

## **Efficient Non-catalytic Oxidative and Extractive Desulfurization of Liquid Fuels using Ionic Liquids**

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*Supplementary Information*

## Kinetic studies

**Table S1: Kinetic parameters of fitted data (DBT)**

Temp., °C	$k_1$ (DBT), g/(mol s)	$R^2$	$k_2$ (DBT) $\times 10^{-7}$ , g <sup>2</sup> /(mol s) <sup>2</sup>	$R^2$
30.0	71.6	0.9988	1.4	0.9724
37.5	102.5	0.9993	2.0	0.9832
40.0	182.8	0.9976	4.2	0.9872

$k_1$ : second order rate constant.  $k_2$ : third order rate constant.

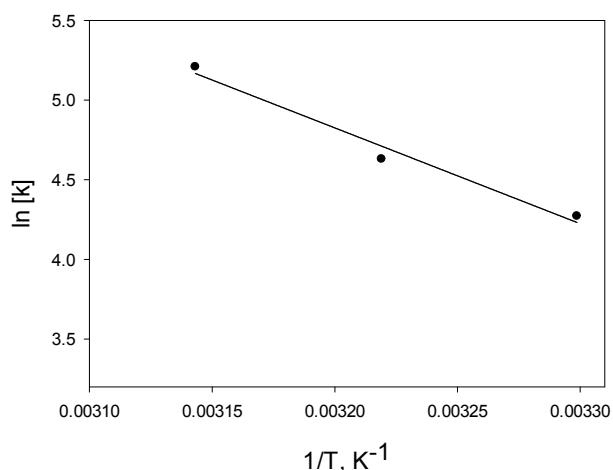


Figure S1: Arrhenius plot for DBT second order kinetic model

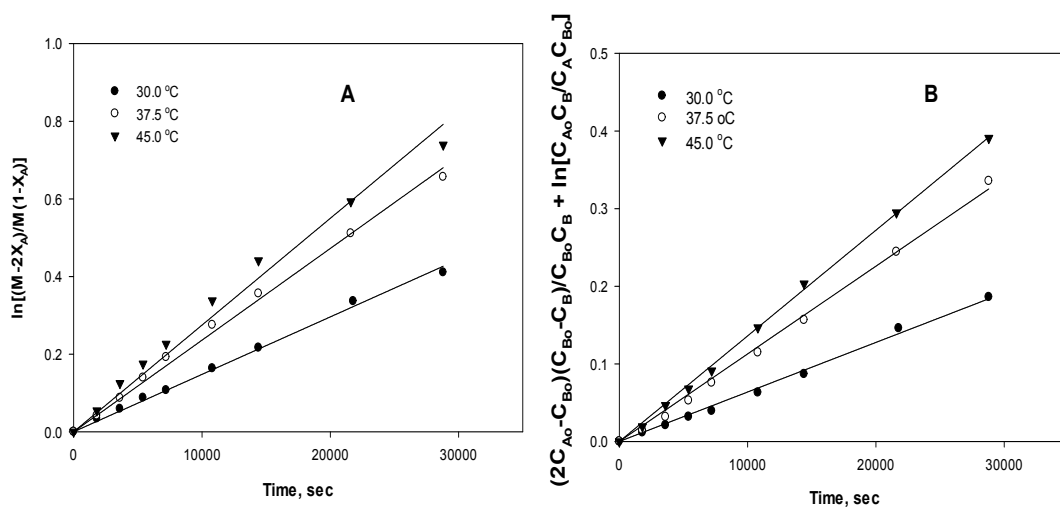
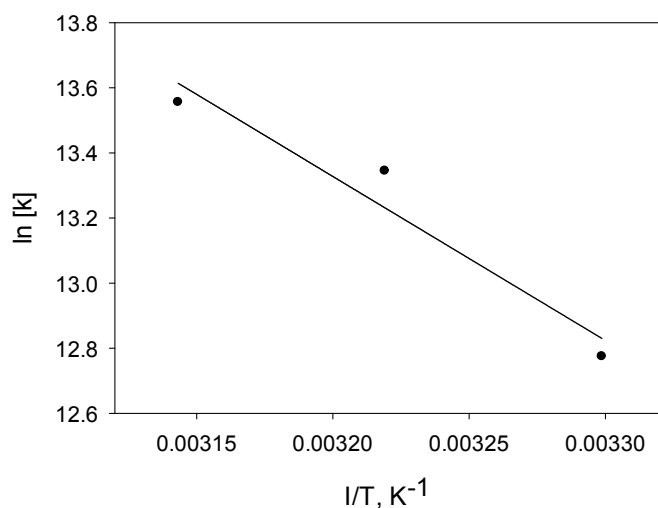


Figure S2: A- The plot of  $\ln [(M-2X_A)/(M(1-X_A))]$  versus time at different temperature (Bimolecular),  $M=3$ . B- The plot of  $(2C_{A0}-C_{B0})(C_{B0}-C_B)/(C_{B0} C_B) + \ln[C_{A0} C_B]/C_A C_{B0}$  against time at different temperature (Trimolecular) for BT.

Table S2: Kinetic parameters of fitted data (BT)

Temp., °C	$k_1$ (BT), g/(mol s)	$R^2$	$k_2$ (BT) $\times 10^{-5}$ , g <sup>2</sup> /(mol s) <sup>2</sup>	$R^2$
30.0	3.5	0.9960	3.5	0.9948
37.5	5.6	0.9952	6.2	0.9960
40.0	6.5	0.9825	7.7	0.9989

$k_1$ : second order rate constant.  $k_2$ : third order rate constant.



**Figure S3: Arrhenius plot for BT second order kinetic model**

$$r_{BT} = k_{BT} C_{BT} C_{mCPBA}^2 \quad k_{BT} = 6.21 \times 10^{12} e^{-41905/RT}$$

**S1**

### **Preliminary extractive and oxidative desulfurization experiment ([P<sub>i444,1</sub>][Tos])**

The comparison between the EDS and EODS as function of reaction time using the [P<sub>i444,1</sub>][Tos] (Figure S4) shows an improvement upon addition of an oxidation step for both %SR (BT) and %SR (DBT). For BT after 120 min of EODS experiment, SR increased from 57% to 60%. The corresponding increase for DBT was 59% to 76%.

Figure S5 shows the comparison between EDS and EODS as functions of temperature. It can be seen that although the %SR (BT) in EODS increases with reaction temperature, the improvement was not as desired, going from 54% to 68% at 80 °C and from 53% to 64% at 60 °C. For DBT, the increase was from 62% to 98% at 80 °C and 62% to 90% at 60 °C.

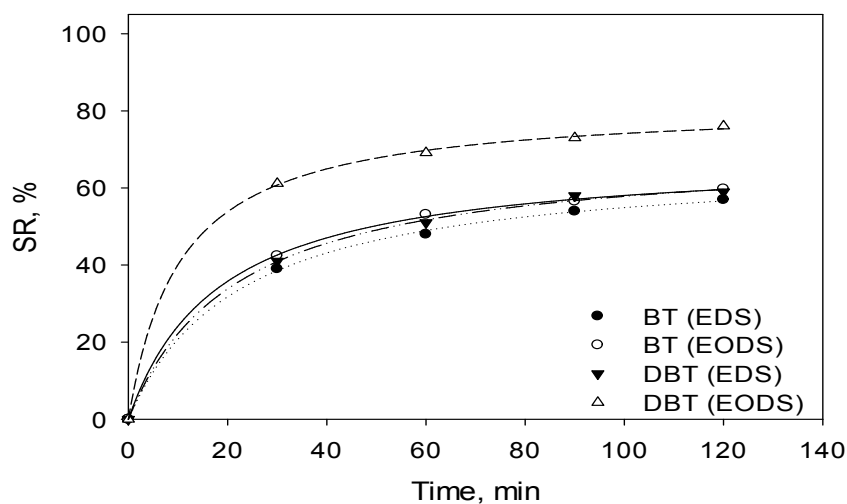


Figure S4: Comparison between EDS and EODS as a function of time using  $[P_{i444,1}][Tos]$  at 30 °C, 600 rpm

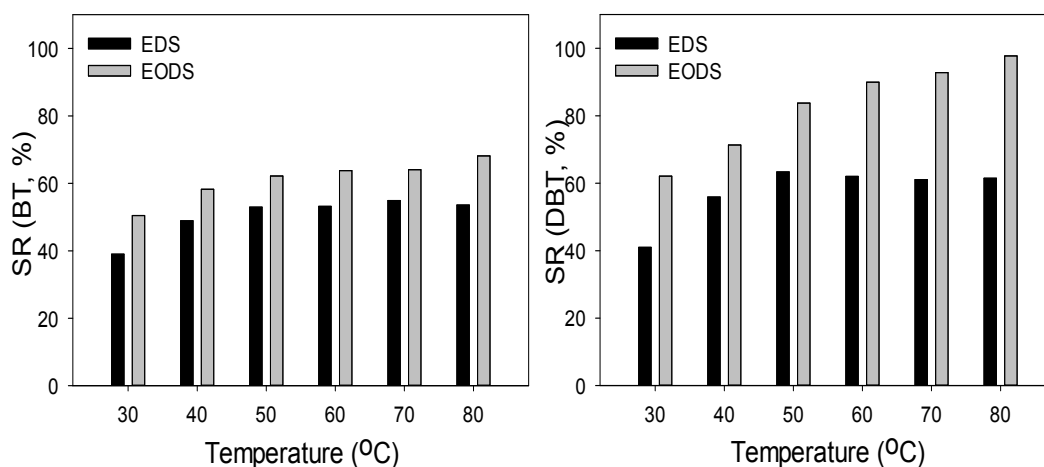


Figure S5: Comparison between EDS and EODS as a function of temperature using  $[P_{i444,1}][Tos]$  at 30 min, 600 rpm

### Optimization of the EODS of simulated fuel using $[P_{i444,1}][Tos]$

Table S3 and Table S4 show the design matrix for the EODS of BT and DBT, respectively, using  $[P_{i444,1}][Tos]$ . This resulted in 30 experimental runs, responses of which were fitted to a quadratic model. Table S5 shows the ANOVA of the EODS of BT using the  $[P_{i444,1}][Tos]$  IL. The model was found to be significant with an F value of 45.3 and p-value of < 0.01%. All independent

variables possess significant effect on the efficiency of the process. Furthermore, the mass fraction is the most significant term (F value  $\approx 180$ ).

Reaction temperature is the next most significant variable (F value  $\approx 61$ ) followed by reaction time (F value  $\approx 55$ ) and O/S (F value  $\approx 7$ ). Other significant terms include time-O/S, temperature-mass fraction and temperature-O/S. No second order term is significant and as result the model was reduced to two factor interaction (2FI) model. The model, adjusted and predicted  $R^2$  were found to be 0.9411, 0.9199 and 0.7881 respectively. The plot of predicted response (SR) against the experimental response is shown in Figure S6.

Table S6 present the ANOVA of the EODS of DBT using  $[P_{i444,1}][Tos]$  IL. Similarly the model is significant with F value of  $\sim 63$  and p-value of  $<0.01\%$ . All the independent variables are significant model terms with reaction temperature being the most significant with F value of  $\sim 310$  followed by reaction time with an F value of  $\sim 208$ . All interaction terms are significant with the exception of time-O/S and temperature-O/S. The second order terms of all the independent variables are significant with the exception of mass fraction. The model  $R^2$  was calculated as 0.9793 while the adjusted and predicted  $R^2$  were found to be 0.9619 and 0.9073 respectively.

**Table S3: Experimental design matrix for EODS of BT using [P<sub>i444,1</sub>][Tos]**

Run	Coded Values				Actual Values				%SR	
	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	X <sub>4</sub>	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	X <sub>4</sub>	Y <sub>exp</sub>	R*
1	0	0	0	0	47.5	45	0.67	6	53.01	4.88
2	1	-1	-1	-1	80.0	30	0.50	3	63.16	1.70
3	-1	-1	-1	1	15.0	30	0.50	9	46.81	0.11
4	-1	1	1	1	15.0	60	0.83	9	30.38	-10.14
5	1	1	-1	1	80.0	60	0.50	9	78.62	-3.51
6	-1	-1	1	-1	15.0	30	0.83	3	20.91	1.86
7	1	1	1	-1	80.0	60	0.83	3	48.50	3.51
8	-1	1	-1	-1	15.0	60	0.50	3	58.41	1.94
9	1	-1	1	1	80.0	30	0.83	9	29.04	-5.05
10	0	0	0	0	47.5	45	0.67	6	52.83	4.69
11	1	1	-1	-1	80.0	60	0.50	3	62.38	-4.31
12	0	0	0	0	47.5	45	0.67	6	49.19	1.83
13	-1	-1	-1	-1	15.0	30	0.50	3	45.50	-4.19
14	-1	1	-1	1	15.0	60	0.50	9	65.71	3.50
15	1	-1	1	-1	80.0	30	0.83	3	25.81	-3.13
16	1	-1	-1	1	80.0	30	0.50	9	63.85	-1.22
17	-1	1	1	-1	15.0	60	0.83	3	29.53	-3.69
18	1	1	1	1	80.0	60	0.83	9	66.06	7.18
19	-1	-1	1	1	15.0	30	0.83	9	16.15	1.97
20	0	0	0	0	47.5	45	0.67	6	49.40	2.05
21	0	0	1	0	47.5	45	0.83	6	37.63	1.01
22	0	0	0	0	47.5	45	0.67	6	49.30	-0.88
23	0	-1	0	0	47.5	30	0.67	6	45.34	3.06
24	0	0	0	0	47.5	45	0.67	6	49.87	-0.31
25	1	0	0	0	80.0	45	0.67	6	54.95	-2.76
26	0	1	0	0	47.5	60	0.67	6	58.69	0.62
27	0	0	0	-1	47.5	45	0.67	3	47.45	1.12
28	0	0	-1	0	47.5	45	0.50	6	63.24	-0.50
29	0	0	0	1	47.5	45	0.67	9	52.93	-0.27
30	-1	0	0	0	15.0	45	0.67	6	43.80	1.15

\*R-residual,  $R = Y_{exp} - Y_{pred}$

**Table S4: Experimental design matrix for EODS of DBT using [P<sub>i444,1</sub>][Tos]**

Run	Coded Values				Actual Values				%SR	
	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	X <sub>4</sub>	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	X <sub>4</sub>	Y <sub>exp</sub>	R
1	0	0	0	0	47.5	45	0.67	6	87.60	0.78
2	1	-1	-1	-1	80.0	30	0.50	3	78.68	4.87
3	-1	-1	-1	1	15.0	30	0.50	9	60.29	-2.17
4	-1	1	1	1	15.0	60	0.83	9	71.79	-2.15
5	1	1	-1	1	80.0	60	0.50	9	100.00	-1.49
6	-1	-1	1	-1	15.0	30	0.83	3	35.11	2.76
7	1	1	1	-1	80.0	60	0.83	3	95.43	0.20
8	-1	1	-1	-1	15.0	60	0.50	3	74.52	-1.52
9	1	-1	1	1	80.0	30	0.83	9	64.10	-1.98
10	0	0	0	0	47.5	45	0.67	6	87.51	0.69
11	1	1	-1	-1	80.0	60	0.50	3	90.15	0.55
12	0	0	0	0	47.5	45	0.67	6	87.99	0.36
13	-1	-1	-1	-1	15.0	30	0.50	3	50.80	0.23
14	-1	1	-1	1	15.0	60	0.50	9	95.28	5.75
15	1	-1	1	-1	80.0	30	0.83	3	62.92	-2.50
16	1	-1	-1	1	80.0	30	0.50	9	85.99	-1.31
17	-1	1	1	-1	15.0	60	0.83	3	71.69	-1.59
18	1	1	1	1	80.0	60	0.83	9	99.08	1.57
19	-1	-1	1	1	15.0	30	0.83	9	30.93	-1.90
20	0	0	0	0	47.5	45	0.67	6	86.46	-1.16
21	0	0	1	0	47.5	45	0.83	6	88.05	4.69
22	0	0	0	0	47.5	45	0.67	6	88.10	-1.26
23	0	-1	0	0	47.5	30	0.67	6	72.98	2.10
24	0	0	0	0	47.5	45	0.67	6	89.40	0.04
25	1	0	0	0	80.0	45	0.67	6	94.93	0.11
26	0	1	0	0	47.5	60	0.67	6	98.00	-1.33
27	0	0	0	-1	47.5	45	0.67	3	78.95	-3.00
28	0	0	-1	0	47.5	45	0.50	6	89.55	-5.81
29	0	0	0	1	47.5	45	0.67	9	93.05	3.67
30	-1	0	0	0	15.0	45	0.67	6	72.31	0.89

R-residual,  $Y_{\text{pred}} = Y_{\text{exp}} - R$



**Table S5: ANOVA table for EODS of BT using [P<sub>i444,1</sub>][Tos]**

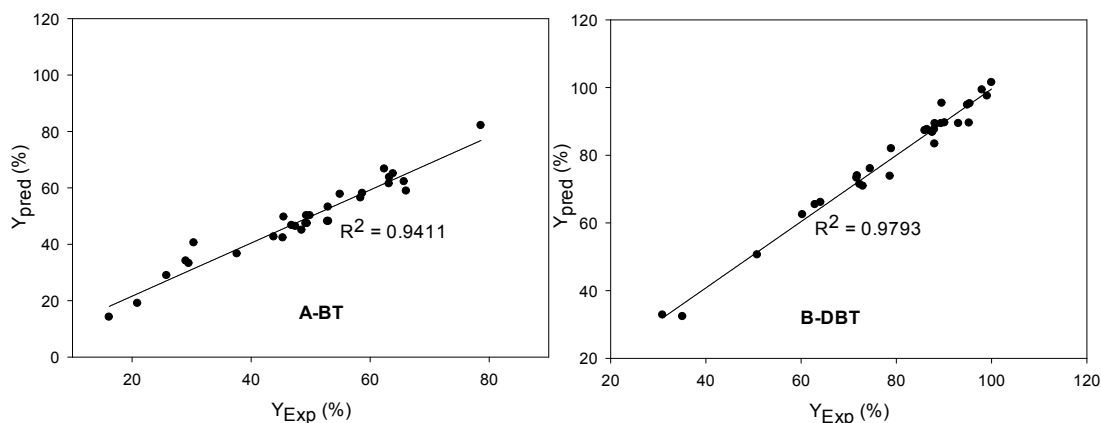
Source	SS <sup>b</sup>	DF <sup>b</sup>	MS <sup>b</sup>	F <sup>b</sup> Value	p-value Prob > F
Block	43.19	2	21.59		
Model	5824.35	7	832.05	45.32	< 0.0001
X <sub>1</sub>	1015.20	1	1015.2	55.29	< 0.0001
X <sub>2</sub>	1121.03	1	1121.03	61.06	< 0.0001
X <sub>3</sub>	3307.59	1	3307.59	180.15	< 0.0001
X <sub>4</sub>	133.73	1	133.73	7.28	0.0138
X <sub>1</sub> X <sub>4</sub>	65.72	1	65.72	3.58	0.0731
X <sub>2</sub> X <sub>3</sub>	85.98	1	85.98	4.68	0.0427
X <sub>2</sub> X <sub>4</sub>	105.76	1	105.76	5.76	0.0262
Residual	367.21	20	18.36		
Lack of Fit	367.01	17	21.59	314.57	0.0003
Pure Error	0.2059	3	0.0686		
Cor Total	6234.75	29			

<sup>a</sup>R<sup>2</sup> = 94.11%, R<sup>2</sup>(adj) = 91.99%, R<sup>2</sup>(pred)=78.81%. <sup>b</sup>SS: Sum of square, DF: Degree of freedom of different source, MS: Mean of square, F: Degree of freedom, P: Probability

**Table S6: ANOVA table for the EODS of DBT using [P<sub>i444,1</sub>][Tos]**

Source	SS <sup>b</sup>	DF <sup>b</sup>	MS <sup>b</sup>	F <sup>b</sup> Value	p-value Prob > F
Block	766.20	2	383.10		
Model	8145.41	11	740.49	63.03	< 0.0001
X <sub>1</sub>	2448.18	1	2448.18	208.38	< 0.0001
X <sub>2</sub>	3641.34	1	3641.34	309.93	< 0.0001
X <sub>3</sub>	647.24	1	647.24	55.09	< 0.0001
X <sub>4</sub>	225.36	1	225.36	19.18	0.0005
X <sub>1</sub> X <sub>2</sub>	126.46	1	126.46	10.76	0.0047
X <sub>1</sub> X <sub>3</sub>	99.44	1	99.44	8.46	0.0102
X <sub>2</sub> X <sub>3</sub>	244.35	1	244.35	20.80	0.0003
X <sub>3</sub> X <sub>4</sub>	125.83	1	125.83	10.71	0.0048
X <sub>1</sub> <sup>2</sup>	106.23	1	106.23	9.04	0.0084
X <sub>2</sub> <sup>2</sup>	49.68	1	49.68	4.23	0.0564
X <sub>4</sub> <sup>2</sup>	41.15	1	41.15	3.50	0.0797
Residual	187.98	16	11.75		
Lack of Fit	185.97	13	14.31	21.32	0.0141
Pure Error	2.01	3	0.6709		
Cor Total	9099.59	29			

<sup>a</sup>R<sup>2</sup> = 97.93%, R<sup>2</sup>(adj) = 96.19%, R<sup>2</sup>(pred)=90.73%. <sup>b</sup>SS: Sum of square, DF: Degree of freedom of different source, MS: Mean of square, F: Degree of freedom, P: Probability



**Figure S6: A plot of predicted response against experimental response for EODS of A-BT and B-DBT using  $[P_{i444,1}][Tos]$**

### **Optimization of the EODS of simulated fuel using $[P_{i444,1}][Tos]$**

Table S7 presents the experimental design matrix for the OEDS of BT using the  $[P_{i444,1}][Tos]$  IL. Thirty experimental runs were carried out and the responses were fitted to a quadratic model. Table S8 shows the ANOVA of the EODS of BT using the  $[P_{i444,1}][Tos]$  IL. The model was found to be significant with an F-value of  $\sim 83$  and p-value of  $< 0.01\%$ . All independent variables possess significant effect on the efficiency of the process. Furthermore, temperature is the most significant variable (F value  $\approx 267$ ). Interestingly, mass fraction is the least significant with F value of  $\sim 19$ . According to the assumption made earlier, this means the %SR is no longer limited significantly by mass transfer and therefore a high %SR as compared to EODS strategy should be expected. Other significant terms include time-temperature, mass fraction-O/S and the second order term of time. The model, adjusted and predicted  $R^2$  were found to be 0.9678, 0.9552 and 0.9102 respectively. Finally, Figure S7 shows a plot of the experimental response against the predicted response for this experiment.

**Table S7: Experimental design matrix for OEDS of BT using [P<sub>i444,1</sub>][Tos]**

Run	Coded Values				Actual Values				%SR	
	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	X <sub>4</sub>	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	X <sub>4</sub>	Y <sub>exp</sub>	R*
1	0	0	0	0	48.0	45	0.67	6	34.52	-5.23
2	1	-1	-1	-1	81.0	30	0.50	3	73.38	-3.10
3	-1	-1	-1	1	15.0	30	0.50	9	97.41	-3.71
4	-1	1	1	1	15.0	60	0.83	9	56.90	0.28
5	1	1	-1	1	81.0	60	0.50	9	72.98	2.22
6	-1	-1	1	-1	15.0	30	0.83	3	71.74	0.37
7	1	1	1	-1	81.0	60	0.83	3	15.04	5.66
8	-1	1	-1	-1	15.0	60	0.50	3	73.10	1.74
9	1	-1	1	1	81.0	30	0.83	9	65.40	0.81
10	0	0	0	0	48.0	45	0.67	6	69.46	0.95
11	1	1	-1	-1	81.0	60	0.50	3	85.96	-0.07
12	0	0	0	0	48.0	45	0.67	6	97.10	-0.82
13	-1	-1	-1	-1	15.0	30	0.50	3	48.65	-1.62
14	-1	1	-1	1	15.0	60	0.50	9	33.98	-2.57
15	1	-1	1	-1	81.0	30	0.83	3	84.32	3.68
16	1	-1	-1	1	81.0	30	0.50	9	25.18	0.52
17	-1	1	1	-1	15.0	60	0.83	3	76.75	4.92
18	1	1	1	1	81.0	60	0.83	9	72.78	0.94
19	-1	-1	1	1	15.0	30	0.83	9	78.07	5.41
20	0	0	0	0	48.0	45	0.67	6	31.91	-10.40
21	0	0	1	0	48.0	45	0.83	6	73.79	1.01
22	0	0	0	0	48.0	45	0.67	6	59.14	-3.08
23	0	-1	0	0	48.0	30	0.67	6	81.79	6.12
24	0	0	0	0	48.0	45	0.67	6	70.44	-6.96
25	1	0	0	0	81.0	45	0.67	6	71.52	-1.25
26	0	1	0	0	48.0	60	0.67	6	55.92	0.48
27	0	0	0	-1	48.0	45	0.67	3	83.05	-0.29
28	0	0	-1	0	48.0	45	0.50	6	50.81	1.84
29	0	0	0	1	48.0	45	0.67	9	72.57	4.41
30	-1	0	0	0	15.0	45	0.67	6	87.81	-2.30

\*R-residual,  $R = Y_{exp} - Y_{pred}$

Source	SS <sup>b</sup>	DF <sup>b</sup>	MS <sup>b</sup>	F <sup>b</sup> Value	p-value	Prob > F
Block	371.29	2	185.64			
Model	11790.28	7	1684.33	83.20		< 0.0001
X <sub>1</sub>	3208.02	1	3208.02	158.46		< 0.0001
X <sub>2</sub>	5409.23	1	5409.24	267.19		< 0.0001
X <sub>3</sub>	383.79	1	383.79	18.96		0.0003
X <sub>4</sub>	2008.62	1	2008.62	99.22		< 0.0001
X <sub>1</sub> X <sub>2</sub>	131.78	1	131.78	6.51		0.0190
X <sub>3</sub> X <sub>4</sub>	123.53	1	123.53	6.10		0.0226
X <sub>1</sub> <sup>2</sup>	525.30	1	525.30	25.95		< 0.0001
Residual	404.90	20	20.24			
Lack of Fit	393.49	17	23.15	6.09		0.0810
Pure Error	11.40	3	3.80			
Cor Total	12566.47	29				

<sup>a</sup>R<sup>2</sup> = 96.78%, R<sup>2</sup>(adj) = 95.52%, R<sup>2</sup>(pred) = 91.02%. <sup>b</sup>SS: Sum of square, DF: Degree of freedom of different source, MS: Mean of square, F: Degree of freedom, P: Probability

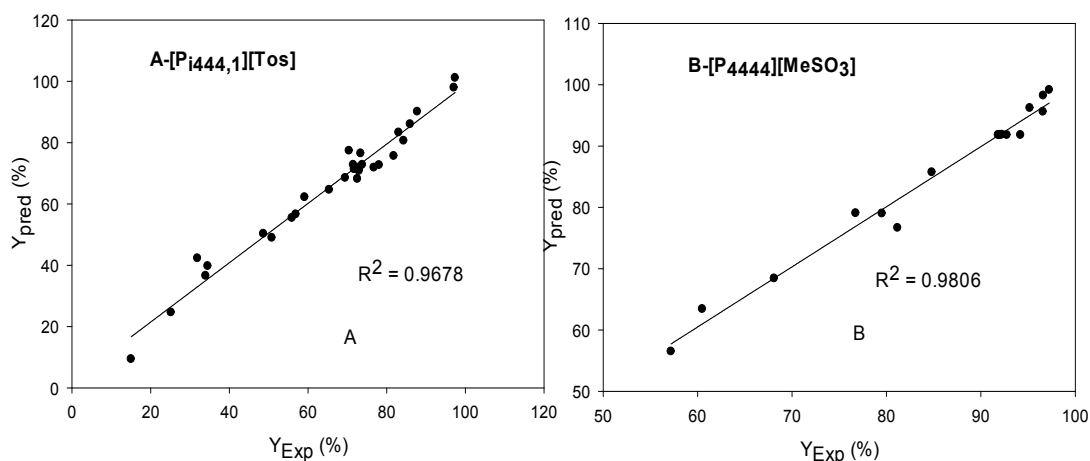


Figure S7: A plot of predicted response against experimental response for EODS of A-[P<sub>i444,1</sub>][Tos], B-[P<sub>4444</sub>][MeSO<sub>3</sub>]

### Optimization of the EODS of simulated fuel using [P<sub>4444</sub>][MeSO<sub>3</sub>]

The ANOVA table of the OEDS of BT using [P<sub>4444</sub>][MeSO<sub>3</sub>] is presented as Table S10. The model is significant with F value of ~65. All the independent variables considered are significant with time as the most significant (F value of ~178) and mass fraction as by far the least significant

factor (F value  $\approx$  33). Time-mass fraction and mass fraction-O/S are the only significant interaction terms. Second order terms of time and O/S are also significant. The model, adjusted and predicted  $R^2$  were determined as 0.9806, 0.9654 and 0.8924 respectively.

**Table S9: Experimental design matrix for the OEDS of BT using the [P<sub>4444</sub>][MeSO<sub>3</sub>] IL**

Run	Coded values			Actual values			%SR	
	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	Y <sub>exp</sub>	R
1	1	-1	0	81	0.50	6	96.59	1.00
2	0	0	0	48	0.67	6	94.20	2.40
3	-1	0	1	15	0.67	9	81.19	4.54
4	0	-1	1	48	0.5	9	96.61	-1.63
5	0	0	0	48	0.67	6	92.05	0.26
6	0	1	1	48	0.83	9	95.19	-1.01
7	-1	-1	0	15	0.50	6	76.75	-2.30
8	-1	0	-1	15	0.67	3	57.19	0.68
9	0	-1	-1	48	0.50	3	84.81	-0.92
10	1	1	0	81	0.83	6	92.23	0.37
11	-1	1	0	15	0.83	6	60.50	-2.92
12	1	0	-1	81	0.67	3	79.53	0.53
13	0	0	0	48	0.67	6	91.84	0.04
14	1	0	1	81	0.67	9	97.25	-1.90
15	0	0	0	48	0.67	6	92.76	0.96
16	0	0	0	48	0.67	6	92.00	0.20
17	0	1	-1	48	0.83	3	68.11	-0.30

R-residual,  $Y_{pred} = Y_{exp} - R$

**Table S10: ANOVA for the OEDS of BT using the [P<sub>4444</sub>][MeSO<sub>3</sub>]**

Source	SS <sup>b</sup>	DF <sup>b</sup>	MS <sup>b</sup>	F <sup>b</sup> Value	p-value Prob > F
Model	2584.58	7	369.23	64.80	< 0.0001
X <sub>1</sub>	1011.57	1	1011.57	177.52	< 0.0001
X <sub>3</sub>	187.45	1	187.45	32.90	0.0003
X <sub>4</sub>	812.02	1	812.02	142.50	< 0.0001
X <sub>1</sub> X <sub>3</sub>	35.37	1	35.37	6.21	0.0343
X <sub>3</sub> X <sub>4</sub>	58.35	1	58.35	10.24	0.0108
X <sub>1</sub> <sup>2</sup>	366.55	1	366.55	64.33	< 0.0001
X <sub>4</sub> <sup>2</sup>	91.44	1	91.44	16.05	0.0031
Residual	51.28	9	5.70		
Lack of Fit	47.47	5	9.49	9.96	0.0224
Pure Error	3.81	4	0.95		
Cor Total	2635.86	16			

<sup>a</sup> $R^2 = 98.06\%$ ,  $R^2(\text{adj}) = 96.54\%$ ,  $R^2(\text{pred})=89.24\%$ . <sup>b</sup>SS: Sum of square, DF: Degree of freedom of different source, MS: Mean of square, F: Degree of freedom, P: Probability

**Table S11: Coefficients of the fitted quadratic model for the EODS/OEDS sulfur compounds using the respective ILs**

	$[P_{i444,1}]$ [Tos] EODS		$[P_{i444,1}]$ [Tos] OEDS	$[P_{4444}]$ [MeSO <sub>3</sub> ] OEDS
	BT	DBT	BT	BT
		48.56	87.93	71.99
X <sub>1</sub>	7.54	11.70	13.35	11.24
X <sub>2</sub>	7.89	14.23	17.34	
X <sub>3</sub>	-13.56	-6.00	-4.62	-4.84
X <sub>4</sub>	2.73	3.54	10.56	10.07
X <sub>1</sub> X <sub>2</sub>		-2.82	-2.87	
X <sub>1</sub> X <sub>3</sub>		2.50		2.97
X <sub>1</sub> X <sub>4</sub>	2.03			
X <sub>2</sub> X <sub>3</sub>	2.32	3.91		
X <sub>2</sub> X <sub>4</sub>	2.57			
X <sub>3</sub> X <sub>4</sub>		-2.80	2.78	3.82
X <sub>1</sub> <sup>2</sup>		-6.24	-10.46	-9.32
X <sub>2</sub> <sup>2</sup>		-4.26		
X <sub>3</sub> <sup>2</sup>				
X <sub>4</sub> <sup>2</sup>		-3.87		-4.65

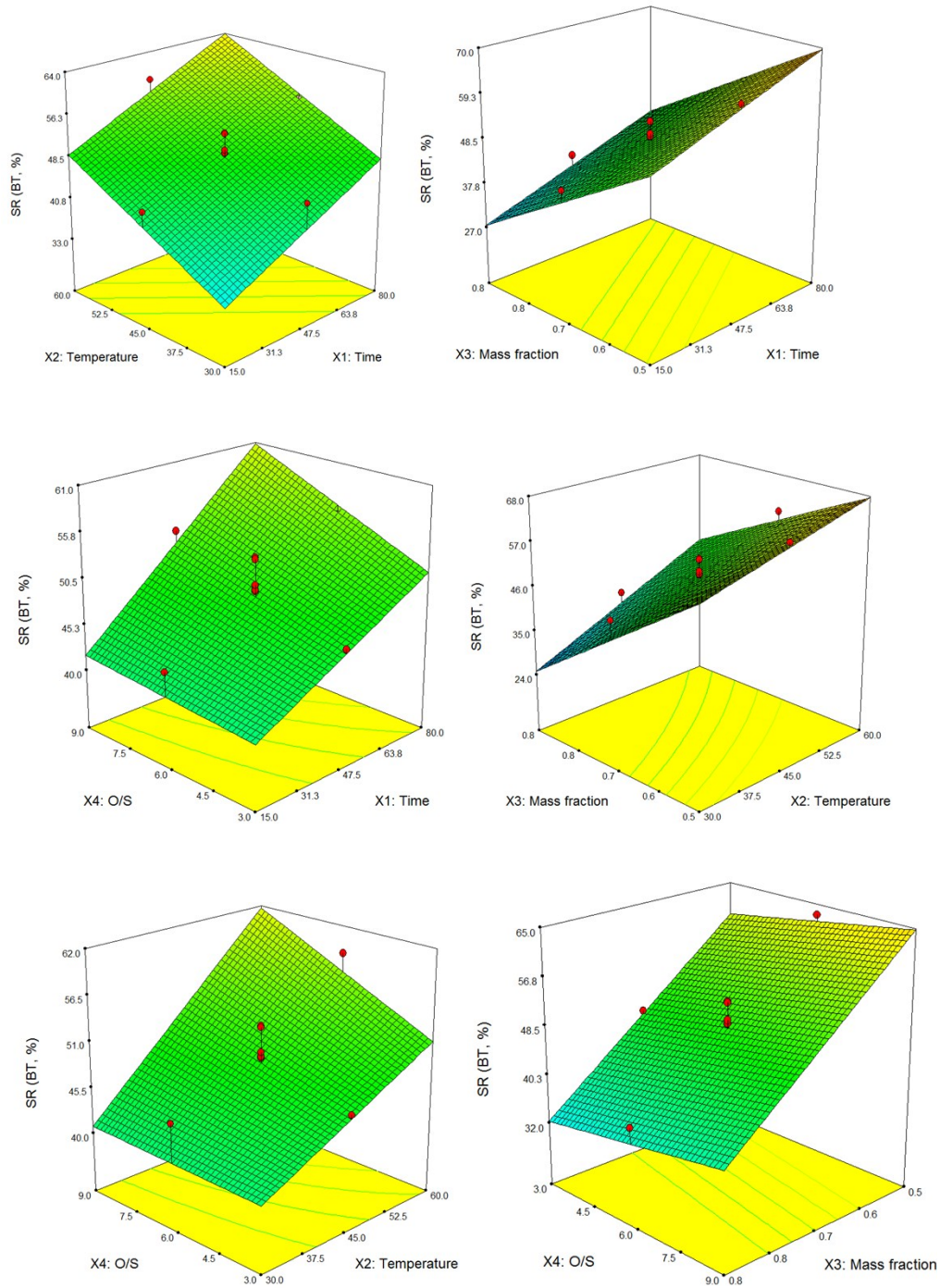


Figure S8: 3D plots for the EODS of BT using the  $[P_{i444,1}][Tos]$

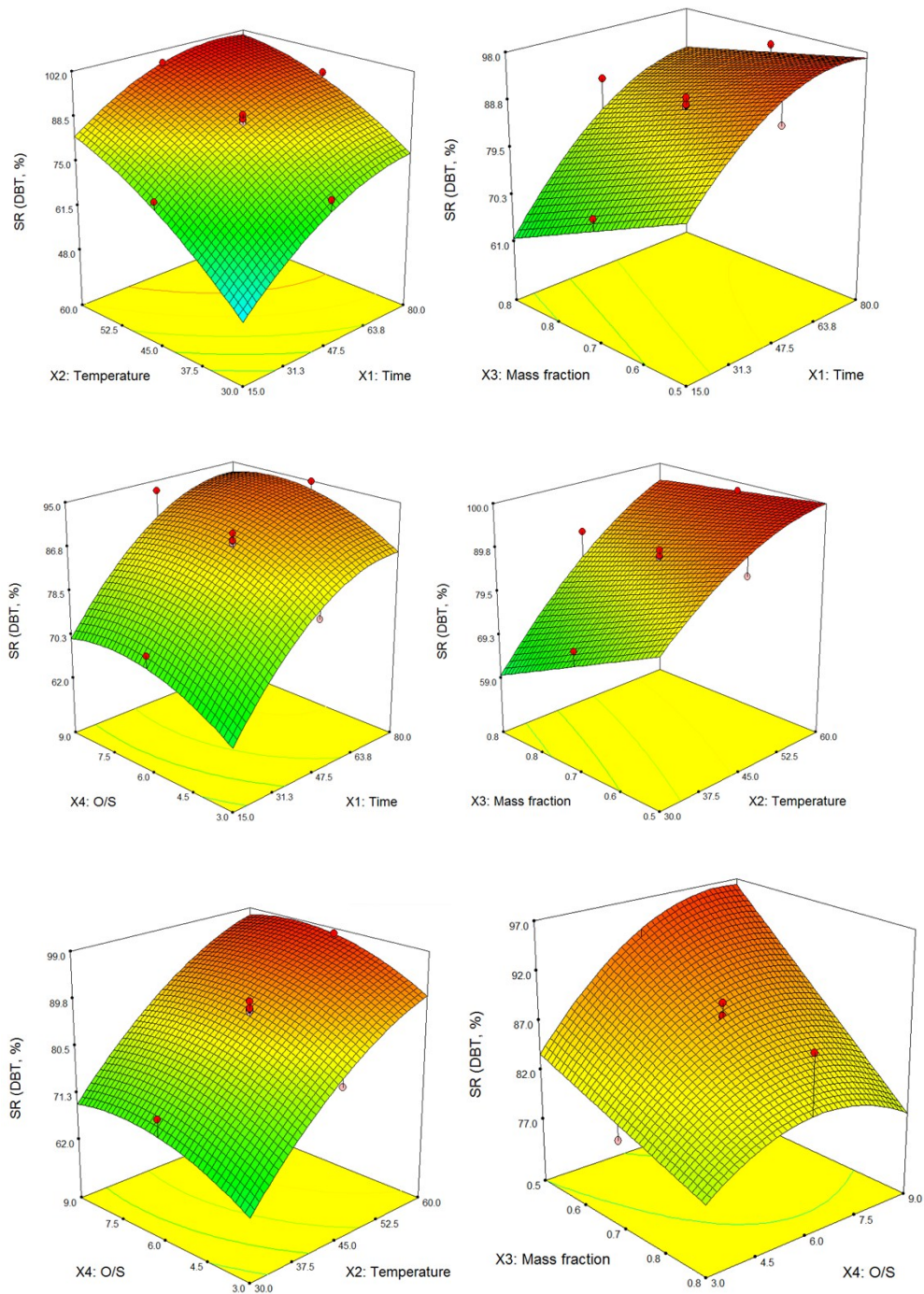


Figure S9: 3D plots for the EODS of DBT using the  $[P_{i444,1}][Tos]$



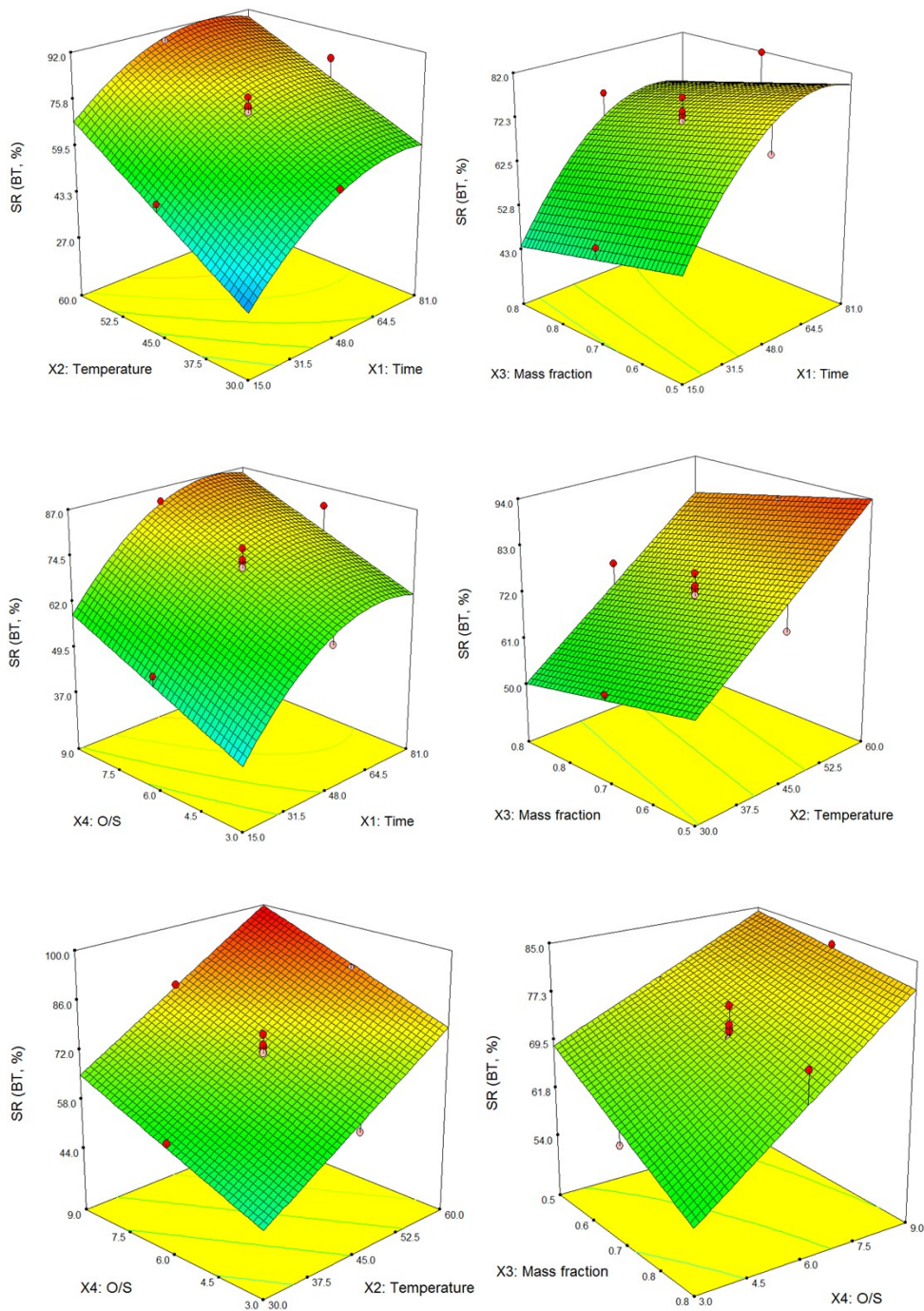


Figure S10: 3D plots for the OEDS of BT using the  $[P_{i444,1}][Tos]$

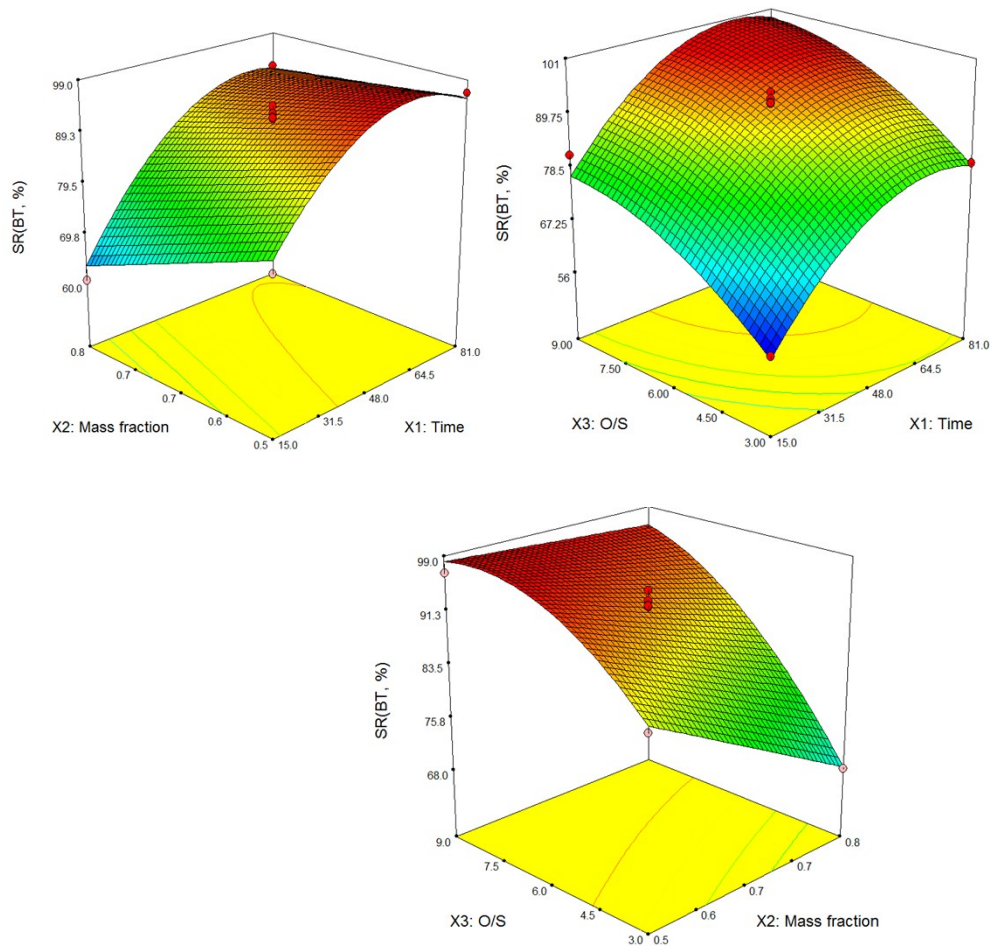


Figure S11: 3D plots for the OEDS of BT using the  $[P_{4444}][MeSO_3]$