Supporting Information for

A double-stranded DNA catalyzed strand displacement system for detection of small genetic variations

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Materials and methods

1. Materials

TE solution, proteinase K and PCR product purification kit were purchased from Tiangen Biotech Co. (Beijing, China). Taq polymerase and ThermoPol reaction buffer were purchased from NEB Co. (Beijing, China). DNA strands were synthesized and purified by HPLC (Sangon Co., China). The sequences of all the probes and targets that have been studied in this work are summarized in Table S1.

Table 31. Sequences	
Stand name	Sequence (from 5' to 3') ^a
EGFR-L858R-FAM	TGGGCGGGCCAAACTGCTAACCTCTCTA-FAM
EGFR-L858R-BHQ	BHQ-TAGAGAGGTTAGCAGTTTGGCCCGCCCA AAATCTGTGATCCAT
EGFR-L858R-MT-12-10	GATCACAGATTTTGGGCGGGCCAAACTGCT
EGFR-L858R-MT-11-10	ATCACAGATTTTGGGCGGGCCAAACTGCT
EGFR-L858R-MT-11-9	ATCACAGATTTTGGGCGGGCCAAACTGC
EGFR-L858R-WT-12-10	GATCACAGATTTTGGGCTGGCCAAACTGCT
EGFR-L858R-WT-11-10	ATCACAGATTTTGGGCTGGCCAAACTGCT
EGFR-L858R-WT-11-9-	ATCACAGATTTTGGGCTGGCCAAACTGC
EGFR-L858R-Blocker17	GCAGTTTGGCCAGCCCA
EGFR-L858R-Blocker16	CAGTTTGGCCAGCCCA
EGFR-L858R-Blocker15	AGTTTGGCCAGCCCA
EGFR-L858R-	GCAGTTTGGCCAGCCCATTTTTT
Blocker17+tail	
EGFR-L858R-	AGTTTGGCCAGCCCATTTTTT
Blocker15+tail	
EGFR-L858R-Invader1	TTGGGCGGGCCAAACTGCTAACCTCTCTA
EGFR-L858R-Invader2	TTTGGGCGGGCCAAACTGCTAACCTCTCTA
EGFR-L858R-Invader3	TTTTGGGCGGGCCAAACTGCTAACCTCTCTA
EGFR-L858R-Invader4	ATTTTGGGCGGGCCAAACTGCTAACCTCTCTA
EGFR-L858R-FP	GAACGTACTGGTGAAAACACCG
EGFR-L858R-RP	TCCTTCTGCATGGTATTCTTTCTC
KrasG13D-FAM	TGGTGACGTAGGCAAGAGTGAGCTACA-FAM

Table S1. Sequences used in this wo

KrasG13D-BHQ	BHQ-TGTAGCTCACTCTTGCCTACGTCACCAGCTCCAACTACCACA
KrasG13D-MT	GTAGTTGGAGCTGGTGACGTAGGCAAGAG
KrasG13D-WT	GTAGTTGGAGCTGGTGGCGTAGGCAAGAG
KrasG13D-Invader2	GCTGGTGACGTAGGCAAGAGTGAGCTACA
KrasG13D-Blocker17	TCTTGCCTACGCCACCA
ShareY-FAM	GTCTCGCCGACGGAG-FAM
ShareY-BHQ	BHQ-GGCCGTCACACGTGT
KrasG13D-Y-fam	TGGTGACGTAGGCAAGAGTGAGCTACAGTATCATAGCATAAGGCCGC
KrasG13D-Y-bhq	ACACGTGTGACGGCCTGTAGCTCACTCTTGCCTACGTCACCAGCTCCAACTACCAC
KrasG13D-Y-MT	GTAGTTGGAGCTGGTGACGTAGGCAAGAG
KrasG13D-Y-WT	GTAGTTGGAGCTGGTGGCGTAGGCAAGAG
KrasG13D-Y-Invader0	TGGTGACGTAGGCAAGAGTGAGCTACA
KrasG13D-Y-Invader1	CTGGTGACGTAGGCAAGAGTGAGCTACA
KrasG13D-Y-Invader2	GCTGGTGACGTAGGCAAGAGTGAGCTACA
KrasG13D-Y-Blocker17	TCTTGCCTACGCCACCA
ShareX-FAM	AAGGGTGTTGCTTATGCTATGATAC-FAM
ShareX-BHQ	BHQ-GTAGGAGAGAGAGAGAGAGGTGG
KrasG13D-X-fam	TGGTGACGTAGGCAAGAGTGAGCTCATAGCATAAGCAACACCCTT
KrasG13D-X-bhq	CCACCTCTATCTCTCCGCTCACTCTTGCCTACGTCACCAGCTCCAACTACCACA
KrasG13D-X-MT	GTAGTTGGAGCTGGTGACGTAGGCAAGAG
KrasG13D-X-WT	GTAGTTGGAGCTGGTGGCGTAGGCAAGAG
KrasG13D-X-Invader0	TGGTGACGTAGGCAAGAGTGAGCTACA
KrasG13D-X-Invader1	CTGGTGACGTAGGCAAGAGTGAGCTACA
KrasG13D-X-Invader2	GCTGGTGACGTAGGCAAGAGTGAGCTACA
KrasG13D-X-Blocker17	TCTTGCCTACGCCACCA
BRCArs3765640-Y-fam	
BRCArs3765640-Y-bhq	ACACGTGTGACGGCCTGTAGCTCAGGTTTTAGAATGATA CAAACCAAAGAACTAATG
BRCArs3765640-Y-MT	ТАGTTCTTTGGTTTGTATCATTCTAAAACC

BRCArs3765640-Y-WT	TAGTTCTTTGGTTTGTATTATTCTAAAACC
BRCArs3765640-Y-	TTTGTATCATTCTAAAACCTGAGCTACA
Invader	
BRCArs3765640-Y-	GGTTTTAGAATAATACA
Blocker	
MTRRA66G-Y-fam	GAAATGTGTGAGCAAGCTGAGCTACAGTATCATAGCAT AAGGCCGC
MTRRA66G-Y-bhq	ACACGTGTGACGGCCTGTAGCTCAGCTTGCTCACACATT TCTTCTGCGATGGCCTTT
MTRRA66G-Y-MT	GGCCATCGCAGAAGAAATGTGTGAGCAAGC
MTRRA66G-Y-WT	GGCCATCGCAGAAGAAATATGTGAGCAAGC
MTRRA66G-Y-Invader	AAGAAATGTGTGAGCAAGCTGAGCTACA
MTRRA66G-Y-Blocker	GCTTGCTCACATATTTC
MTHFRA1298C-Y-fam	TGAAGCAAGTGTCTTTGTGAGCTACAGTATCATAGCAT AAGGCCGC
MTHFRA1298C-Y-bhq	ACACGTGTGACGGCCTGTAGCTCACAAAGACACTTGCTTCACTGGTCAGCTCCTCCC
MTHFRA1298C-Y-MT	AGGAGCTGACCAGTGAAGCAAGTGTCTTTG
MTHFRA1298C-Y-WT	AGGAGCTGACCAGTGAAGAAAGTGTCTTTG
MTHFRA1298C-Y-	AGTGAAGCAAGTGTCTTTGTGAGCTACA
Invader	
MTHFRA1298C-Y-	CAAAGACACTTTCTTCA
Blocker	
MTHFRC677T-Y-fam	GGGAGTCGATTTCATCATGAGCTACAGTATCATAGCATAAGGCCGC
MTHFRC677T-Y-bhq	ACACGTGTGACGGCCTGTAGCTCATGATGAAATCGACTCCCGCAGACACCTTCTCCT
MTHFRC677T-Y-MT	AGAAGGTGTCTGCGGGAGTCGATTTCATCA
MTHFRC677T-Y-WT	AGAAGGTGTCTGCGGGAGCCGATTTCATCA
MTHFRC677T-Y-Invader	GCGGGAGTCGATTTCATCATGAGCTACA
MTHFRC677T-Y-Blocker	TGATGAAATCGGCTCCC
BRCArs1799949-Y-fam	GACAGTGATACTTTCCCTGAGCTACAGTATCATAGCAT AAGGCCGC
BRCArs1799949-Y-bhq	ACACGTGTGACGGCCTGTAGCTCAGGGAAAGTATCACTG TCATGTCTTTACTTGTC
BRCArs1799949-Y-MT	AAGTAAAAGACATGACAGTGATACTTTCCC
BRCArs1799949-Y-WT	AAGTAAAAGACATGACAGCGATACTTTCCC

BRCArs1799949-Y-	ATGACAGTGATACTTTCCCTGAGCTACA
Invader	
BRCArs1799949-Y-	GGGAAAGTATCGCTGTC
Blocker	
BRCArs16940-Y-fam	TTTCACTGGTACCTGGTTGAGCTACAGTATCATAGCATAAGGCCGC
BRCArs16940-Y-bhq	ACACGTGTGACGGCCTGTAGCTCAACCAGGTACCAGTGA AATACTGCTACTCTCTA
BRCArs16940-Y-MT	GAGAGTAGCAGTATTTCACTGGTACCTGGT
BRCArs16940-Y-WT	GAGAGTAGCAGTATTTCATTGGTACCTGGT
BRCArs16940-Y-Invader	TATTTCACTGGTACCTGGTTGAGCTACA
BRCArs16940-Y-Blocker	ACCAGGTACCAATGAAA
BRCArs80357234-Y-fam	GCCTATAAGAAAGTACGTGAGCTACAGTATCATAGCATAAGGCCGC
BRCArs80357234-Y-bhq	ACACGTGTGACGGCCTGTAGCTCACGTACTTTCTTATA GGCTCCTGAAATTAAATT
BRCArs80357234-Y-MT	TTTAATTTCAGGAGCCTATAAGAAAGTACG
BRCArs80357234-Y-WT	TTTAATTTCAGGAGCCTACAAGAAAGTACG
BRCArs80357234-Y-	GCCTATAAGAAAGTACGTGAGCTACA
Invader	
BRCArs80357234-Y-	CGTACTTTCTTGTAGGC
Blocker	
MTRRA66G-FP	TCAGTTTCACTGTTACATGCCTTGAAGTG
MTRRA66G-RP	TCCACTGTAACGGCTCTAACCTTATCGGA
MTHFRA1298C-FP	CCCTCTGTCAGGAGTGTG
MTHFRA1298C-RP	CACTCCAGCATCACTCACT
BRCArs1799949-FP	CAAGAAGAGTAACAAGCCAAATG
BRCArs1799949-RP	TAAAAGAACCAGGTGCATTTGT
BRCArs16940-FP	GACCCCAAAGATTTTTGCAAACTG
BRCArs16940-RP	CCAGTAACGAGATACTTTCCTGAGTG

^aAll the modification sites of interest were highlighted in red.

2. DNA sequence design

NCBI was used for consulting the corresponding SNP site sequence information. According to the probe structure, sequences were designed using NUPACK software to reduce secondary

structures and the interaction among the DNA strands.

3. DNA strand preparation and concentration quantification

TE solution was used for dissolving the dry powder of DNA strands to the required concentration. UV spectrophotometer was used for measuring the concentration of the DNA strands at 260 nm.

4. Non-universal probe preparation

The Dissociation strand and Template strand were mixed in a PCR tube at a ratio of 1.2: 1 with 1 × thermopol reaction buffer for the preparation of the probe to ensure the full bonding. After mixing, put the tube at 85 ° C for 1 minute, and then left at 55 ° C for 1 minute. Finally, the tube is transferred to 37 ° C, and kept at a constant temperature for 1 hour to several hours until use.

5. Universal probe preparation

The Dissociation strand, Template strand, Invader strand, and BHQ strand were mixed in a PCR tube at a ratio of 1.2: 1:1:1 with 1 × thermopol reaction buffer (NEB) for the preparation of the probe to ensure the full bonding. After mixing, put the tube at 85 $^{\circ}$ C for 5 minutes, and then left at 55 $^{\circ}$ C for 5 minutes. Finally, the tube was transferred to 37 $^{\circ}$ C, and kept at a constant temperature for 3 hours to several hours until use.

6. Two-step asymmetric PCR

The first step was to perform conventional PCR with 1: 1 primer, and then took 1 ul of the PCR product of the first step, diluted it 100 times, and took 1 ul as the template for second step. The second step was to perform PCR with 10:1 primer and obtained a large number of target single strands.

7. Fluorescence signal detection

Add probes, target Fuel strands, Invader strands, Blocker strands to the ELISA Plate Strips. Centrifugated it with a palm centrifuge and quickly put the plate strips into the Bio-Tek ELISA instrument for fluorescence detection. Preformed the fluorometric assay with an excitation/emission wavelengths of 485/582nm and gained value of 60. Fluorescence signal was collected once every 1 minute and lasted for hours.

Modelling and theoretical calculations

1. Demonstration of the chemical kinetic reaction process of dsCSD system.

We use initial letters to represent the ingredients in dsCSD system such as $F_{M/W}$ stands for Fuel_{MT/WT}, B stands for Blocker, I for Invader, D for Dissociation strand and T for Template strand. Take Fuel_{MT} as example:

As we pre-treated and mixed Template strand and Dissociation strand, Fuel strand and Blocker for the preparation of the probe and the reactant system, based on the principle of base pairing, following reactions would occur respectively:

$$T + D \rightarrow PRB$$
$$F_M + B \rightarrow F_M B$$

When all the ingredients were mixed and centrifugated in the ELISA Plate Strips, our dsCSD system would work as:

$F_M + B \rightarrow F_M B$	(1)
$F_M + PRB \rightarrow F_M T + D$	(2)
$F_M B + PRB \rightarrow F_M T + DB$	(3)
$I + B \rightarrow IB$	(4)
$I + PRB \rightarrow TI + D$	(5)
$IB + PRB \rightarrow TI + DB$	(6)
$F_M T + I \rightarrow TI + F_M$	(7)
$F_M T + IB \rightarrow TI + F_M B$	(8)

Considering Blocker strand was far more sufficient in the reaction system and they could easily bond with Fuel and Invader, reaction (1) and (4) would be finished in a short time, resulting in reaction (2), (5) and (7) being omitted in our modeling calculation. To summarize and simplify the above-mentioned reaction process, we could obtain a net reaction as following:

$$IB + PRB \xrightarrow{F_M B; F_M T} TI + DB$$
(9)

It was clear that the net reaction shared the same reactants and products with (6), thus we could take reaction (6) as the background. To summarize, we could view the whole dsCSD system as a reaction of Invader taking the place of Dissociation stand with $F_M B$ and $F_M T$ as catalyzers, that is the parataxis of reaction (3) and (8).

Similarly, for Fuel_{WT}, we have:

$$F_W B + PRB \rightarrow F_W T + DB \tag{10}$$

$$F_W T + IB \rightarrow TI + F_W B \tag{11}$$

With the net reaction:

$$IB + PRB \xrightarrow{F_WB; F_WT} TI + DB$$
(12)

Above all, in our modeling, the concentration of DB (noted as $^{[DB]}$)could stand for the fluorescence intensity. However, as we were eager to obtain the equation of $^{[DB]}$ versus time, the reaction rate constant of reaction (3), (8), (10) and (11) remained unknown. Therefore, it was obligatory for us to further detailing the reaction process to modeling.

For reaction (3), for example, it could be further detailed into the following 3 steps:

$$F_{M}B + PRB \stackrel{k1}{\Leftrightarrow} F_{M}B \cdot PRB \tag{13}$$

$$F_{M}B \cdot PRB \stackrel{k2}{\Leftrightarrow} F_{M}T \cdot DB \tag{14}$$

$$F_{M}T \cdot DB \stackrel{k3}{\Leftrightarrow} F_{M}T + DB \tag{15}$$

 $F_M B \cdot PRB$ in equation (13) represents the intermediate state of the reactants. In this case, that is the accomplishment of the free bases in Invader pairing with Template strand before the occurrence of strand displacement. Equation (14) represents the process of strand displacement and equation (15) represents the dissociation of $F_M T$ and DB. Similarly, for reaction (8):

$$F_{M}T + IB \stackrel{k4}{\Leftrightarrow} F_{M}T \cdot IB \tag{16}$$

$$F_{M}T \cdot IB \Leftrightarrow TI \cdot F_{M}B \tag{17}$$

$$TI \cdot F_M B \Leftrightarrow TI + F_M B \tag{18}$$

For the same reason, we could extract reaction (10) and (11) into another 6 equations based on the above principles.

2. Theoretical calculation of dsCSD system model

Based on the principles of chemical kinetics, the corresponding ordinary differential equations for Fuel (MT) are:

$$\begin{aligned} \frac{d[DB]}{dt} &= k_{3+} \left[F_{M} T \cdot DB \right] - k_{3-} \left[F_{M} T \right] \cdot [DB] \\ \frac{d[IB]}{dt} &= -k_{4+} \left[F_{M} T \right] \cdot [IB] + k_{4-} \left[F_{M} T \cdot IB \right] \\ \frac{d[F_{M}B]}{dt} &= -k_{1+} \left[F_{M} B \right] \cdot [PRB] + k_{1-} \left[F_{M} B \cdot PRB \right] + k_{6+} \left[TI \cdot F_{M} B \right] - k_{6-} \left[F_{M} B \right] \cdot [TI] \\ \frac{d[F_{M}T]}{dt} &= k_{3+} \left[F_{M} T \cdot DB \right] - k_{3-} \left[F_{M} T \right] \cdot [DB] - k_{4+} \left[F_{M} T \right] \cdot [IB] + k_{4-} \left[F_{M} T \cdot IB \right] \\ \frac{d[PRB]}{dt} &= -k_{1+} \left[F_{M} B \right] \cdot [PRB] + k_{1-} \left[F_{M} B \cdot PRB \right] \\ \frac{d[ITI]}{dt} &= k_{6+} \left[TI \cdot F_{M} B \right] - k_{6-} \left[F_{M} B \right] \cdot [TI] \\ \frac{d[F_{M} B \cdot PRB]}{dt} &= k_{1+} \left[F_{M} B \right] \cdot [PRB] - k_{1-} \left[F_{M} B \cdot PRB \right] - k_{2+} \left[F_{M} B \cdot PRB \right] + k_{2-} \left[F_{M} T \cdot DB \right] \\ \frac{d[F_{M} T \cdot DB]}{dt} &= k_{2+} \left[F_{M} B \cdot PRB \right] - k_{2-} \left[F_{M} T \cdot DB \right] - k_{3+} \left[F_{M} T \cdot DB \right] + k_{3-} \left[F_{M} T \right] \cdot [DB] \\ \frac{d[F_{M} T \cdot IB]}{dt} &= k_{4+} \left[F_{M} T \right] \cdot [IB] - k_{4-} \left[F_{M} T \cdot IB \right] - k_{5+} \left[F_{M} T \cdot IB \right] + k_{5-} \left[TI \cdot F_{M} B \right] \\ \frac{d[TI \cdot F_{M} B]}{dt} &= k_{5+} \left[F_{M} T \cdot IB \right] - k_{5-} \left[TI \cdot F_{M} B \right] - k_{6+} \left[TI \cdot F_{M} B \right] + k_{6-} \left[F_{M} B \right] \cdot [TI] \end{aligned}$$

Similarly, we could obtain the corresponding ordinary differential equations for Fuel (WT).

3. Simulation and calculation of reaction rate constant

For reaction (13), ${}^{F}{}_{M}{}^{B}$ and PRB are two different double-strand structures that formed during the preparation of the probe and the reaction platform. There exist several free and matched bases at the 3' end of the Template strand and the 5' end of Fuel strand. ${}^{k}{}_{1}$ + represents the reaction rate constant of bases binding. According to literature searching and simulation, the binding rate constant could be assumed to be 3 × 10⁵ M⁻¹s⁻¹. For the same reason, ${}^{k}{}_{3}$ -, ${}^{k}{}_{4}$ + and ${}^{k}{}_{6}$ - for those who represents the binding of free bases, could be assumed to be 3 × 10⁵ M⁻¹s⁻¹. Their reverse rate constants could be calculated as

$$k_{-} = \frac{k_{+}}{K_{eq}} = k_{+} e^{\Delta G_{rxn}^{0}/R\tau}$$

where ΔG_{rxn}^{o} denotes the standard free energy of the relevant reaction. By using

NUPACK to predict free energy of secondary structure for reactants and products, ΔG_{rxn}^{o} for different reactions or sequences can be obtained. Thus, the reverse rate constants for the binding process can be calculated.

Equation (14) and (17) represent the process of strand displacement. Considering there is no relevant data on the rate constant of strand displacement, more experimental explorations and simulations are needed.

4. Simulation and calculation of model by MATLAB

The ordinary differential equations mentioned above are simulated using MATLAB's stiff "ode23s" solver with the initial concentration of IB, $F_{M/W}B$ and PRB are 1uM, 100nM and 1uM respectively. By outputting the consequence of [DB] versus time in different condition, we could identify and evaluate their DF for the consultants of Invader optimization. Since the construction of our modeling is based on simulation and matching, it sure needs more perfection not only in the estimation of ΔG , but also in more reveals of the chemical kinetic information of strand displacement process. We believe that with the in-depth study for kinetic process of strand displacement reaction, our model could serve as a powerful tool for the optimization of experiment conditions.

Supplementary figures and tables



1. Principle of target DNA catalyzing DNA strand displacement reactions

Figure S1. Schematic illustration of the reaction pathways of ssCSD system toward MT and WT.

2. The feasibility of dsCSD system was identified by polyacrylamide gelelectrophoresis (PAGE).



Identification of the feasibility for double-stranded DNA catalyzed strand displacement system by polyacrylamide gel electrophoresis (PAGE)

Figur

e S2.Identification of the feasibility of dsCSD system by PAGE.



3. Optimization of dsCSD system targeting the detection of EGFR-L858R

re S3. Optimization of the toehold region for the target strand and the length of Blocker. (a)The target MT strands were set 11-9 with the length of Blocker from 15 to 17 nt. (b) The target MT strands were set 11-10 with the length of Blocker from 15 to 17 nt. (c) The target MT strands were set 12-10 with the length of Blocker from 15 to 17 nt. (d) The target WT strands were set 12-10 with the length of Blocker from 15 to 17 nt. (e) The efficiency ratio of dsCSD with different MT and Blocker in 30 minutes. (f) The discrimination factor of dsCSD with 12-10 target and different Blocker in 30 minutes.



Figure S4. Optimization of the length for Invader strand. (a) Fuel (12-10) + BLK17 + Invader-1. (b) Fuel (12-10) + BLK17 + Invader-2. (c) Fuel (12-10) + BLK17 + Invader-3. (d) Fuel (12-10) + BLK17 + Invader-4.

4. The detection limit of the dsCSD system targeting KrasG13D mutation in synthesized DNA sample



Figure S5. The detection limit of the dsCSD system targeting KrasG13D mutation in synthesized sample.

5. Optimization of universal dsCSD system



Figure S6. The discrimination factors (DF) of the universal dsCSD systems toward MT and WT with the length of invader chain ranging from 0 to 2nt. The concentration of invader chain was fixed at 1μ M. (a)Y-type universal dsCSD system. (b) X-type universal dsCSD system.



Figure S7. Fluorescence intensity responses of the Y-type universal dsCSD system in detection of the MT and WT with Invader-0/1/2. (a) Invader-0. (b) Invader-1. (c) Invader-2.



Figure S8. The discrimination factors (DF) of Y-type universal dsCSD system towards MT and WT with the concentration of invader chain ranging from 1 to 2μ M. The length of invader chain was fixed at 0nt.



Figure S9. Fluorescence intensity responses of the Y-type universal dsCSD system in detection of the MT and WT with the concentration of invader chain ranging from 1 to 2μ M. The length of invader chain was fixed at 0nt. (a) the concentration of invader chain was 1μ M. (b) the concentration of invader chain was 1.5μ M. (c) the concentration of invader chain was 2μ M.



Figure S10. Fluorescence intensity responses of the X-type universal dsCSD system in detection of the MT and WT with the length of invader chain ranging from 0 to 2nt. The concentration of invader chain was fixed at 1μ M. (a) the length of invader chain was 0nt. (b) the length of invader chain was 1nt. (c) the length of invader chain was 2nt.

6. The detection limit of Y-type universal dsCSD system targeting KrasG13D and BRCArs80357234 mutation in synthesized DNA sample



Figure S11. Fluorescence intensity responses of the dsCSD system in detection of the MT target with various abundances by using the Y-type universal probe. (a) Kras G13D. (b) BRCA rs80357234.



7. Genotyping using the Y-type universal dsCSD system to identify homozygous, heterozygous and wild type

Figure S12. Genotyping using the Y-type universal dsCSD system. (a)BRCA rs1799949. (b)BRCA rs3765640. (c)BRCA rs16940. (d)MTRR A66G. (e)MTHFR A1298C. (f) MTHFR C677T.

8. The Sanger sequencing results of clinical samples used in this work



Figure S13. The sequencing results of the blood samples of (a) lung cancer patient and (b) healthy volunteer.



Figure S14. The sequencing results of the blood samples of ovarian cancer patients and healthy volunteers. (a)BRCA rs16940. (b)BRCA rs1799949. (c)MTRR A66G. (d)MTHFR A1298C.