111	159	\rightarrow	165	-0.22772
				160	\rightarrow	165	-0.26915
				160	\rightarrow	166	0.13342
				160	\rightarrow	167	0.44171
				160	\rightarrow	168	-0.10538
				160	\rightarrow	169	0.15538
				160	\rightarrow	174	0.10104
				160	\rightarrow	175	-0.11932
22	3.6958	335.47	0.0141	158	\rightarrow	164	0.11306
				159	\rightarrow	166	0.64024
				159	\rightarrow	167	-0.10092
				159	\rightarrow	168	-0.10274
				160	\rightarrow	167	0.13294
23	3.7341	332.03	0.0019	158	\rightarrow	164	0.23671
				158	\rightarrow	165	0.25976
				158	\rightarrow	167	0.17903
				158	\rightarrow	169	0.127
				158	\rightarrow	174	0.12433
				158	\rightarrow	175	-0.14653
				159	\rightarrow	166	-0.20462
				160	\rightarrow	166	0.11361
				160	\rightarrow	167	0.30854
				160	\rightarrow	169	-0.1477
				160	\rightarrow	175	0.11462
24	3.79	327.13	0.0024	158	\rightarrow	164	0.32067
				158	\rightarrow	165	0.10072
				159	\rightarrow	165	-0.2366
				159	\rightarrow	167	0.16925
				160	\rightarrow	165	-0.10794
				160	\rightarrow	167	-0.22615
				160	\rightarrow	168	-0.17609
				160	\rightarrow	169	0.28555
				160	\rightarrow	174	0.11155
				160	\rightarrow	175	-0.11473
25	3.8339	323.39	0.0165	158	\rightarrow	164	0.47711
				158	\rightarrow	165	-0.14735

				159	\rightarrow	165	0.20272
				159	\rightarrow	167	-0.2103
				159	\rightarrow	169	-0.14822
				159	\rightarrow	174	-0.12039
				159	\rightarrow	175	0.13913
26	3.8639	320.88	0.0256	155	\rightarrow	161	0.16727
				158	\rightarrow	164	0.2246
				158	\rightarrow	165	-0.23193
				158	\rightarrow	167	-0.12109
				158	\rightarrow	174	-0.10867
				158	\rightarrow	175	0.13113
				159	\rightarrow	167	0.38139
				160	\rightarrow	168	0.25824
27	3.8871	318.96	0.0547	154	\rightarrow	161	-0.16351
				155	\rightarrow	161	0.62267
				160	\rightarrow	168	-0.14156
28	3.9378	314.86	0.0273	155	\rightarrow	161	-0.13939
				158	\rightarrow	165	0.14354
				158	\rightarrow	166	0.33926
				158	\rightarrow	167	-0.12669
				159	\rightarrow	166	0.10158
				159	\rightarrow	167	0.32266
				159	\rightarrow	168	0.14617
				159	\rightarrow	169	-0.209
				159	\rightarrow	174	-0.11845
				159	\rightarrow	175	0.15899
				160	\rightarrow	176	0.12387
29	3.9531	313.64	0.0032	158	\rightarrow	165	-0.20312
				158	\rightarrow	166	0.50263
				159	\rightarrow	166	-0.10669
				159	\rightarrow	167	-0.27039
				159	\rightarrow	168	-0.11475
				159	\rightarrow	169	0.13065
30	3.9805	311.48	0.0235	154	\rightarrow	161	0.66212
				155	\rightarrow	161	0.15827
31	4.0191	308.48	0.0089	158	\rightarrow	165	-0.14445
				158	\rightarrow	174	0.10803
				158	\rightarrow	175	-0.14306
				160	\rightarrow	168	0.44253
				160	\rightarrow	169	0.3834
32	4.035	307.27	0.0089	158	\rightarrow	165	0.44612
				158	\rightarrow	166	0.18909
				158	\rightarrow	169	-0.15472
				158	\rightarrow	172	0.1034
				158	\rightarrow	174	-0.13505
				158	\rightarrow	175	0.17691

				159	\rightarrow	167	-0.13549
				160	\rightarrow	168	0.20851
				160	\rightarrow	169	0.11724
33	4.077	304.1	0.0179	154	\rightarrow	162	-0.1302
				158	\rightarrow	176	-0.12718
				159	\rightarrow	169	-0.2127
				159	\rightarrow	176	0.26348
				160	\rightarrow	168	-0.20746
				160	\rightarrow	169	0.26085
				160	\rightarrow	172	0.14924
				160	\rightarrow	174	-0.16903
				160	\rightarrow	175	0.23243
				160	\rightarrow	176	-0.14635
34	4.101	302.33	0.0104	153	\rightarrow	162	0.12978
				155	\rightarrow	162	0.16653
				159	\rightarrow	168	0.56992
				159	\rightarrow	169	0.23856
35	4.1265	300.46	0.0046	156	\rightarrow	167	-0.10141
				158	\rightarrow	166	0.17594
				158	\rightarrow	167	0.5874
36	4.1483	298.88	0.0061	154	\rightarrow	162	-0.2583
				154	\rightarrow	163	-0.1924
				155	\rightarrow	162	0.43544
				155	\rightarrow	163	0.36516
37	4.1931	295.68	0.0094	152	\rightarrow	161	-0.11306
				153	\rightarrow	161	0.57195
				157	\rightarrow	164	0.22731
				157	\rightarrow	165	-0.13977
				158	\rightarrow	165	0.10644
				159	\rightarrow	169	0.11139
38	4.1993	295.25	0.0085	154	\rightarrow	162	0.51088
				155	\rightarrow	162	0.39059
				159	\rightarrow	168	-0.11353
				159	\rightarrow	169	-0.14266
39	4.2152	294.14	0.0019	154	\rightarrow	162	0.34754
				154	\rightarrow	163	-0.13827
				155	\rightarrow	162	-0.29348
				155	\rightarrow	163	0.46181
				157	\rightarrow	164	-0.10464
40	4.2429	292.21	0.0154	152	\rightarrow	161	0.1161
				153	\rightarrow	161	-0.25031
				155	\rightarrow	163	0.15479
				157	\rightarrow	164	0.15815
				157	\rightarrow	165	-0.13643
				159	\rightarrow	168	-0.13313
				159	\rightarrow	169	0.33122

160	→	168	-0.10803
160	→	169	0.11074
160	→	171	0.14329
160	→	176	0.22993

Table S12. TDDFT calculated transitions for *mer*-[Ru(Q3PzH_b)(Q3Pz)₂].

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.05	604.8	0.0021	160	→	161 0.22522	
				160	→	162 0.63855	
				160	→	163 -0.18391	
2	2.105	589	0.0491	160	→	161 0.65707	
				160	→	162 -0.23575	
				158	→	163 -0.14256	
3	2.2279	556.51	0.0687		→	163 0.19692	
					→	162 0.15977	
					→	163 0.61792	
					→	161 0.56041	
4	2.4162	513.13	0.0011	159	→	162 -0.28042	
					→	163 -0.29103	
					→	161 0.39152	
5	2.5253	490.98	0.063	159	→	162 0.26847	
					→	163 0.48567	
					→	163 -0.12131	
					→	161 0.1356	
6	2.6339	470.73	0.1475	158	→	163 -0.32897	
					→	161 0.11248	
					→	162 0.50287	
					→	163 -0.28114	
					→	161 0.19709	
7	2.6757	463.37	0.0123	158	→	162 0.64448	
					→	163 0.10021	
					→	161 0.62174	
8	2.7257	454.87	0.0292	158	→	162 -0.1458	
					→	163 0.26	
					→	161 -0.18475	
9	2.8445	435.87	0.0264	158	→	162 0.17956	
					→	163 0.5037	
					→	162 0.23753	
					→	163 -0.1693	
					→	163 0.21045	
10	3.1317	395.9	0.0497	156	→	161 -0.18305	
					→	161 0.649	
11	3.1776	390.18	0.0598	156	→	161 0.13066	
					→	162 0.17954	
					→	162 0.64185	
12	3.2243	384.53	0.0066	156	→	163 0.11219	

				157	\rightarrow	161	0.10106
				157	\rightarrow	163	-0.38716
				160	\rightarrow	165	0.49158
				160	\rightarrow	167	0.16612
13	3.2508	381.4	0.0559	156	\rightarrow	161	-0.21498
				156	\rightarrow	162	-0.2083
				157	\rightarrow	162	0.1192
				157	\rightarrow	163	0.43618
				160	\rightarrow	165	0.39221
				160	\rightarrow	167	0.1073
14	3.2794	378.07	0.0146	156	\rightarrow	161	0.1399
				156	\rightarrow	162	0.28107
				156	\rightarrow	163	-0.11981
				157	\rightarrow	162	-0.15277
				157	\rightarrow	163	0.12002
				160	\rightarrow	164	0.55695
15	3.3153	373.98	0.0273	160	\rightarrow	165	0.1353
				156	\rightarrow	161	0.14614
				156	\rightarrow	162	0.46162
				156	\rightarrow	163	-0.15214
				157	\rightarrow	162	-0.12153
				157	\rightarrow	163	0.23056
16	3.3215	373.27	0.0029	160	\rightarrow	164	-0.39773
				156	\rightarrow	161	0.5656
				156	\rightarrow	162	-0.31876
				156	\rightarrow	163	-0.14923
				157	\rightarrow	161	0.16675
				157	\rightarrow	163	0.10392
17	3.4573	358.62	0.0004	160	\rightarrow	166	0.67858
18	3.4923	355.02	0.0025	156	\rightarrow	161	0.14629
				156	\rightarrow	163	0.62565
				157	\rightarrow	163	0.23336
				160	\rightarrow	165	-0.2402
				160	\rightarrow	167	0.63166
				159	\rightarrow	164	-0.25426
20	3.5832	346.02	0.0013	159	\rightarrow	164	0.52838
				159	\rightarrow	165	0.24906
				159	\rightarrow	167	0.17416
				159	\rightarrow	175	0.59394
				159	\rightarrow	166	0.25569
				159	\rightarrow	167	0.16429
21	3.6196	342.53	0.0035	159	\rightarrow	164	0.11461
				159	\rightarrow	165	0.11691
				159	\rightarrow	166	0.1709
				160	\rightarrow	167	0.14083
				160	\rightarrow	168	0.3057

				160	→	169	0.45327
				160	→	175	-0.17804
				160	→	176	0.11962
23	3.8034	325.98	0.0353	158	→	164	-0.15359
				158	→	165	0.46547
				158	→	167	0.2195
				158	→	172	-0.12216
				158	→	175	0.23619
				160	→	168	0.19858
24	3.8348	323.31	0.0445	155	→	161	0.10406
				159	→	164	0.10341
				159	→	166	-0.22806
				160	→	168	0.47279
				160	→	169	-0.32601
				160	→	176	-0.12645
25	3.8392	322.95	0.0075	159	→	164	-0.18923
				159	→	166	0.54007
				159	→	168	0.13538
				159	→	175	-0.11173
				160	→	168	0.12259
				160	→	169	-0.2506
26	3.8884	318.86	0.0559	160	→	176	-0.10461
				155	→	161	0.63949
				155	→	162	-0.11501
				159	→	166	0.13433
				159	→	167	0.10026
				155	→	161	-0.13702
27	3.9222	316.11	0.0039	158	→	164	0.19265
				158	→	165	0.1273
				159	→	165	-0.33388
				159	→	167	0.41604
				159	→	168	-0.14686
				159	→	172	-0.1056
28	3.9574	313.3	0.0037	159	→	175	0.20063
				154	→	162	0.1245
				158	→	164	0.58172
				158	→	165	0.20161
				159	→	168	0.1042
				155	→	162	0.41787
29	4.0002	309.95	0.0187	155	→	163	0.52247
				154	→	162	0.11675
				155	→	162	-0.19497
				158	→	166	0.10067
				159	→	166	-0.16081
				159	→	167	0.41637
30	4.0089	309.27	0.0017	159	→	168	0.25414

				159	→	169	0.10412
				159	→	172	0.11704
				159	→	175	-0.2201
				160	→	175	-0.10648
31	4.0493	306.19	0.0088	154	→	162	0.20165
				155	→	161	0.12539
				155	→	162	0.44287
				155	→	163	-0.4052
				158	→	166	0.18802
32	4.0672	304.84	0.0052	154	→	161	0.35458
				154	→	162	0.3779
				155	→	162	-0.19992
				158	→	164	-0.12792
				158	→	165	0.18357
				158	→	175	-0.11712
				159	→	169	-0.10937
33	4.0878	303.3	0.0004	154	→	161	0.17844
				158	→	164	0.16871
				158	→	165	-0.28177
				158	→	166	0.3033
				158	→	167	0.21157
				158	→	169	-0.13237
				158	→	175	0.14451
				158	→	176	-0.11856
				160	→	168	0.13179
				160	→	175	0.16123
				160	→	176	0.17178
34	4.1004	302.37	0.0045	154	→	161	0.49631
				154	→	162	-0.17227
				155	→	163	-0.10929
				158	→	165	-0.10143
				158	→	166	-0.33086
				159	→	167	0.10557
35	4.1209	300.87	0.0175	154	→	161	-0.18127
				154	→	162	0.43808
				158	→	165	-0.13408
				158	→	166	-0.3914
				158	→	167	0.17441
36	4.1802	296.6	0.0047	153	→	161	-0.11884
				154	→	163	0.18928
				158	→	166	-0.14617
				158	→	167	-0.13833
				158	→	176	-0.14075
				159	→	168	0.25628
				159	→	169	-0.20578
				160	→	169	-0.17505

				160	\rightarrow	174	0.10666
				160	\rightarrow	176	0.37194
37	4.2051	294.84	0.0059	153	\rightarrow	162	-0.12595
				153	\rightarrow	163	-0.17732
				154	\rightarrow	162	-0.11043
				154	\rightarrow	163	0.14896
				157	\rightarrow	164	-0.12992
				158	\rightarrow	167	0.39431
				159	\rightarrow	169	-0.12575
				160	\rightarrow	168	-0.19048
				160	\rightarrow	171	0.13674
				160	\rightarrow	172	0.14893
				160	\rightarrow	175	-0.24299
38	4.2356	292.72	0.0029	153	\rightarrow	161	0.11901
				154	\rightarrow	163	-0.25261
				156	\rightarrow	164	0.13911
				156	\rightarrow	166	0.16013
				157	\rightarrow	164	0.37388
				158	\rightarrow	166	-0.13031
				158	\rightarrow	167	0.11021
				159	\rightarrow	168	-0.23717
				160	\rightarrow	169	-0.11427
				160	\rightarrow	172	0.10002
				160	\rightarrow	175	-0.15614
				160	\rightarrow	176	0.16002
39	4.2558	291.33	0.0101	153	\rightarrow	161	-0.17751
				153	\rightarrow	163	-0.11374
				154	\rightarrow	161	0.105
				154	\rightarrow	163	0.46414
				156	\rightarrow	164	0.10098
				157	\rightarrow	164	0.18721
				158	\rightarrow	167	-0.16289
				159	\rightarrow	168	-0.27594
40	4.2659	290.64	0.0147	150	\rightarrow	163	-0.11217
				153	\rightarrow	161	0.10127
				154	\rightarrow	163	0.15786
				156	\rightarrow	166	0.12042
				157	\rightarrow	164	0.35248
				157	\rightarrow	166	-0.11845
				158	\rightarrow	167	0.1557
				158	\rightarrow	169	0.10993
				158	\rightarrow	176	0.12004
				159	\rightarrow	168	0.29835
				159	\rightarrow	175	0.15786
				160	\rightarrow	175	0.10362

Table S13. TDDFT calculated transitions for *mer*-[Ru(Q3PzH_c)(Q3Pz)₂].

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	1.9785	626.65	0.0066	160	→	161	0.69684
2	2.1641	572.9	0.1234	158	→	162	-0.10213
				160	→	162	0.69115
3	2.3491	527.78	0.0419	158	→	161	-0.20997
				158	→	163	-0.1464
				159	→	161	0.18997
				160	→	163	0.6112
4	2.4337	509.45	0.0161	158	→	161	0.62668
				159	→	161	0.27198
				160	→	163	0.13446
5	2.4998	495.99	0.0197	158	→	162	-0.25727
				159	→	161	-0.17761
				159	→	162	0.61769
6	2.5234	491.34	0.0457	158	→	161	-0.21062
				159	→	161	0.4726
				159	→	162	0.21067
				159	→	163	0.36998
				160	→	163	-0.17196
7	2.6194	473.33	0.1175	158	→	162	0.62621
				158	→	163	-0.12143
				159	→	162	0.2316
				160	→	162	0.11687
8	2.6768	463.18	0.0342	158	→	162	0.13717
				158	→	163	0.45775
				159	→	161	0.23798
				159	→	163	-0.4337
9	2.8517	434.77	0.0069	157	→	162	-0.11114
				158	→	163	0.46693
				159	→	161	-0.21458
				159	→	163	0.35056
				160	→	163	0.2259
10	3.0785	402.74	0.0164	157	→	161	0.60551
				157	→	162	-0.33711
11	3.1077	398.96	0.0018	157	→	161	0.33405
				157	→	162	0.59528
				160	→	164	-0.10918
12	3.2283	384.06	0.0086	160	→	164	0.66472
13	3.3406	371.14	0.1166	156	→	162	-0.1597
				157	→	163	0.65593
				160	→	165	0.12129
14	3.3933	365.38	0.0095	157	→	163	-0.1337
				160	→	165	0.54129
				160	→	166	-0.3238
				160	→	169	-0.17162

15	3.4206	362.46	0.0123	156	→	162	0.47992
				157	→	163	0.13772
				160	→	165	-0.27543
				160	→	166	-0.37773
16	3.4526	359.1	0.0144	156	→	162	0.45944
				157	→	163	0.10474
				160	→	165	0.24521
				160	→	166	0.44118
17	3.4657	357.75	0.003	156	→	161	0.68059
				156	→	162	-0.10273
18	3.5379	350.45	0.0033	159	→	164	-0.39898
				159	→	167	-0.13182
				160	→	164	-0.1394
				160	→	167	0.48197
19	3.5663	347.66	0.0113	158	→	164	-0.15887
				159	→	164	0.49672
				159	→	167	0.13663
				160	→	167	0.33868
20	3.6635	338.43	0.006	156	→	163	0.57433
				158	→	164	-0.12835
				160	→	166	0.1157
				160	→	167	0.16376
				160	→	169	-0.15766
21	3.7155	333.7	0.0181	156	→	163	0.35181
				159	→	165	-0.12474
				159	→	169	0.13805
				159	→	173	-0.10913
				159	→	175	0.14009
				160	→	166	-0.12049
				160	→	167	-0.16659
				160	→	169	0.34823
				160	→	173	-0.15731
				160	→	175	0.18872
22	3.7233	333	0.0487	158	→	164	0.60188
				158	→	167	0.14759
				160	→	167	0.20395
23	3.7733	328.58	0.0012	158	→	165	-0.11198
				158	→	166	0.11092
				158	→	169	0.12909
				159	→	165	0.27458
				159	→	166	-0.20375
				159	→	169	-0.21918
				159	→	173	0.16722
				159	→	175	-0.20102
				160	→	168	-0.24969
				160	→	169	0.18012

				160	→	177	0.11936
24	3.8156	324.94	0.0192	155	→	161	0.38368
				155	→	162	-0.1201
				159	→	166	-0.12658
				160	→	168	0.50882
25	3.8293	323.78	0.0559	155	→	161	0.52716
				158	→	165	0.10007
				159	→	167	0.1193
				160	→	168	-0.32136
26	3.8673	320.6	0.0122	154	→	162	0.12397
				155	→	162	0.59288
				159	→	165	0.23614
				159	→	167	0.11768
27	3.8794	319.59	0.0109	160	→	168	0.15737
				155	→	161	-0.11715
				155	→	162	-0.26252
				159	→	164	-0.11613
				159	→	165	0.48669
				159	→	166	0.26918
28	3.8962	318.22	0.0112	159	→	167	0.19886
				158	→	165	0.15885
				159	→	164	0.15723
				159	→	166	0.48043
				159	→	167	-0.3354
				159	→	175	-0.118
29	3.9326	315.27	0.0031	160	→	169	0.10869
				155	→	162	-0.12353
				158	→	165	0.51648
				158	→	166	-0.12732
				158	→	169	-0.10026
				159	→	165	0.15153
				159	→	166	-0.23399
30	3.9556	313.44	0.0053	160	→	169	0.14443
				158	→	164	-0.126
				158	→	165	0.33549
				158	→	166	0.47456
				158	→	167	0.19808
				158	→	169	0.12256
				158	→	175	0.10587
31	3.9675	312.5	0.0117	159	→	165	-0.12209
				158	→	164	-0.19415
				158	→	166	-0.3809
				158	→	167	0.47549
				158	→	169	0.13125
32	4.032	307.5	0.0243	158	→	175	0.11439
				154	→	161	0.28871

				155	→	163	0.12822
				158	→	166	-0.11211
				158	→	167	-0.1457
				159	→	165	-0.17582
				159	→	166	0.17711
				159	→	167	0.42723
				159	→	169	-0.17684
				159	→	173	0.11882
				159	→	175	-0.14388
				160	→	169	0.10799
33	4.0558	305.69	0.0225	154	→	161	0.54376
				155	→	161	0.10366
				158	→	165	-0.10476
				159	→	167	-0.13104
				160	→	176	-0.12529
				160	→	177	-0.19239
34	4.096	302.7	0.005	154	→	161	0.24835
				158	→	167	-0.21998
				158	→	175	0.1178
				158	→	176	-0.10452
				158	→	177	-0.18598
				159	→	167	-0.18614
				159	→	169	0.10611
				159	→	175	0.12018
				160	→	171	0.10735
				160	→	175	-0.13141
				160	→	176	0.17318
				160	→	177	0.30158
				160	→	179	0.11518
35	4.1241	300.64	0.0005	154	→	161	-0.10649
				154	→	163	0.14134
				155	→	163	0.66693
36	4.1455	299.08	0.0017	157	→	165	-0.12413
				158	→	165	0.11138
				158	→	166	-0.18231
				158	→	167	-0.28542
				158	→	169	0.2987
				158	→	173	-0.14584
				158	→	175	0.15327
				158	→	176	0.10699
				158	→	177	0.17642
				160	→	169	-0.27465
				160	→	173	-0.12168
				160	→	175	0.13937
37	4.2009	295.14	0.0042	154	→	162	0.67733
				155	→	162	-0.14715

38	4.2611	290.97	0.0036	152	→	162	-0.11243
				153	→	162	-0.14844
				157	→	164	0.19522
				157	→	165	0.28069
				157	→	166	0.10748
				159	→	168	0.51169
39	4.2811	289.61	0.0082	152	→	162	-0.11365
				157	→	164	0.2867
				157	→	165	0.39913
				158	→	168	-0.19707
				159	→	168	-0.34666
40	4.3057	287.95	0.0043	152	→	162	0.10428
				153	→	162	-0.18162
				157	→	164	0.41715
				157	→	165	-0.30078
				157	→	166	0.17478
				157	→	167	0.11418
				158	→	168	-0.27242

Table S14. TDDFT calculated transitions for *mer*-[Ru(Q3Pz)₃]⁻.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	1.9128	648.19	0.0425	158	→	161	-0.11438
				159	→	161	-0.10268
				160	→	161	0.67766
2	1.9663	630.54	0.0234	159	→	161	0.13227
				160	→	162	0.67406
3	2.0862	594.3	0.0042	159	→	161	0.45802
				159	→	162	0.29278
				159	→	163	-0.29943
				160	→	163	0.30971
4	2.1036	589.38	0.014	159	→	161	-0.32783
				159	→	162	-0.22413
				159	→	163	-0.14866
				160	→	162	0.10005
				160	→	163	0.53577
5	2.2089	561.29	0.0926	158	→	161	0.16303
				159	→	161	-0.32122
				159	→	162	0.5689
				160	→	162	0.12544
6	2.3787	521.22	0.1362	158	→	161	0.48143
				158	→	163	-0.12466
				159	→	161	0.16206
				159	→	163	0.42057
				160	→	161	0.12266
				160	→	163	0.11115
7	2.4012	516.35	0.0172	158	→	161	-0.35088

				158	\rightarrow	162	0.40927
				158	\rightarrow	163	-0.32398
				159	\rightarrow	162	0.10428
				159	\rightarrow	163	0.25686
				160	\rightarrow	163	0.1133
8	2.4887	498.19	0.0507	158	\rightarrow	161	0.16216
				158	\rightarrow	162	0.51664
				158	\rightarrow	163	0.41489
				159	\rightarrow	161	-0.1003
9	2.6729	463.85	0.0209	158	\rightarrow	161	-0.23608
				158	\rightarrow	162	-0.17502
				158	\rightarrow	163	0.41739
				159	\rightarrow	163	0.33632
				160	\rightarrow	163	0.25745
10	3.0187	410.71	0.0046	157	\rightarrow	161	0.60107
				157	\rightarrow	162	-0.33389
11	3.1017	399.73	0.0039	157	\rightarrow	162	0.11392
				160	\rightarrow	164	0.67884
12	3.1264	396.57	0.0158	157	\rightarrow	161	0.34012
				157	\rightarrow	162	0.59993
13	3.2438	382.22	0.1292	156	\rightarrow	161	0.10392
				156	\rightarrow	162	-0.10187
				157	\rightarrow	163	0.60144
				160	\rightarrow	165	0.28
14	3.2501	381.48	0.0369	156	\rightarrow	162	0.13852
				157	\rightarrow	163	-0.24744
				159	\rightarrow	164	-0.10608
				160	\rightarrow	165	0.60435
15	3.2706	379.09	0.0785	155	\rightarrow	161	-0.16167
				155	\rightarrow	162	-0.15264
				156	\rightarrow	161	0.61138
				156	\rightarrow	162	0.23077
16	3.2968	376.08	0.0009	156	\rightarrow	161	-0.20262
				156	\rightarrow	162	0.2619
				157	\rightarrow	163	0.21273
				159	\rightarrow	164	-0.38807
				160	\rightarrow	165	-0.10073
				160	\rightarrow	166	0.40336
17	3.3157	373.94	0.0362	155	\rightarrow	161	-0.16396
				156	\rightarrow	161	-0.19506
				156	\rightarrow	162	0.5149
				157	\rightarrow	163	0.11492
				159	\rightarrow	164	0.26899
				160	\rightarrow	166	-0.26786
18	3.3292	372.41	0.0046	159	\rightarrow	164	0.49636
				160	\rightarrow	166	0.47746

19	3.4015	364.49	0.0114	155	→	161	0.58536
				155	→	162	-0.31501
				156	→	162	0.20017
20	3.4504	359.34	0.0059	155	→	161	0.2241
				155	→	162	0.52343
				156	→	161	0.14608
				156	→	162	0.16306
				156	→	163	0.14022
				159	→	165	0.26165
21	3.4755	356.73	0.0029	155	→	161	-0.12038
				155	→	162	-0.24679
				159	→	165	0.54908
				159	→	166	-0.19876
				159	→	174	-0.12134
				160	→	169	0.10871
22	3.5316	351.07	0.0059	155	→	162	-0.12695
				156	→	163	0.37589
				158	→	164	-0.23135
				159	→	165	0.10526
				159	→	166	0.49569
23	3.5341	350.82	0.007	155	→	163	0.18114
				156	→	163	0.52556
				158	→	164	0.27153
				159	→	165	-0.12725
				159	→	166	-0.24627
24	3.5498	349.27	0.0044	156	→	163	-0.14461
				158	→	164	0.53085
				159	→	165	0.13776
				159	→	166	0.35559
				160	→	167	-0.11758
25	3.588	345.55	0.0006	155	→	163	-0.14997
				158	→	164	0.25578
				160	→	165	0.13241
				160	→	167	0.46115
				160	→	168	0.20609
				160	→	169	-0.21944
				160	→	174	0.17645
26	3.6379	340.81	0.0063	155	→	163	0.60403
				156	→	163	-0.14371
				160	→	167	0.29728
27	3.6655	338.25	0.0108	155	→	163	0.19543
				158	→	165	-0.23476
				158	→	174	0.10175
				160	→	167	-0.3048
				160	→	168	0.49086
28	3.6899	336.01	0.0137	155	→	163	-0.10414

				158	\rightarrow	165	0.3777
				158	\rightarrow	174	-0.16433
				160	\rightarrow	168	0.41644
				160	\rightarrow	169	0.20868
29	3.7222	333.09	0.0272	158	\rightarrow	165	0.32698
				159	\rightarrow	165	0.20587
				159	\rightarrow	167	0.22333
				159	\rightarrow	168	0.11954
				159	\rightarrow	169	-0.2776
				159	\rightarrow	174	0.23451
				159	\rightarrow	175	0.11621
				160	\rightarrow	169	-0.22822
30	3.7848	327.58	0.0014	158	\rightarrow	165	0.1517
				158	\rightarrow	166	0.46637
				159	\rightarrow	168	-0.1118
				159	\rightarrow	169	0.18271
				159	\rightarrow	174	-0.20582
				160	\rightarrow	169	-0.31479
31	3.7913	327.03	0.0052	154	\rightarrow	161	0.60292
				154	\rightarrow	162	-0.34179
32	3.8008	326.2	0.0175	158	\rightarrow	165	-0.13917
				158	\rightarrow	166	0.505
				159	\rightarrow	168	0.12462
				159	\rightarrow	169	-0.15701
				159	\rightarrow	174	0.18878
				160	\rightarrow	167	0.10051
				160	\rightarrow	169	0.2797
33	3.874	320.04	0.0272	158	\rightarrow	165	-0.10332
				159	\rightarrow	167	0.59139
				159	\rightarrow	168	0.10838
				159	\rightarrow	169	0.20237
				160	\rightarrow	169	0.119
34	3.8976	318.1	0.0032	158	\rightarrow	165	0.32845
				158	\rightarrow	167	0.17774
				158	\rightarrow	168	0.1055
				158	\rightarrow	169	-0.26546
				158	\rightarrow	172	0.13753
				158	\rightarrow	174	0.392
				160	\rightarrow	169	0.18461
				160	\rightarrow	174	0.10747
35	3.9103	317.07	0.0056	154	\rightarrow	161	0.2841
				154	\rightarrow	162	0.46634
				159	\rightarrow	167	0.18175
				159	\rightarrow	168	-0.34691
36	3.922	316.12	0.0127	154	\rightarrow	161	0.15322
				154	\rightarrow	162	0.36675

					159	\rightarrow	168	0.53938
37	3.9712	312.21	0.0012		158	\rightarrow	175	-0.13643
					160	\rightarrow	167	0.11601
					160	\rightarrow	169	-0.10681
					160	\rightarrow	174	-0.28979
					160	\rightarrow	175	0.38255
					160	\rightarrow	177	0.17553
					160	\rightarrow	178	0.26876
38	4.0333	307.4	0.0004		154	\rightarrow	163	0.68149
39	4.1089	301.74	0.0098		157	\rightarrow	164	-0.23374
					157	\rightarrow	166	0.13383
					158	\rightarrow	167	0.56334
					158	\rightarrow	168	-0.16393
					158	\rightarrow	169	0.12566
					158	\rightarrow	174	-0.12546
40	4.1378	299.64	0.0015		157	\rightarrow	164	0.4839
					157	\rightarrow	166	-0.28471
					158	\rightarrow	167	0.27653
					158	\rightarrow	168	-0.14195

Table S15. TDDFT calculated transitions for *fac*-[Ru(Q1Pz)₃]²⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.6579	466.47	0.0397	160	\rightarrow	161	0.61016
				160	\rightarrow	162	0.30257
				160	\rightarrow	163	-0.11447
2	2.7384	452.76	0.057	160	\rightarrow	161	-0.27803
				160	\rightarrow	162	0.61761
				160	\rightarrow	163	0.14906
3	2.7957	443.48	0.0195	159	\rightarrow	161	-0.44303
				159	\rightarrow	163	0.14653
				160	\rightarrow	161	0.17672
				160	\rightarrow	163	0.47806
4	2.8713	431.8	0.0365	159	\rightarrow	161	0.49076
				159	\rightarrow	162	0.19132
				159	\rightarrow	163	0.29721
				160	\rightarrow	162	-0.10441
				160	\rightarrow	163	0.30856
5	2.8843	429.85	0.0144	159	\rightarrow	162	0.50451
				159	\rightarrow	163	-0.4586
				160	\rightarrow	163	0.12661
6	2.9321	422.85	0.0125	158	\rightarrow	162	-0.22788
				159	\rightarrow	161	-0.19492
				159	\rightarrow	162	0.42159
				159	\rightarrow	163	0.36902
				160	\rightarrow	163	-0.26509
7	3.0549	405.85	0.013	158	\rightarrow	161	0.64756

				158	\rightarrow	162	-0.10007
				158	\rightarrow	163	0.21463
8	3.1478	393.88	0.1004	158	\rightarrow	161	-0.18567
				158	\rightarrow	162	0.13484
				158	\rightarrow	163	0.6397
9	3.1991	387.56	0.0323	158	\rightarrow	161	0.10724
				158	\rightarrow	162	0.61772
				159	\rightarrow	163	0.10759
				160	\rightarrow	163	-0.17095
10	3.6405	340.57	0.0006	159	\rightarrow	170	0.12994
				159	\rightarrow	175	-0.10693
				160	\rightarrow	164	0.31012
				160	\rightarrow	165	0.10986
				160	\rightarrow	166	0.15838
				160	\rightarrow	167	0.23609
				160	\rightarrow	168	-0.15146
				160	\rightarrow	170	0.19329
				160	\rightarrow	171	0.19798
				160	\rightarrow	174	0.23589
				160	\rightarrow	175	-0.15015
11	3.7125	333.97	0.0073	158	\rightarrow	170	-0.13728
				158	\rightarrow	175	0.11155
				159	\rightarrow	165	-0.13656
				159	\rightarrow	167	0.15968
				159	\rightarrow	168	-0.12698
				159	\rightarrow	170	0.2866
				159	\rightarrow	175	-0.2097
				160	\rightarrow	165	0.22492
				160	\rightarrow	167	-0.11417
				160	\rightarrow	169	0.10522
				160	\rightarrow	170	-0.16919
				160	\rightarrow	171	0.12447
				160	\rightarrow	174	0.12034
				160	\rightarrow	175	0.12094
12	3.7815	327.87	0.0039	158	\rightarrow	171	-0.15949
				158	\rightarrow	174	-0.17568
				159	\rightarrow	164	-0.15754
				159	\rightarrow	167	-0.18447
				159	\rightarrow	168	0.10074
				159	\rightarrow	170	-0.22837
				159	\rightarrow	175	0.16815
				160	\rightarrow	164	0.1593
				160	\rightarrow	165	0.32465
				160	\rightarrow	170	-0.14442
				160	\rightarrow	171	0.11234
				160	\rightarrow	174	0.12203

				160	\rightarrow	175	0.10266
13	3.8194	324.61	0.0691	155	\rightarrow	161	0.14179
				156	\rightarrow	161	0.10239
				157	\rightarrow	161	0.64399
				160	\rightarrow	164	0.10168
14	3.8655	320.75	0.0507	155	\rightarrow	161	-0.16224
				156	\rightarrow	161	0.39733
				156	\rightarrow	162	0.2017
				156	\rightarrow	163	-0.21445
				157	\rightarrow	162	0.2549
				157	\rightarrow	163	-0.26084
				159	\rightarrow	165	-0.10184
				160	\rightarrow	166	-0.15562
15	3.8933	318.45	0.0215	156	\rightarrow	161	-0.22883
				160	\rightarrow	164	0.46698
				160	\rightarrow	165	-0.31117
				160	\rightarrow	166	-0.18795
16	3.9137	316.8	0.0305	155	\rightarrow	161	0.14085
				155	\rightarrow	163	-0.18871
				156	\rightarrow	161	-0.16672
				156	\rightarrow	162	-0.21881
				157	\rightarrow	162	0.48096
				157	\rightarrow	163	-0.26699
				160	\rightarrow	166	0.15219
17	3.9306	315.43	0.061	155	\rightarrow	162	-0.21659
				156	\rightarrow	162	-0.32725
				156	\rightarrow	163	-0.1027
				157	\rightarrow	162	0.17639
				157	\rightarrow	163	0.35887
				160	\rightarrow	164	-0.16801
				160	\rightarrow	165	-0.12275
				160	\rightarrow	166	-0.20037
				160	\rightarrow	167	0.10632
18	3.9451	314.28	0.0867	155	\rightarrow	162	-0.16706
				156	\rightarrow	161	0.18878
				156	\rightarrow	163	-0.12638
				157	\rightarrow	163	0.2715
				160	\rightarrow	164	0.22041
				160	\rightarrow	165	0.1454
				160	\rightarrow	166	0.32426
				160	\rightarrow	167	-0.14347
				160	\rightarrow	169	-0.11716
				160	\rightarrow	171	-0.15095
				160	\rightarrow	174	-0.13645
19	4.012	309.03	0.0038	156	\rightarrow	161	0.19883
				156	\rightarrow	162	-0.20777

				158	→	170	0.10578
				159	→	164	0.3496
				159	→	165	0.1504
				159	→	171	0.116
				159	→	174	0.11325
				160	→	164	0.15217
				160	→	166	-0.14431
				160	→	167	-0.25379
				160	→	168	0.17474
20	4.0228	308.2	0.0061	156	→	161	0.11915
				156	→	162	-0.18645
				157	→	162	-0.14396
				157	→	163	-0.11728
				158	→	167	-0.10917
				158	→	171	-0.12178
				158	→	174	-0.13276
				160	→	165	-0.35956
				160	→	166	0.36219
				160	→	171	0.11189
				160	→	174	0.10127
21	4.0378	307.06	0.0179	155	→	161	0.13012
				155	→	162	0.11833
				156	→	161	0.29954
				156	→	162	-0.27679
				156	→	163	0.32809
				157	→	162	-0.11558
				159	→	164	-0.22884
				159	→	165	-0.16937
22	4.0738	304.35	0.0104	155	→	161	0.267
				156	→	161	0.14501
				156	→	162	0.3001
				156	→	163	0.34353
				157	→	161	-0.12349
				157	→	162	0.182
				157	→	163	0.14414
				159	→	165	0.19987
23	4.1003	302.37	0.0099	156	→	163	0.2324
				157	→	162	0.12518
				158	→	164	-0.1031
				159	→	164	0.39534
				159	→	165	-0.20303
				159	→	166	-0.29856
				159	→	170	-0.12038
				160	→	167	0.2086
24	4.1201	300.93	0.0056	155	→	161	0.47553
				155	→	162	-0.11118

				155	\rightarrow	163	0.1551
				156	\rightarrow	163	-0.22957
				157	\rightarrow	162	-0.11138
				157	\rightarrow	163	-0.12075
				158	\rightarrow	167	-0.10747
				158	\rightarrow	170	-0.1145
				160	\rightarrow	166	-0.11697
				160	\rightarrow	167	0.19301
25	4.1238	300.66	0.0024	155	\rightarrow	161	-0.2627
				156	\rightarrow	162	-0.11904
				156	\rightarrow	163	0.17602
				158	\rightarrow	164	-0.19788
				158	\rightarrow	167	-0.15919
				158	\rightarrow	170	-0.13402
				159	\rightarrow	164	0.10877
				159	\rightarrow	165	0.27142
				159	\rightarrow	166	0.2278
				160	\rightarrow	166	-0.15361
				160	\rightarrow	168	-0.22911
				160	\rightarrow	169	-0.12036
26	4.1738	297.06	0.0087	155	\rightarrow	162	-0.30734
				156	\rightarrow	163	0.10397
				157	\rightarrow	163	-0.15765
				159	\rightarrow	164	0.15332
				159	\rightarrow	165	-0.19345
				159	\rightarrow	166	0.36711
				159	\rightarrow	167	-0.20836
				160	\rightarrow	166	0.12049
				160	\rightarrow	168	0.18647
27	4.177	296.82	0.004	155	\rightarrow	162	0.50264
				157	\rightarrow	162	0.12314
				157	\rightarrow	163	0.18288
				159	\rightarrow	164	0.13098
				159	\rightarrow	166	0.29552
				159	\rightarrow	167	-0.19889
				160	\rightarrow	167	0.10888
28	4.1869	296.13	0.0031	155	\rightarrow	161	-0.10973
				155	\rightarrow	163	0.142
				158	\rightarrow	165	0.20304
				158	\rightarrow	171	0.10502
				159	\rightarrow	165	0.21311
				160	\rightarrow	167	0.26921
				160	\rightarrow	168	0.33877
				160	\rightarrow	169	0.27267
29	4.2124	294.33	0.0062	155	\rightarrow	163	0.43768
				157	\rightarrow	162	0.13864

				158	\rightarrow	164	-0.29281
				159	\rightarrow	164	-0.12724
				159	\rightarrow	165	-0.19744
				160	\rightarrow	167	-0.14056
30	4.2233	293.57	0.0006	155	\rightarrow	163	-0.31126
				158	\rightarrow	164	-0.31093
				158	\rightarrow	165	0.13952
				158	\rightarrow	166	0.16237
				158	\rightarrow	167	-0.11563
				159	\rightarrow	165	-0.11342
				160	\rightarrow	167	-0.10788
				160	\rightarrow	169	0.34358
				160	\rightarrow	170	0.12714
31	4.2471	291.93	0.0071	154	\rightarrow	163	-0.10958
				155	\rightarrow	163	0.29804
				158	\rightarrow	164	0.19017
				159	\rightarrow	164	0.10682
				159	\rightarrow	167	-0.10519
				159	\rightarrow	169	-0.10876
				160	\rightarrow	168	-0.28634
				160	\rightarrow	169	0.3897
32	4.3008	288.28	0.0126	154	\rightarrow	161	-0.10948
				158	\rightarrow	165	0.49328
				158	\rightarrow	166	0.11516
				159	\rightarrow	165	0.10822
				159	\rightarrow	167	-0.20375
				160	\rightarrow	168	-0.17255
				160	\rightarrow	169	-0.12116
				160	\rightarrow	170	-0.10509
				160	\rightarrow	171	0.14525
				160	\rightarrow	174	0.13249
33	4.3386	285.77	0.0202	158	\rightarrow	164	0.12344
				158	\rightarrow	166	-0.14076
				158	\rightarrow	169	0.10246
				159	\rightarrow	165	-0.19143
				159	\rightarrow	166	0.20199
				159	\rightarrow	167	0.17886
				159	\rightarrow	168	0.30096
				159	\rightarrow	169	0.32839
				159	\rightarrow	171	0.10809
				160	\rightarrow	170	-0.17793
34	4.3549	284.7	0.0103	153	\rightarrow	162	-0.11232
				154	\rightarrow	161	0.1134
				158	\rightarrow	164	0.18997
				158	\rightarrow	166	0.50654
				158	\rightarrow	167	-0.19821

				158	\rightarrow	168	-0.11927
				159	\rightarrow	167	0.20428
				159	\rightarrow	168	0.11067
35	4.4099	281.15	0.0028	158	\rightarrow	164	0.16942
				158	\rightarrow	165	0.23257
				158	\rightarrow	166	-0.25886
				158	\rightarrow	169	-0.14261
				158	\rightarrow	171	-0.10102
				159	\rightarrow	166	0.15795
				159	\rightarrow	167	0.27196
				159	\rightarrow	169	-0.19497
				159	\rightarrow	170	-0.16783
				160	\rightarrow	170	0.20597
				160	\rightarrow	175	-0.10372
36	4.4177	280.65	0.0113	158	\rightarrow	164	-0.19568
				158	\rightarrow	167	0.37166
				158	\rightarrow	168	-0.12875
				158	\rightarrow	169	-0.10079
				159	\rightarrow	165	0.16571
				159	\rightarrow	167	0.25906
				159	\rightarrow	169	-0.10897
				160	\rightarrow	167	0.16266
				160	\rightarrow	168	-0.11807
				160	\rightarrow	169	0.11246
				160	\rightarrow	170	-0.1913
				160	\rightarrow	171	-0.11034
				160	\rightarrow	175	0.11297
37	4.4467	278.82	0.0389	154	\rightarrow	161	-0.12169
				158	\rightarrow	164	0.14658
				158	\rightarrow	168	-0.10116
				158	\rightarrow	169	-0.2178
				158	\rightarrow	171	-0.14731
				158	\rightarrow	174	-0.12854
				159	\rightarrow	168	-0.25353
				159	\rightarrow	169	0.44419
				160	\rightarrow	171	-0.14949
				160	\rightarrow	174	-0.12471
38	4.5049	275.22	0.0215	154	\rightarrow	161	0.13419
				158	\rightarrow	166	-0.12615
				158	\rightarrow	168	-0.23755
				159	\rightarrow	168	0.41132
				159	\rightarrow	170	0.20792
				159	\rightarrow	171	-0.14328
				159	\rightarrow	174	-0.12893
				160	\rightarrow	170	0.15502
39	4.5365	273.31	0.0094	153	\rightarrow	162	-0.1185

					153	\rightarrow	163	-0.10032
					154	\rightarrow	161	-0.20885
					158	\rightarrow	167	0.17287
					158	\rightarrow	168	0.32773
					159	\rightarrow	168	0.18064
					159	\rightarrow	171	-0.23452
					159	\rightarrow	174	-0.18883
					160	\rightarrow	167	-0.11943
					160	\rightarrow	170	0.17333
40	4.5551	272.19	0.0212		152	\rightarrow	161	0.18764
					152	\rightarrow	163	0.11388
					154	\rightarrow	161	0.31825
					154	\rightarrow	162	-0.14142
					154	\rightarrow	163	0.19737
					155	\rightarrow	164	0.12767
					157	\rightarrow	164	0.27488
					157	\rightarrow	166	0.15675
					158	\rightarrow	167	0.12311
					158	\rightarrow	168	0.12356
					159	\rightarrow	168	-0.10598
					159	\rightarrow	169	0.13691
					160	\rightarrow	168	-0.10528

Table S16. TDDFT calculated transitions for *mer*-[Ru(Q1Pz)₃]²⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.7322	453.8	0.1456	159	\rightarrow	161	0.12057
				160	\rightarrow	161	0.68977
2	2.758	449.54	0.0186	160	\rightarrow	162	0.69195
3	2.8662	432.57	0.0369	159	\rightarrow	161	0.6602
				160	\rightarrow	161	-0.11424
				160	\rightarrow	163	0.17636
4	2.9116	425.82	0.015	159	\rightarrow	162	0.63799
				160	\rightarrow	163	0.23489
5	2.9233	424.12	0.0077	158	\rightarrow	161	0.1609
				158	\rightarrow	162	0.17165
				159	\rightarrow	161	-0.16821
				159	\rightarrow	162	-0.14067
				159	\rightarrow	163	0.36482
				160	\rightarrow	163	0.48767
6	2.982	415.77	0.0139	158	\rightarrow	161	-0.23777
				158	\rightarrow	162	-0.11
				159	\rightarrow	162	0.16003
				159	\rightarrow	163	0.5676
				160	\rightarrow	163	-0.22435
7	3.017	410.95	0.0066	158	\rightarrow	161	0.62115
				158	\rightarrow	162	-0.1452

				158	\rightarrow	163	0.17863
				159	\rightarrow	163	0.10099
				160	\rightarrow	163	-0.1818
8	3.1107	398.58	0.0158	158	\rightarrow	162	0.28322
				158	\rightarrow	163	0.61117
9	3.1874	388.98	0.0687	158	\rightarrow	161	0.10392
				158	\rightarrow	162	0.57056
				158	\rightarrow	163	-0.20743
				159	\rightarrow	162	0.1628
				160	\rightarrow	163	-0.22748
10	3.5977	344.62	0.0049	159	\rightarrow	170	-0.10885
				159	\rightarrow	175	-0.10609
				160	\rightarrow	165	0.3733
				160	\rightarrow	168	-0.15303
				160	\rightarrow	169	-0.21777
				160	\rightarrow	170	0.1672
				160	\rightarrow	171	0.24796
				160	\rightarrow	174	-0.20542
				160	\rightarrow	175	0.16892
11	3.7011	334.99	0.0054	158	\rightarrow	165	-0.12632
				158	\rightarrow	170	-0.14211
				158	\rightarrow	175	-0.13268
				159	\rightarrow	170	0.12047
				159	\rightarrow	171	-0.15677
				159	\rightarrow	174	0.14586
				160	\rightarrow	164	-0.18189
				160	\rightarrow	166	0.28757
				160	\rightarrow	167	0.15902
				160	\rightarrow	170	0.23048
				160	\rightarrow	171	-0.18635
				160	\rightarrow	174	0.17521
				160	\rightarrow	175	0.16218
12	3.7679	329.05	0.0063	157	\rightarrow	161	0.66216
13	3.772	328.69	0.008	157	\rightarrow	161	0.14856
				158	\rightarrow	165	0.12656
				158	\rightarrow	166	-0.10319
				158	\rightarrow	171	0.22854
				158	\rightarrow	174	-0.19689
				159	\rightarrow	164	-0.10931
				159	\rightarrow	165	0.19693
				159	\rightarrow	167	0.14226
				159	\rightarrow	168	-0.15234
				159	\rightarrow	170	0.31204
				159	\rightarrow	175	0.25258
14	3.82	324.57	0.0017	156	\rightarrow	161	-0.14381
				160	\rightarrow	164	0.56479

				160	\rightarrow	166	-0.17329
15	3.8893	318.78	0.2	155	\rightarrow	161	-0.12863
				156	\rightarrow	161	0.47108
				157	\rightarrow	162	0.17905
				157	\rightarrow	163	0.38522
				160	\rightarrow	164	0.20959
16	3.9498	313.9	0.1198	155	\rightarrow	162	0.20255
				156	\rightarrow	162	0.61127
				157	\rightarrow	162	0.21873
17	3.9638	312.79	0.0111	156	\rightarrow	161	-0.35834
				156	\rightarrow	162	-0.16474
				157	\rightarrow	162	0.54616
				157	\rightarrow	163	0.14888
18	3.9754	311.88	0.0144	157	\rightarrow	163	-0.16138
				158	\rightarrow	165	0.15267
				158	\rightarrow	166	-0.1186
				158	\rightarrow	171	0.20799
				158	\rightarrow	174	-0.1686
				159	\rightarrow	164	0.11922
				159	\rightarrow	165	-0.22741
				159	\rightarrow	166	0.10694
				159	\rightarrow	168	0.11172
				159	\rightarrow	171	-0.1366
				159	\rightarrow	174	0.11795
				160	\rightarrow	165	-0.25541
				160	\rightarrow	166	0.26571
				160	\rightarrow	168	0.12302
				160	\rightarrow	171	0.11389
19	3.9889	310.82	0.0169	156	\rightarrow	162	-0.10846
				157	\rightarrow	162	0.22163
				157	\rightarrow	163	-0.25161
				159	\rightarrow	164	0.12505
				159	\rightarrow	165	0.11657
				159	\rightarrow	166	-0.15813
				159	\rightarrow	171	0.11371
				160	\rightarrow	164	0.17265
				160	\rightarrow	165	0.2897
				160	\rightarrow	166	0.33154
20	4.0013	309.86	0.0128	155	\rightarrow	161	-0.1073
				156	\rightarrow	161	-0.31458
				156	\rightarrow	162	0.14113
				157	\rightarrow	162	-0.2259
				157	\rightarrow	163	0.38991
				160	\rightarrow	164	0.10494
				160	\rightarrow	165	0.17171
				160	\rightarrow	166	0.26569

				160	\rightarrow	168	0.11113
21	4.0375	307.08	0.009	157	\rightarrow	163	0.11678
				159	\rightarrow	164	0.30105
				159	\rightarrow	165	0.17117
				159	\rightarrow	166	-0.29989
				159	\rightarrow	167	-0.13756
				160	\rightarrow	165	-0.21725
				160	\rightarrow	167	0.23538
				160	\rightarrow	168	-0.22481
				160	\rightarrow	170	0.1155
22	4.0674	304.82	0.0096	159	\rightarrow	164	0.52045
				160	\rightarrow	165	0.13298
				160	\rightarrow	166	-0.12973
				160	\rightarrow	167	-0.29219
				160	\rightarrow	168	0.13719
23	4.121	300.86	0.0139	156	\rightarrow	163	0.63677
				157	\rightarrow	161	-0.10561
				160	\rightarrow	169	-0.14414
24	4.1327	300	0.0088	158	\rightarrow	164	0.38062
				158	\rightarrow	165	-0.14701
				158	\rightarrow	166	-0.1558
				158	\rightarrow	167	-0.20859
				158	\rightarrow	168	0.11114
				158	\rightarrow	170	-0.14073
				159	\rightarrow	164	-0.17317
				159	\rightarrow	165	0.16708
				159	\rightarrow	166	-0.14876
				160	\rightarrow	166	0.15293
				160	\rightarrow	167	-0.23778
25	4.1406	299.43	0.0023	154	\rightarrow	161	0.12266
				154	\rightarrow	163	-0.1098
				155	\rightarrow	161	-0.18126
				156	\rightarrow	163	0.1528
				157	\rightarrow	163	-0.10328
				158	\rightarrow	166	-0.14016
				160	\rightarrow	165	0.1239
				160	\rightarrow	166	-0.17727
				160	\rightarrow	167	0.3497
				160	\rightarrow	168	0.3478
				160	\rightarrow	169	0.18947
26	4.1599	298.05	0.0159	155	\rightarrow	161	0.63391
				157	\rightarrow	163	0.17318
				160	\rightarrow	167	0.12774
				160	\rightarrow	168	0.13269
27	4.1745	297	0.0054	156	\rightarrow	163	-0.13413
				158	\rightarrow	164	0.23095

				158	→	166	0.10112
				158	→	171	-0.10577
				159	→	164	0.18005
				159	→	165	0.16332
				159	→	166	0.29404
				160	→	167	0.25044
				160	→	169	-0.26707
				160	→	170	-0.11838
				160	→	171	0.10486
				160	→	174	-0.10008
28	4.1995	295.23	0.0028	158	→	164	0.17379
				159	→	166	0.2773
				159	→	168	0.10089
				160	→	165	0.10766
				160	→	168	-0.31298
				160	→	169	0.44879
29	4.2438	292.15	0.0043	155	→	162	-0.14705
				158	→	164	0.40403
				158	→	165	0.18318
				158	→	170	0.11492
				159	→	165	-0.29728
				159	→	166	-0.17251
				159	→	168	-0.16784
				160	→	168	-0.14956
				160	→	169	-0.14574
				160	→	171	-0.11835
30	4.2589	291.12	0.0039	155	→	162	0.55035
				156	→	162	-0.16351
				158	→	166	0.1159
				159	→	165	-0.13882
				159	→	167	0.1687
				159	→	168	-0.14075
31	4.2841	289.41	0.002	155	→	162	0.31075
				155	→	163	0.14905
				158	→	164	0.11853
				158	→	165	0.19788
				158	→	166	-0.16916
				158	→	168	-0.14178
				159	→	165	0.14941
				159	→	166	0.11348
				159	→	167	-0.27568
				159	→	168	0.15944
				160	→	169	-0.13137
				160	→	170	0.12799
				160	→	171	-0.15528
				160	→	174	0.10558

32	4.3162	287.25	0.0064	158	\rightarrow	165	0.13119
				158	\rightarrow	166	0.50491
				158	\rightarrow	168	0.11429
				158	\rightarrow	169	-0.13233
				159	\rightarrow	165	0.12908
				159	\rightarrow	167	-0.22656
				160	\rightarrow	168	0.13316
33	4.3338	286.09	0.0008	155	\rightarrow	162	-0.10767
				155	\rightarrow	163	0.6345
34	4.3645	284.07	0.011	158	\rightarrow	165	0.13892
				158	\rightarrow	168	-0.13937
				159	\rightarrow	165	0.2916
				159	\rightarrow	166	-0.10798
				159	\rightarrow	167	0.40084
				159	\rightarrow	169	0.31783
35	4.4003	281.76	0.0152	158	\rightarrow	166	0.13648
				158	\rightarrow	168	0.10726
				159	\rightarrow	166	-0.18731
				159	\rightarrow	167	0.18146
				159	\rightarrow	168	0.53594
				159	\rightarrow	169	-0.21833
36	4.4361	279.49	0.0024	155	\rightarrow	163	0.16153
				158	\rightarrow	165	-0.10674
				158	\rightarrow	168	-0.13203
				158	\rightarrow	171	0.11192
				159	\rightarrow	165	-0.1034
				159	\rightarrow	166	0.11023
				159	\rightarrow	167	0.1362
				159	\rightarrow	168	-0.10811
				159	\rightarrow	171	0.3077
				159	\rightarrow	174	-0.1864
				160	\rightarrow	168	0.19514
				160	\rightarrow	170	0.28254
				160	\rightarrow	175	0.16217
37	4.4378	279.38	0.004	158	\rightarrow	164	-0.1123
				158	\rightarrow	165	0.4331
				158	\rightarrow	167	-0.23423
				158	\rightarrow	168	0.22277
				158	\rightarrow	170	-0.10023
				159	\rightarrow	167	0.16601
				159	\rightarrow	168	-0.11606
				159	\rightarrow	169	-0.20751
				159	\rightarrow	170	-0.15117
38	4.4843	276.48	0.0083	152	\rightarrow	162	0.14347
				154	\rightarrow	161	0.10403
				158	\rightarrow	167	0.24176

				158	\rightarrow	168	0.44267
				158	\rightarrow	171	0.12446
				159	\rightarrow	169	0.26203
				159	\rightarrow	171	0.16145
39	4.4983	275.63	0.0017	158	\rightarrow	165	0.11264
				158	\rightarrow	167	0.29137
				158	\rightarrow	171	-0.25782
				158	\rightarrow	174	0.14261
				159	\rightarrow	169	-0.17646
				159	\rightarrow	170	0.15783
				159	\rightarrow	175	0.11734
				160	\rightarrow	165	-0.10295
				160	\rightarrow	171	0.29363
				160	\rightarrow	174	-0.12121
40	4.5674	271.46	0.0292	153	\rightarrow	163	-0.10447
				154	\rightarrow	161	0.12446
				157	\rightarrow	164	-0.13285
				158	\rightarrow	169	0.50166
				159	\rightarrow	167	-0.12732
				159	\rightarrow	169	0.1793
				159	\rightarrow	170	0.15004

Table S17. TDDFT calculated transitions for *cis-fac-[Ru(DQPz)₂]²⁺.*

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.5239	491.24	0.0214	175	\rightarrow	176	0.68051
				175	\rightarrow	178	-0.15364
2	2.578	480.93	0.0204	175	\rightarrow	177	0.66938
				175	\rightarrow	179	-0.17212
3	2.6846	461.83	0.0358	174	\rightarrow	176	-0.17112
				175	\rightarrow	176	0.14066
				175	\rightarrow	178	0.65541
4	2.7572	449.67	0.0868	174	\rightarrow	176	0.65132
				174	\rightarrow	178	-0.18347
				175	\rightarrow	178	0.1281
5	2.7753	446.75	0.0898	174	\rightarrow	177	0.66026
				174	\rightarrow	179	0.17921
6	2.8755	431.18	0.0152	174	\rightarrow	176	0.17132
				174	\rightarrow	178	0.64558
				174	\rightarrow	186	0.10165
				175	\rightarrow	178	0.11477
7	2.8787	430.7	0.1011	174	\rightarrow	179	-0.28052
				175	\rightarrow	177	0.12147
				175	\rightarrow	179	0.61664
8	3.0822	402.26	0.0039	172	\rightarrow	177	0.24866
				173	\rightarrow	177	0.65476
9	3.1104	398.61	0.0315	172	\rightarrow	176	0.25232

				173	→	176	0.63454
				174	→	179	-0.13205
10	3.2662	379.6	0.0128	172	→	178	0.23171
				173	→	178	0.63987
11	3.2913	376.7	0.0011	173	→	176	0.13629
				174	→	177	-0.14444
				174	→	179	0.58003
				175	→	177	0.12415
				175	→	179	0.24948
12	3.4167	362.88	0.0017	172	→	179	0.24361
				173	→	179	0.64105
13	3.5113	353.1	0.335	172	→	176	0.64162
				173	→	176	-0.24562
14	3.517	352.53	0.0831	171	→	176	-0.15073
				172	→	177	0.63183
				173	→	177	-0.24286
15	3.6056	343.86	0.0186	175	→	180	0.66452
				175	→	183	0.13726
16	3.672	337.64	0.0118	171	→	176	0.59797
				171	→	178	-0.13329
				172	→	177	0.14301
				174	→	186	-0.14567
				174	→	189	-0.12558
				175	→	180	-0.10111
17	3.6803	336.89	0.0269	171	→	177	-0.12096
				172	→	178	0.4382
				173	→	178	-0.19023
				175	→	181	-0.43505
				175	→	182	0.18774
18	3.7145	333.78	0.0578	171	→	177	0.67152
				175	→	181	-0.10504
19	3.7168	333.58	0.0096	172	→	178	0.47488
				173	→	178	-0.13516
				175	→	181	0.42026
				175	→	182	-0.18715
20	3.7403	331.48	0.0034	171	→	176	0.27324
				171	→	178	0.22739
				171	→	186	0.12369
				174	→	178	-0.1389
				174	→	180	-0.19958
				174	→	186	0.26297
				174	→	189	0.21469
				174	→	191	0.13138
				175	→	186	0.22371
				175	→	189	0.16616
				175	→	191	0.10195

21	3.7974	326.5	0.0088	171	→	176	0.12755
				174	→	180	0.59936
				174	→	186	0.17831
				174	→	189	0.14023
22	3.8654	320.76	0.0018	174	→	182	-0.1499
				175	→	181	0.22114
				175	→	182	0.61506
				175	→	193	-0.11872
23	3.9013	317.81	0.0042	171	→	178	0.41096
				172	→	179	-0.3925
				173	→	179	0.19629
				174	→	180	-0.13929
				175	→	183	0.11196
				175	→	186	-0.21226
				175	→	189	-0.12516
24	3.9202	316.27	0.0128	171	→	178	0.3844
				173	→	179	-0.11629
				174	→	180	0.21572
				174	→	183	0.12734
				174	→	186	-0.26961
				174	→	189	-0.19886
				174	→	191	-0.11146
				175	→	183	-0.13843
				175	→	186	0.21733
				175	→	189	0.13729
25	3.9336	315.19	0.0071	171	→	178	0.27575
				172	→	179	0.51177
				173	→	179	-0.14064
				175	→	180	-0.11415
				175	→	183	0.15885
				175	→	186	-0.20656
				175	→	189	-0.13095
26	3.9379	314.85	0.0579	174	→	181	0.49635
				174	→	182	-0.46272
27	4.0143	308.85	0.0025	175	→	183	0.62124
				175	→	186	0.19382
				175	→	189	0.12391
28	4.0268	307.9	0.0001	165	→	177	-0.10335
				166	→	176	0.134
				171	→	179	0.10948
				174	→	181	0.41348
				174	→	182	0.46101
				175	→	182	0.15349
29	4.0867	303.39	0.0002	168	→	176	-0.1321
				168	→	178	-0.15558
				174	→	181	0.10869

				175	\rightarrow	184	0.61922
30	4.1069	301.89	0.004	167	\rightarrow	178	-0.13729
				168	\rightarrow	177	-0.12754
				168	\rightarrow	179	-0.11498
				170	\rightarrow	176	-0.12116
				174	\rightarrow	183	-0.30427
				175	\rightarrow	185	0.53023
31	4.1183	301.05	0.0036	170	\rightarrow	177	0.10341
				171	\rightarrow	179	0.63689
				173	\rightarrow	180	0.19083
32	4.1537	298.49	0.0055	165	\rightarrow	176	-0.13211
				166	\rightarrow	177	0.14679
				174	\rightarrow	183	0.5141
				174	\rightarrow	185	0.10751
				175	\rightarrow	183	0.13117
				175	\rightarrow	185	0.32237
33	4.2076	294.67	0.0034	172	\rightarrow	186	0.13022
				172	\rightarrow	189	0.11364
				173	\rightarrow	186	0.2654
				173	\rightarrow	189	0.21077
				173	\rightarrow	191	0.13192
				174	\rightarrow	184	-0.11439
				174	\rightarrow	193	-0.13383
				175	\rightarrow	181	0.1861
				175	\rightarrow	187	0.11952
				175	\rightarrow	188	0.11844
				175	\rightarrow	190	-0.17481
				175	\rightarrow	193	0.33713
34	4.3017	288.22	0.0167	172	\rightarrow	181	0.22001
				172	\rightarrow	182	-0.12274
				173	\rightarrow	181	0.54102
				173	\rightarrow	182	-0.2699
				175	\rightarrow	186	0.13302
35	4.3154	287.31	0.0012	169	\rightarrow	176	-0.25953
				171	\rightarrow	179	-0.1773
				172	\rightarrow	180	0.18453
				173	\rightarrow	180	0.46577
				174	\rightarrow	184	-0.26211
36	4.3387	285.76	0.017	166	\rightarrow	176	0.12983
				168	\rightarrow	176	-0.114
				168	\rightarrow	178	-0.10036
				169	\rightarrow	176	-0.25793
				173	\rightarrow	180	0.1781
				174	\rightarrow	184	0.52247
				175	\rightarrow	184	-0.13207
37	4.3551	284.69	0.0266	169	\rightarrow	177	-0.11701

					170	\rightarrow	176	0.64123
					174	\rightarrow	183	-0.10575
					174	\rightarrow	185	-0.12926
					175	\rightarrow	185	0.11252
38	4.3847	282.77	0.0002		169	\rightarrow	176	0.41724
					170	\rightarrow	177	0.42387
					171	\rightarrow	179	-0.13404
					173	\rightarrow	180	0.24994
39	4.3873	282.6	0.0093		168	\rightarrow	177	-0.10429
					169	\rightarrow	177	0.23362
					170	\rightarrow	176	0.14591
					170	\rightarrow	178	-0.10884
					173	\rightarrow	182	-0.11699
					174	\rightarrow	183	-0.1083
					174	\rightarrow	185	0.5352
					175	\rightarrow	185	-0.15798
40	4.3925	282.26	0.0004		169	\rightarrow	176	-0.38261
					170	\rightarrow	177	0.52228
					173	\rightarrow	180	-0.15848

Table S18. TDDFT calculated transitions for *trans-fac*-[Ru(DQPz)₂]²⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.4483	506.42	0.0857	175	\rightarrow	176	0.69657
2	2.5288	490.28	0.0011	174	\rightarrow	177	0.24198
				175	\rightarrow	177	0.63377
				175	\rightarrow	178	-0.14427
3	2.6351	470.51	0.1097	174	\rightarrow	177	0.14497
				174	\rightarrow	178	0.10024
				175	\rightarrow	178	0.67201
4	2.6923	460.51	0.0147	175	\rightarrow	179	0.68245
				175	\rightarrow	186	-0.11093
5	2.8531	434.56	0.0019	173	\rightarrow	179	0.10621
				174	\rightarrow	177	0.61984
				175	\rightarrow	177	-0.24778
				175	\rightarrow	178	-0.11273
6	2.8885	429.23	0.0194	174	\rightarrow	176	0.68108
				174	\rightarrow	179	-0.10013
7	3.0387	408.01	0.0023	171	\rightarrow	177	0.25966
				173	\rightarrow	177	0.54703
				174	\rightarrow	176	0.1272
				174	\rightarrow	179	0.28621
8	3.0629	404.8	0.0048	173	\rightarrow	176	0.29807
				174	\rightarrow	178	0.62263
9	3.1366	395.29	0.0006	171	\rightarrow	177	-0.13879
				173	\rightarrow	177	-0.29166
				174	\rightarrow	179	0.57001

				174	\rightarrow	186	-0.14784
10	3.1854	389.23	0.2184	171	\rightarrow	176	0.23419
				173	\rightarrow	176	0.57874
				174	\rightarrow	178	-0.2893
11	3.3252	372.86	0.0261	171	\rightarrow	178	0.23104
				173	\rightarrow	178	0.65225
12	3.4597	358.36	0.0016	171	\rightarrow	177	0.15242
				172	\rightarrow	176	0.67137
13	3.4642	357.9	0.0404	171	\rightarrow	179	0.21667
				172	\rightarrow	177	-0.19002
				173	\rightarrow	179	0.48134
				175	\rightarrow	181	0.2435
				175	\rightarrow	183	0.15839
				175	\rightarrow	185	0.11308
				175	\rightarrow	192	0.16653
14	3.4968	354.56	0.024	175	\rightarrow	180	0.67433
				175	\rightarrow	182	-0.11241
15	3.5149	352.74	0.3068	171	\rightarrow	176	0.1672
				172	\rightarrow	177	0.62555
				175	\rightarrow	183	0.12757
16	3.5317	351.06	0.0014	171	\rightarrow	176	-0.16867
				171	\rightarrow	179	-0.10493
				173	\rightarrow	179	-0.36666
				175	\rightarrow	181	0.46207
				175	\rightarrow	183	0.22365
				175	\rightarrow	185	0.12713
				175	\rightarrow	192	0.13902
17	3.5648	347.8	0.0009	171	\rightarrow	177	0.57743
				172	\rightarrow	176	-0.17058
				173	\rightarrow	177	-0.2945
18	3.5939	344.99	0.0633	171	\rightarrow	176	0.6042
				172	\rightarrow	177	-0.21535
				173	\rightarrow	176	-0.21926
				175	\rightarrow	181	0.11455
19	3.6321	341.36	0.0007	171	\rightarrow	177	0.13475
				174	\rightarrow	179	-0.19034
				174	\rightarrow	186	-0.16431
				174	\rightarrow	189	-0.12391
				174	\rightarrow	190	-0.11963
				175	\rightarrow	179	0.12739
				175	\rightarrow	180	0.13455
				175	\rightarrow	182	0.17668
				175	\rightarrow	184	0.11533
				175	\rightarrow	186	0.39496
				175	\rightarrow	189	0.24124
				175	\rightarrow	190	0.22777

20	3.6878	336.2	0.008	172	→	178	0.69391
21	3.7524	330.41	0.0038	171	→	178	0.61965
				172	→	179	0.11524
				173	→	178	-0.22009
22	3.7861	327.47	0.0031	171	→	177	0.11926
				171	→	178	0.1943
				172	→	179	-0.2968
				174	→	179	0.18118
				174	→	186	0.32784
				174	→	189	0.23548
				174	→	190	0.22498
				175	→	182	0.15659
				175	→	186	0.11199
23	3.8344	323.35	0.0026	172	→	179	0.58882
				174	→	186	0.19029
				174	→	189	0.13301
				174	→	190	0.13094
				175	→	184	0.11566
24	3.8577	321.4	0.0064	171	→	179	0.12732
				173	→	179	-0.10775
				175	→	181	-0.36505
				175	→	183	0.54944
25	3.8852	319.12	0.0138	171	→	179	0.57911
				171	→	186	-0.10723
				173	→	179	-0.26707
				175	→	183	-0.1815
26	3.9187	316.39	0.0081	175	→	182	0.61772
				175	→	184	-0.18015
				175	→	186	-0.15661
27	3.9918	310.6	0.0108	168	→	178	-0.10866
				172	→	179	-0.1273
				174	→	180	0.29274
				175	→	182	0.12223
				175	→	184	0.53391
				175	→	186	-0.14618
28	4.011	309.11	0.0299	174	→	180	0.61194
				175	→	184	-0.28147
29	4.0111	309.1	0.0032	170	→	176	-0.13266
				175	→	181	-0.15091
				175	→	183	-0.16767
				175	→	185	0.59498
				175	→	192	0.1064
30	4.0882	303.28	0.0018	170	→	176	-0.11627
				171	→	179	-0.15924
				171	→	186	-0.10288
				173	→	186	-0.11332

				174	→	181	0.42345
				174	→	192	0.19
				175	→	181	-0.12327
				175	→	185	-0.15087
				175	→	188	-0.13084
				175	→	192	0.26398
31	4.1689	297.4	0.0014	170	→	176	-0.15383
				171	→	179	0.15783
				171	→	186	0.15302
				171	→	189	0.11431
				171	→	190	0.10832
				173	→	180	-0.19135
				173	→	182	0.12682
				173	→	186	0.16957
				173	→	189	0.12177
				173	→	190	0.1091
				174	→	181	0.41197
				175	→	188	0.10166
				175	→	192	-0.20154
32	4.1984	295.31	0.0028	171	→	180	0.20694
				173	→	180	0.60581
				175	→	192	-0.11852
33	4.2454	292.04	0.0077	167	→	177	-0.14584
				168	→	177	0.15219
				170	→	177	-0.26051
				171	→	181	0.11231
				172	→	180	-0.10671
				173	→	181	0.44224
				174	→	182	0.21427
34	4.2859	289.29	0.026	168	→	178	0.1187
				170	→	177	0.47616
				171	→	181	0.12857
				171	→	192	0.10029
				173	→	181	0.23622
				173	→	183	0.25172
				174	→	182	-0.11205
				175	→	184	0.13435
35	4.2879	289.15	0.0002	169	→	177	-0.12159
				170	→	176	0.61179
				174	→	181	0.18694
				175	→	185	0.13149
36	4.3201	286.99	0.0006	167	→	176	0.20756
				167	→	179	-0.1072
				168	→	176	-0.28769
				170	→	179	-0.13149
				172	→	181	0.13823

					173	→	182	-0.14969
					173	→	184	0.10346
					174	→	183	0.4274
37	4.3443	285.39	0.0048		167	→	177	-0.11687
					168	→	177	0.18653
					170	→	177	0.20861
					170	→	178	0.37162
					173	→	181	-0.12006
					173	→	183	-0.10293
					173	→	185	-0.17743
					174	→	182	0.31579
					175	→	184	0.13946
					175	→	186	-0.10128
38	4.4035	281.56	0.0116		168	→	177	-0.10827
					169	→	176	-0.25852
					170	→	177	0.26456
					170	→	178	-0.34439
					174	→	182	0.38365
					174	→	184	-0.18461
39	4.4072	281.32	0.0037		167	→	176	-0.14821
					168	→	176	0.27733
					169	→	177	-0.15174
					170	→	179	0.12952
					173	→	182	0.22368
					174	→	181	-0.24246
					174	→	183	0.32957
					174	→	185	0.13243
					175	→	192	0.14335
40	4.4483	278.72	0.0058		165	→	177	-0.11717
					166	→	178	0.13034
					167	→	176	0.24413
					168	→	176	0.23372
					168	→	179	0.14565
					169	→	177	0.29449
					170	→	179	0.16169
					172	→	181	0.10068
					173	→	182	-0.21138
					173	→	184	-0.17896
					174	→	185	0.13166
					175	→	185	0.16009
					175	→	187	-0.13029

Table S19. TDDFT calculated transitions for C-R_a-mer-[Ru(DQPz)₂]²⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.5239	491.24	0.0214	175	→	176	0.68051
				175	→	178	-0.15364

2	2.578	480.93	0.0204	175	→	177	0.66938
				175	→	179	-0.17212
3	2.6846	461.83	0.0358	174	→	176	-0.17112
				175	→	176	0.14066
				175	→	178	0.65541
4	2.7572	449.67	0.0868	174	→	176	0.65132
				174	→	178	-0.18347
				175	→	178	0.1281
5	2.7753	446.75	0.0898	174	→	177	0.66026
				174	→	179	0.17921
6	2.8755	431.18	0.0152	174	→	176	0.17132
				174	→	178	0.64558
				174	→	186	0.10165
				175	→	178	0.11477
7	2.8787	430.7	0.1011	174	→	179	-0.28052
				175	→	177	0.12147
				175	→	179	0.61664
8	3.0822	402.26	0.0039	172	→	177	0.24866
				173	→	177	0.65476
9	3.1104	398.61	0.0315	172	→	176	0.25232
				173	→	176	0.63454
				174	→	179	-0.13205
10	3.2662	379.6	0.0128	172	→	178	0.23171
				173	→	178	0.63987
11	3.2913	376.7	0.0011	173	→	176	0.13629
				174	→	177	-0.14444
				174	→	179	0.58003
				175	→	177	0.12415
				175	→	179	0.24948
12	3.4167	362.88	0.0017	172	→	179	0.24361
				173	→	179	0.64105
13	3.5113	353.1	0.335	172	→	176	0.64162
				173	→	176	-0.24562
14	3.517	352.53	0.0831	171	→	176	-0.15073
				172	→	177	0.63183
				173	→	177	-0.24286
15	3.6056	343.86	0.0186	175	→	180	0.66452
				175	→	183	0.13726
16	3.672	337.64	0.0118	171	→	176	0.59797
				171	→	178	-0.13329
				172	→	177	0.14301
				174	→	186	-0.14567
				174	→	189	-0.12558
				175	→	180	-0.10111
17	3.6803	336.89	0.0269	171	→	177	-0.12096
				172	→	178	0.4382

				173	→	178	-0.19023
				175	→	181	-0.43505
				175	→	182	0.18774
18	3.7145	333.78	0.0578	171	→	177	0.67152
				175	→	181	-0.10504
19	3.7168	333.58	0.0096	172	→	178	0.47488
				173	→	178	-0.13516
				175	→	181	0.42026
				175	→	182	-0.18715
20	3.7403	331.48	0.0034	171	→	176	0.27324
				171	→	178	0.22739
				171	→	186	0.12369
				174	→	178	-0.1389
				174	→	180	-0.19958
				174	→	186	0.26297
				174	→	189	0.21469
				174	→	191	0.13138
				175	→	186	0.22371
				175	→	189	0.16616
				175	→	191	0.10195
21	3.7974	326.5	0.0088	171	→	176	0.12755
				174	→	180	0.59936
				174	→	186	0.17831
				174	→	189	0.14023
22	3.8654	320.76	0.0018	174	→	182	-0.1499
				175	→	181	0.22114
				175	→	182	0.61506
				175	→	193	-0.11872
23	3.9013	317.81	0.0042	171	→	178	0.41096
				172	→	179	-0.3925
				173	→	179	0.19629
				174	→	180	-0.13929
				175	→	183	0.11196
				175	→	186	-0.21226
				175	→	189	-0.12516
24	3.9202	316.27	0.0128	171	→	178	0.3844
				173	→	179	-0.11629
				174	→	180	0.21572
				174	→	183	0.12734
				174	→	186	-0.26961
				174	→	189	-0.19886
				174	→	191	-0.11146
				175	→	183	-0.13843
				175	→	186	0.21733
				175	→	189	0.13729
25	3.9336	315.19	0.0071	171	→	178	0.27575

				172	→	179	0.51177
				173	→	179	-0.14064
				175	→	180	-0.11415
				175	→	183	0.15885
				175	→	186	-0.20656
				175	→	189	-0.13095
26	3.9379	314.85	0.0579	174	→	181	0.49635
				174	→	182	-0.46272
27	4.0143	308.85	0.0025	175	→	183	0.62124
				175	→	186	0.19382
				175	→	189	0.12391
28	4.0268	307.9	0.0001	165	→	177	-0.10335
				166	→	176	0.134
				171	→	179	0.10948
				174	→	181	0.41348
				174	→	182	0.46101
				175	→	182	0.15349
29	4.0867	303.39	0.0002	168	→	176	-0.1321
				168	→	178	-0.15558
				174	→	181	0.10869
				175	→	184	0.61922
30	4.1069	301.89	0.004	167	→	178	-0.13729
				168	→	177	-0.12754
				168	→	179	-0.11498
				170	→	176	-0.12116
				174	→	183	-0.30427
				175	→	185	0.53023
31	4.1183	301.05	0.0036	170	→	177	0.10341
				171	→	179	0.63689
				173	→	180	0.19083
32	4.1537	298.49	0.0055	165	→	176	-0.13211
				166	→	177	0.14679
				174	→	183	0.5141
				174	→	185	0.10751
				175	→	183	0.13117
				175	→	185	0.32237
33	4.2076	294.67	0.0034	172	→	186	0.13022
				172	→	189	0.11364
				173	→	186	0.2654
				173	→	189	0.21077
				173	→	191	0.13192
				174	→	184	-0.11439
				174	→	193	-0.13383
				175	→	181	0.1861
				175	→	187	0.11952
				175	→	188	0.11844

					175	\rightarrow	190	-0.17481
					175	\rightarrow	193	0.33713
34	4.3017	288.22	0.0167		172	\rightarrow	181	0.22001
					172	\rightarrow	182	-0.12274
					173	\rightarrow	181	0.54102
					173	\rightarrow	182	-0.2699
					175	\rightarrow	186	0.13302
35	4.3154	287.31	0.0012		169	\rightarrow	176	-0.25953
					171	\rightarrow	179	-0.1773
					172	\rightarrow	180	0.18453
					173	\rightarrow	180	0.46577
					174	\rightarrow	184	-0.26211
36	4.3387	285.76	0.017		166	\rightarrow	176	0.12983
					168	\rightarrow	176	-0.114
					168	\rightarrow	178	-0.10036
					169	\rightarrow	176	-0.25793
					173	\rightarrow	180	0.1781
					174	\rightarrow	184	0.52247
					175	\rightarrow	184	-0.13207
37	4.3551	284.69	0.0266		169	\rightarrow	177	-0.11701
					170	\rightarrow	176	0.64123
					174	\rightarrow	183	-0.10575
					174	\rightarrow	185	-0.12926
					175	\rightarrow	185	0.11252
38	4.3847	282.77	0.0002		169	\rightarrow	176	0.41724
					170	\rightarrow	177	0.42387
					171	\rightarrow	179	-0.13404
					173	\rightarrow	180	0.24994
39	4.3873	282.6	0.0093		168	\rightarrow	177	-0.10429
					169	\rightarrow	177	0.23362
					170	\rightarrow	176	0.14591
					170	\rightarrow	178	-0.10884
					173	\rightarrow	182	-0.11699
					174	\rightarrow	183	-0.1083
					174	\rightarrow	185	0.5352
					175	\rightarrow	185	-0.15798
40	4.3925	282.26	0.0004		169	\rightarrow	176	-0.38261
					170	\rightarrow	177	0.52228
					173	\rightarrow	180	-0.15848

Table S20. TDDFT calculated transitions for C-S_a-mer-[Ru(DQPz)₂]²⁺.

Excited State	Energy (eV)	Wavelength (nm)	f	Transitions			
1	2.5609	484.14	0.0393	175	\rightarrow	176	0.70108
2	2.5837	479.86	0.0028	174	\rightarrow	179	-0.11643
				175	\rightarrow	177	0.65509
				175	\rightarrow	178	-0.20702

3	2.7008	459.06	0.0814	171	→	177	0.11345
				174	→	177	0.65404
				175	→	179	-0.20869
4	2.7277	454.53	0.0003	174	→	176	-0.36106
				174	→	179	-0.14567
				175	→	177	0.17741
				175	→	178	0.54913
5	2.7655	448.32	0.117	174	→	176	0.59438
				175	→	178	0.35087
6	2.8312	437.92	0.0363	174	→	177	0.15324
				174	→	178	-0.40905
				175	→	179	0.5303
7	2.8842	429.88	0.1108	174	→	177	0.12788
				174	→	178	0.53744
				175	→	179	0.39873
8	3.0739	403.34	0.0113	173	→	177	0.69483
9	3.1214	397.21	0	173	→	176	0.68615
				174	→	179	0.15186
10	3.278	378.23	0.0013	172	→	177	-0.12019
				173	→	176	-0.14694
				174	→	179	0.62677
				175	→	177	0.14715
				175	→	178	0.11292
11	3.2871	377.19	0.0191	173	→	178	0.68563
12	3.4129	363.28	0.0018	173	→	179	0.68405
13	3.5226	351.97	0.0838	171	→	176	0.16151
				172	→	177	0.66457
				174	→	179	0.10798
14	3.5272	351.51	0.3704	171	→	177	0.10032
				172	→	176	0.67968
15	3.6145	343.02	0.0287	175	→	180	0.66674
				175	→	182	-0.14316
16	3.677	337.19	0.0235	171	→	177	0.59372
				172	→	176	-0.11943
				174	→	177	-0.12471
				174	→	186	0.18581
				174	→	189	0.17113
17	3.6879	336.19	0.0199	171	→	176	0.62466
				172	→	177	-0.17644
				172	→	178	0.15368
				174	→	180	0.13918
18	3.7195	333.34	0	171	→	176	-0.21833
				172	→	178	0.61795
				174	→	180	0.17601
				175	→	181	-0.12546
19	3.7527	330.39	0.0043	174	→	180	0.47826

					174	\rightarrow	182	-0.1104
					175	\rightarrow	181	0.44025
					175	\rightarrow	183	-0.10886
					175	\rightarrow	186	-0.11434
20	3.7536	330.3	0.0336		171	\rightarrow	177	-0.32319
					171	\rightarrow	178	-0.26243
					171	\rightarrow	186	0.11958
					171	\rightarrow	189	0.11332
					174	\rightarrow	178	0.17036
					174	\rightarrow	186	0.33241
					174	\rightarrow	189	0.29786
					174	\rightarrow	191	0.12533
					174	\rightarrow	194	-0.12244
21	3.7786	328.12	0.0079		172	\rightarrow	178	0.25697
					174	\rightarrow	180	-0.35794
					175	\rightarrow	181	0.4924
					175	\rightarrow	186	0.10396
22	3.8649	320.8	0.0087		171	\rightarrow	178	-0.11081
					174	\rightarrow	181	-0.27195
					175	\rightarrow	180	0.16427
					175	\rightarrow	182	0.56122
					175	\rightarrow	192	-0.12977
23	3.9062	317.41	0.007		171	\rightarrow	178	0.49821
					172	\rightarrow	179	0.37929
					174	\rightarrow	186	0.14381
					174	\rightarrow	189	0.11175
					175	\rightarrow	182	0.16444
24	3.9193	316.34	0.0139		173	\rightarrow	179	-0.12229
					173	\rightarrow	180	0.10154
					173	\rightarrow	192	0.13071
					174	\rightarrow	180	0.2512
					175	\rightarrow	183	0.30123
					175	\rightarrow	186	0.39655
					175	\rightarrow	189	0.28302
					175	\rightarrow	191	0.1068
					175	\rightarrow	194	-0.10548
25	3.9215	316.17	0.0142		171	\rightarrow	178	0.18088
					172	\rightarrow	179	-0.42616
					174	\rightarrow	181	0.47747
					175	\rightarrow	182	0.1515
26	3.9334	315.21	0.0305		171	\rightarrow	178	-0.30329
					172	\rightarrow	179	0.37224
					174	\rightarrow	181	0.3881
					174	\rightarrow	183	-0.12594
					174	\rightarrow	186	-0.14559
					174	\rightarrow	189	-0.11244

				175	\rightarrow	182	0.18933
27	4.0155	308.76	0.0009	171	\rightarrow	179	-0.15409
				174	\rightarrow	182	-0.34593
				175	\rightarrow	183	0.48749
				175	\rightarrow	186	-0.19183
				175	\rightarrow	189	-0.1308
28	4.0546	305.79	0.0018	167	\rightarrow	178	0.10383
				168	\rightarrow	176	-0.12215
				174	\rightarrow	182	0.48221
				175	\rightarrow	183	0.33229
				175	\rightarrow	184	-0.23716
				175	\rightarrow	186	-0.12347
29	4.093	302.92	0.0005	171	\rightarrow	179	0.6114
				173	\rightarrow	180	0.13555
				174	\rightarrow	182	-0.19864
				175	\rightarrow	184	-0.15242
30	4.1084	301.78	0.0044	165	\rightarrow	176	-0.12391
				166	\rightarrow	177	-0.10234
				167	\rightarrow	179	0.10225
				168	\rightarrow	177	-0.11796
				170	\rightarrow	176	0.12175
				174	\rightarrow	183	0.44021
				174	\rightarrow	184	-0.12216
				175	\rightarrow	185	0.39914
31	4.1283	300.33	0.0025	167	\rightarrow	178	-0.10358
				168	\rightarrow	176	0.11051
				171	\rightarrow	179	0.19125
				173	\rightarrow	180	0.1446
				174	\rightarrow	182	0.18208
				174	\rightarrow	185	-0.1295
				175	\rightarrow	183	0.14875
				175	\rightarrow	184	0.5476
32	4.1519	298.62	0.0007	166	\rightarrow	177	0.10016
				167	\rightarrow	176	0.16207
				168	\rightarrow	178	-0.12622
				173	\rightarrow	186	0.10432
				174	\rightarrow	183	-0.38908
				174	\rightarrow	184	-0.22981
				175	\rightarrow	185	0.39
				175	\rightarrow	192	0.1231
33	4.2031	294.98	0.0043	173	\rightarrow	186	0.26134
				173	\rightarrow	189	0.23689
				174	\rightarrow	183	0.17519
				175	\rightarrow	182	0.21895
				175	\rightarrow	185	-0.22305
				175	\rightarrow	187	0.11251

				175	\rightarrow	188	0.11048
				175	\rightarrow	190	-0.12898
				175	\rightarrow	192	0.32446
				175	\rightarrow	193	-0.13902
34	4.2916	288.9	0.0091	167	\rightarrow	176	-0.13905
				168	\rightarrow	178	0.11351
				173	\rightarrow	186	0.10167
				174	\rightarrow	184	0.53708
				175	\rightarrow	182	0.10565
				175	\rightarrow	185	0.30154
35	4.2988	288.42	0.0006	166	\rightarrow	176	0.10314
				167	\rightarrow	177	0.10142
				167	\rightarrow	178	0.10324
				169	\rightarrow	176	0.14823
				173	\rightarrow	180	0.27717
				173	\rightarrow	182	-0.11723
				174	\rightarrow	185	0.488
				175	\rightarrow	184	0.1793
36	4.3202	286.99	0.0053	169	\rightarrow	176	0.23872
				171	\rightarrow	179	-0.12845
				173	\rightarrow	180	0.47684
				174	\rightarrow	185	-0.31384
				175	\rightarrow	184	-0.16851
37	4.3396	285.7	0.0233	173	\rightarrow	181	0.67619
38	4.3675	283.88	0.0265	169	\rightarrow	177	0.10588
				170	\rightarrow	176	0.65211
				174	\rightarrow	183	-0.11063
39	4.3785	283.17	0.0004	170	\rightarrow	177	0.66725
				171	\rightarrow	179	-0.12834
40	4.3872	282.61	0.0095	169	\rightarrow	177	0.6691
				170	\rightarrow	176	-0.12461