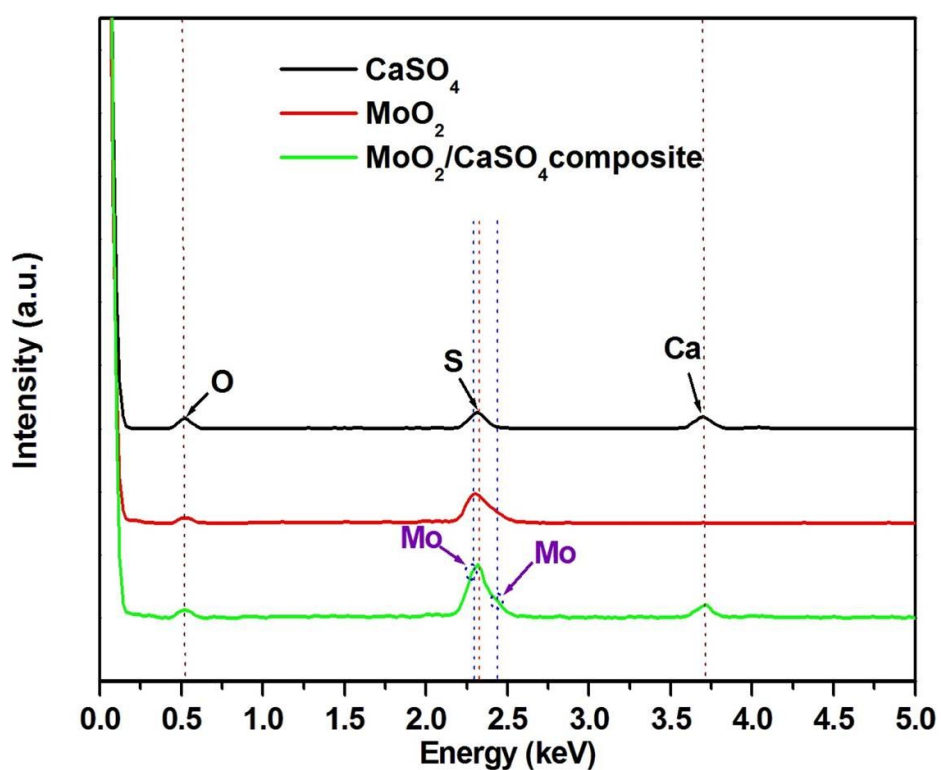


## Electronic Supplementary Information (ESI)

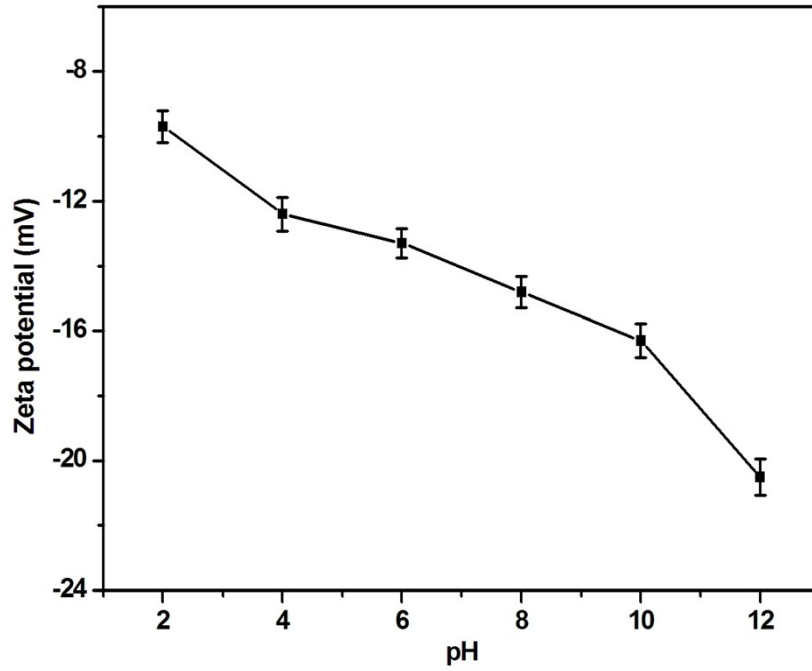
### Facile synthesis of $\text{MoO}_2/\text{CaSO}_4$ composites as highly efficient adsorbents for Congo red and Rhodamine B

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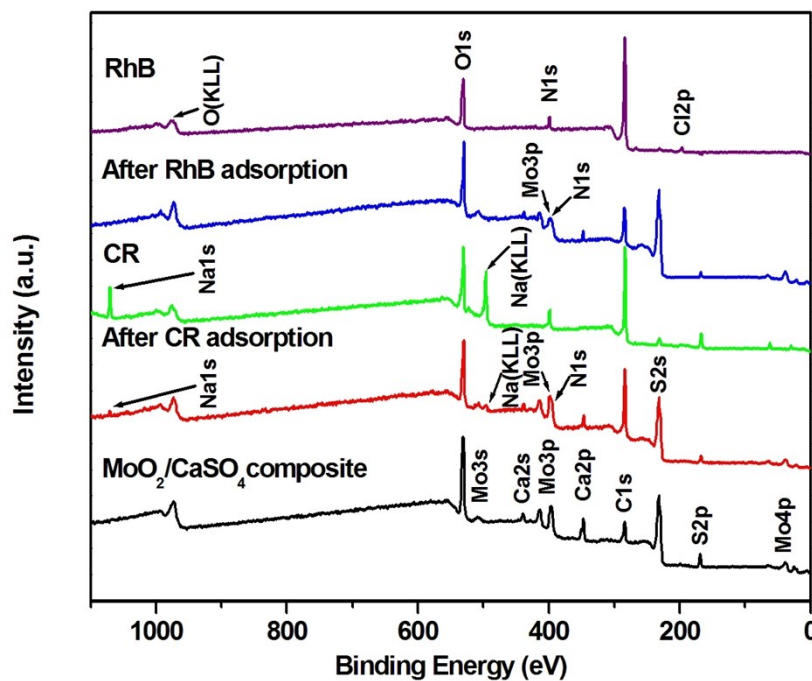
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**Fig. S1.** EDX patterns of  $\text{CaSO}_4$ ,  $\text{MoO}_2$  and  $\text{MoO}_2/\text{CaSO}_4$  composites.



**Fig. S2** Zeta potential values of the MoO<sub>2</sub>/CaSO<sub>4</sub> composite over a pH range between 2.0 and 12.0.



**Fig. S3.** XPS survey scan spectra of MoO<sub>2</sub>/CaSO<sub>4</sub> composites, MoO<sub>2</sub>/CaSO<sub>4</sub> composites after CR adsorption, CR, MoO<sub>2</sub>/CaSO<sub>4</sub> composites after RhB adsorption and RhB.

**Eq. S1.** Equation for the removal efficiency ( $R_e$ ) of a dye onto an adsorbent.

$$R_e = \frac{C_0 - C_t}{C_0} \times 100\%$$

$C_0$  ( $\text{mg}\cdot\text{L}^{-1}$ ) is the initial concentration of a dye solution;  $C_t$  ( $\text{mg}\cdot\text{L}^{-1}$ ) is the dye concentration at time  $t$ .

**Eq. S2.** Equation for the adsorption capacity ( $q_e$ ,  $\text{mg}\cdot\text{g}^{-1}$ ) of a dye onto an adsorbent at equilibrium.

$$q_e = \frac{C_0 - C_e}{m} V$$

$C_e$  ( $\text{mg}\cdot\text{L}^{-1}$ ) is the equilibrium concentration of a dye solution;  $m$  (g) is the mass of an adsorbent; and  $V$  (L) is the volume of a dye solution.

**Eq. S3.** Equation for the adsorption quantity ( $q_t$ ,  $\text{mg}\cdot\text{g}^{-1}$ ) of a dye onto an adsorbent at time  $t$ .

$$q_t = \frac{C_0 - C_t}{m} V$$

**Eq. S4.** Equation for the Langmuir model.

$$\frac{C_e}{q_e} = \frac{C_e}{q_{max}} + \frac{1}{q_{max}k_L}$$

In this model,  $q_{max}$  ( $\text{mg}\cdot\text{g}^{-1}$ ) and  $k_L$  ( $\text{L}\cdot\text{mg}^{-1}$ ) are Langmuir isotherm constants separately representing the maximum adsorbed quantity and a function associated with the adsorption free energy.

**Eq. S5.** Equation for the separation factor  $R_L$ .

$$R_L = \frac{1}{1 + k_L C_0}$$

**Eq. S6.** Equation for the Freundlich model.

$$\ln q_e = \ln k_F + \frac{1}{n} \ln C_e$$

In this model,  $k_F$  ( $(\text{mg}\cdot\text{g}^{-1})(\text{L}\cdot\text{mg}^{-1})^{1/n}$ ) and  $n$  are Freundlich isotherm coefficients, which are separately related to the adsorption capability and the adsorption intensity.

**Eq. S7.** Equation for the D–R model.

$$\ln q_e = \ln q_m - k_D \varepsilon^2$$

In this model,  $q_m$  ( $\text{mg}\cdot\text{g}^{-1}$ ) and  $k_D$  ( $\text{mol}^2\cdot\text{kJ}^{-2}$ ) are the D–R isotherm constants related to the maximum adsorption quantity and the mean adsorption free energy, respectively.

**Eq. S8.** Equation for the Polanyi potential  $\varepsilon$ .

$$\varepsilon = RT \ln \left( 1 + \frac{1}{C_e} \right)$$

In this model,  $R$  ( $8.314 \text{ J}\cdot\text{mol}^{-1}\cdot\text{K}^{-1}$ ) is the molar gas constant, and  $T$  is the absolute temperature expressed in K.

**Eq. S9.** Equation for the mean adsorption free energy.

$$E = \frac{1}{\sqrt{2k_D}}$$

**Eq. S10.** Equation for the Temkin model.

$$q_e = \frac{RT}{b} \ln k_T + \frac{RT}{b} \ln C_e$$

In this model,  $b$  (equal to  $-\Delta H$ ,  $\text{kJ}\cdot\text{mol}^{-1}$ ) denotes the adsorption heat, and  $k_T$  ( $\text{L}\cdot\text{mg}^{-1}$ ) is the Temkin isotherm constant.

**Eq. S11.** Equation for the Gibb's free energy  $\Delta G^0$ .

$$\Delta G^0 = -RT \ln Kq$$

In this equation,  $R$  ( $8.314 \text{ J}\cdot\text{mol}^{-1}\cdot\text{K}^{-1}$ ) is the molar gas constant,  $T$  is the absolute temperature expressed in K, and  $K_q$  ( $\text{L}\cdot\text{g}^{-1}$ ) is the distribution coefficient of an

adsorbent that equals to  $q_e \cdot C_e^{-1}$ .

**Eq. S12.** Equation for the  $\ln Kq$ .

$$\ln Kq = \frac{\Delta S^0}{R} - \frac{\Delta H^0}{RT}$$

**Eq. S13.** Equation for the pseudo-first-order kinetic model.

$$\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303} t$$

In this model,  $k_1$  ( $\text{min}^{-1}$ ) represents the kinetic rate constant of the pseudo-first-order adsorption.

**Eq. S14.** Equation for the pseudo-second-order kinetic model.

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t$$

In this model,  $k_2$  ( $\text{g} \cdot \text{mg}^{-1} \cdot \text{min}^{-1}$ ) denotes the rate constant of the pseudo-second-order adsorption.

**Eq. S15.** Equation for the Elovich kinetic model.

$$q_t = \frac{1}{\beta} \ln(\alpha\beta) + \frac{1}{\beta} \ln t$$

In this model,  $\alpha$  ( $\text{mg} \cdot \text{g}^{-1} \cdot \text{min}^{-1}$ ) refers to the initial adsorption rate, and  $\beta$  ( $\text{g} \cdot \text{mg}^{-1}$ ) represents the Elovich desorption constant.

**Eq. S16.** Equation for the intra-particle diffusion model.

$$q_t = k_{id} t^{0.5} + C_i$$

In this model,  $k_{id}$  ( $\text{mg} \cdot \text{g}^{-1} \cdot \text{min}^{-1/2}$ ) denotes the kinetic rate constant of the intra-particle diffusion at stage  $i$ , and  $C_i$  is a constant whose value directly affects the boundary layer thickness of molecular diffusion.

**Table S1.** Chemical composition of FDG gypsum confirmed by XRF analysis.

Material	Content/ wt.%										
	Ca	S	Si	Mg	Al	F	Fe	K	Na	Cl	P
FGD gypsum	59.78	26.17	4.18	4.03	1.81	1.34	1.29	0.57	0.35	0.34	0.14

**Table S2.** Chemical composition of FDG gypsum confirmed by EDX analysis.

Material	Content/ wt.%						
	O	Ca	S	Mg	Si	Al	Fe
FGD gypsum	55.77	24.43	13.24	3.12	1.68	0.91	0.85

**Table S3.** Chemical composition of the purified FDG gypsum confirmed by EDX analysis.

Material	Content/ wt.%		
	O	Ca	S
The purified FGD gypsum	58.15	22.27	19.58

**Table S4.** Isotherm parameters of four different models for the adsorption of CR and RhB onto MoO<sub>2</sub>/CaSO<sub>4</sub> composites.

Isotherm models/parameters	CR	RhB
Langmuir		
$q_{max}$ (mg·g <sup>-1</sup> )	853.54	86.38
$k_L$ (L·mg <sup>-1</sup> )	0.0151	0.1913
$R^2$	0.9979	0.9912
$R_L$	0.027-0.143	0.022-0.054
Freundlich		
$k_F$ ((mg·g <sup>-1</sup> )(L·mg <sup>-1</sup> ) <sup>1/n</sup> )	100.33	49.55
$n$	3.0252	9.1466
$R^2$	0.8587	0.8498
D-L		
$q_m$ (mg·g <sup>-1</sup> )	703.42	70.25
$k_D$ (mol <sup>2</sup> ·kJ <sup>-2</sup> )	1.22 x 10 <sup>-4</sup>	2.13 x 10 <sup>-7</sup>
$E$ (kJ·mol <sup>-1</sup> )	0.0433	1.2654
$R^2$	0.8944	0.7564
Temkin		
$k_T$ (L·mg <sup>-1</sup> )	0.21	646.77
$b$ (kJ·mol <sup>-1</sup> )	0.0144	0.3423
$R^2$	0.9653	0.8501

**Table S5.** An adsorptive capacity comparison of the MoO<sub>2</sub>/CaSO<sub>4</sub> composite with other adsorbents.

Adsorbents	$q_{\max}$ (mg·g <sup>-1</sup> )	References
Activated carbon	6.7 (CR)	[40, 41]
	39.22 (RhB)	
Jute stick powder	35.7 (CR)	[42]
	87.7 (RhB)	
Kaolinite	22.99 (CR)	[43, 44]
	46.08 (RhB)	
$\alpha$ -MoO <sub>3</sub> /polyaniline composite	76.22 (CR)	[23]
	36.36 (RhB)	
MoO <sub>2</sub> /CaSO <sub>4</sub> composite	853.54 (CR)	This study
	86.38 (RhB)	

**Table S6.** Thermodynamic parameters for the adsorption of CR and RhB onto MoO<sub>2</sub>/CaSO<sub>4</sub> composites.

Samples	$\Delta H^0$ , kJ·mol <sup>-1</sup>	$\Delta S^0$ , J·mol <sup>-1</sup> ·K <sup>-1</sup>	$\Delta G^0$ , kJ·mol <sup>-1</sup>					$R^2$
			20 °C	25 °C	30 °C	35 °C	40 °C	
CR	-22.31	-13.02	-18.11	-18.44	-18.33	-18.02	-17.22	0.9221
RhB	40.11	193.25	-16.19	-17.63	-18.64	-19.01	-20.22	0.9755



**Table S7.** Kinetic parameters of four different models for the adsorption of CR and RhB onto MoO<sub>2</sub>/CaSO<sub>4</sub> composites.

Kinetic models/Parameters	CR	RhB
Pseudo-first-order		
$q_e$ (exp) (mg·g <sup>-1</sup> )	750.63	66.64
$q_e$ (cal) (mg·g <sup>-1</sup> )	522.60	23.22
$k_1$ (min <sup>-1</sup> )·10 <sup>-3</sup>	5.20	6.03
$R^2$	0.8875	0.9064
Pseudo-second-order		
$q_e$ (cal) (mg·g <sup>-1</sup> )	746.27	66.85
$k_2$ (g·mg <sup>-1</sup> ·min <sup>-1</sup> )·10 <sup>-4</sup>	0.25	9.40
$R^2$	0.9508	0.9992
Elovich		
$\alpha$ (mg·g <sup>-1</sup> ·min <sup>-1</sup> )	239.83	46.75
$\beta$ (g·mg <sup>-1</sup> )·10 <sup>-3</sup>	11.08	116.95
$R^2$	0.8007	0.9225
Intra-particle diffusion		
$k_{1d}$ (mg·g <sup>-1</sup> ·min <sup>-1/2</sup> )	126.93	12.31
$C_1$	0	0
$(R_1)^2$	1.0000	1.0000
$K_{2d}$ (mg·g <sup>-1</sup> ·min <sup>-1/2</sup> )	18.64	3.77
$C_2$	266.77	20.20
$(R_2)^2$	0.8897	0.9124
$K_{3d}$ (mg·g <sup>-1</sup> ·min <sup>-1/2</sup> )	6.61	0.53
$C_3$	568.79	53.79
$(R_3)^2$	0.9492	0.9784