## 1 Effect of NH<sub>3</sub> and HCOOH on $H_2O_2 + HO \rightarrow HO_2 + H_2O$ reaction in

the troposphere: competition between one-step and stepwise mechanism

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S. NO	Caption
2	<b>Table S1</b> Energy barriers ( $\Delta E$ ) for the H <sub>2</sub> O <sub>2</sub> + HO $\rightarrow$ HO <sub>2</sub> + H <sub>2</sub> O reaction at different theoretical methods with zero-point correction involved and unsigned error (UE) (in kcal·mol <sup>-1</sup> )
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6	<b>Table S2</b> Relative energies (( $\Delta E$ ), ( $\Delta E$ + ZPE)), enthalpies ( $\Delta H$ ) and free energies ( $\Delta G$ ) for the possible stable complexes between H <sub>2</sub> O <sub>2</sub> (or HO) and the catalyst <i>X</i> ( <i>X</i> = NH <sub>3</sub> and HCOOH) at the CCSD(T)-F12a/cc-pVDZ-F12//M06-2X/aug-cc-pVTZ level
7	<b>Table S3</b> Equilibrium constants (cm <sup>3</sup> ·molecule <sup>-1</sup> ) for the formation of two-body complexes between $H_2O_2$ (or HO) and catalyst $X$ ( $X = NH_3$ and HCOOH) within the temperature range of 213-320 K
8	Table S4 Equilibrium constants (cm <sup>3</sup> ·molecule <sup>-1</sup> ) for three-body complexes constituted by $H_2O_2$ , HO and catalyst X (X = NH <sub>3</sub> and HCOOH) within the temperature range of 213-320 K
9	Fig. S4 Optimized geometries for $NH_3$ catalyzed $H_2O_2 + HO \rightarrow HO_2 + H_2O$ reaction at the M06-2X/aug-cc-pVTZ level
10	Fig. S5 Optimized geometries for HCOOH catalyzed $H_2O_2 + HO \rightarrow HO_2 + H_2O$ reaction at the M06-2X/aug-cc-pVTZ level
11- 12	<b>Table S5</b> Relative energies $((\Delta E) (\Delta E + ZPE))$ , enthalpies $(\Delta H)$ , and free energies for the reactants, intermediate, and transition states involved in the H <sub>2</sub> O <sub>2</sub> + HO $\rightarrow$ HO <sub>2</sub> + H <sub>2</sub> O reaction with catalyst $X (X = NH_3 \text{ and HCOOH})$ at the CCSD(T)-F12a/cc-pVDZ-F12// M06-2X/aug-cc-pVTZ level
13	<b>Table S6</b> Calculated rate coefficients (cm <sup>3</sup> ·molecules <sup>-1</sup> ·s <sup>-1</sup> ) for the $H_2O_2 + HO \rightarrow HO_2 + H_2O$ reaction in the presence of catalyst $X$ ( $X = NH_3$ and HCOOH) within the temperature range of 213-320 K
14	<b>Table S7</b> Effective rate coefficients $(k_1)$ (cm <sup>3</sup> ·molecules <sup>-1</sup> ·s <sup>-1</sup> ) for the H <sub>2</sub> O <sub>2</sub> + HO $\rightarrow$ HO <sub>2</sub> + H <sub>2</sub> O reaction with basic (NH <sub>3</sub> ) and acidic (HCOOH) catalysts within the temperature range of 280-320 K
15	<b>Table S8</b> Concentrations of $X$ ( $X = H_2O$ , NH <sub>3</sub> , and HCOOH) (in molecule·cm <sup>-3</sup> ) within the temperature range of 280-320 K at 0 km altitude
16- 21	<b>Table S9</b> Coordinates and geometrical structures for the reactants, pre-reactive complexes, transition states, post-reactive complexes and products involved in catalyst $X (X = NH_3 \text{ and HCOOH})$ assisted $H_2O_2 + HO \rightarrow HO_2 + H_2O$ reaction at the M06-2X/aug-cc-pVTZ level

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Ζ.	methous with zero-point correction involved and unsig	glieu error (O	E) (III KCal	· 1101 )		_
	Methods	$\Delta E^a$	$\Delta E^b$	$\Delta E^{c}$	UE	
	W3X-I//M06-2X/aug-cc-pVTZ	-13.4	2.7	-35.1	0.00	
	W2X//M06-2X/aug-cc-pVTZ	-13.2	3.2	-35.0	0.26	
	CCSD(T)-F12a/pVDZ-F12//M06-2X/aug-cc-pVTZ	-13.7	2.6	-35.4	0.23	

**Table S1** Energy barriers ( $\Delta E$ ) for the H<sub>2</sub>O<sub>2</sub> + HO  $\rightarrow$  HO<sub>2</sub> + H<sub>2</sub>O reaction at different theoretical 2 methods with zero-point correction involved and unsigned error (UE) (in kcal:mol<sup>-1</sup>)



Fig. S1 Schematic potential energy diagrams for the  $H_2O_2 + HO \rightarrow HO_2 + H_2O$  reaction without and with  $H_2O$  at the CCSD(T)-F12a/cc-pVDZ-F12//M06-2X/aug-cc-pVTZ level

The  $H_2O_2 + HO \rightarrow HO_2 + H_2O$  reaction were investigated theoretically in the previous reports.<sup>1-6</sup> In this study, we have reinvestigated this reaction at the CCSD(T)-F12a/cc-pVDZ -F12//M06-2X/aug-cc-pVTZ level in order to confirm the catalytic effect of catalyst X ( $X = NH_3$ and HCOOH). As seen, beginning with  $H_2O_2 + HO$  reactants, five-membered ring (O2···H3-O3···H2-O1) complex IM1 has been formed with two weak hydrogen bonds involved. The stabilization energy of IM1 is 11.8 kcal·mol<sup>-1</sup>. After complex IM1, the reaction proceeded via Habstraction transition state TS1 to form the post-reactive complex IMF1. From an energetic standpoint, transition state TS1 was predicted to be 2.3 kcal·mol<sup>-1</sup> above the reactants, which was slightly different from the corresponding value (1.5 kcal·mol<sup>-1</sup>) obtained by our previous result. The complex IMF1 then dissociates to produce the final products  $H_2O + HO_2$ , which lies 31.7 kcal·mol<sup>-1</sup> below the energy of  $H_2O_2 + HO$  reactants.

- [1] G. L. Vaghjiani, A. R. Ravishankara and N. Cohen, J. Phys. Chem., 1989, 93, 7833-7837.
- [2] F. Atadinc, H. Günaydin, A. S. Özen and V. Aviyente, Int. J. Chem. Kinet., 2005, 37, 502-514.
- [3] R. R. Baldwin and R. W. Walker, J. Chem. Soc. Faraday T., 1979, 75, 140-154.
- [4] P. H. Wine, D. H. Semmes and A. R. Ravishankara, J. Chem. Phys., 1981, 75, 4390-4395.
- [5] R. J. Buszek, M. Torrent-Sucarrat, J. M. Anglada and J. S. Francisco, J. Phys. Chem. A, 2012, 116, 5821.
- [6] T. L. Zhang, X. G. Lan, Y. H. Zhang, R. Wang, Y. Q. Zhang, Z. Y. Qiao and N. Li, *Mol. Phys.*, 2019, 117, 516-530.



Fig. S2 Schematic potential energy diagrams for less favorable channels involved in HCOOH catalyzed  $H_2O_2 + HO \rightarrow HO_2 + H_2O$  reaction at the CCSD(T)-F12a/cc-pVDZ-F12//M06-2X /augcc-pVTZ level



Fig. S3 Optimized geometries of all complexes for the  $H_2O_2 + HO \rightarrow HO_2 + H_2O$  reaction with acidic (HCOOH) and basic (NH<sub>3</sub>) catalysts at the M06-2X/aug-cc-pVTZ level

**Table S2** Relative energies (( $\Delta E$ ), ( $\Delta E$  + ZPE)), enthalpies ( $\Delta H$ ) and free energies ( $\Delta G$ ) for the possible stable complexes between H<sub>2</sub>O<sub>2</sub> (or HO) and the catalyst *X* (*X* = NH<sub>3</sub> and HCOOH) at the CCSD(T)-F12a/cc-pVDZ-F12//M06-2X/aug-cc-pVTZ level

Species	$\Delta E(298 \text{ K})$ (kcal·mol <sup>-1</sup> )	$\Delta H(298 \text{ K})$ (kcal·mol <sup>-1</sup> )	$\Delta G(298 \text{ K})$ (kcal·mol <sup>-1</sup> )	$\Delta(E + ZPE)$ (298 K) (kcal·mol <sup>-1</sup> )
$H_2O_2 + NH_3$	0.0	0.0	0.0	0.0
$H_2O_2$ ····N $H_3$	-8.6	-6.9	0.8	-6.6
$HO + NH_3$	0.0	0.0	0.0	0.0
HO…NH3	-7.8	-6.3	1.1	-5.5
NH <sub>3</sub> ···HO	-1.6	-0.4	6.2	0.0
$H_2O_2 + HCOOH$	0.0	0.0	0.0	0.0
H <sub>2</sub> O <sub>2</sub> ···HCOOH	-12.1	-10.5	-0.5	-10.1
Н₂О₂…НСООНа	-9.6	-8.0	1.5	-7.8
H <sub>2</sub> O <sub>2</sub> …HCOOHb	-7.2	-5.6	2.9	-5.7
H <sub>2</sub> O <sub>2</sub> …HCOOHc	-4.8	-3.3	4.7	-3.5
HO + HCOOH	0.0	0.0	0.0	0.0
но…нсоон	-5.5	-4.1	4.4	-4.9
НО…НСООНа	-3.2	-2.1	4.6	-2.0

<i>T</i> /K	$K_{eq}(H_2O_2\cdots H_2O)$	$K_{eq}(H_2O_2\cdots NH_3)$	K <sub>eq</sub> (HO…NH <sub>3</sub> )	K <sub>eq</sub> (NH <sub>3</sub> ···HO)	K <sub>eq</sub> (H <sub>2</sub> O <sub>2</sub> ···HCOOH)
213	5.05×10 <sup>-23</sup>	2.01×10 <sup>-20</sup>	6.20×10 <sup>-21</sup>	1.22×10 <sup>-25</sup>	2.13×10 <sup>-18</sup>
230	3.20×10 <sup>-23</sup>	8.90×10 <sup>-21</sup>	3.36×10 <sup>-21</sup>	1.60×10 <sup>-25</sup>	5.05×10 <sup>-19</sup>
259	1.71×10 <sup>-23</sup>	2.88×10-21	1.43×10 <sup>-21</sup>	2.37×10 <sup>-25</sup>	6.80×10 <sup>-20</sup>
280	1.20×10 <sup>-23</sup>	1.49×10 <sup>-21</sup>	8.65×10 <sup>-22</sup>	3.04×10 <sup>-25</sup>	2.10×10 <sup>-20</sup>
290	1.03×10 <sup>-23</sup>	1.13×10 <sup>-21</sup>	7.00×10 <sup>-22</sup>	3.39×10 <sup>-25</sup>	1.28×10 <sup>-20</sup>
298	9.20×10 <sup>-24</sup>	9.20×10 <sup>-22</sup>	5.95×10 <sup>-22</sup>	3.69×10 <sup>-25</sup>	8.75×10 <sup>-21</sup>
Con.	7.05×10 <sup>3</sup> (100% RH)	65.50 (2900 ppbv) 0.23 (10 ppbv)	0.42 (2900 ppbv) 1.49×10 <sup>-3</sup> (10 ppbv) (1.35×10 <sup>-3</sup> ) <sup>a</sup>	2.62×10 <sup>-4</sup> (2900 ppbv) 9.2×10 <sup>-7</sup> (10 ppbv)	2.10 (High) 0.17 (Average)
300	8.95×10 <sup>-24</sup>	8.75×10-22	5.75×10 <sup>-22</sup>	3.76×10 <sup>-25</sup>	8.00×10 <sup>-21</sup>
310	7.85×10 <sup>-24</sup>	6.90×10 <sup>-22</sup>	4.79×10 <sup>-22</sup>	4.15×10 <sup>-25</sup>	5.20×10 <sup>-21</sup>
320	7.00×10 <sup>-24</sup>	5.55×10 <sup>-22</sup>	4.04×10 <sup>-22</sup>	4.57×10 <sup>-25</sup>	3.49×10 <sup>-21</sup>
<i>T</i> /K	K <sub>eq</sub> (H <sub>2</sub> O <sub>2</sub> ···HCOOHa)	K <sub>eq</sub> (H <sub>2</sub> O <sub>2</sub> ···HCOOHb)	K <sub>eq</sub> (H <sub>2</sub> O <sub>2</sub> ···HCOOHc)	K <sub>eq</sub> (HO····HCOOH)	K <sub>eq</sub> (HO····HCOOHa)
213	2.11×10 <sup>-20</sup>	7.10×10 <sup>-22</sup>	1.59×10 <sup>-23</sup>	5.05×10-23	1.72×10 <sup>-23</sup>
230	7.50×10 <sup>-21</sup>	3.67×10-22	1.14×10 <sup>-23</sup>	3.80×10 <sup>-23</sup>	1.55×10 <sup>-23</sup>
259	1.80×10 <sup>-21</sup>	1.49×10 <sup>-22</sup>	7.35×10 <sup>-24</sup>	2.57×10 <sup>-23</sup>	1.36×10 <sup>-23</sup>
280	7.80×10 <sup>-22</sup>	8.80×10 <sup>-23</sup>	5.80×10 <sup>-24</sup>	2.05×10-23	1.28×10 <sup>-23</sup>
290	5.50×10 <sup>-22</sup>	7.05×10 <sup>-23</sup>	5.25×10 <sup>-24</sup>	1.86×10 <sup>-23</sup>	1.25×10 <sup>-23</sup>
298	4.22×10 <sup>-22</sup>	6.00×10 <sup>-23</sup>	4.88×10 <sup>-24</sup>	1.74×10 <sup>-23</sup>	1.23×10 <sup>-23</sup>
Con.	0.10 (High) 8.00×10 <sup>-3</sup> (Average)	0.01 (High) 1.14×10 <sup>-3</sup> (Average)	1.17×10 <sup>-3</sup> (High) 9.25×10 <sup>-5</sup> (Average)	4.17×10 <sup>-5</sup> (High) 3.30×10 <sup>-6</sup> (Average) (4.90×10 <sup>-5</sup> ) <sup>a</sup>	2.95×10 <sup>-5</sup> (High) 2.34×10 <sup>-6</sup> (Average)
300	3.96×10 <sup>-22</sup>	5.80×10 <sup>-23</sup>	4.80×10 <sup>-24</sup>	1.71×10 <sup>-23</sup>	1.23×10 <sup>-23</sup>
310	2.93×10 <sup>-22</sup>	4.81×10 <sup>-23</sup>	4.43×10 <sup>-24</sup>	1.58×10 <sup>-23</sup>	1.21×10 <sup>-23</sup>
320	2.21×10 <sup>-22</sup>	4.05×10 <sup>-23</sup>	4.13×10 <sup>-24</sup>	1.47×10 <sup>-23</sup>	1.20×10 <sup>-23</sup>

**Table S3** Equilibrium constants (cm<sup>3</sup>·molecule<sup>-1</sup>) for the formation of two-body complexes between  $H_2O_2$  (or HO) and the catalyst X ( $X = NH_3$  and HCOOH) within the temperature range of 213-320 K

<sup>a</sup> The Value was from Ref (S. Mallick, S. Sarkar, P. Kumar and B. Bandyopadhyay, J. Phys. Chem. A, 2018, 122, 350-363.)

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<i>T</i> /K	$K_{eq}(R1)$	$K_{eq}(R_WM)$	$K_{eq}(R_AM1)$	K <sub>eq</sub> (R_AM2a)	$K_{eq}(R_AM2b)$	K <sub>eq</sub> (R_AM3a)
213	1.46×10 <sup>-11</sup>	2.47×10 <sup>-24</sup>	2.20×10 <sup>-17</sup>	8.20×10 <sup>-28</sup>	1.60×10 <sup>-21</sup>	1.05×10 <sup>-23</sup>
230	1.44×10 <sup>-12</sup>	1.77×10 <sup>-24</sup>	5.80×10 <sup>-18</sup>	1.06×10 <sup>-27</sup>	7.20×10 <sup>-22</sup>	7.95×10 <sup>-24</sup>
259	5.55×10 <sup>-14</sup>	1.09×10 <sup>-24</sup>	9.05×10 <sup>-19</sup>	1.50×10 <sup>-27</sup>	2.40×10 <sup>-22</sup>	5.40×10 <sup>-24</sup>
280	8.05×10 <sup>-15</sup>	8.10×10 <sup>-25</sup>	3.01×10 <sup>-19</sup>	1.84×10 <sup>-27</sup>	1.26×10 <sup>-22</sup>	4.33×10 <sup>-24</sup>
290	3.54×10 <sup>-15</sup>	7.15×10 <sup>-25</sup>	1.89×10 <sup>-19</sup>	2.00×10 <sup>-27</sup>	9.65×10-23	3.94×10 <sup>-24</sup>
298	1.91×10 <sup>-15</sup>	6.50×10 <sup>-25</sup>	1.33×10 <sup>-19</sup>	2.13×10 <sup>-27</sup>	7.90×10 <sup>-23</sup>	3.68×10 <sup>-24</sup>
300	1.65×10 <sup>-15</sup>	6.35×10 <sup>-25</sup>	1.22×10 <sup>-19</sup>	2.16×10 <sup>-27</sup>	7.50×10 <sup>-23</sup>	3.62×10 <sup>-24</sup>
310	8.05×10 <sup>-16</sup>	5.70×10 <sup>-25</sup>	8.15×10 <sup>-20</sup>	2.32×10 <sup>-27</sup>	5.95×10 <sup>-23</sup>	3.34×10 <sup>-24</sup>
320	4.11×10 <sup>-16</sup>	5.10×10 <sup>-25</sup>	5.60×10 <sup>-20</sup>	2.48×10-27	4.81×10 <sup>-23</sup>	3.10×10 <sup>-24</sup>
<i>T</i> /K	$K_{eq}(R_AM3b)$	$K_{eq}(R_FA1)$	K <sub>eq</sub> (R_FA2a)	$K_{eq}(R_FA2b)$	K <sub>eq</sub> (R_FA3a)	$K_{eq}(R_FA3b)$
213	3.33×10 <sup>-15</sup>	2.49×10-21	1.28×10-21	4.40×10 <sup>-15</sup>	3.57×10-23	1.55×10 <sup>-14</sup>
230	4.73×10 <sup>-16</sup>	4.50×10 <sup>-20</sup>	7.80×10 <sup>-22</sup>	6.40×10 <sup>-16</sup>	2.96×10-23	2.14×10 <sup>-15</sup>
259	3.09×10 <sup>-17</sup>	1.09×10 <sup>-20</sup>	3.93×10 <sup>-22</sup>	4.42×10 <sup>-17</sup>	2.34×10 <sup>-23</sup>	1.36×10 <sup>-16</sup>
280	6.15×10 <sup>-18</sup>	4.70×10 <sup>-21</sup>	2.64×10 <sup>-22</sup>	9.10×10 <sup>-18</sup>	2.06×10-23	2.67×10 <sup>-17</sup>
290	3.10×10 <sup>-18</sup>	3.30×10 <sup>-21</sup>	2.24×10 <sup>-22</sup>	4.68×10 <sup>-18</sup>	1.96×10 <sup>-23</sup>	1.35×10 <sup>-17</sup>
298	1.86×10 <sup>-18</sup>	2.53×10-21	1.98×10 <sup>-22</sup>	2.84×10 <sup>-18</sup>	1.89×10 <sup>-23</sup>	8.05×10 <sup>-18</sup>
300	1.64×10 <sup>-18</sup>	2.38×10-21	1.92×10 <sup>-22</sup>	2.52×10 <sup>-18</sup>	1.87×10 <sup>-23</sup>	7.10×10 <sup>-18</sup>
310	9.05×10 <sup>-19</sup>	1.75×10 <sup>-21</sup>	1.67×10 <sup>-22</sup>	1.41×10 <sup>-18</sup>	1.80×10 <sup>-23</sup>	3.92×10 <sup>-18</sup>
320	5.20×10 <sup>-19</sup>	1.32×10-21	1.47×10 <sup>-22</sup>	8.20×10 <sup>-19</sup>	1.74×10 <sup>-23</sup>	2.25×10-18

**Table S4** Equilibrium constants (cm<sup>3</sup>·molecule<sup>-1</sup>) for three-body complexes constituted by  $H_2O_2$ , HO and catalyst  $X(X = NH_3 \text{ and HCOOH})$  within the temperature range of 213-320 K



Fig. S4 Optimized geometries for  $NH_3$  catalyzed  $H_2O_2 + HO \rightarrow HO_2 + H_2O$  reaction at the M06-2X/aug-cc-pVTZ level

<sup>b</sup> Value was from the NIST chemistry Webbook (http://webbook.nist.gov/ chemistry. )



Fig. S5 Optimized geometries for HCOOH catalyzed  $H_2O_2 + HO \rightarrow HO_2 + H_2O$  reaction at the M06-2X/aug-cc-pVTZ level

° Value was from the NIST chemistry Webbook (http://webbook.nist.gov/chemistry.)

**Table S5** Relative energies  $((\Delta E), (\Delta E + ZPE))$ , enthalpies  $(\Delta H)$ , and free energies for the reactants, intermediate, and transition states involved in the H<sub>2</sub>O<sub>2</sub> + HO  $\rightarrow$  HO<sub>2</sub> + H<sub>2</sub>O reaction with catalyst *X* (*X* = NH<sub>3</sub> and HCOOH) at the CCSD(T)-F12a/cc-pVDZ-F12//M06-2X/ aug-cc-pVTZ level

Species	$\frac{\Delta E(298)}{(\text{kcal}\cdot\text{mol}^{-1})}$	$\Delta H(298)$ (kcal·mol <sup>-1</sup> )	$\Delta G(298)$ (kcal·mol <sup>-1</sup> )	$\frac{\Delta(E + \text{ZPE})(298)}{(\text{kcal} \cdot \text{mol}^{-1})}$
$H_2O_2 + HO$	0.0	0.0	0.0	0.0
IM1	-13.7	-12.5	-5.1	-11.8
TS1	2.6	0.9	9.0	2.3
IMF1	-35.4	-33.5	-28.2	-33.4
$H_2O + HO_2$	-32.0	-31.7	-32.9	-31.7
$H_2O_2 + H_2O + HO$	0.0	0.0	0.0	0.0
$H_2O_2\cdots H_2O + HO$	-7.1	-5.3	3.1	-4.7
IM_WM	-12.5	-9.5	7.0	-8.5
TS_WM	-6.4	-6.3	12.0	-4.5
IMF_WM	-52.7	-48.9	-31.0	-47.4
$2H_2O + HO_2$	-32.0	-31.7	-32.9	-31.7
$H_2O_2 + NH_3 + HO$	0.0	0.0	0.0	0.0
$H_2O_2$ ····N $H_3 + HO$	-8.6	-6.9	0.8	-6.6
IM AM1	-20.1	-17.1	-1.0	-16.1
TS AM1	-8.7	-8.3	8.6	-6.9
IMF AM1	-53.8	-50.2	-33.2	-49.1
$H_2O + HO_2 + NH_3$	-32.0	-31.7	-32.9	-31.7
$H_2O_2 + NH_3 + HO$	0.0	0.0	0.0	0.0
$H_2O_2\cdots NH_3 + HO$	-8.6	-6.9	0.8	-6.6
$HO\cdots NH_3 + H_2O_2$	-7.8	-6.3	1.1	-5.5
IM AM2	-10.5	-8.3	9.7	-6.5
TS AM2	-7.2	-5.5	12.0	-3.9
IM AM3	-16.4	-12.9	4.2	-11.8
TS AM3	-8.2	-9.0	8.6	-7.4
IMF AM3	-53.8	-50.2	-33.1	-49.1
$H_2O + HO_2 + NH_3$	-32.0	-31.7	-32.9	-31.7
$\frac{1}{H_2O_2 + NH_3 + HO}$	0.0	0.0	0.0	0.0
$H_2O_2\cdots NH_3 + HO$	-8.6	-6.9	0.8	-6.6
$NH_2 \cdots HO + H_2O_2$	-1.6	-0.4	6.2	0.0
IM AM4	-13.5	-10.9	5.5	-9.8
TS_AM4	-8.0	-6.2	11.4	-4.6
IM AM5	-17.4	-14 4	2.5	-13 3
TS_AM5	21.1	19.6	39.8	22.1
IME AM5	-53.0	-49.4	-31.9	-48.2
$H_2O + HO_2 + NH_3$	-32.0	-31.7	-32.9	-31.7
$\frac{1}{1} \frac{1}{1} \frac{1}$	0.0	0.0	0.0	0.0
$H_2O_2$ HCOOH + HO	-12.1	-10.5	-0.5	-10.1
IM FA1	-19.5	-16.8	1.6	-16.0
TS FA1	-10.7	-11.0	8.8	-9.5
IME FA1	-50.8	-47 7	-29.8	-47.3
$H_2O + HO_2 + HCOOH$	-32.0	-31.7	-32.9	-31.7
$\frac{H_2O + HO2}{H_2O_2 + HCOOH + HO}$	0.0	0.0	0.0	0.0
$H_2O_2$ ····HCOOH + HO	-12.1	-10.5	-0.5	-10.1
$HO$ ··· $HCOOH + H_2O_2$	-5.5	-4.1	4.4	-4.9
IM FA2	-18 3	-153	2.0	-14 7
TS FA2	-14 2	-12.3	62	-11.3
IM FA3	-19.8	-16.9	13	-16.2
TS FA3	-79	-8.6	10.2	-7 3
		5.0		

IMF_FA3	-40.9	-37.7	-22.8	-37.5
$H_2O + HO_2 + HCOOH$	-32.0	-31.7	-32.9	-31.7
$H_2O_2 + HCOOH + HO$	0.0	0.0	0.0	0.0
$H_2O_2$ ···HCOOH + HO	-12.1	-10.5	-0.5	-10.1
$HO$ ··· $HCOOH + H_2O_2$	-5.5	-4.1	4.4	-4.9
IM_FA4	-15.7	-13.0	4.2	-12.6
TS_FA4	-12.6	-10.4	8.5	-9.2
IM_FA5	-19.9	-17.1	0.8	-16.4
TS_FA5	19.6	16.1	37.2	18.4
IMF_FA5	-42.6	-39.6	-23.1	-39.4
$H_2O + HO_2 + HCOOH$	-32.0	-31.7	-32.9	-31.7

<i>T</i> /K	$k_{ m R\_WM}$	$k_{\rm R\_AM1}$	$k_{ m R\_AM2a}$	$k_{ m R\_AM2b}$	$k_{\rm R\_AM3a}$	$k_{\rm R\_AM3b}$
213	9.46×10 <sup>-12</sup>	1.11×10-9	2.71×10 <sup>-17</sup>	5.72×10 <sup>-10</sup>	5.13×10 <sup>-36</sup>	1.63×10 <sup>-27</sup>
230	8.48×10 <sup>-12</sup>	5.31×10 <sup>-10</sup>	5.13×10 <sup>-17</sup>	2.78×10 <sup>-10</sup>	1.20×10 <sup>-35</sup>	7.13×10 <sup>-28</sup>
259	7.34×10 <sup>-12</sup>	2.15×10 <sup>-10</sup>	1.23×10 <sup>-16</sup>	1.04×10 <sup>-10</sup>	6.34×10 <sup>-35</sup>	3.63×10 <sup>-28</sup>
280	6.82×10 <sup>-12</sup>	1.35×10 <sup>-10</sup>	2.06×10 <sup>-16</sup>	5.91×10 <sup>-11</sup>	2.49×10-34	3.54×10 <sup>-28</sup>
290	6.65×10 <sup>-12</sup>	1.13×10 <sup>-10</sup>	2.54×10 <sup>-16</sup>	4.68×10 <sup>-11</sup>	4.98×10 <sup>-34</sup>	3.92×10 <sup>-28</sup>
298	6.53×10 <sup>-12</sup>	9.95×10-11	2.98×10 <sup>-16</sup>	3.93×10 <sup>-11</sup>	8.84×10 <sup>-34</sup>	4.47×10 <sup>-28</sup>
300	6.51×10 <sup>-12</sup>	9.64×10-11	3.09×10 <sup>-16</sup>	3.75×10 <sup>-11</sup>	1.02×10 <sup>-33</sup>	4.63×10 <sup>-28</sup>
310	6.41×10 <sup>-12</sup>	8.39×10 <sup>-11</sup>	3.70×10 <sup>-16</sup>	3.06×10 <sup>-11</sup>	2.14×10 <sup>-33</sup>	5.81×10 <sup>-28</sup>
320	6.27×10 <sup>-12</sup>	7.43×10 <sup>-11</sup>	4.38×10 <sup>-16</sup>	2.55×10 <sup>-11</sup>	4.58×10 <sup>-33</sup>	7.69×10 <sup>-28</sup>
<i>T</i> /K	$k_{\rm R_FA1}$	$k_{\rm R_FA2a}$	$k_{\rm R_FA2b}$	$k_{\rm R_FA3a}$	$k_{\rm R_FA3b}$	
213	2.50×10-11	5.90×10 <sup>-13</sup>	3.58×10-6	6.11×10-32	2.65×10 <sup>-23</sup>	
230	5.48×10 <sup>-10</sup>	5.10×10 <sup>-13</sup>	6.64×10 <sup>-7</sup>	1.14×10 <sup>-31</sup>	8.24×10 <sup>-24</sup>	
259	1.80×10 <sup>-10</sup>	4.27×10 <sup>-13</sup>	6.84×10 <sup>-8</sup>	3.92×10-31	2.28×10 <sup>-24</sup>	
280	9.50×10 <sup>-11</sup>	3.95×10 <sup>-13</sup>	1.86×10 <sup>-8</sup>	1.07×10 <sup>-30</sup>	1.38×10 <sup>-24</sup>	
290	7.32×10 <sup>-11</sup>	3.87×10 <sup>-13</sup>	1.09×10 <sup>-8</sup>	1.78×10-30	1.22×10 <sup>-24</sup>	
298	6.07×10 <sup>-11</sup>	3.82×10 <sup>-13</sup>	7.29×10 <sup>-9</sup>	2.70×10-30	1.15×10 <sup>-24</sup>	
300	5.81×10 <sup>-11</sup>	3.81×10 <sup>-13</sup>	6.64×10 <sup>-9</sup>	3.00×10 <sup>-30</sup>	1.14×10 <sup>-24</sup>	
310	4.67×10 <sup>-11</sup>	3.78×10 <sup>-13</sup>	4.20×10-9	5.17×10-30	1.13×10 <sup>-24</sup>	
320	3.83×10-11	3.79×10 <sup>-13</sup>	2.76×10-9	9.05×10 <sup>-30</sup>	1.17×10 <sup>-24</sup>	

**Table S6** Calculated rate coefficients (cm<sup>3</sup>·molecules<sup>-1</sup>·s<sup>-1</sup>) for the  $H_2O_2 + HO \rightarrow HO_2 + H_2O$  reaction in the presence of catalyst  $X (X = NH_3 \text{ and } HCOOH)$  within the temperature range of 213-320 K

T/K	<i>k</i> t'(R_AM1) (10 ppbv)	<i>k</i> t'(R_AM1) (2900 ppbv)	<i>k</i> t'(R_AM2a) (10 ppbv)	<i>k</i> t'(R_AM2a) (2900 ppbv)	kt'(R_AM2b) (10 ppbv)	<i>k</i> t'(R_AM2b) (2900 ppbv)	<i>k</i> t'(R_AM3a) (10 ppbv)	<i>k</i> t'(R_AM3a) (2900 ppbv)	<i>k</i> <sub>t</sub> '(R_AM3b) (10 ppbv)	<i>k</i> t'(R_AM3b) (2900 ppbv)
280	5.25×10 <sup>-20</sup>	1.53×10 <sup>-17</sup>	7.97×10 <sup>-26</sup>	2.33×10 <sup>-23</sup>	1.33×10 <sup>-20</sup>	3.88×10 <sup>-18</sup>	9.65×10 <sup>-44</sup>	2.82×10 <sup>-41</sup>	2.80×10 <sup>-41</sup>	8.18×10 <sup>-39</sup>
290	3.20×10 <sup>-20</sup>	9.35×10 <sup>-18</sup>	7.18×10 <sup>-26</sup>	2.10×10 <sup>-23</sup>	8.18×10 <sup>-21</sup>	2.39×10 <sup>-18</sup>	1.41×10 <sup>-43</sup>	4.11×10 <sup>-41</sup>	3.32×10-41	9.70×10-39
298	2.29×10 <sup>-20</sup>	6.50×10 <sup>-18</sup>	6.85×10 <sup>-26</sup>	1.95×10 <sup>-23</sup>	5.84×10 <sup>-21</sup>	1.66×10 <sup>-18</sup>	2.03×10 <sup>-43</sup>	5.77×10-41	4.12×10-41	1.17×10 <sup>-38</sup>
300	2.02×10 <sup>-20</sup>	5.99×10 <sup>-18</sup>	6.49×10 <sup>-26</sup>	1.92×10 <sup>-23</sup>	5.18×10 <sup>-21</sup>	1.53×10 <sup>-18</sup>	2.15×10-43	6.35×10 <sup>-41</sup>	4.18×10 <sup>-41</sup>	1.24×10 <sup>-38</sup>
310	1.39×10 <sup>-20</sup>	3.99×10 <sup>-18</sup>	6.13×10 <sup>-26</sup>	1.76×10 <sup>-23</sup>	3.52×10-21	1.01×10 <sup>-18</sup>	3.55×10 <sup>-43</sup>	1.02×10 <sup>-40</sup>	5.78×10 <sup>-41</sup>	1.66×10-38
320	9.49×10 <sup>-21</sup>	2.76×10 <sup>-1</sup> 8	5.59×10 <sup>-26</sup>	1.63×10 <sup>-23</sup>	2.37×10 <sup>-21</sup>	6.90×10 <sup>-19</sup>	5.85×10 <sup>-43</sup>	1.70×10 <sup>-40</sup>	8.08×10 <sup>-41</sup>	2.35×10 <sup>-38</sup>
T/K	k <sub>t</sub> '(R_FA1) (Low,0.01 ppbv)	kt'(R_FA1) (High,10 ppbv)	<i>k</i> <sub>t</sub> '(R_FA2a) (Low,0.01 ppbv)	<i>k</i> t'(R_FA2a) (High,10 ppbv)	<i>k</i> <sub>t</sub> '(R_FA2b) (Low,0.01 ppbv)	<i>k</i> t'(R_FA2b) (High,10 ppbv)	<i>k</i> <sub>t</sub> '(R_FA3a) (Low,0.01 ppbv)	<i>k</i> t'(R_FA3a) (High,10 ppbv)	<i>k</i> <sub>t</sub> '(R_FA3b) (Low,0.01 ppbv)	<i>k</i> t'(R_FA3b) (High,10 ppbv)
280	5.19×10 <sup>-22</sup>	5.19×10 <sup>-19</sup>	2.16×10-24	2.16×10-21	9.90×10 <sup>-23</sup>	9.90×10 <sup>-20</sup>	5.83×10 <sup>-42</sup>	5.83×10 <sup>-39</sup>	7.38×10 <sup>-39</sup>	7.38×10-36
290	2.34×10 <sup>-22</sup>	2.34×10 <sup>-19</sup>	1.24×10 <sup>-24</sup>	1.24×10 <sup>-21</sup>	5.05×10 <sup>-23</sup>	5.05×10 <sup>-20</sup>	5.68×10 <sup>-42</sup>	5.68×10 <sup>-39</sup>	5.69×10 <sup>-39</sup>	5.69×10 <sup>-36</sup>
298	1.27×10 <sup>-22</sup>	1.27×10 <sup>-19</sup>	8.03×10 <sup>-25</sup>	8.03×10 <sup>-22</sup>	3.05×10 <sup>-23</sup>	3.05×10 <sup>-20</sup>	5.67×10 <sup>-42</sup>	5.67×10 <sup>-39</sup>	4.80×10 <sup>-39</sup>	4.80×10 <sup>-36</sup>
300	1.12×10 <sup>-22</sup>	1.12×10 <sup>-19</sup>	7.31×10 <sup>-25</sup>	7.31×10 <sup>-22</sup>	2.72×10 <sup>-23</sup>	2.72×10 <sup>-20</sup>	5.76×10 <sup>-42</sup>	5.76×10-39	4.67×10-39	4.67×10-36
310	5.82×10 <sup>-23</sup>	5.82×10 <sup>-20</sup>	4.72×10 <sup>-25</sup>	4.72×10 <sup>-22</sup>	1.59×10 <sup>-23</sup>	1.59×10 <sup>-20</sup>	6.45×10 <sup>-42</sup>	6.45×10 <sup>-39</sup>	4.27×10 <sup>-39</sup>	4.27×10 <sup>-36</sup>
320	3.07×10 <sup>-23</sup>	3.07×10 <sup>-20</sup>	3.04×10 <sup>-25</sup>	3.04×10 <sup>-22</sup>	9.33×10 <sup>-24</sup>	9.33×10 <sup>-21</sup>	7.26×10 <sup>-42</sup>	7.26×10 <sup>-39</sup>	3.96×10 <sup>-39</sup>	3.96×10-36

**Table S7** Effective rate coefficients  $(k_t)$  (cm<sup>3</sup>·molecules<sup>-1</sup>·s<sup>-1</sup>) for the H<sub>2</sub>O<sub>2</sub> + HO  $\rightarrow$  HO<sub>2</sub> + H<sub>2</sub>O reaction with basic (NH<sub>3</sub>) and acidic (HCOOH) within the temperature range of 280-320 K

Catalyst		280 K	290 K	298 K	300 K	310 K	320 K
	20% RH	5.2×10 <sup>16</sup>	9.6×10 <sup>16</sup>	1.5×10 <sup>17</sup>	1.7×10 <sup>17</sup>	2.9×10 <sup>17</sup>	4.1×10 <sup>17</sup>
	40% RH	1.0×10 <sup>17</sup>	1.9×10 <sup>17</sup>	3.1×10 <sup>17</sup>	3.4×10 <sup>17</sup>	5.8×10 <sup>17</sup>	9.4×10 <sup>17</sup>
H <sub>2</sub> O	60% RH	1.5×10 <sup>17</sup>	2.9×10 <sup>17</sup>	4.5×10 <sup>17</sup>	5.1×10 <sup>17</sup>	8.8×10 <sup>17</sup>	1.4×10 <sup>17</sup>
	80% RH	2.1×10 <sup>17</sup>	3.8×10 <sup>17</sup>	6.2×10 <sup>17</sup>	6.9×10 <sup>17</sup>	1.2×10 <sup>17</sup>	1.9×10 <sup>17</sup>
	100% RH	2.6×10 <sup>17</sup>	4.8×10 <sup>17</sup>	7.7×10 <sup>17</sup>	8.6×10 <sup>17</sup>	1.5×10 <sup>18</sup>	2.3×10 <sup>18</sup>
	0.1 ppbv	2.6×10 <sup>9</sup>	2.5×10 <sup>9</sup>	2.5×10 <sup>9</sup>	2.4×10 <sup>9</sup>	2.4×10 <sup>9</sup>	2.3×10 <sup>9</sup>
NH <sub>3</sub>	10 ppbv	2.6×10 <sup>11</sup>	2.5×10 <sup>11</sup>	2.5×10 <sup>11</sup>	2.4×10 <sup>11</sup>	2.4×10 <sup>11</sup>	2.3×10 <sup>11</sup>
	2900 ppbv	7.6×10 <sup>13</sup>	7.3×10 <sup>13</sup>	7.1×10 <sup>13</sup>	7.1×10 <sup>13</sup>	6.9×10 <sup>13</sup>	6.7×10 <sup>13</sup>
	High	2.6×10 <sup>11</sup>	2.5×10 <sup>11</sup>	2.4×10 <sup>11</sup>	2.4×10 <sup>11</sup>	2.4×10 <sup>11</sup>	2.3×10 <sup>11</sup>
НСООН	Average	2.0×10 <sup>10</sup>	1.9×10 <sup>10</sup>	1.9×10 <sup>10</sup>	1.9×10 <sup>10</sup>	1.8×10 <sup>10</sup>	1.8×10 <sup>10</sup>
	Low	2.6×10 <sup>8</sup>	2.5×10 <sup>8</sup>	$2.4 \times 10^{8}$	2.4×10 <sup>8</sup>	$2.4 \times 10^{8}$	2.3×10 <sup>8</sup>
H <sub>2</sub> SO <sub>4</sub>		3.9×10 <sup>8</sup>	3.8×10 <sup>8</sup>	3.7×10 <sup>8</sup>	3.7×10 <sup>8</sup>	3.6×10 <sup>8</sup>	3.4×10 <sup>8</sup>

**Table S8** Concentrations of  $X (X = H_2O, NH_3, HCOOH and H_2SO_4)$  (in molecule cm<sup>-3</sup>) within the temperature range of 280-320 K at 0 km altitude

The Value was from Ref (S. Sarkar, S. Mallick, Deepak, P. Kumar and B. Bandyopadhyay, Phys. Chem. Chem. Phys., 2017, 19, 27848-27858.)

**Table S9** Coordinates and geometrical structures for the reactants, pre-reactive complexes, transition states, post-reactive complexes and products involved in catalyst X ( $X = NH_3$  and HCOOH) assisted  $H_2O_2 + HO \rightarrow HO_2 + H_2O$  reaction at the M06-2X/aug-cc-pVTZ level

	(1) <b>4</b> 0010 <b>1</b> 0 <b>1</b> 0 <b>1</b>	<u> </u>					
		Coordinate			Frequer	ncy	Structure
$H_2O_2$							
							(0.95)
0	0.00000000	0.71154400	-0.05812700				0.96
Н	0.78644300	0.90348800	0.46501400	373.20	1044.11	1355.52	142 5 5 0
0	0.00000000	-0.71154400	-0.05812700	1464.95	3837.21	3838.44	(1.48) 18 94.5
Н	-0.78644300	-0.90348800	0.46501400				JJ - 22
но							
110				1			
0	0.0000000	0.0000000	0 10700000				H
0	0.00000000	0.00000000	0.10/99800	3744.37			0.97
п	0.00000000	0.76273400	-0.80398300				(0.97)
HO <sub>2</sub>							
							(0.97) 0.97
0	0.05507400	-0.60010800	0.00000000				<b>01</b> 7- <sup>119</sup>
Н	-0.88118600	-0.86505400	0.00000000	1225.01	1462.80	3690.48	1.31 (1.33) 185,8
0	0.05507400	0.70824000	0.00000000				02 0
H <sub>2</sub> O							
0	0.00000000	0.00000000	0.11635900	1000-	2071		0.96
H	0.00000000	0.76273400	-0.46543500	1616.15	3871.58	3975.57	
н	0.00000000	-0.76273400	-0.46543500				(104.5)
NH							
11113							
N	0.00002600	0.00002600	-0 11246200				H2
Н	-0.56199200	0.75354600	0.26242100	1034 34	1660 37	1661 74	107.1
н	0.93368900	0 10967600	0 26246600	3508 74	3631.81	3638.12	N (IIIII)
Н	-0.37188100	-0.86340400	0.26234800	5500.71	2021.01	5050.12	H1 1.01 H3
	0.57100100	0.000 10 100	0.2025 .000				(1.01)
нсос	ЭН						
C	0.13498200	0.39878300	-0.00000100			1054.00	(1.34)
H	0.11130600	1.49338900	0.00002400	645.75	676.77	1074.92	(0.97) 01 1.34 125.0
0	1.12637700	-0.26486600	-0.00007800	1159.99	1317.64	1409.70	0.97
0	-1.11039500	-0.08900800	0.00007000	1869.19	3120.09	3791.33	H1 1.19
Н	-1.04905500	-1.05509200	0.00004600				(1.20)
H,O,	···NH3						
0	0.88714000	0.77306500	0.00826100	1			
0	1 22028000	0.77500500	0.00820100	60.20	06.96	207.80	
U U	0.00051100	-0.00/14/00	-0.110/9000	238 24	204.88	207.80	1.85 H3
н	1 70982200	-0.75728200	0.08490800	805 77	1037.65	1083.02	01 N-H2
N	-1 77359500	-0.05618800	0.02027800	1373.96	1575.41	1654 79	159.2
н	-1 41706300	-0.96824900	-0 24227100	1659.96	3419 71	3498.60	HE
н	-2 37903000	0 26444400	-0 72444600	3617.01	3632.93	3847 12	2.67
н	-2 34029500	-0 17188800	0.85028200	5017.01	5052.75	5047.12	
HOW	<u>2.5 1025500</u>	0.17100000	0.05020200				
но…	NH3						
0	-1.63607200	0.00002000	0.00000500		<b></b>		N7 H2
H	-0.64793100	0.00074400	0.00002700	205.86	215.26	227.96	A
	1.26201500	0.00029000	0.00000700	609.57	746.91	1101.28	1.91 H3
	1.63291400	-0.48603000	-0.80/00100	1657.89	1658.23	3421.11	0.99 H4
	1.63324700	-0.45/89900	0.82315100	3501.26	3621.82	3624.48	<b>–</b>
н	1.03024200	0.94099400	-0.01020/00				
NH <sub>3</sub> …	но						
0	-1.37047200	-0.09049300	-0.00000200				a 26 LL2
Н	-1.34904800	0.88052400	0.00022400	129.12	161.62	263.61	2.50
Ν	1.32844400	-0.05387500	-0.00007700	319.84	373.93	963.28	
Н	0.82538600	-0.36848200	0.81946100	1644.35	1652.56	3506.10	2.30 98.3
Н	0.82493000	-0.36729500	-0.81978900	3638.91	3650.31	3756.60	H9 H1
Н	1.36339500	0.95632100	0.00065300				
H <sub>2</sub> O <sub>2</sub> ··	••нсоон						
0	1.55584000	0.69661000	0.13281900				
ŏ	1.73992300	-0.65781100	-0.26179400	75.77	162.03	189.64	
Ĥ	0.84669000	-1.02544900	-0.09887800	208.41	254.68	357.11	01 13.1.8204
C	-1.61073800	-0.12441600	0.00431400	682.05	706.19	910.57	160.8
Н	-2.70341600	-0.14075900	-0.04153800	1043.44	1095.07	1252.68	
0	-0.94617700	-1.11693300	0.17563100	1369.79	1400.60	1435.54	H402 168.7
0	-1.13719200	1.09317100	-0.14785100	1555.16	1808.67	3135.61	1.76 11 03
Н	-0.15362300	1.07050600	-0.07639500	3379.09	3545.07	3821.65	- 🖤
Н	1.97562300	0.72189500	1.00048500				
Hana	··НСООН»						
202							

0	1 38408000	0 13909100 0 4	59856100	
ŏ	1.87547100	-0.17417000 -0	60242000	73 57 115 02 163 43
U U	2 76075400	0.20600600 0	57514200	102 82 222 06 261 40
п	2.70073400	0.20009000 -0.	.3/314200	193.82 222.90 201.49 1.90 1.20
	-1.00885100	0.05150400 -0	0.17420800	083.93 /31.48 82/.12
Н	-2.63246/00	-0.06303800 -	0.54329200	
0	-1.06660400	1.12035300 -0	0.05227700	1381.43 1435.73 1501.96
0	-1.07371900	-1.12175300 0	0.11180400	1820.45 3126.70 3544.13
H	-0.15486200	-0.99140400 0	0.42294600	3608.98 3836.78
Н	0.72574500	0.83235900 0.4	49545500	
по	ПСООШ			
$H_2O_2$	-нсоонь			
0	-1.86089400	-0.81414000 0	0.11985700	
0	-2.04315800	0.53933900 -0	).28694400	48.59 70.13 130.07
Н	-1.17878700	0.91765500 -0	0.04818100	142.82 212.37 261.94
C	1.11575900	-0.14804700 -0	0.08924200	646.04 663.01 688.14
Н	0.49652700	-0.98233300 -0	0.42710800	1040.96 1094.6 1180.61
0	0.68405200	0.91828500 0.2	25856300	1333.58 1377.9 1419.56
0	2.40845400	-0.45580700 -0	0.10303800	1523.22 1827.7 3163.83
Н	2.90660100	0.31543100 0.2	20517500	3648.86 3782.81 3847.92
Н	-2.42652700	-0.86388600 0	0.89805400	
Н.О	··HCOOHe			
n <sub>2</sub> O <sub>2</sub>		0.0155500	12122000	1
0	-1.84107100	-0.817/5500 0	0.13133900	40.04 (0.64 115.05
0	-2.09715500	0.51458100 -0	0.30052100	49.84 60.64 115.26 H1
H	-1.25012200	0.93851800 -0	0.09870900	125.07 176.00 249.22
C	1.29461400	-0.28553000 -0	0.08176200	534.54 646.88 655.63
Н	0.52958500	-1.03873600 -0	0.28846900	1043.31 1083.28 1138.60 152.5
0	2.47410200	-0.44608000 -0	0.10402200	1290.81 1376.40 1427.71
0	0.70794300	0.89417600 0.2	21966100	1501.95 1880.10 3156.23
Н	1.40843900	1.53851400 0.3	39701900	3741.16 3792.45 3841.16
Н	-2.40613600	-0.88449900 0	0.90907300	
но…	нсоон			
0	2 02456200	0.04244200 0	00002400	
	-2.02430300	0.04344200 -0	0.00003400	192.22 192.57 205.69
H	-1.40220800	-0./18/4400 -	0.00004600	
	1.13252600	-0.0946/000 -0	0.00005400	
Н	2.22563700	-0.05031300 -0	0.00025100	
0	0.51081400	-1.12601500 0.	.00005800	
0	0.60754600	1.11894800 0.0	00003000	3130.91 3531.54 3591.88
H	-0.36896200	1.04608200 0.	.00018400	
но…	НСООНа			
0	2 56597000	-0 27267900 -0	00002600	236
й	1.81621500	0.35782000 0.0	00005300	41.85 71.59 189.22
C	-0.63058700	-0.22076600 0.0	00003800	41.03   11.09   109.22   01   178.25   04
u u	0.12053200	1 10357300 0	00003800	684 12 1082 41 1185 40
	-0.0589/300	0.83/87300 0	00001300	
	1 05125100	0.35487500 0.	0.0001300	2154 01 2610 22 2771 21 2.23 Q3
U U	-1.93123100	0.52516200 0	0.00002000	5154.91 5010.25 5771.51
п	-2.34933700	0.52510500 -0	0.00009100	
IM1				
0	-0.95522900	-0.73526400 0	0.01828600	
Н	-0.02774900	-0.97402600 -	0.13811700	179.12 196.21 223.65
0	-0.86558300	0.68416000 0	.09032400	274.29 432.39 566.24
0	1.84145000	-0.02945500 -0	0.03015800	1040.23 1369.77 1512.90 1.42 75.4
H	-1.33684200	0.95242300 -0	0.70684500	3642.06 3728.66 3831.80
Н	1,19948700	0.66607000 0.2	21734600	2.07
T61				
151				
0	-1.24106100	-0.45309600 -	0.14211000	
H	-1.62022800	-0.60532400 0	0.73199600	-1493.30 135.36 238.40
0	-0.48707800	0.70571500 0.	.06782000	362.52 404.19 688.58
0	1.68977700	-0.11037900 -0	0.02767000	1068.87 1366.07 1518.61
H	0.45016300	0.43890100 -0.	.28222200	1820.29 3778.57 3828.05
H	1.47695900	-0.97149700 0.	.36590600	
IMF1				
0	1.20764500	-0.55952100 0.	.00291800	211
Н	2.17920000	-0.61549000 0.	.02280300	43.10 119.05 151.14
0	0.92203300	0.71591900 -0	.00671400	158.58 272.84 410.06
õ	-2.02690500	-0.01271000 0	0.00965200	1259.89 1457.48 1643.40
Ĥ	-1.16455000	0.41516100 0	.00030700	3669.96 3834.54 3953.88
H	-1.83683400	-0.94917300 -	0.06995700	3.07
		0.7 1717000 -		
I IM A	.IVI I			

0	1.24635200	0.48811400 -0.701179	00
Ĥ	0.31172100	0.61133300 -0.92047	00 9749 11291 13280 > 2.14
0	1 21177200	0.41010700 0.717476	10 156 22 202 22 217 66
0	0.25005100	1 95279500 0.0660	
0	-0.33093100	-1.852/8500 -0.0669	
н	1.06259900	-0.53898200 0.850422	00 563.03 650.82 764.52
Н	-0.88842200	-1.03713100 -0.2005	400   1040.45 1130.49 1434.87   🔥 " 🕮 🖓 🍟
Ν	-1.68512600	0.77471700 0.01341	00 1455.63 1656.14 1669.38
Н	-1.97981800	1.50244300 -0.62699	2.21
н	-1 05324700	1 19291400 0 690919	00 361145 374158 375638 H3
н	-2 51433500	0.48292200 0.51795	00
	- <u>2.51</u> +55500	0.40292200 0.51795.	
0	-0.88705500	_0.89193200 _0.5243	700
0	1 22221500	0 15045700 0 5613	2400 975 11 162 10 240 05
U U	-1.52521500	-0.13943700 0.3013	3400 $-375.11$ $103.10$ $240.03$
н	-0.1/838500	-1.4/136800 -0.131/	500 270.25 306.41 364.62 100.5 H5
0	0.02447500	1.61052800 -0.23243	100 464.21 513.67 577.92
Н	-0.74098500	0.98946300 0.2803	1900 709.46 727.11 870.18
Н	0.79769700	1.01977200 -0.17912	000 1070.61 1155.82 1222.46
Ν	1.72813600	-0.43522800 0.07095	600 1494.56 1684.50 1719.38 02 02
Н	1.02716800	-0.43768600 0.80913	600 1756.89 3323.65 3429.54
н	2 59748300	-0 11407800 0 50696	000 3454 33 3511 98 3596 62
н	1 88643400	-1.41261300 -0.21869	
	1.000 15 100	1.11201300 0.2100)	
IMF	AMI		
0	-1.64897900	0.02409200 0.021218	00
H	-0.89957000	0.73221400 0.013973	00   43.28 99.66 142.55   7
0	-1.03807100	-1.12643000 -0.0208	600 162.74 201.14 231.46
0	1,78508800	-0.83382000 -0.00789	300 344.92 349.60 403.13
н	0 84884700	-1.09586100 _0.01713	200 565 78 601 30 1036 63
н	2 20622200	-163438500 0115500	00 1187 41 1316 61 1632 26 02
N	2.27033200	1 60240100 0.113380	
	0.40354400	1.09249100 -0.003904	
H	0.48866500	2.23952/00 -0.851673	
Н	1.20709100	1.06782900 0.047901	0 3623.20 3662.27 3950.80
Н	0.44951900	2.33250500 0.779162	0 0
IM_4	AM2		
Ν	1.00904500	1.44344100 -0.172170	00
Н	1.21073400	2.07911300 0.596363	0 -14.68 65.48 84.79 03
н	0.00320000	1 24394800 -0 151879	00 144 04 168 43 321 11
н	1 22723200	1 94238900 -1 035469	00 374 52 478 17 558 85
0	1 70208500	0.76152700 0.5106	200 - 700 52 - 746.06 - 852.27
	-1./9398300	-0.70132700 -0.5190	
Н	-0.82399700	-0.90028400 -0.6537	
0	-1.77/82000	0.23393500 0.504120	00 1500.36 1662.09 1677.91 H5
0	2.45658300	-1.19631400 0.157085	00 3199.73 3381.83 3495.66 <b>022</b>
Н	2.00965400	-0.29981200 0.047969	00 3504.90 3548.72 3620.69
Н	-1.76836000	-0.37819800 1.26937	300
TS_A	AM2		
N	1 32621200	1 35207400 -0.091720	00
ц	1.52021200	1.93228400 0.714400	41 50 52 60 70 62
	0.20470900	1.22700200 0.12214	
H	0.304/9800	1.33/90800 -0.183144	
Н	1./055/400	1.82653800 -0.912798	00 350.79 417.43 502.02
0	-1.39925300	-0.57600400 -0.5691	900 558.70 582.11 911.60
Н	-0.46573600	-0.67898300 -0.3254	500   1030.06 1140.57 1436.16   💯 👯 1
0	-1.85365400	0.38700000 0.386589	00   1561.74 1663.82 1670.36   🚬 🏹 🖓 🛺
0	1.68342500	-1.43549500 0.196113	00   3146.26 3375.52 3384.10   🖽 🧥 2.43 🖓 🖬 🖤 🖤
Н	2.23697500	-0.60176100 0.111759	00 3493.33 3550.44 3718.41
Н	-2.05809200	-0.28450700 1.12892	100
ТМ	4M3		I
	_1 38184800	0.12501100 0.665154	00
	-1.30104000	0.12301100 0.003130	
	-1.203/6900	-0.00581000 -0.5132	800 32.05 80.59 105.11 156 (1 225.41 252.61
H	-0./6265700	0.85275500 0.458822	00 156.61 225.41 253.61
H	-2.09054100	-0.47560100 -0.9691	400 277.23 284.84 369.27 He He He
N	1.66050500	-0.91399300 0.108710	00   635.77 700.14 978.54   🧥 🦾
Н	0.76269200	-1.32860900 -0.12410	400   1041.36 1132.41 1375.70   🤎 💆 🛁
Н	1.86679500	-1.15462800 1.07034	00   1499.76 1649.19 1662.41   🚬 📥 📃 💦 🕮
Н	2.36795300	-1.34427300 -0.47302	200 3097.90 3480.66 3555.53 🛛 🗳 😡 🖓 👘
0	0.77008200	1.67355900 -0.22482	00 3596.56 3628.42 3840.80
Н.	1,23650100	0.78622800 -0.140530	00
TS 4			
1 10 1	AM3		
0	-1 26627500	0.06992800 0.50502	00
0	-1.26627500 -1.16049300	0.06992800 0.595024	00
0 0 н	AM3 -1.26627500 -1.16049300 -0.75068900	0.06992800 0.595024 -0.95649200 -0.3426 0.89420300 0.137502	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
0 0 Н	AM3 -1.26627500 -1.16049300 -0.75068900 -1.85573000	0.06992800 0.595024 -0.95649200 -0.3426 0.89420300 0.137592 -0.75376200 0.0915	00 '400 -1912.93 45.84 105.50 00 141.63 202.68 239.29 000 251.77 315.98 394.60
O O H H	-1.26627500 -1.16049300 -0.75068900 -1.85573900	0.06992800         0.595024           -0.95649200         -0.3426           0.89420300         0.137593           -0.75376200         -0.9815           0.5150100         0.74220	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
O O H H N	AM3 -1.26627500 -1.16049300 -0.75068900 -1.85573900 1.88116900 1.09042425	0.06992800         0.595024           -0.95649200         -0.3426           0.89420300         0.137592           -0.75376200         -0.9815           -0.59150100         0.074392           -0.1012000         0.0174392	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
O O H H N H	AM3 -1.26627500 -1.16049300 -0.75068900 -1.85573900 1.88116900 1.08940400	0.06992800         0.595024           -0.95649200         -0.3426           0.89420300         0.137592           -0.75376200         -0.9815           -0.59150100         0.074392           -1.21135900         -0.06543	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
O O H H N H H	AM3 -1.26627500 -1.16049300 -0.75068900 -1.85573900 1.88116900 1.08940400 2.17941700	0.06992800         0.595024           -0.95649200         -0.3426           0.89420300         0.13759           -0.75376200         -0.9815           -0.59150100         0.07439           -1.21135900         -0.06543           -0.68857700         1.036860	00 400 -1912.93 45.84 105.50 00 141.63 202.68 239.29 000 251.77 315.98 394.69 00 525.59 830.04 971.59 300 1084.58 1110.08 1288.73 00 1376.86 141.846 1649.38 111 1288.73 1376.86 141.846 1649.38 111 1288.73 12988 1298 1298 1298 1298 1298 1298 1298 1298 1298 12
О О Н Н Н Н Н Н	AM3 -1.26627500 -1.16049300 -0.75068900 -1.85573900 1.88116900 1.08940400 2.17941700 2.63800500	0.06992800         0.595024           -0.95649200         -0.3426           0.89420300         0.137592           -0.75376200         -0.9815           -0.59150100         0.074392           -1.21135900         -0.06543           -0.68857700         1.036866           -0.91083100         -0.51631	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
О О Н Н Н Н Н Н О	AM3 -1.26627500 -1.16049300 -0.75068900 -1.85573900 1.88116900 1.08940400 2.17941700 2.63800500 0.24400700	0.066992800         0.595024           -0.95649200         -0.3426           0.89420300         0.137592           -0.75376200         -0.9815           -0.59150100         0.074392           -1.21135900         -0.06543           -0.68857700         1.036866           -0.91083100         -0.51631           1.61776100         -0.243322	00 400 -1912.93 45.84 105.50 00 141.63 202.68 239.29 000 251.77 315.98 394.69 00 525.59 830.04 971.59 300 1084.58 1110.08 1288.73 00 1376.86 1418.46 1649.38 100 1663.06 3220.46 3486.95 00 3602.55 3631.31 3794.75

DO	13.60				
IMF_	_AM3		1	-	
0	1.78508000	-0.83386600 -0.00776700		H6	
Н	0.84882800	-1.09584600 -0.01757600	44.09 100.24 142.57		
Н	2.29613600	-1.63435400 0.11705800	163.25 201.20 231.46	03	
0	-1.03811700	-1.12637700 -0.02159500	344.92 349.63 403.20	88.7	
0	-1.64896300	0.02412600 0.02192500	565.70 601.56 1036.59	1.99	
H	-0.89954500	0.73223800 0.01444200	1187.39 1316.58 1632.29		
N	0.40359100	1.69245800 -0.00410000	1638.63 1666.16 1702.02		
H	0.44920900	2.33370500 0.77797600	2610.63 3449.64 3575.68		
п	0.48913900	2.23813200 -0.83209300 1.06783700 0.04898600	3023.21 3002.20 3930.09	1.62	
п	1.20708900	1.00785700 0.04898000			
	AM4		1		
0	0.92862500	-1.34090100 -0.23364700	20.17 01.12 120.40	1.77	
0	-0.38560800	-0.89864900 0.16621500	39.17 91.12 128.40	NH2	
H	1.43334500	-0.4/094100 $-0.146/3000$	143.32 165.68 275.39		
N	1 06030800	1 20539600 0.3693700	616 15 709 80 973 41	HE 02	
н	1 10819200	1 73890800 -0 09008100	1001.60 1152.21 1345.46	5.04	
Н	2.63379100	1.52965800 -0.66640800	1624.16 1667.70 1672.72	2.04	
Н	2.34306900	1.45524100 0.94925600	3058.08 3408.24 3417.81	He	
0	-2.88604100	0.79286900 -0.08041200	3525.91 3554.59 3896.75		
Н	-2.04632800	0.25209300 -0.11414700		<b>9</b>	
TS_A	M4				
0	-1.77760200	-0.42289000 -0.08748000		бн.	
0	-0.52755900	-1.09102100 -0.00093700	-74.69 44.16 136.85	2.06	
Н	-1.50318600	0.51628400 0.08266300	157.95 179.61 192.78		
Н	-0.50874100	-1.37625500 0.96853400	322.26 356.90 407.58	H5 145.2 84.3	
0	2.21890600	-0.62029800 -0.04634400	543.38 736.71 863.36	2.92	
H	1.41104600	-1.18228100 -0.10315300	1051.66 1114.47 1499.21	N /5	
N	0.07073800	1.84330600 0.08013100	1540.52 1653.00 1668.44	97	
H	0.94101700	1.41/96900 -0.23619000	3235.96 3407.43 3449.34	HE	
H U	0.31426100	2./0491200 0.55614/00	3560.25 3591.64 3598.51	03	
	-0.45952700	2.08989000 -0.75082500			
	1 25(50000	1 2701 4100 0 10 440 500		1	
N	1.25650800	-1.3/014100 0.10449500	45.95 06.00 100.01	H3	
п	1.548/9000	-1./5138/00 0.99545500	45.85 96.25 122.21	H4 1.77 N H2	
п	1.69184400	-0.43777300 -0.00347200	278 26 302 55 405 18		
0	-1 39701300	-0.73067600 -0.28611700	447 24 661 86 906 76	HS	
н	-0.46611000	-1.04087600 -0.12122600	1043 24 1136 46 1365 24	<u> </u>	
0	-1.32679500	0.61882100 0.16353400	1614.10 1653.87 1663.09		
0	1.26261500	1.71106100 -0.11269900	3197.83 3479.61 3558.14	Н6 2.21	
Н	0.31961200	1.43296800 -0.08866300	3596.37 3625.90 3842.05	03	
Н	-1.82436100	0.59024500 0.98750400			
TS_A	M5				
Ν	1.38678000	-0.97400100 0.11261500		на	
Н	1.90910900	-1.27139400 0.92568100	-1762.73 155.55 222.28	1.13	
Н	1.49587600	0.48898200 -0.14733500	240.79 307.04 365.47	1.44 H4 N. H2	
H	1.71927100	-1.44796700 -0.71813600	445.74 565.68 596.92	147.6	
0	-1.0398/100	-0.88956/00 -0.32954400	/15./9 /53.93 822.53	H5	
Н	0.2/153600	-1.09318600 0.2306/500	1195.26 1242.05 13/4.30	<b>140.7 H1</b>	
	-1.55515900	1.67542700 -0.05727500	1545.55 1556.70 1598.18	106.6	
Н	-0 07784600	1 52000300 -0 55677200	3538 63 3643 03 3821 43	.93	
H	-1.74351900	0.07640600 1.10847600	5556.05 5045.05 5021.45	-03	
IMF	AM5		•	-	
N	1 38678000	-0.97400100 0.11261500		<b>.</b>	
H	1.36078000	-1.27139400 0.92568100	69.85 124.01 137.14	H3	
Н	1.40554988	0.72600159 0.35705823	175.18 243.60 255.36		
Н	1.71927100	-1.44796700 -0.71813600	286.05 337.98 381.27		
0	-1.03987100	-0.88956700 -0.32954400	577.61 848.17 926.53	93.0 1.77	
Н	0.39093290	-0.99965973 -0.06051388	1121.96 1303.41 1628.93	02	
0	-1.35515900	0.28228600 0.18295700	1641.30 1669.11 1676.99	10 <sup>3</sup> .9 H	
0	0.99423517	1.59713616 0.43445141	3033.20 3229.62 3469.00		
H	0.03635947	1.46865649 0.43663497	3591.88 3632.35 3930.19	H5 1.61	
H H	-2.30979096	0.37578268 0.03860952			
IM_FA1					
0	0.98457400	-1.15247200 -0.48798900	62.54 103.93 135.85		
0	1.1/4/0300	-1.04694200 0.91651400	155.58 191.57 217.18	1.99. 44 65	
н С	0.310/0300	-0.37243800 1.16287600 0.38659100 0.08974000	<u>460 31 564 72 600 50</u>	73.2	
н	-1./3043/00	0.30037100 0.089/4900	728 24 1020 67 1040 55	1.98	
0	-0.86118500	0.94496300 0.68879400	1108 63 1287 46 1412 02	1.96 03	
ŏ	-1.62280300	-0.68072900 -0.64837800	1432.83 1450.80 1496.28	📩 🔉 🏊 🖑	
Ĥ	-0.66248700	-0.95449400 -0.67310400	1780.66 3119.42 3152.72		
Н	1.48799900	-0.38541700 -0.81589500	3606.04 3651.17 3666.69		

0	1.71653500	1.56206600	-0.50746000			
п	0.80039000	1.03/22800	-0.02492700			
	FAI	0.50100000	0.64650400			
0	-1.23543600	0.58199900	-0.64650400	-1814 76 66 03 105 55		
H	-0.50661800	0.93890200	1.03048900	152.06 186.53 213.53	2.22	
C	1.79202500	-0.10708500	0.15251000	227.46 260.04 399.69	74.8	
H	2.85505700	-0.35551000	0.21506600	452.80 645.25 699.28	05 ····	
0	1.03582400	-0.2118/000	-1 04280200	1099.85 1263.69 1363.11	03	
Ĥ	0.48142600	0.47801600	-1.06144200	1405.50 1433.70 1502.86		
Н	-1.60042800	-0.40870800	-0.50387000	1685.35 1791.13 3146.68	1.77	
	-1.31074700	-1.65090800	-0.16011600	3341.69 3588.78 3725.75		
	-0.00112900	-1.34292400	0.55850900			
0	1.42386100	-0.78711200	-0 72364600			
0	1.51198600	-0.84493200	0.57358200	83.51 93.55 116.01		
H	0.56579500	-0.67776100	0.90725100	139.03 139.52 185.36		
C	-1.64038200	-0.18119800	0.11876200	208.57 225.52 253.10	01 1.58 H	
H	-2.69906000	0.07843700	0.18123800	286.75 358.29 722.34 836.44 027.15 1008.72	<b>* (3)</b> <del>* * * 63</del> <b>05</b>	
0	-0.97364700	-0.40937300	-1 10975300	830.44 927.13 1098.72 1291 57 1319 54 1419 81	нз	
H	-0.23445400	-0.41294500	-1.10970500	1468.71 1625.39 1658.99	02 H2 04 2.68	
Н	1.33637700	1.87705700	-0.46622900	1772.65 2858.10 3163.67	1.74	
0	0.51336400	2.02800700	0.00580100	3265.83 3863.25 3963.04		
H	0.76964200	2.15533400	0.92220500			
IM_	FA2					
0	2.40585100	-0.03204800	0.20506300	42 21 40 25 72 45		
H	0.96747200	-1.17900100	-0.16015900	128.03 175.59 202.24	LIN 05	
C	-0.72687800	0.86239400	-0.06565300	231.71 253.77 373.51	1.95	
Н	-1.67717400	1.39695800	-0.14829000	401.80 562.86 656.86	A H3	
0	-0.67089500	-0.34455200	0.05962900	714.98 939.69 1042.78		
н	0.30764900	1.65895200	-0.11503800	1423 03 1444 24 1543 73		
Н	2.75861200	-0.26193000	1.07276600	1779.22 3154.62 3336.31	1.73 H1 03	
0	-3.50916200	-0.67501000	0.07471600	3591.57 3624.60 3822.82		
Н	-2.54989200	-0.86999100	0.09169100			
TS_I	FA2					
0	0.25353100	1.87980100	0.20203500	<i></i>		
	1.38119700	1.21452400	-0.35346000	-66.64 52.19 /4.04 145.85 152.47 101.20	Н	
C	-1.66430300	-0.88008500	-0.03840500	197.68 225.09 296.82	2.09 1.95	
Н	-2.53237600	-1.53938400	-0.13086700	333.34 516.00 563.44	2.35	
0	-0.53377300	-1.29065000	0.09812500	698.24 930.82 1045.76		
0	-2.00246000	0.38689100	-0.09172300	1092.63 1261.64 1378.75	🜱 🦾 на	
Н	0 59584900	2.21545300	1 04051800	1792 28 3143 58 3346 54		
0	2.22674700	-1.53078800	0.06640900	3635.93 3652.60 3822.58	1.72 1.72	
Н	1.31711200	-1.89152500	0.09036900			
IM_I	FA3					
0	-1.12029800	-1.05448000	0.56600600			
0	-1.63026800	-0.78236600	-0.73510100	52.82 67.33 91.29	05	
	-1./8039300 1.93962900	0.18131400	-0.03199100	114.10 195.25 197.90 223.46 250.78 315.08	8 10.7.2	
Н	3.00581100	0.20875600	-0.35354300	481.94 572.55 686.66	13	
0	1.23919100	1.12570000	-0.01809800	809.59 888.41 1045.43	<b>1</b>	
0	1.55615300	-1.09627700	0.04686100	1094.54 1252.94 1342.43	🏀 🙆 🙀	
н	-1 79208400	-1.13928100	0.25548800	1396.49 1433.10 1503.69 1813 38 3132 48 3426 31	1 5200 Htt	
0	-1.44425900	1.79040900	0.17840200	3484.66 3569.53 3839.66	H	
Н	-0.47022600	1.62978400	0.19302800			
TS_I	FA3					
0	-1.15684600	-1.19233300	0.26882200			
0	-2.18793200	-0.27497100	0.07067700	-1967.03 39.26 80.79	05 Ha 1.88	
	-1./0980900	0.54653600	-0.4312/800	94.72     151.31     182.66       215.47     243.39     736.81	04	
H	3.06006500	0.06956300	-0.05269700	458.87 540.58 686.04	0>H3 H2	
0	1.34735100	0.73745300	0.79636800	839.94 869.65 1080.44		
0	1.45530300	-0.90657600	-0.72490900	1095.19 1234.15 1331.79	<u></u>	
Н   µ	0.48778000	-0.95797400	-0.57477600	1382.71 1413.50 1429.46 1496.93 1810.95 3140.50	1.86	
0	-1.00967500	1.62389300	-0.48509500	3520.11 3585.96 3786.33	H4	
Н	-0.24516700	1.46323300	0.10737200			
IMF FA3						

0	-1.47013800	-1.21764300 0.23416900		
0	-2.45186200	-0 41906400 -0 10196200	10 79 47 71 57 67	
й	1 48710200	1 52648400 0 23468200	80.00 123.80 141.37	<b>95</b>
	-1.46/19200	0.20096400 -0.23408300	171.25 100.02 251.20	H3 199
C	2.15213000	-0.20886400 0.0148/400	1/1.35 180.93 251.39	04
Н	3.22992800	-0.40670100 -0.02479300	367.70 390.09 487.32	7
0	1.67007900	0.83984200 0.34631500	662.36 755.09 1085.06	
0	1.45949000	-1.28897000 -0.35027100	1183.74 1249.8 1345.60	01
H	0 51018900	-1.07707100 -0.30233900	1425 60 1459 54 1650 24	
п	1 00170500	2 01070700 0 62700000	1827.08 2112.57 2625.62	2.06
п	-1.881/2300	-2.010/9/00 0.02/00900	1827.08 3112.37 3033.02	
0	-0.86516300	2.25/10400 -0.15//5300	3692.63 3802.09 3899.10	
Н	-0.02321800	1.85112600 0.08156900		
IM	FA4			
	1.07005400	0.01152000 0.25000500		
0	-1.07885400	0.84453900 0.25898600		
0	-0.33259600	1.94294600 -0.24956300	35.14 68.10 80.44	H1.1.79.05
H	0.57742000	1.58563800 -0.18303200	125.00 161.25 184.44	01
C	1 80124300	-0.75871200 -0.00580100	198 71 224 42 244 12	123.3
ц	2 64856000	1 45000800 0.03730300	350.76 377.22 671.08	
	2.04650000	-1.45000800 -0.05750500	710 72 9(7.12 1049.49	<b>1.9</b>
0	1.936//900	0.43994700 0.02012300	/10./3 86/.12 1048.48	на 04
0	0.65833500	-1.40725000 -0.00110300	1094.60 1219.24 1357.01	71.2
Н	-0.09365300	-0.77960300 0.05199300	1370.29 1418.87 1548.77	2.40
Н	-1.32983500	1.14225700 1.14129600	1811.03 3130.98 3496.48	
0	-2 41966400	-1 23083000 -0 04876200	3560 28 3756 93 3823 49	<b>*</b> 👧
й	_2 72104700	-0.66082600 -0.77560300	5150.20 5750.95 5025.19	<b>•</b>
	-2.72174700	0.00002000 -0.77500500		
_TS_	FA4			
0	-1.34914100	0.86909900 0.08380200		
Ó	-0.60387500	2.04113300 -0.22455800	-65.45 38.27 101.12	H 1.71
ц	0 31054700	1 73382900 _0.06025000	117 20 155 81 166 08	01 05
	1 96020700	0.40182100 0.02270400	100 40 277 20 210 44	136- 15
C	1.86930/00	-0.49182100 0.032/9600	190.49 277.29 310.64	
Н	2.87705200	-0.91274300 0.05538700	666.72 690.99 781.01	. 2.36
0	1.64683900	0.68813800 0.16120800	803.35 871.27 1041.14	
0	0.95714200	-1.42136800 -0.15109800	1081.02 1232.19 1366.77	2.42 59.
H	0.06317000	-1.00451300 -0.12789600	1381 28 1424 33 1517 56	
ц	1 71253000	1.06111100 0.05684000	1806.17 2150.67 2186.11	2.21
п	-1./1233000	1.00111100 0.95084900	1800.17 3139.07 3180.11	
0	-1.98503200	-1.80506200 0.05416800	3522.36 3556.24 3814.82	
Н	-2.08154/00	-0.90228000 -0.40894000		
IM	FA5			
	1.02026200	0.22614000 0.71002000		
0	1.92026300	-0.32614000 0./1092000	21.05 52.05 112.45	
0	1.61903400	-0.68803200 -0.63620500	31.85 73.87 112.47	
H	0.69004200	-0.98858000 -0.53735100	117.42 183.70 196.47	
C	-1.90973100	-0.50885500 0.10142400	220.48 232.56 255.96	H1 1.75
Н	-2.91990200	-0.87189900 0.31397100	458.28 627.41 697.74	<b>9</b>
0	-1.00345100	-1 25303100 -0 18597700	735 23 908 00 1037 48	13.2
ŏ	1 84012200	0.79610600 0.20170900	1004 84 1256 40 1248 04	04
	-1.64012200	0.79010000 0.20170900	1094.84 1230.49 1348.94	176. H4
н	-0.92884200	1.13151400 0.01425200	1393.85 1425.25 1549.64	
0	0.63293700	1.88832400 -0.27502200	1806.27 3138.62 3331.58	
Н	1.32354000	1.34716000 0.16328900	3487.16 3613.52 3854.90	
H	2.66425800	-0.90288000 0.91390600		
тс	FA5			
1.5		0.20502500 0.02120550	1	[
0	-2.00179900	0.39593500 0.03420700		
0	-2.07241200	-0.89611000 0.07974400	-1962.88 -79.16 98.27	122
H	-0.81069200	-1.16490500 0.01078700	116.39 141.90 221.97	1.29 H1 1.32 05 H5
C	1.67037200	-0.88797600 0.00576000	336.56 384.36 444.36	
H	2,53606100	-1.58201100 0.03511300	510.47 647 78 695 90	- Stor
	0 49527700	-1 30086300 _0.00052600	753 47 1073 56 1157 16	H2 02
	2 05020000	0.25867200 0.04252700	1240.08 1276.02 1200.26	- <u>U</u>
	2.03920800	0.5380/200 0.04253/00	1240.98 1270.83 1308.20	80 H4 31
H	1.03715700	1.1/5/1600 0.09814400	13/4./1 1414.56 1502.93	H3 👝 🔊
0	0.29460100	1.97462600 -0.09425500	1561.71 1683.14 1836.66	<b>U</b> 3/`
Н	-0.29284200	1.94907900 0.67603500	2992.09 3276.32 3780.11	-
H	<u>-2.719</u> 71800	0.63790200 -0.63549900		
ІМІ	F FA5			
	2 20001400	0.30143400 0.04076500		
	2.50091400	-0.50145400 -0.040/6500	45.01 70.76 07.50	
0	1.58445900	-1.41690/00 -0.04204700	45.91 /2.76 87.50	
Н	-0.36258100	-1.14908200 -0.01578500	135.12 150.57 168.43	1.97 H
C	-2.10393800	-0.35693800 0.02593200	179.42 189.61 210.72	
H	-3.14487400	-0.66888600 0.16622100	312.49 364.35 497.17	114.5
0	-1 29674600	-1.41213800 0.10803700	669.62 805.38 1086.07	<b>11 02</b> 04
۱ŏ.	_1 76877000	0.78149400 _0.17410200	1185.85 1100.23 1242.40	1. P. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.
	-1.70077500	2.01011000 - 0.1204700	1415 22 1452 07 1657 06	Nr 11
П	-0.20146500	2.01011900 0.01304/00	1413.32 1433.87 1057.00	H3H
0	0.65826700	2.44037500 0.11952600	1811.61 3126.12 3589.66	03
H	1.28423000	1.79559900 -0.22155400	1616.43 1789.37 3912.61	-
H	3.22340200	-0.57724700 0.13731100		