Electronic Supporting Information (ESI) Surfactin functionalized poly(methyl methacrylate) as eco-friendly nano-adsorbent: from size controlled scalable fabrication to adsorptive removal of inorganic and organic pollutants 4 Debasree Kundu^{a,‡}, Chinmay Hazra^{a,‡}, Aniruddha Chatterjee^{b,*}, Ambalal Chaudhari^a, 5 Satyendra Mishra^b, Amol Kharat^c and Kiran Kharat^d *^aSchool of Life Sciences, North Maharashtra University, Jalgaon, Maharashtra, India ^bUniversity Institute of Chemical Technology, North Maharashtra University, Jalgaon, Maharashtra, India ^cModern College of Pharmacy, Moshi, Pune, Maharashtra, India ^dDepartment of Biotechnology, Deogiri college, Aurangabad, Maharashtra, India* *Corresponding author. Present address: Maharashtra Institute of Technology, Aurangabad, 18 Maharashtra, India. E-mail: aniruddha chatterjee2006@yahoo.co.in; aniruddha.chatterjee@mit.asia

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2 **Fig. S1.** Overall chemical structure of surfactin lipopeptide.

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Determination of monomer conversion, solid content, molecular weights and polydispersity index (PDI)

The percentage of monomer conversion to polymer and latex yield was determined by gravimetric analysis. A small sample (5-10 ml) was taken and placed quickly into a capped vial containing several drops of hydroquinone inhibitor solution to stop the polymerization. The sample was then poured into a pre-weighed watch glass and weighed. It was then dried in an oven at 120 \degree C until constant weight. A final measurement of the watch glass + dry polymer sample was then made. For each set of operating conditions, experiments were repeated and the repeatability of measurements was within $\pm 10\%$, as indicated by error bars on the graphical plots.

The total number of latex particles in the system (*NP*) and the number of polymer chains per particle (*N*) as well as the conversion (X_m) are calculated according to the following equations:

$$
N_P = \frac{6\rho_0 V X_m}{\rho \pi D^3} \tag{1}
$$

$$
N = \frac{4}{3} \frac{\rho \pi (D/2)^3 N_A}{\overline{M}_n} \tag{2}
$$

$$
X_m\left(\%\right) = \frac{W_1}{W_2} \times 100\tag{3}
$$

where ρ_0 is the density of MMA (0.94 g cm⁻³ at 25 °C), *V* is the total volume of MMA, X_m is polymerization conversion, ρ is the density of PMMA (g cm⁻³ at 25 °C), D is the diameter of the particle, N_A is 6.02×10²³ mol⁻¹, M_n is the number-average molecular weight, and W_I and *W²* are the weights of the polymer and MMA, respectively.

Energy calculations

1. Energy delivered during conventional mechanically stirred emulsion polymerization method

Voltage input in magnetic stirrer = 230 V.

Current measured using digital multimeter (Model 801, Meco Instruments Pvt. Ltd., India) =

$$
37 \text{ mA} = 37 \times 10^{-3} \text{ A}.
$$

Power input in overhead stirrer = voltage input \times current measured = 230 (V) \times 37 \times 10⁻³ (A) $= 8.51$ W (J/s).

Time required for completion of reaction $= 1$ h (3600 s).

Net energy delivered during conventional method = power input in magnetic stirrer \times time required for completion of reaction = 8.51 J/s \times 3600 s = 30636 J = 30.636 kJ.

Energy supplied in form of heat to maintain reaction temperature 55 °C = mC_p , $_{mix}$ (T_{process} - T_{ref}) = 130.38 × 4.0058 × (55 - 25) = 15668.3 J = 15.67 kJ.

Total energy supplied during conventional method = $30.636 + 15.67 = 46.31$ kJ.

Quantity of material processed = quantity of [water + KPS + surfactin + MMA] = 100 ml +

 0.25 g + 0.025 g + 5 g = 105.28 g.

Net energy supplied for processing of material using conventional method $=$ net energy delivered during conventional method/quantity of material processed = 46.31 (kJ) / 105.28 $(g) = 43.98 \times 10^{-2}$ (kJ/g). (A)

2. Energy delivered during sonochemical polymerization

Energy delivered during sonication = energy required to synthesize nPMMA.

Electrical energy delivered during sonication (indicated by the power meter) = 53.5 kJ.

Efficiency of horn taken for the calculation $= 18.9\%$ (estimated independently using calorimetric studies).

Actual energy delivered by horn during sonication = energy delivered during sonication using horn \times efficiency of horn = 53.5 \times 18.9/100 = 10.11 kJ.

Quantity of material processed = quantity of $[water + KPS + surf (water + MMA] = 100$ ml + 0.25 g + 0.025 g + 5 g = 105.28 g.

Net energy supplied for processing of material using sonochemical method = actual energy delivered by horn during sonication/quantity of material processed = 10.11 (kJ) / 105.28 (g) = 9.60×10^{-2} (kJ/g). (B)

3. Energy saved

Net energy saved = [net energy supplied for processing of material using atomized microemulsion method (A)] - [net energy supplied for processing of material using sonochemical emulsion polymerization (B)] = 43.98×10^{-2} (kJ/g) - 9.60×10^{-2} (kJ/g) = 34.38 1024 J

$$
\times
$$
 10⁻² (kJ/g).

Calculation of cavitational yield

1. Conventional mechanically stirred emulsion polymerization

Rate of polymerization = 1.26 g l^{-1}

Power density $(J l^{-1})$ = supplied total electrical energy = 46.31 kJ = 46310 J l⁻¹

Cavitational yield = 1.26 (g l⁻¹) / 46310 (J l⁻¹) = 0.27 × 10⁻⁴ g J⁻¹

2. sonochemical polymerization

Rate of polymerization = 1.51 g l⁻¹

Power density $(J l^{-1})$ = supplied total electrical energy = 10.11 kJ = 10110 J l⁻¹

Cavitational yield = 1.51 (g l⁻¹) / 10110 (J l⁻¹) = 1.5 × 10⁻⁴ g J⁻¹

Fig. S2. Effect of surfactin concentration (wt. % of MMA) on morphology and size of nPMMASP particles: (a) 1%, (b) 2%, (c) 3% and (d) 4%. Other conditions are same as Fig. 1.

Fig. S3. The pH dependence of zeta-potential of nPMMA_{SP} and nPMMA_{CP} particles. (Reaction conditions: nPMMA_{SP}: monomer-to-water 20 wt.%; monomer-to-initiator 0.4 wt.%; surfactin 4 wt.%, calculated vs monomer; temperature, 55 ± 2 °C; time, 1 h; nPMMA_{CP}: monomer-to-water 20 wt.%; monomer-to-initiator 0.4 wt.%; surfactin 4 wt.%, calculated vs monomer; temperature, 55 ± 2 °C; agitation, 250 rpm; time, 1 h).

Fig. S4. XRD patterns of (a) nPMMA_{SP}, (b) nPMMA_{CP} and (c) bulk PMMA.

The diffraction peak observed at 15.10° was assigned to the amorphous phase of PMMA. This peak was more prominent in nPMMA_{SP}. It suggested the crystalline nature of nPMMA_{SP} was more than nPMMA_{CP} and bulk PMMA.

Fig. S5. DSC curves of (a) nPMMA_{SP} and (b) nPMMA_{CP} and (c) bulk PMMA.

It was observed that first scan of nPMMA_{SP} showed two step exothermic peaks at 128 and 135 °C that were attributed to T_{g1} along with respective peaks of T_m arising due to the presence of little amount of surfactin (Fig. S5a). This finding corroborated with the thin shell layer of biosurfactants observed in TEM. The lower value of T_{g1} (Fig. S5b) for nPMMA_{CP} (116 \degree C) was due to its relatively large size and lower surface area as compared to nPMMASP. Moreover, the peak for surfactin shell could not be detected due to poor grafting of surfactin onto nPMMA in case of nPMMA_{CP}. Bulk PMMA showed regular T_g at 108 °C like commercial grade PMMA (Fig. S5c). The reason for high T_g of polymer nanoparticles than bulk PMMA might be a decrease in particle size to nano-scale that results in an increase in surface area and higher surface energy.

Fig. S6. TGA thermogram of (a) nPMMA_{SP} and (b) nPMMA_{CP} and (c) bulk PMMA.

A remarkable change in thermal behaviour between $nPMMA_{SP}$, $nPMMA_{CP}$ and bulk PMMA was observed. The nPMMA_{SP} showed higher thermal stability $[d_{on} = 372 \text{ °C}$ and $d_{off} = 415 \text{ °C}$ with % weight loss (W_L) = 100%] than nPMMA_{CP} [d_{on} = 352 °C and d_{off} = 406 °C with % weight loss (W_L) = 100%] and bulk PMMA $[d_{on} = 282 \degree C$ and $d_{off} = 356 \degree C$ with 100% W_L]. Thus, the thermal stability pattern followed the order: $nPMMA_{SP} > nPMMA_{CP} > \text{bulk}$ PMMA.

Fig. S7. Plot of the adsorption capacities against the covalent indices.

Table S1. ICP-AES instrumental operating parameters used for the determination of potentially toxic metals binding to nano-adsorbents used in this study.

*: the time when the colour of the microemulsion turns blue

Table S2. Effect of monomer-to-initiator weight ratios on particle size, PDI, conversion, *N^P* and *N* of the particles. Conditions are as in Fig. 1.

Table S3. Effect of MMA concentration on particle size, PDI, conversion, *N^P* and *N* of the particles. Other conditions are same as Fig. 1.

Table S4. Effect of acoustic amplitude on particle size, PDI, conversion, N_P and N of nPMMA_{SP} particles.

Run	Wt. % biosurfactant (of MMA)	Particle size (nm)		Polydispersity index	$N_p \times 10^{18}$	\boldsymbol{N}
		DLS	TEM			
Sonochemical emulsion polymerization						
	1.0	120.077	85.027	0.704	5.544	14
$\overline{2}$	2.0	90.022	67.512	0.632	6.751	14
3	3.0	110.037	82.044	0.734	6.613	13
4	4.0	85.054	60.036	0.572	7.577	14
Conventional polymerization (with mechanical stirring)						
	1.0	120.022	85.082	0.791	6.233	17
$\overline{2}$	2.0	90.016	67.555	0.651	7.264	15
$\overline{3}$	3.0	110.052	82.023	0.762	7.172	18
4	4.0	85.073	70.516	0.513	6.735	14

Table S5. Effect of surfactin concentration on particle size, PDI, conversion, *N^P* and *N* of the particles. Other conditions are same as Fig. 1.

Table S6. Kinetic model parameters and error function data for the metal ions sorption onto nPMMA_{SP} particles.

Table S7. Isotherm parameters and error deviation data for the adsorption of Co^{2+} , Zn^{2+} , Ni²⁺ and Cr^{3+} onto nPMMA_{SP}.

Table S8. Parametric sensitivity of the model parameters for Co^{2+} .

Table **S9.** Thermodynamic parameters for the metal ions sorption onto nPMMA_{SP}.