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## Supplementary Information: Effects of Shear Flow on Structure and Dynamics of Ionic Liquid in Metallic Nanoconfinement

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#### S1 Density and interfacial structure

Apart from narrowing of the peaks from shearing, the interface is predominantly unchanged in its structure. This is exemplified by the density profile of the anions in Figure 4 where the system is at a shear velocity of  $v_{slab} = \pm 10 \text{ m s}^{-1}$ . Similarly, at a velocity of  $v_{slab} = \pm 20 \text{ m s}^{-1}$ , the interfacial structure shown in Figures S1, S2 and S3 remains essentially identical to that of an equilibrium system.

### S2 Orientation of cations

We describe further the interfacial structure by looking at the orientation of the cations. Just has already been discussed in the main text, the cations, to a significant extent, retain their equilibrium orientation. This is so, irrespective of shearing velocity and temperature as demostrated by the distributions of angles in Figures S4, S5, S6, S7 and S8.



Fig. S1 Denstity profile of anions at slab velocity of  $\pm 20\,ms^{-1}$ . The blue dashed line represents the density profile of anions at  $298\,K$  at equilibrium, where no shear is applied and the thermostat is applied to the whole system.

#### S3 Steinhardt order parameter

We calculated the global Steinhardt order by averaging the local orientational order parameter for the *i*th atom

$$q_6(i) = \sqrt{\frac{4\pi}{13} \sum_{m=-6}^{6} |q_{6m}(i)|^2}$$
(1)

where  $q_{6m}(i)$  are components of a 13-dimensional complex vector, used to describe the locality of *i*th atom. It is defined as

$$q_{6m}(i) = \frac{1}{N_{nn}(i)} \sum_{j=1}^{N_{nn}(i)} Y_{6m}(\theta_{ij}, \phi_{ij})$$
(2)

which is an average over all nearest neighbours of the *i*th atom,  $N_{nn}(i)$  of the spherical harmonics  $Y_{6m}(\theta_{ij}, \phi_{ij})$  of polar and azimuthal angles  $\theta_{ij}$  and  $\phi_{ij}$  made by the vector  $\mathbf{r}_{ij}$  to some reference coordinate. The global order parameter  $Q_6$  is then calculated as the average of  $q_6(i)$  over all atoms.

Figures S9 and S10 show the  $Q_6$  profiles at slab velocities of

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Fig. S2 Denstity profile of cations at slab velocity of  $\pm 10\,m\,s^{-1}$ . The blue dashed line represents the density profile of cations at 298 K and without shear, and with the whole system connected to the thermostat.



Fig. S3 Denstity profile of cations at slab velocity of  $\pm 20\,ms^{-1}.$  The blue dashed line represents the density profile of cations at  $298\,K$  and without shear.



Fig. S4 Distribution of angle made by cation tail at the interface at slab velocity of  $\pm 10\,m\,s^{-1}$ . The blue dashed line represents that with the whole system thermostatted at 298 K and without shear.

 $10 \text{ m s}^{-1}$  and  $20 \text{ m s}^{-1}$ , respectively, at the two temperature levels. The temperature profiles are only included to demonstrate the parabolic nature of the  $Q_6$  profile.

#### S4 Shear viscosity and shear thinning

We show in the following tables the shear viscosity at different slab velocities calculated for the whole cavity of ionic liquid bounded by  $\pm 118.575$  Å and for the midsection bounded by  $\pm 20$  Å where we observe ideal Couette flow. We report also the velocities at these bounds and the average temperature within the bounds.



Fig. S5 Distribution of angle made by plane of imidazolium ring at the interface at slab velocity of  $\pm 10\,m\,s^{-1}$ . The blue dashed line represents that at  $298\,K$  and without shear.



Fig. S6 Distribution of angle made by the axis through the imidazolium, at the interface with slab velocity of  $\pm 20\,m\,s^{-1}$ . The blue dashed line represents the same distribution with the whole system thermostatted at  $298\,K$  in equilibrium.



Fig. S7 Distribution of angle made by cation tail at the interface at slab velocity of  $\pm 20\,ms^{-1}$ . The blue dashed line represents the same distribution at  $298\,K$  and without shear.

In our simulations, we have the flow of the liquid in the direction y and a velocity gradient in the direction z. We calculate the shear viscosities from the components in these directions of average pressure tensor in the corresponding region R and the shear rate  $\dot{\gamma}_R$  using the velocity  $v_B$  at the boundary to that region in this way:

$$\eta_R = -\frac{\langle P_{yz} \rangle}{\dot{\gamma}_R} \tag{3}$$



**Fig. S8** Distribution of angle made by plane of imidazolium ring at the interface at slab velocity of  $\pm 20 \, {\rm m \, s^{-1}}$ . The blue dashed line represents that at 298 K and without shear.



**Fig. S9**  $Q_6$  and temperature profiles at  $\pm 10 \,\mathrm{m\,s^{-1}}$  slab velocity. Dotted curves represent temperature profiles while joined curves represent the  $Q_6$  profiles. The blue is the  $Q_6$  profile for an equilibrium system thermostatted at 298 K.



**Fig. S10**  $Q_6$  at  $\pm 20 \text{ ms}^{-1}$  slab velocity. Dotted curves represent temperature profiles while joined curves represent the  $Q_6$  profiles. The blue is the  $Q_6$  profile for an equilibrium system thermostatted at 298 K.

where  $\dot{\gamma}_R = \frac{2 \times v_B}{h_R}$ ,  $h_R$  being the thickness of the region *R*.

Table SI Boundary velocity, average temperature and viscosity at slab velocity  $\pm 10\,m\,s^{-1}$  for low and high temperatures.

| Bounds/Å      | Low           | temper      | ature                              | High temperature       |             |                                    |  |
|---------------|---------------|-------------|------------------------------------|------------------------|-------------|------------------------------------|--|
|               | $v_B/ms^{-1}$ | $\bar{T}/K$ | $\eta/\mathrm{mPa}\cdot\mathrm{s}$ | $v_B/\mathrm{ms^{-1}}$ | $\bar{T}/K$ | $\eta/\mathrm{mPa}\cdot\mathrm{s}$ |  |
| ±20.0         | 2.8           | 229.2       | 14.3                               | 2.4                    | 323.3       | 9.9                                |  |
| $\pm 118.575$ | 10.0          | 202.1       | 22.7                               | 10.0                   | 302.4       | 17.9                               |  |

Table SII Boundary velocity, average temperature and viscosity at slab velocity  $\pm 20 \text{ ms}^{-1}$  for low and high temperatures.

| Bounds/Å | Low temperature        |             |                                    | High temperature       |             |                                    |  |
|----------|------------------------|-------------|------------------------------------|------------------------|-------------|------------------------------------|--|
|          | $v_B/\mathrm{ms^{-1}}$ | $\bar{T}/K$ | $\eta/\mathrm{mPa}\cdot\mathrm{s}$ | $v_B/\mathrm{ms^{-1}}$ | $\bar{T}/K$ | $\eta/\mathrm{mPa}\cdot\mathrm{s}$ |  |
| ±20.0    | 6.3                    | 253.0       | 6.7                                | 4.8                    | 339.2       | 6.3                                |  |
| ±118.575 | 20.0                   | 202.9       | 12.3                               | 20.0                   | 303.6       | 8.2                                |  |

# S5 Pressure in "frozen" layer and normal stress coefficients

We show here in Table SIII a comparison of the average pressure in the "frozen" layer to that of the rest of the liquid for all our simulations. The pressure in a region is calculated from the average pressure tensor  $\mathbf{P}$  of all atoms in that region as

$$p = \frac{1}{3V} \operatorname{Tr}(\mathbf{P}) \tag{4}$$

where V is the volume of the region under consideration.

The average differences in normal stress coefficients are crucial in determining whether or not the liquid is readily deformable in certain direction—whether or not the liquid is Newtonian. However, it necessary to have a converge pressure tensor. In Fig. S11 we show an example convergence of the diagonal components of the pressure tensor and their total, over time, for our low temperature system at  $10 \text{ ms}^{-1}$  slab velocity.

**Table SIII** Average pressure in "frozen" layer  $p_f$  ( $0 < z \le \lambda$ ) in comparison with average pressure of rest of ionic liquid  $p_r$  ( $|z| < \lambda$ ).

| $v_{\rm slab}/m{\rm s}^{-1}$ | Low temp. |            |           | High temp. |            |           |
|------------------------------|-----------|------------|-----------|------------|------------|-----------|
|                              | λ/Å       | $p_f$ /MPa | $p_r/MPa$ | λ/Å        | $p_f$ /MPa | $p_r/MPa$ |
| 10                           | 10.60     | -344.01    | -100.44   | 5.96       | -337.10    | 47.08     |
| 20                           | 16.51     | -257.19    | -74.91    | 6.49       | -281.27    | 73.77     |

The first and second normal stress coefficients are defined here as

$$\psi_1 = \frac{\langle P_{zz} - P_{yy} \rangle}{\dot{\gamma}^2} \tag{5}$$

and

$$\psi_2 = \frac{\langle P_{xx} - P_{zz} \rangle}{\dot{\gamma}^2} \tag{6}$$

Table SIV shows the normal stress coefficients and their ratios, calculated from the diagonal elements of the pressure tensor according to these equations.

#### S6 Load and friction

We increased the load on the ionic liquid by moving the each gold slab in steps of 0.5 Å towards the other every 10 ps until the desired reduction in the slab separation is reached, and then a run of 52 ns. For a given slab separation reduction of *s* the load

**Table SIV** Average first and second normal stress coefficients, and their ratios at low and high temperatures.

| $v_{\rm slab}/{\rm ms^{-1}}$ | Lo              | ow temp.        | High temp.               |                                   |                 |                          |  |
|------------------------------|-----------------|-----------------|--------------------------|-----------------------------------|-----------------|--------------------------|--|
|                              | $\psi_1/pPas^2$ | $\psi_2/pPas^2$ | $\frac{-\psi_2}{\psi_1}$ | $\psi_1/p\mathrm{Pa}\mathrm{s}^2$ | $\psi_2/pPas^2$ | $\frac{-\psi_2}{\psi_1}$ |  |
| 10                           | 1050.88         | -653.16         | 0.62                     | 935.25                            | -555.63         | 0.59                     |  |
| 20                           | 265.15          | -164.93         | 0.62                     | 235.33                            | -138.66         | 0.59                     |  |



Fig. S11 Convergence of the diagonal components of the pressure tensor for lower temperature system with slab velocity of  $\pm 10\,ms^{-1}.$ 



Fig. S12 Convergence of  $\psi_1$  and  $\psi_2$  for lower temperature system with slab velocity of  $\pm 10\,m\,s^{-1}.$ 

 $L_s$  corresponding to a slab separation of  $h = h_0 - s$  where  $h_0$  is the equilibrium slab separation, is calculated by difference in the average normal forces on the slabs. The average force on the lower slab, say, is calculate every 1 ps as

$$F^{\text{lower}} = \sum_{i \in \text{lower}} \langle \mathbf{f}_i(t) \rangle \tag{7}$$

then the load per area is evaluated as  $f_L = 0.5 \times (F_z^{\text{upper}} - F_z^{\text{lower}})/(L_x L_y)$ . Table SV shows the load at different temperatures, velocities and slab separations. Figures S13 to S16 show the density profiles at the smallest slab separation simulated,  $h_0 - 12$ Å. The dashed lines indicate the corresponding density profiles at slab separation of  $h_0$ .

**Table SV** Load on systems. Each  $L_s$  is the load for system with slab separation  $h = h_0 - s$  where  $h_0 = 237.15$  Å.

| $v_{\rm slab}/m{\rm s}^{-1}$ | temper    | emperature High |                     |           | n temperature |                     |
|------------------------------|-----------|-----------------|---------------------|-----------|---------------|---------------------|
|                              | $L_0/GPa$ | $L_6/GPa$       | $L_{12}/\text{GPa}$ | $L_0/GPa$ | $L_6/GPa$     | $L_{12}/\text{GPa}$ |
| 10                           | -0.09     | -0.01           | 0.09                | 0.06      | 0.15          | 0.27                |
| 20                           | -0.07     | 0.02            | 0.12                | 0.08      | 0.17          | 0.32                |



**Fig. S13** Density profile of anions at slab velocity of  $\pm 10 \text{ ms}^{-1}$  at slab separation of  $h_0 - 12\text{\AA}$  The dashed line represents the corresponding density profile of anions at slab separation of  $h_0$ .



**Fig. S14** Density profile of anions at slab velocity of  $\pm 20 \text{ ms}^{-1}$  at slab separation of  $h_0 - 12\text{\AA}$  The dashed line represents the corresponding density profile of anions at slab separation of  $h_0$ .



**Fig. S15** Density profile of cations at slab velocity of  $\pm 10 \text{ ms}^{-1}$  at slab separation of  $h_0 - 12\text{ Å}$  The dashed line represents the corresponding density profile of cations at slab separation of  $h_0$ .



**Fig. S16** Density profile of cations at slab velocity of  $\pm 20 \,\mathrm{m\,s^{-1}}$  at slab separation of  $h_0 - 12 \,\mathrm{\AA}$  The dashed line represents the corresponding density profile of cations at slab separation of  $h_0$ .