

## Supplementary Information

### Three-dimensional “Skin-Framework” Hybrid Network as Electroactive Material Platform for High-Performance Solid-state Asymmetric Supercapacitor

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## S1. Calculations

### 1. 1. Calculation of the areal specific capacitance of the single electrode

(1) The areal specific capacitance of the electrodes was calculated from the CV curves using Equation (1):

$$C_a = \frac{Q}{\Delta U \times S} \quad (1)$$

where  $C_a$  (mF/cm<sup>2</sup>) is the areal specific capacitance,  $Q$  is the average charge during electrode charging and discharging,  $\Delta U$  (V) is the working voltage window of the electrode, and  $S$  (cm<sup>2</sup>) is the test area of the electrodes.

(2)  $C_a$  was calculated by galvanostatic charging-discharging using Equation (2):

$$C_a = \frac{I \times \Delta t}{\Delta U \times S} \quad (2)$$

where  $I$  is the current during electrode discharging (A), and  $\Delta t$  (s) is the DC discharge time of the electrode.

(3) The mass specific capacitance with respect to the three-electrode configuration was derived from galvanostatic charging-discharging based on Equations (3) and (4):

$$C_s = \frac{Q(\text{MnO}_2 + \text{MWCNT}) - Q(\text{MWCNT})}{\Delta U_1 \times m_1} \quad (3)$$

$$C_s = \frac{Q(\text{AC} + \text{MWCNT}) - Q(\text{MWCNT})}{\Delta U_2 \times m_2} \quad (4)$$

where  $C_s$  is the mass specific capacitance,  $Q$  is the charge obtained from the galvanostatic charging-discharging based on the MnO<sub>2</sub>-MCN, AC-MCN and MCN electrodes,  $\Delta U_1$  (=0.8 V) and  $\Delta U_2$  (=1.0 V) constitute the voltage range,  $m_1$  is the mass of MnO<sub>2</sub> loaded on the MnO<sub>2</sub>-

MCN electrode, and  $m_2$  is the mass of AC loading on the AC-MCN electrode.

**1. 2. Calculation of volume specific capacitance, power density, and energy density of the  $MnO_2$ -MCN//AC-MCN solid-state ASC device**

(1) The volume specific capacitance of the electrodes was calculated from the CV curves and from Equations (5) and (6):

$$C_{cell} = \frac{Q}{\Delta U} \quad (5)$$

$$C_V = \frac{C_{cell}}{V} = \frac{Q}{V \times \Delta U} \quad (6)$$

where  $C_{cell}$  is the capacitance and  $C_V$  is the volume specific capacitance of the device,  $Q$  is the average charge during electrode charging and discharging,  $\Delta U$  (V) is the working voltage window of the device.  $V$  ( $cm^3$ ) is the volume of the device, including the volumes of the positive and negative electrode pieces, gel electrolyte, and diaphragm. The area, thickness, and volume of the  $MnO_2$ -MCN//AC-MCN solid-state ASC device were  $1.0 \text{ cm}^2$ ,  $521 \text{ }\mu\text{m}$  (see Fig. S9), and  $0.521 \text{ cm}^3$ , respectively.

(2) The specific capacitance of the device was calculated from the discharging curve using Equations (7) and (8):

$$C_{cell} = \frac{I \times \Delta t}{\Delta U} \quad (7)$$

$$C_s = \frac{C_{cell}}{m} = \frac{I \times \Delta t - C_{MWCNT} m_{MWCNT}}{m \times \Delta U} \quad (8)$$

where  $C_{cell}$  is the capacitance and  $C_s$  is the mass specific capacitance of the device;  $I$  is the

current during the device discharging (A), and  $\Delta t$  (s) is the DC discharge time of the device;  $\Delta U$  (V) is the working voltage window of the device;  $m$  (g) is the mass of the active material, where  $m$  includes the  $\text{MnO}_2$  and AC.

(3) Equations (9)–(11) were used to calculate the energy density ( $E$ ,  $\text{mWh/cm}^3$ ), equivalent series resistance (ESR, i.e., the internal resistance of the capacitor,  $\Omega$ ), and power density ( $P$ ,  $\text{mW/cm}^3$ ) of the device, respectively:

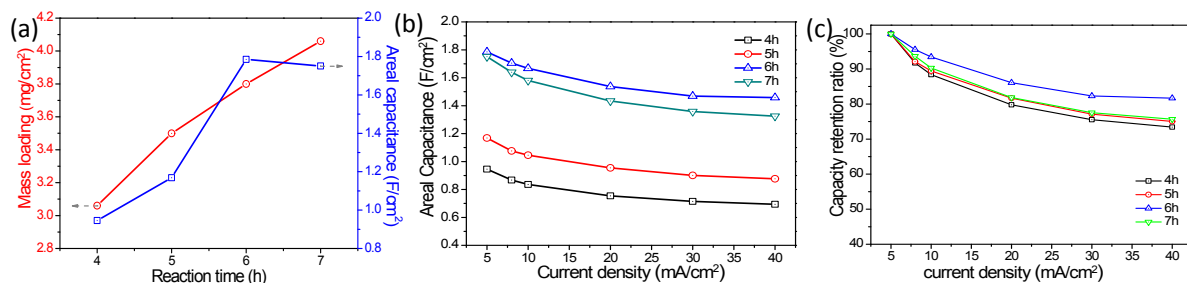
$$E = \frac{1}{2 \times 3600} C_v \Delta U^2 \quad (9)$$

$$ESR = \frac{iR_{drop}}{2 \times I} \quad (10)$$

$$P = \frac{\Delta U^2}{4 \times ESR \times V} \quad (11)$$

where  $C_v$  is the volume specific capacitance of the device,  $\Delta U$  (V) is the working voltage window, and  $iR_{drop}$  is the voltage drop.

## S2. Various graphs and curves

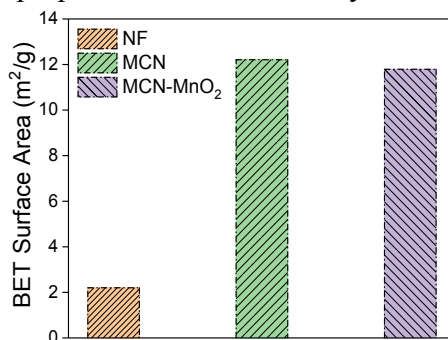


**Fig. S1** (a) Mass loading and areal specific capacitance of the  $\text{MnO}_2$ -MCN electrode as a function of reaction times; (b) areal capacitance; and (c) capacitance retention rate of the  $\text{MnO}_2$ -MCN electrode as functions of the current density.

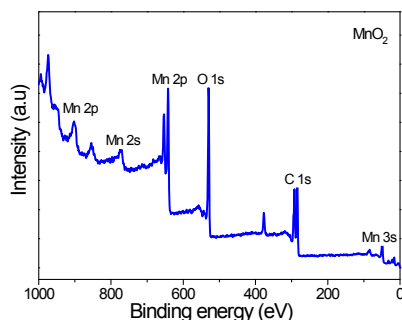
As expected, and as shown in Fig. S1a, when MCN is used as the active material platform, the mass loading of  $\text{MnO}_2$  increases proportionally with the reaction time. However, the areal specific capacity of the  $\text{MnO}_2$ -MCN electrode initially increases and then decreases with time. This is because  $\text{MnO}_2$  nanoparticles substantially aggregates on the MWCNT surface with increasing the reaction time, with adverse effects on the electrochemical performance of the  $\text{MnO}_2$ -MCN electrode. Fig. S1b and c show the electrodes area specific capacity and capacity retention as a function of current density at different times. Obviously, the  $\text{MnO}_2$ -MCN electrode prepared with reaction time for 6h has a larger area specific capacity and a better capacity retention. The experimental results thus indicate an optimal reaction time of 6h, and this was adopted for further electrochemical investigation in this work.



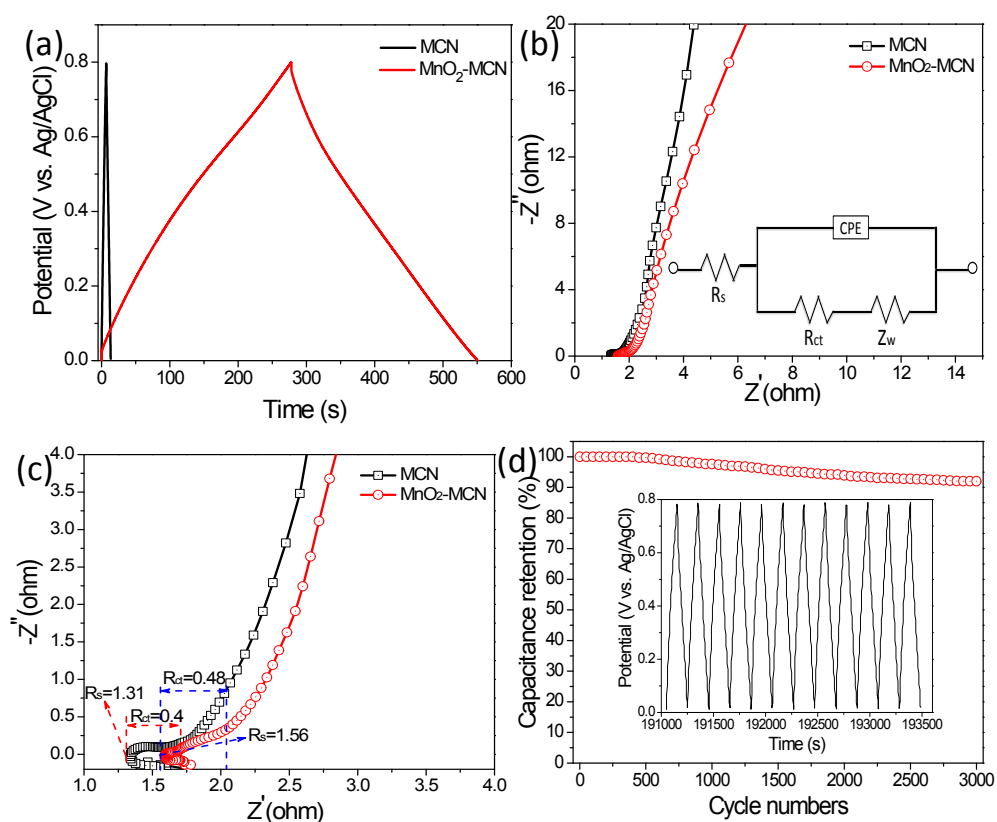
**Fig. S2** Display of large-scale preparation of the MCN hybrid materials.



**Fig. S3** Histogram of the specific surface area of the NF, MCN, and MnO<sub>2</sub>-MCN electrode materials.



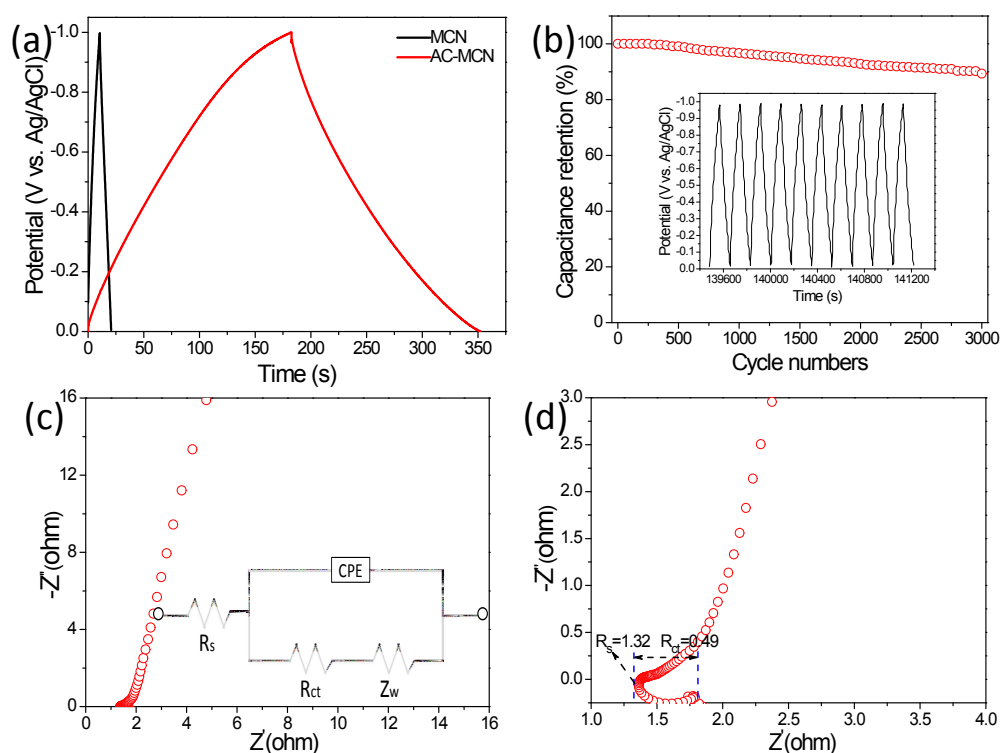
**Fig. S4** XPS full spectra of the MnO<sub>2</sub>-MCN electrode.



**Fig. S5** (a) GCD curves of the MCN and MnO<sub>2</sub>-MCN electrodes collected at a current density of 5 mA/cm<sup>2</sup>; (b) Nyquist plots of the MCN and MnO<sub>2</sub>-MCN electrodes with the equivalent circuit diagram used for fitting the EIS data ( inset); (c) Nyquist plots of the

MCN and MnO<sub>2</sub>-MCN electrodes with the corresponding high-frequency parts; and (d) cycle performance of the MnO<sub>2</sub>-MCN electrode at current density of 10 mA/cm<sup>2</sup>.

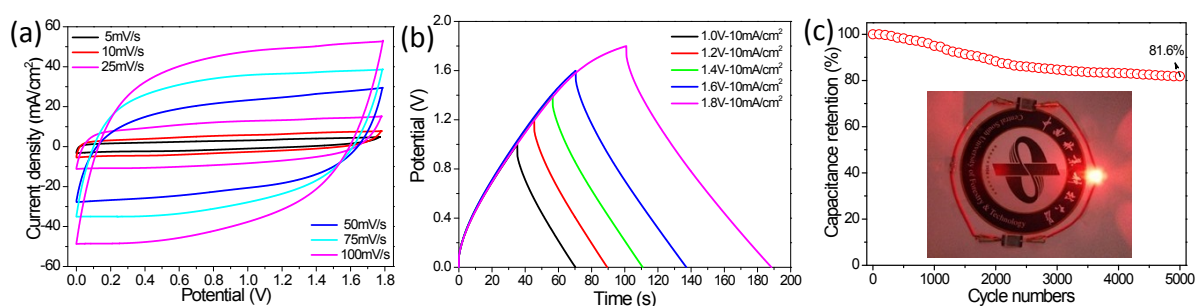
As shown in Fig. S5 (b), the equivalent circuit diagram used for the fitting of the EIS data includes the equivalent series resistance ( $R_s$ ), the charge transfer resistance ( $R_{ct}$ ), the diffusion impedance ( $Z_w$ ), and the constant phase element (CPE) to account for the double layer capacitance. It is seen that the MCN electrode had smaller  $R_s$  and  $R_{ct}$  compared with the MnO<sub>2</sub>-MCN electrode. This mainly attributed to the poor electronic conductivity of nano-MnO<sub>2</sub> ( $1 \times 10^{-5}$  to  $1 \times 10^{-6}$  S/cm) loaded onto the MCN platform, resulting in a large  $R_{ct}$  of the MnO<sub>2</sub>-MCN electrode. Further, when the MnO<sub>2</sub> nanoparticles was loaded, the insufficiently developed porous structure of the MnO<sub>2</sub>-MCN electrode combined with the poor liquid absorption ability led to the increase in the  $Z_w$  of the MnO<sub>2</sub>-MCN electrode to become large.



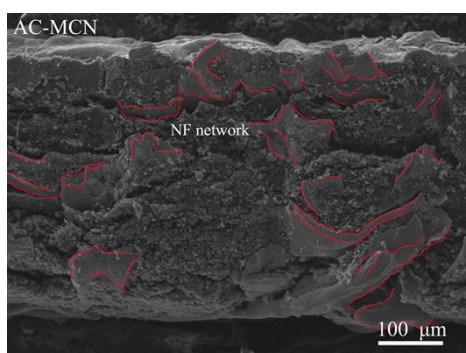
**Fig. S6** (a) GCD curves of the MCN and AC-MCN electrodes collected at a current density of 5 mA/cm<sup>2</sup>; (b) cycle performance of the AC-MCN electrode at a current density of 10 mA/cm<sup>2</sup>; (c) Nyquist plots of the AC-MCN electrode with the equivalent circuit

diagram used for fitting the EIS data (inset); and (d) Nyquist plots of the AC-MCN electrode with the corresponding high-frequency part.

The equivalent circuit diagram used for the fitting of the EIS data is presented in inset of Fig. S6 (c), which includes the equivalent series resistance ( $R_s$ ), the charge transfer resistance ( $R_{ct}$ ), the diffusion impedance ( $Z_w$ ), and the constant phase element (CPE) to account for the double layer capacitance. As shown in Fig. S6 (d), It can be seen that the AC-MCN electrode had a low  $R_s$  (1.32  $\Omega$ ) and  $R_{ct}$  (0.49 $\Omega$ ). This mainly attributed to the good electronic conductivity of MCN electroactive platform.

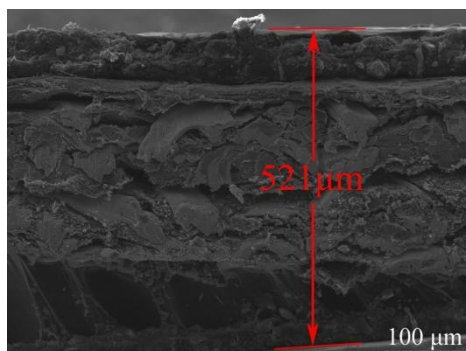


**Fig. S7** (a) CV curves of the MnO<sub>2</sub>-MCN//AC-MCN solid-state ASC device collected at scan rates of 5–100 mV/s; (b) GCD curves of the ASC device within various operation voltage windows at a current density of 10 mA/cm<sup>2</sup>; and (c) cycle performance of the MnO<sub>2</sub>-MCN//AC-MCN solid-state ASC device and (inset) photograph of an LED indicator (3 V) powered by two 1 cm × 1 cm units of the ASC device in series.





**Fig. S8** Cross-sectional SEM image of the AC-MCN electrode sheet.



**Fig. S9** Cross-sectional SEM image of the MnO<sub>2</sub>-MCN//AC-MCN solid-state ASC device.

### **S3. Video**

**Video S1** Demonstration of the structural stability of the MWCNT/CNF “skin” in the MCN platform by ultrasonic treatment.

**Video S2** Demonstration of the good wettability of the MCN, MnO<sub>2</sub>-MCN and AC-MCN electrodes.