## **Supporting Information**

## Proposition of Deposition and Bias Conditions for Optimal Signal-to-Noise-Ratio in Resistorand FET-type Gas Sensors

Wonjun Shin<sup>‡</sup>, Gyuweon Jung<sup>‡</sup>, Seongbin Hong, Yujeong Jeong, Jinwoo Park, Donghee Kim, Dongkyu Jang, Dongseok Kwon, Jong-Ho Bae<sup>\*\*</sup>, Byung-Gook Park, and Jong-Ho Lee<sup>\*</sup>

Department of Electrical and Computer Engineering and Inter-university Semiconductor Research Center, Seoul National University, Seoul 08826, Republic of Korea

\*\*Department of Electrical Engineering and Computer Sciences, University of California at Berkeley, Berkeley, CA 94720 USA.

\*E-mail address: ljh@snu.ac.kr



**Figure S1**. Schematic cross-sectional views of key process steps cut along dotted lines A-A' and B-B' in Figure 1a. A nitride layer formed on the SiO<sub>2</sub> layer (pad oxide) grown on *n*-type Si substrate is patterned to define active regions (a). Then a 550 nm thick oxide is grown and the nitride is removed (b). The pad oxide is removed and a sacrificial SiO<sub>2</sub> layer is grown. Then ion implantation for the threshold control is performed and the sacrificial layer is removed. After growing 10 nm thick gate oxide,  $n^+$  polycrystalline Si is deposited to form the FG (equivalently gate electrode for normal FETs) (c). Then SiO<sub>2</sub> (10nm)/Si<sub>3</sub>N<sub>4</sub> (20nm)/SiO<sub>2</sub> (10nm) is formed as a passivation layer (O/N/O) (d). After defining contact holes, Cr (30 nm) and Au (50 nm) layers are consecutively formed as the CG, source, and drain electrodes for the FET-type gas sensors and electrodes for the resistor-type gas sensors (e). Then *n*-type In<sub>2</sub>O<sub>3</sub> film for sensing layer is deposited (f).



**Figure S2.** Top SEM images of the fabricated (a) resistor- and (b) FET-type gas sensors. The size of the resistortype gas sensor is  $100 \times 125 \ \mu\text{m}^2$  and the distance between the metal electrodes is 2  $\mu$ m. The FET-type gas sensor has a FG and a CG facing each other in a horizontal direction. The Width/Length of the FET channel is 2  $\mu$ m/2  $\mu$ m and the distance between CG and FG is 0.5  $\mu$ m. The length ( $L_f$ ) and number ( $N_f$ ) of FG fingers are 10  $\mu$ m and 4, respectively.



**Figure S3.** Top SEM images of  $In_2O_3$  films deposited at RF powers of (a) 50 W, (b) 100 W, and (c) 230 W.  $In_2O_3$  film deposited at an RF power of 50 W shows the smallest grain size and  $In_2O_3$  film deposited at an RF power of 100 W shows the largest grain size. The further increase in RF power (230 W) results in a decrease in grain size of  $In_2O_3$  film.



**Figure S4.** Schematic diagram of the system measuring the gas reaction and the LFN of the sensors. To measure the LFN power spectral density of the sensors, a low noise current amplifier (SR570) and signal analyzer (35670A) are used. The voltage applied to the electrodes (V) of the resistor-type gas sensor is supplied by the SR570. The gate voltage and the drain bias of the FET-type gas sensor are supplied by the B1500A and SR570, respectively. The output current of the resistor-type gas sensor or the drain current of the FET-type gas sensor is connected to the SR570 which converts the current fluctuation into a voltage fluctuation. 35670A converts the dynamic signal from SR570 to a power spectral density. The LFN measurement frequency ranges from 10 Hz to  $10^4$  Hz.



**Figure S5.** Schematic diagram of the system measuring the gas reaction and the LFN of the sensors. Gas sensing characteristics of the sensors are analyzed by using a semiconductor parameter analyzer (B1500A) and the probe station that contains a test chamber, chuck, gas inlet, and outlet.  $H_2S$  gas is used as a target gas and gas flow is controlled by a mass flow controller (MFC). The target gas is mixed with dry air with a relative humidity of 4% for controlling the gas concentration and then the gas is injected into the test chamber. The response of the sensor to the  $H_2S$  gas molecules is measured at  $180^{\circ}$ C.



**Figure S6.** Log-Log plot of  $S_{ID}/I_D^2$  versus  $I_D$  of a *p*-type MOSFET with FG as its gate electrode. Dashed dot line represents the fitted LFN characteristics in Figure 3d. The noise characteristics of the *p*-type MOSFET represented in Figure S5 are almost the same as those of the FET type gas sensors represented in Figure 3d. Note that the *p*-type MOSFET and FET-type sensors are fabricated on the same Si substrate and have the same channel size (*W*/*L*= 2 µm/2µm). The result demonstrates that sensing material deposition condition does not affect the intrinsic device noise of the FET-type gas sensor. The LFN characteristics of FET-type gas sensors are determined by the *p*-type MOSFET channel noise. It is believed that the additional noise that can be generated at the sensing material has a lower level than the MOSFET channel noise.



**Figure S7.** Normalized current noise power spectral density ( $S_1$ ) of resistor-type gas sensor with In<sub>2</sub>O<sub>3</sub> deposited at an RF power of 100 W at 27 °C and 180 °C. The increase of  $\gamma$  is observed at 180 °C.



**Figure S8.** Normalized current noise power spectral density  $(S_1/I^2)$  of resistor-type gas sensor with In<sub>2</sub>O<sub>3</sub> deposited at an RF power of 100 W with various RH. At 180 °C, pure steam (100°C dew point) will register only ~5.9% on the relative humidity (RH) scale. Figure S7 shows the normalized current noise power spectral density  $(S_{ID})$  of resistor-type gas sensors with In<sub>2</sub>O<sub>3</sub> deposited at an RF power of 100 W with various RH. The humidity does not affect the LFN characteristics of the sensor at 180 °C.