

## **Electronic Supplementary Information**

### **A novel surfactant-polymer flooding system of the biobased zwitterionic surfactant and hydrophobically associating polymer with ultralow interfacial tensions**

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## 1. Material

Daqing oil sands (specific surface area of 1.43 m<sup>2</sup>/g), Daqing crude oil (a density of 0.85 g/cm<sup>3</sup>, viscosity of 19.81 mPa at 45 °C). Other materials were all analytical reagents. All of the aqueous solutions used in this study were prepared with simulated formation water (Table 1).

**Table 1 The formation of simulate formation water**

Substance	Concentration (mg/L)
NaHCO <sub>3</sub>	3176.0
NaCl	1597.1
Na <sub>2</sub> CO <sub>3</sub>	381.6
CaCl <sub>2</sub>	112.7
MgCl <sub>2</sub>	42.8
Na <sub>2</sub> SO <sub>4</sub>	17.0

## 2. Methods

### 2.1 Interfacial tension measurement

The interfacial tension was measured by a spinning drop interfacial tensiometer, TX500C. The measuring range of TX500C is 100 mN/m -10<sup>-5</sup> mN/m. A capillary tube filled with surfactant solution and a fresh drop of crude oil, was spun at 4500 rpm. Unless otherwise specified, the temperature was 45 °C in this study. The measure time is one hour for the POAPMB solutions and two hours for POAPMB/AP-P3 system. The interfacial tension between Daqing crude oil and simulated formation water was 9.90 mN/m at 45 °C.

### 2.2 Dilution resistance measurement

The POAPMB/AP-P3 system was mixed with simulated formation water at the volume ratio of 1:1, 1:2, 1:3...1:8. After mixing, the interfacial tension with crude oil was measured at 45 °C to determine the dilution resistance of the system. The initial concentration of surfactant was 0.50 g/L, and AP-P3 was 1.50 g/L.

### 2.3 Adsorption resistance measurement

The solutions with a surfactant concentration of 0.50 g/L and with an AP-P3 concentration of 1.50 g/L were prepared. The solutions (8.00 g) and oil sands (0.89 g) were mixed in 10 mL colorimetric tube. Shaking them at 45 °C for 24 h by shaking water bath SW22. The supernatants were collected by centrifuge 3-18 (5000 rpm, 5 min), then measured IFT between Daqing crude oil and the supernatants. If the value of IFT was below 0.01 mN/m, fresh sands were added to the remaining supernatants at the weight fraction ratio of 0.1/0.9. Repeat the above operation until the IFT of the solution is above 0.01 mN/m. The resistance of a surfactant formulation against adsorption were evaluated by the total number of times that an ultralow IFT was achieved.

### 2.4 Viscosity stability measurement

The viscosity stability of SP flooding was determined under the conditions of 45 °C, shear rates 7.34 s<sup>-1</sup> by Programmable Rheometer DV-III. The accuracy of Programmable Rheometer DV-III is the plus or minus one percent of the result of the measurement.

### 2.5 Phase behavior study

The solution and crude oil were preheated to 45 °C, then 25 mL of crude oil and 25 mL of POAPMB/AP-P3 system were mixed in a 50 mL colorimetric tube and shaken by hand for 5 minutes. An emulsion was formed and allowed to settle at 45 °C, and equilibrium was assumed when there was no observable change in the phase levels. The final observed levels were recorded.

### 2.6 Particle size and Zeta potential

Particle size and Zeta potential were measured using Zetasizer procured from Malvern instruments, Model ZEN3690, USA at 45 °C.

## 3. Results of interfacial properties

### 3.1 Interfacial tension

Dynamic interfacial tensions (average of three measurements) between Daqing crude oil and different concentrations of surfactant solutions alone and in the presence of 1.50 g/L AP-P3 were showed in Fig. 1a and 1b.

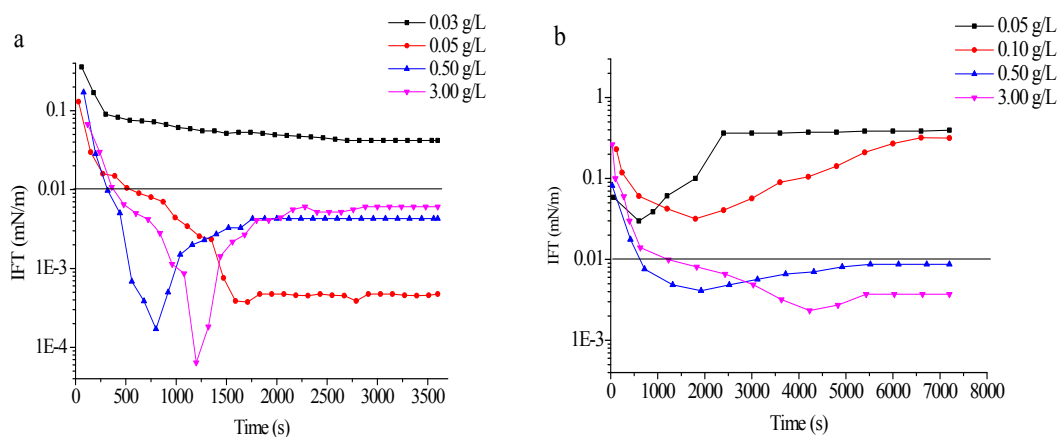


Figure 1. The IFT between crude oil and different concentrations of POAPMB solutions (a) and in the presence of 1.50 g/L AP-P3 (b)

### 3.2 Effect of temperature

Fig.2 showed IFTs (average of three measurements) of surfactant solution and POAPMB/AP-P3 system at different temperatures. The concentrations of POAPMB and AP-P3 in binary system were 0.50 g/L and 1.50 g/L, respectively.

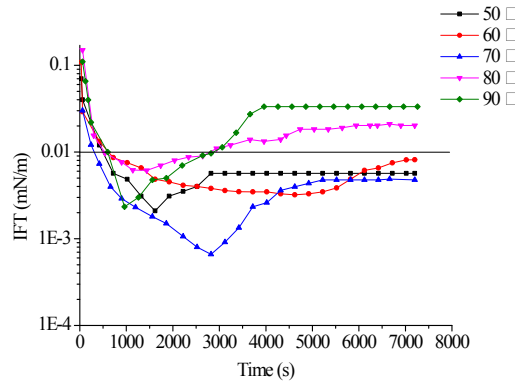


Figure 2. Effect of temperature on the IFTs between crude oil and POAPMB/AP-P3 system

### 3.3 Effect of salt

The effect of NaCl and Ca<sup>2+</sup> concentration on IFTs (average of three measurements) was showed in Fig. 3 and Fig. 4. The concentrations of POAPMB and AP-P3 in binary system were 0.50 g/L and 1.50 g/L, respectively.

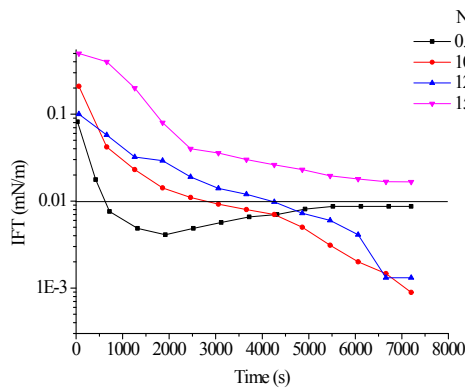


Figure 3. Effect of concentrations of NaCl on the IFTs between crude oil and POAPMB/AP-P3 system

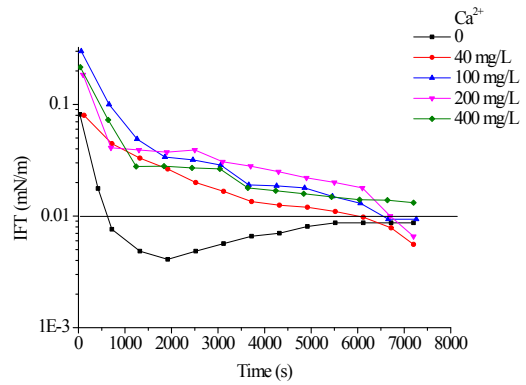


Figure 4. Effect of concentrations of Ca<sup>2+</sup> on the IFTs between crude oil and POAPMB/AP-P3 system

### 3.4 Dilution performance

Table 2 showed the IFTs of 3.00 g/L POAPMB solution with 1.50 g/L AP-P3 after dilution against crude oil.

Table 2 The minimum IFTs and the equilibrium IFTs between crude oil and the aqueous solutions after dilution

Dilution multiple	3.0 g/L	3.0 g/L
	POAPMB	POAPMB
	+1.5 g/L AP-P3	+1.5 g/L AP-P3
1	$(2.3 \pm 0.4) \times 10^{-4}$	$(4.1 \pm 0.4) \times 10^{-3}$
2	$(4.2 \pm 0.5) \times 10^{-4}$	$(5.6 \pm 0.5) \times 10^{-3}$
3	$(4.1 \pm 0.3) \times 10^{-4}$	$(4.3 \pm 0.3) \times 10^{-3}$
4	$(3.8 \pm 0.4) \times 10^{-4}$	$(2.5 \pm 0.2) \times 10^{-3}$
5	$(3.9 \pm 0.3) \times 10^{-4}$	$(3.6 \pm 0.2) \times 10^{-3}$
6	$(5.7 \pm 0.6) \times 10^{-4}$	$(2.6 \pm 0.3) \times 10^{-3}$
7	$(3.2 \pm 0.5) \times 10^{-4}$	$(6.7 \pm 0.4) \times 10^{-3}$
8	$(2.5 \pm 0.4) \times 10^{-4}$	$(7.9 \pm 0.3) \times 10^{-4}$
9	$(5.5 \pm 0.5) \times 10^{-4}$	$(3.4 \pm 0.2) \times 10^{-3}$

10	$(1.4\pm 0.3)\times 10^{-5}$	$(3.5\pm 0.4)\times 10^{-4}$
20	$(1.6\pm 0.4)\times 10^{-4}$	$(3.1\pm 0.2)\times 10^{-3}$
30	$(2.9\pm 0.3)\times 10^{-4}$	$(2.9\pm 0.3)\times 10^{-4}$
40	$(4.5\pm 0.6)\times 10^{-3}$	$(4.5\pm 0.4)\times 10^{-3}$
50	$(4.3\pm 0.4)\times 10^{-2}$	$(4.3\pm 0.3)\times 10^{-2}$

### 3.5 Resistance against adsorption by Daqing oil sands

Table 3 showed the IFTs of 3.00 g/L POAPMB solution with 1.50 g/L AP-P3 after adsorptions against crude oil.

**Table 3 The IFT<sub>min</sub> and IFT<sub>equ</sub> between crude oil and the aqueous solutions after adsorption (45 °C)**

Days	3.0 g/L	3.0 g/L
	POAPMB +1.5 g/L AP-P3	POAPMB +1.5 g/L AP-P3
	IFT <sub>min</sub> (mN/m)	IFT <sub>equ</sub> (mN/m)
1	$(4.1\pm 0.4)\times 10^{-3}$	$(4.1\pm 0.4)\times 10^{-3}$
2	$(1.0\pm 0.2)\times 10^{-3}$	$(5.1\pm 0.1)\times 10^{-3}$
3	$(7.0\pm 0.3)\times 10^{-3}$	$(7.0\pm 0.3)\times 10^{-3}$
4	$(5.4\pm 0.4)\times 10^{-2}$	$(8.8\pm 0.2)\times 10^{-2}$

## 4. Results of viscosity properties

### 4.1 Dilution performance

Table 4 showed the viscosity of 0.50 g/L POAPMB solution with 1.50 g/L AP-P3 after dilution.

**Table 4 The viscosity of POAPMB/AP-P3 system diluted (45 °C)**

Dilution multiple	1	2	3	4	5	6	7	8	9
Viscosity (mPa·s)	46.8±0.4	15.7±0.2	8.9±0.1	6.5±0.1	5.9±0.1	4.3±0.1	3.9±0.1	3.6±0.1	3.4±0.1

### 4.2 Resistance against adsorption by Daqing oil sands

Table 5 showed the viscosity of 0.50 g/L POAPMB solution with 1.50 g/L AP-P3 after adsorption.

**Table 5 The viscosity of POAPMB/AP-P3 system after adsorption (45 °C)**

Adsorption times	0	1	2	3
Viscosity (mPa·s)	46.8±0.4	44.3±0.2	43.7±0.3	42.8±0.2

### 4.3 Effect of temperature

Table 6 showed the viscosity of 0.50 g/L POAPMB solution with 1.50 g/L at different temperature.

**Table 6 Effect of temperature on the viscosity of POAPMB/AP-P3 system**

Temperature (°C)	50	60	70	80	90
Viscosity (mPa·s)	39.7±0.3	36.3±0.3	32.8±0.3	29.5±0.2	25.1±0.1

### 4.4 Effect of salt

Table 7 and Table 8 showed the viscosity of 0.50 g/L POAPMB solution with 1.50 g/L at different concentrations of . NaCl and Ca<sup>2+</sup>.

**Table 7 Effect of the concentration of NaCl on the viscosity of POAPMB/AP-P3 system (45 °C)**

The concentration of NaCl (g/L)	0	10	12.5	15
Viscosity (mPa·s)	46.8±0.4	27.5±0.2	25.9±0.2	24.8±0.2

**Table 8 Effect of the concentration of Ca<sup>2+</sup> on the viscosity of POAPMB/AP-P3 system (45 °C)**

The concentration of Ca <sup>2+</sup> (mg/L)	0	40	100	200	400
Viscosity (mPa·s)	46.8±0.4	42.1±0.3	41.5±0.2	35.9±0.2	26.2±0.1

## 5. Particle size and Zeta potential

Table 9 and Table 10 showed Particle size and Zeta potential results of solutions.

**Table 9 Particle size at 45 °C**

Solution	Peak 1 (nm)	Intensity%	Peak 2 (nm)	Intensity%
0.5 g/L POAPMB	13.7±0.1	100	-	-
1.5 g/L AP-P3	43.4±6.1	100	-	-
0.5 g/L POAPMB+1.5 g/L AP-P3	14.5±1.5	13.5	100.1±8.9	86.5
Middle microemulsion	144.1±9.5	100	-	-
Bottom phase	40.4±9.3	33.7	212.3±19.9	66.3

**Table 10 Particle size at 45 °C**

Solution	ZP (mV)
Middle microemulsion	50.4±2.4

## 6. Previous result

The previous results cited in the paper are summarized in Table 11.

**Table 11 Previous result**

Solution	State
2.5 g/L sugar-based anionic-nonionic surfactant	achieved ultralow IFT <sup>15</sup>
5 mM nonionic + 1.00 g/L polyacrylamide	can't achieve ultralow IFT <sup>10</sup>
0.3~10 mM nonionic surfactant mixed sulfobetaine + 1.00 g/L polyacrylamide	achieved ultralow IFT <sup>10</sup>
gemini-non-ionic mixed surfactant (total 3.00 g/L) + hydrophobically associating polyacrylamide	achieved ultralow IFT after aging for 90 days <sup>5</sup>
nonionic/zwitterionic formulation (total 7.50 mM, mole ratio 1/1) + 1.00 g/L polyacrylamide	achieved the ultralow IFT after adsorption four times <sup>2</sup>
0.50 g/L fatty acid disulfonate+1.75 g/L hydrophobically associating polyacrylamide	67% the initial viscosity retention rate. <sup>5</sup>