

## Supplementary Information

### **Developing physicochemical property-based ecotoxicity characterization factors for silver nanoparticles under mesocosm conditions for use in life cycle assessment**

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*2 figures, 9 tables, 24 pages*

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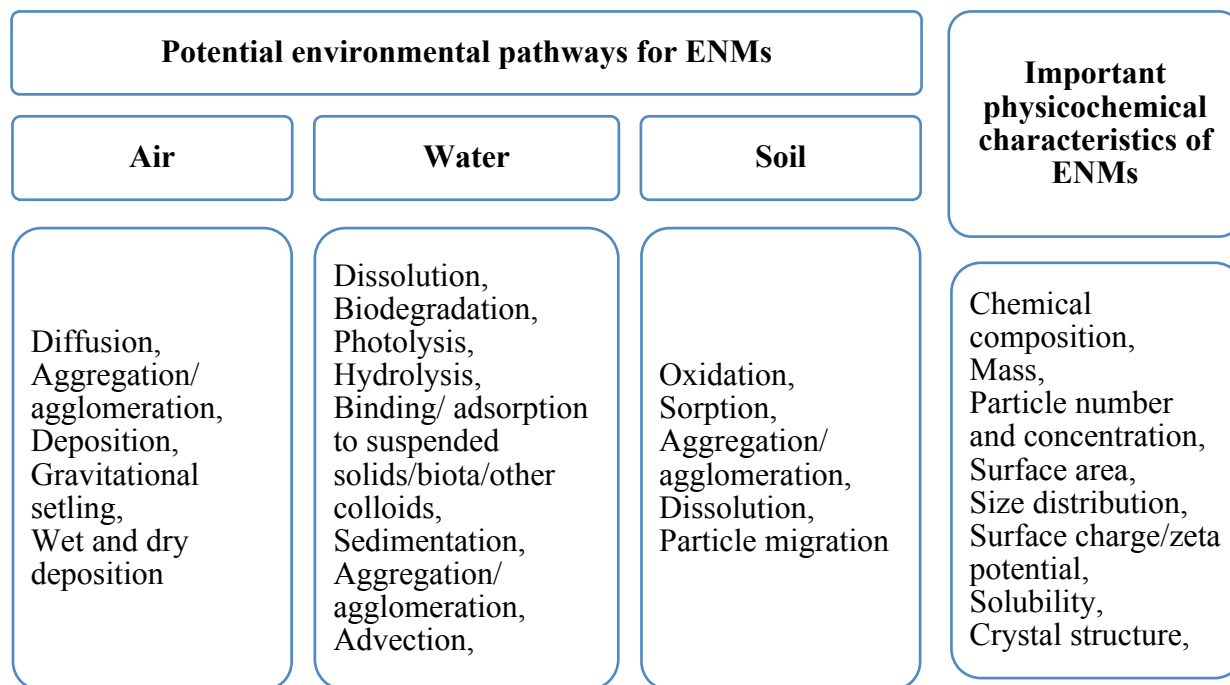


Figure S1. Potential environmental pathways for nanomaterials and physicochemical characteristics of ENMs that affect fate factors (Baun et al., 2017; Lamon et al., 2019; Miseljic and Olsen, 2014; Rosenbaum et al., 2008; Tortella et al., 2020)

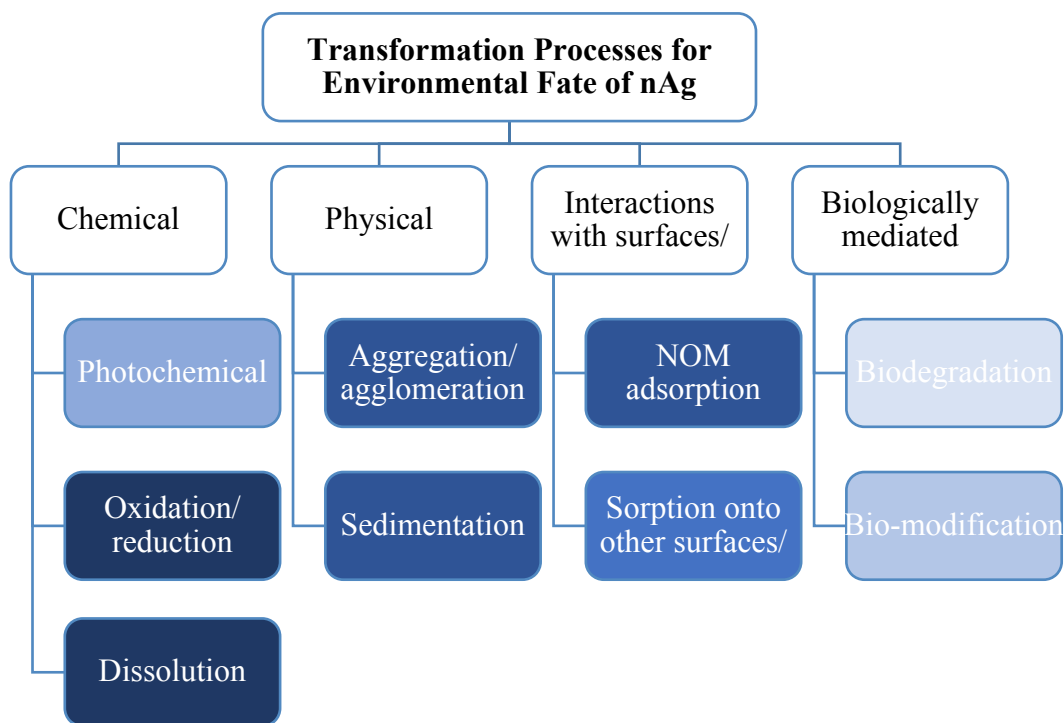


Figure S2. Relative importance of potential transformation processes in modeling environmental fate of nAg (darker shades indicate higher importance) (Baun et al., 2017; Hartmann et al., 2014)

As the current paper aims to develop freshwater ecotoxicity CF for nAg, studies that define fate and behavior of nAg are reviewed and factors affecting the fate of nAg are listed. (Baun et al., 2017; Dale et al., 2013; Furtado et al., 2015; Hartmann et al., 2014; Levard et al., 2012; Maiga et al., 2020; Peng et al., 2017; Tortella et al., 2020) Figure S2 shows the processes that are relevant to nAg and illustrates the relative importance of these processes using a color scheme. (Baun et al., 2017) Throughout the literature, it was found that nAg go through several transformation processes depending on their physicochemical characteristics as well as the properties of the release media with dissolution, oxidation/reduction and aggregation/agglomeration being the most dominant ones among others. Hartmann et al. argued that as nAg are unstable in the presence of light, photochemical transformation process may be

neglected. Also, as being an inorganic ENM, the biodegradation of nAg is not expected to be as relevant as the previously mentioned processes.(Hartmann et al., 2014) Peng et al. and Peijnenburg et al. provided comprehensive assessments on each of the potential environmental transformation process and the impacts of different conditions on those processes.(Peijnenburg et al., 2015; Peng et al., 2017) For instance, after explicitly defining the dynamics of aggregation of metallic ENMs, effects of size, shape, surface coating, pH, ionic strength and presence of organic matter on aggregation are elaborated in detail.(Peijnenburg et al., 2015; Peng et al., 2017; Quik et al., 2011)

### **Review of characterization factor literature for nAg**

In order to explore the previous studies that calculated CFs for nAg, a literature survey is conducted by using an academic search engine, Web of Science Core Collection, by searching combinations of key terms including characterization factors, nanomaterial, nanosilver and nanosilver-enabled. From this search, three studies were identified where CFs are derived for nAg.(Garvey et al., 2019; Miseljic and Olsen, 2014; Pu, 2017) Table S1, yellow shaded cells, present a summary of these studies along with the calculated/assumed FF, XF and EF, and derived CFs.

As being the first CF study for nAg, Miseljic and Olsen used simplifying assumptions to estimate the freshwater ecotoxicity potential of nAg. They suggested that nAg will have a short substance residence time in freshwater (i.e. rapid transformation, aggregation and sedimentation time), which resulted in an FF of 1.(Miseljic and Olsen, 2014) They also assumed that the exposure is equal to the environmental concentration of nAg, and therefore neglected the XF. For EF, Miseljic and Olsen compiled in total of 21  $EC_{50}$  values for three trophic levels (algae,

crustacean and fish) and calculated the EF as 8,576 PAF.m<sup>3</sup>/kg.(Miseljic and Olsen, 2014)

Another study by Pu developed a fate model which involves calculating the FF from rate constants of certain transformation processes, such as advection, dissolution, sedimentation.(Pu, 2017) For EF, Pu compiled toxicity data for three trophic levels (algae, crustacean and fish) and calculated the EF as 14,502 PAF.m<sup>3</sup>/kg. They argued that given that the XF calculation based on USEtox involves partitioning coefficients and they are not representative for ENMs, an *ultra-conservative* XF needs to be assumed which is equal to considering 100% bioavailability.(Pu, 2017) Lastly, Garvey et al. used an adapted version of USEtox model, where they computed *realistic*- and *worst*-case scenarios. They calculated the FF using substance specific partitioning coefficients as USEtox recommended. In order to calculate the EF, Garvey et al. used in total of 73 different toxicity data (including EC<sub>50</sub>, IC<sub>50</sub> and LC<sub>50</sub>) for four phyla (Arthropoda, Chordata, Chlorophyta and Heterokontophyla) and calculated EF with a range of 13,497 – 281,144 PAF.m<sup>3</sup>/kg. For XF, they used statistical simulations since empirically determined exposure factors were not available in the literature, and suggested that nAg is 60-80% bioavailable.(Garvey et al., 2019)

As previously mentioned, the XF and FF depend on the physicochemical properties of nAg and the conditions of the release media.(Lamon et al., 2019; Westerhoff and Nowack, 2013)

Additionally, different size and coating of nAg have a significant impact on EF.(Temizel-Sekeryan and Hicks, 2020) These factors are needed to be considered while developing nAg specific CFs. Overall, previous studies that derive nAg-CFs used various approaches and did not take into account the external (i.e. media dependent) and internal (i.e. ENM dependent) factors, which are critically important.

Table S1. Parameters for fate factor calculation extracted from a mesocosm studies (Espinasse et al., 2018; Geitner et al., 2019, 2017; Stegemeier et al., 2017).

Parameter	Symbol	Unit	Value (Range)
pH	pH	-	7-10
Conductivity	S	μS/cm	111 ± 20
Radius of nAg	$r_{nAg}$	nm	24.65 (PVP-nAg)
Diameter of nAg (DLS)	$d_{nAg}$	nm	49.3 (PVP-nAg)
Radius of SPM	$r_{SPM}$	μm	0.75
Diameter of SPM	$d_{SPM}$	μm	1.5 ± 12
Density of nAg	$\rho_{nAg}$	kg/m <sup>3</sup>	10,500
Mass concentration of SPM	$C_{mass, SPM}$	mg/l	80 ± 12
Aggregation efficiency	$\alpha_{het-agg}$	-	0.012
Depth of water	$h_w$	m	1.2
Volume of water	$V_w$	m <sup>3</sup>	3.56 (H/W/D 0.81/3.66/1.2)
Area of freshwater	$A_{freshwater}$	m <sup>2</sup>	2.97
Area of soil	$A_{soil}$	m <sup>2</sup>	0.732
Water temperature	$T_{water}$	K	295
Dynamic viscosity of water	$\mu_{water}$	Ns/m <sup>2</sup>	0.000958 (22°C)*
Initial concentration of nAg	$C_0$	ppm	10
Dissolved nAg at time t (2 days)	$C_{ions}$	ppm	0.53

\* calculated based on the formula of  $\mu_{water} = (2.414 * 10^{-5}) * 10^{247.8/(T-140)}$



Table S2. Remaining parameters for fate factor calculation that are not available in mesocosms  
(bold values are used in calculation)

Parameter	Symbol	Unit	Value (Range)	Reference
Density of water	$\rho_{water}$	kg/m <sup>3</sup>	1000	(Fantke et al., 2017)
Boltzmann constant	$k_B$	J/K	1.38E-23	(Deng et al., 2017a; Pu, 2017)
Surface water shear rate	$G$	s <sup>-1</sup>	10	(Meesters et al., 2014)
Gravitational acceleration on earth	$g$	m/s <sup>2</sup>	9.81	(Fantke et al., 2017)
Precipitation rate	$k_{precipitation}$	mm/yr	710 (for US)	(Kounina et al., 2014)
Density of SPM	$\rho_{SPM}$	kg/m <sup>3</sup>	<b>1570</b>	<i>averaged value</i>
			2000 <sup>a</sup>	a (Salieri et al., 2015)
			1230 <sup>b</sup>	b (Pu, 2017)
			1100 – 2500 <sup>c</sup>	c (Praetorius et al., 2012)
			1250 (1100 – 2000) <sup>d</sup>	d (Quik, 2013)
Water run-off fraction	$\varphi$	%	37 (for US)	(Kounina et al., 2014)

Table S3. Considerations for calculating the freshwater ecotoxicity characterization factors for ENMs (listed in alphabetical order based on references, shaded cells represent nAg)

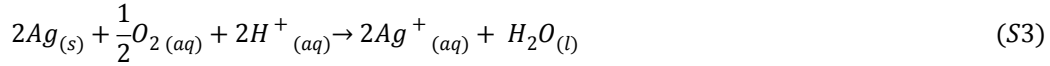
ENM	Considered processes for fate modeling	FF (days)	XF (%)	EF (PAF.m <sup>3</sup> /kg)	CF (PAF.m <sup>3</sup> .day/kg or CTUe/kg)	Reference
CNT	Sedimentation ( $k_{sed} = 6.8 \times 10^{-10} \text{ s}^{-1}$ ) Heteroaggregation ( $k_{hetero-agg} = 6.9 \times 10^{-11} \text{ s}^{-1}$ ) Advection ( $k_{adv} = 6.91 \times 10^{-9} \text{ s}^{-1}$ )	1509	81.1	55.4	6.78+04	(Deng et al., 2017a)
GO	Sedimentation ( $k_{sed} = 2.5 \times 10^{-8} \text{ s}^{-1}$ ) Heteroaggregation ( $k_{hetero-agg} = 2.3 \times 10^{-7} \text{ s}^{-1}$ ) Advection ( $k_{adv} = 4.6 \times 10^{-8} \text{ s}^{-1}$ ) Photodegradation ( $k_{photodeg} = 1.3 \times 10^{-7} \text{ s}^{-1}$ )	27.2	93	30.7	7.78E+02	(Deng et al., 2017b)
SWCNT	Calculated using substance specific partitioning coefficients	S1) 143 S2) matter of days	S1) 100 S2) 98	S1) 200 S2) 200	S1) 29000 S2) 3700	(Eckelman et al., 2012)
Nano-TiO <sub>2</sub>	Dissolution Aggregation	0.633 (free form) 44.8 (aggregated form)	<i>not mentioned</i>	26.9 (9.4–26.9)	1550 (free form)	(Ettrup et al., 2017)
nAg	Calculated using substance specific partitioning coefficients	S1) 30 S2) 130	S1) 60 S2) 80	S1) 13497 S2) 281144	S1) 2.43E+05 S2) 2.92E+07	(Garvey et al., 2019)
Nano-TiO <sub>2</sub>	Calculated using substance specific partitioning coefficients	S1) 0.053 S2) 1	S1) 100 S2) 100	S1) 79 S2) 1180	S1) 4 S2) 1180	(Garvey et al., 2019)

SWCNT	Calculated using substance specific partitioning coefficients	S1) 10 S2) 143	S1) 100 S2) 100	S1) 260 S2) 288	S1) 2600 S2) 41184	(Garvey et al., 2019)
C <sub>60</sub>	Calculated using substance specific partitioning coefficients	S1) 10 S2) 143	S1) 100 S2) 100	S1) 91 S2) 161	S1) 910 S2) 23023	(Garvey et al., 2019)
nAg	Assumed due to many unknowns	1	neglected	8576	8.57E+03	(Miseljic and Olsen, 2014)
Nano-TiO <sub>2</sub>	Assumed due to many unknowns	1	neglected	26.1	2.61E+01	(Miseljic and Olsen, 2014)
nCu	Sedimentation Advection Dissolution	1.15	100	5185	5.96E+03	(Pu et al., 2016)
nAg	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ ) Dissolution ( $k_{diss} = 3.42 \times 10^{-6} \text{ s}^{-1}$ )	1.36 (3.86E-03 – 3.38E+00)	100	14502	1.98E+04	(Pu, 2017)
Al <sub>2</sub> O <sub>3</sub> -NP	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ )	2.28 (3.87E-03 – 1.28E+03)	100	53.083	1.21E+02	(Pu, 2017)
Au-NP	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ )	2.28 (3.87E-03 – 1.18E+03)	100	80.7	1.84E+02	(Pu, 2017)
C <sub>60</sub>	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ )	2.28 (3.87E-03 – 1.33E+03)	100	544	1.24E+03	(Pu, 2017)
CeO <sub>2</sub> -NP	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ )	2.28 (3.87E-03 – 1.24E+03)	100	139	3.18E+02	(Pu, 2017)
nCu	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ ) Dissolution ( $k_{diss} = 5.5 \times 10^{-7} \text{ s}^{-1}$ )	2.06 (3.87E-03 – 2.07E+01)	100	8999	1.85E+04	(Pu, 2017)

nCuO	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ ) Dissolution ( $k_{diss} = 3.87 \times 10^{-7} \text{ s}^{-1}$ )	2.12 (1.37E-01 – 2.92E+01)	100	223	4.74E+02	(Pu, 2017)
Fe <sub>2</sub> O <sub>3</sub> -NP	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ )	2.28 (3.86E-03 – 1.26E+03)	100	228	5.20E+02	(Pu, 2017)
Fe <sub>3</sub> O <sub>4</sub> -NP	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ )	2.28 (3.87E-03 – 1.27E+03)	100	21739	4.96E+04	(Pu, 2017)
NiO-NP	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ ) Dissolution ( $k_{diss} = 2.18 \times 10^{-7} \text{ s}^{-1}$ )	2.19 (3.87E-03 – 5.09E+01)	100	14.2	3.10E+01	(Pu, 2017)
Pt-NP	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ )	2.28 (3.86E-03 – 1.17E+03)	100	126	2.88E+02	(Pu, 2017)
SiO <sub>2</sub> -NP	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ ) Dissolution ( $k_{diss} = 3.79 \times 10^{-6} \text{ s}^{-1}$ )	1.31 (3.86E-03 – 3.05E+00)	100	27.8	3.62E+01	(Pu, 2017)
Nano-TiO <sub>2</sub>	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ )	2.28 (3.87E-03 – 1.27E+03)	100	56.7	1.29E+02	(Pu, 2017)
ZnO-NP	Sedimentation Advection ( $k_{adv} = 8.1 \times 10^{-9} \text{ s}^{-1}$ ) Dissolution ( $k_{diss} = 5.12 \times 10^{-7} \text{ s}^{-1}$ )	2.07 (3.87E-03 – 2.22E+01)	100	2863	5.94E+03	(Pu, 2017)
SWCNT	Calculated using substance specific partitioning coefficients	29	6.5E-04	650	1.25E-01	(Rodriguez-Garcia et al., 2014)

MWCNT	Calculated using substance specific partitioning coefficients	92	100	8	7.40E+02	(Rodriguez-Garcia et al., 2014)
nCu	Calculated using substance specific partitioning coefficients	37	33	4500	5.52E+04	(Rodriguez-Garcia et al., 2014)
Nano-TiO <sub>2</sub>	Sedimentation Heteroaggregation Advection	0.053	100	32.1	2.81E+01	(Salieri et al., 2015)

## **Dissolution**



The second method for  $k_{diss}$  calculation is using modified version of the solubility equilibrium (i.e. Ostwald-Freundlich relation) as presented in equations (S4) and (S5), which enables calculating size-dependent dissolution rates (Axson et al., 2015; Doody et al., 2016; Johnston et al., 2019; Ma et al., 2012). It is hypothesized that the amount of dissolved nAg per unit time is proportional with the surface area of nAg (Molleman and Hiemstra, 2017; Quik et al., 2011) as

$$\frac{dM}{dt} = -k_{diss} * S_{nAg} * A \quad (S4)$$

$$S_{nAg} = S_{bulk} * \exp\left(2 * \gamma * \frac{V_m}{R * T * r_{nAg}}\right) \quad (S5)$$

where  $M$  is the dissolved mass of nAg (kg),  $t$  is time (s),  $S_{nAg}$  is the solubility of nAg (kg/m<sup>3</sup>),  $A$  is the surface area of nAg (m<sup>2</sup>),  $S_{bulk}$  is the solubility of bulk silver (kg/m<sup>3</sup>),  $\gamma$  is the surface tension of nAg (typically 1 for nAg, J/m<sup>2</sup>),  $V_m$  is the molar volume of nAg (m<sup>3</sup>/mol),  $R$  is the gas constant (J/mol.K),  $T$  is the temperature (K) and  $r_{nAg}$  is the radius of nAg (m). Ma et al. calculated the  $k_{diss}$  for PVP coated nAg as  $5.07 \times 10^{-5} \text{ s}^{-1}$  using this method (Ma et al., 2012). Different from the previously explained methods, Dale et al. compiled a list of model parameters for nAg transformation where they included a range for  $k_{diss}$  based on the level of dissolved oxygen in freshwaters from  $1.3 \times 10^{-8} \text{ d}^{-1} (\text{mg O}_2/\text{m}^3)^{-1}$  to  $5.1 \times 10^{-4} \text{ d}^{-1} (\text{mg O}_2/\text{m}^3)^{-1}$  with a nominal value of  $8.5 \times 10^{-6} \text{ d}^{-1} (\text{mg O}_2/\text{m}^3)^{-1}$  (Dale et al., 2015; Levard et al., 2012; Liu et al., 2010).

## **Hetero-aggregation**

$$k_{het-agg} = k_{coll} * \alpha_{het-agg} * C_{SPM} \quad (S6)$$

where  $\alpha_{het-agg}$  is aggregation efficiency,  $C_{SPM}$  is suspended particulate matter concentration ( $1/m^3$ ) and  $k_{coll}$  is the collision rate ( $m^3/s$ ).  $C_{SPM}$  needs to be calculated using equation (S7) as

$$C_{SPM} = \frac{C_{mass,SPM}}{\frac{4}{3} * \rho_{SPM} * \pi * \left(\frac{d_{SPM}}{2}\right)^3} \quad (S7)$$

where  $C_{mass,SPM}$  is the mass concentration of suspended particulate matter in water ( $kg/m^3$ ),  $\rho_{SPM}$  is the density of suspended particulate matter ( $kg/m^3$ ) and  $d_{SPM}$  is the diameter of the suspended particulate matter in water (m). Another component of equation (S6), the collision rate, can be calculated using equation (S8).

$$k_{coll} = \frac{2k_B T_{water}}{3\mu_{water}} * \frac{(r_{nAg} + r_{SPM})^2}{r_{nAg} * r_{SPM}} + \frac{4}{3}G(r_{nAg} + r_{SPM})^3 + \pi(r_{nAg} + r_{SPM})^2 * |v_{set}^{nAg} - v_{set}^{SPM}| \quad (S8)$$

where  $k_B$  is Boltzmann constant ( $JK^{-1}$ ),  $T_{water}$  is the temperature of the water (K),  $\mu_{water}$  is the dynamic viscosity of water ( $Ns/m^2$ ),  $r_{nAg}$  is the radius of nAg (m),  $r_{SPM}$  is the radius of suspended particulate matter (m),  $G$  is the shear rate of the water (1/s),  $v_{set}^{nAg}$  is the settling velocity of nAg (m/s) and  $v_{set}^{SPM}$  is the settling velocity of suspended particulate matter (m/s). Equations (S9) and (S10) are used to calculate the settling velocities of nAg and SPM to be used in the collision rate calculation.

$$v_{set}^{nAg} = \frac{2}{9} * \frac{\rho_{nAg} - \rho_{water}}{\mu_{water}} * g * r_{nAg}^2 \quad (S9)$$

$$v_{set}^{SPM} = \frac{2}{9} * \frac{\rho_{SPM} - \rho_{water}}{\mu_{water}} * g * r_{SPM}^2 \quad (S10)$$

where  $\rho_{nAg}$  is the density of nAg ( $kg/m^3$ ),  $\rho_{water}$  is the density of water ( $kg/m^3$ ),  $\mu_{water}$  is the dynamic viscosity of water ( $Ns/m^2$ ),  $g$  is the gravitational acceleration on earth ( $m/s^2$ ),  $r_{nAg}$  is

the radius of nAg (m),  $\rho_{SPM}$  is the density of suspended particulate matter (kg/m<sup>3</sup>) and  $r_{SPM}$  is the radius of suspended particulate matter (m).

## **Sedimentation**

### *Scenario 2*

$$k_{sed}' = k_{sed}^{nAg} + k_{agg-sed} + k_{att-sed} \quad (S11)$$

where  $k_{sed}^{nAg}$  is the sedimentation rate constant (s<sup>-1</sup>),  $k_{agg-sed}$  is the minimum value of either pseudo-sedimentation rate constant for homo-aggregated nAg or the homo-aggregation rate constant as expressed in equation (S12) (s<sup>-1</sup>) and  $k_{att-sed}$  is the minimum value of either pseudo-sedimentation rate constant for hetero-aggregated (i.e. attached) nAg or the hetero-aggregation (i.e. attachment) rate constant as expressed in equation (S13) (s<sup>-1</sup>).

$$k_{agg-sed} = \text{minimum} (k_{homo-agg}, k_{ps-homo-agg}) \quad (S12)$$

where  $k_{agg}$  is the aggregation rate constant and  $k_{ps-agg}$  is the pseudo-sedimentation rate constant for aggregated nAg. In the current study, homo-aggregation is neglected, therefore this component is not calculated.

$$k_{att-sed} = \text{minimum} (k_{het-agg}, k_{ps-het-agg}) \quad (S13)$$

where  $k_{het-agg}$  is the attachment rate constant and  $k_{ps-het-agg}$  is the pseudo-sedimentation rate constant for attached nAg.

$$k_{sed}^{nAg} = \frac{v_{set}^{nAg}}{h_w} \quad (S14)$$

where  $v_{set}^{nAg}$  is the settling velocity of nAg as expressed in equation (S9) (m/s) and  $h_w$  is the depth of the water compartment (m).

$$k_{ps-het-agg} = \frac{v_{set}^{SPM}}{h_w} \quad (S15)$$



where  $v_{set}^{SPM}$  is the settling velocity of suspended particulate matter as expressed in equation (S10) (m/s) and  $h_w$  is the depth of the water compartment (m).

Table S4. Calculated parameters based on the values presented in Tables S2-S3 (shaded values are used in FF calculation for the respective scenarios)

Parameter	Symbol	Unit	Value (Scenario 1)	Value (Scenario 2)
Dissolution rate constant	$k_{diss}$	s <sup>-1</sup>	3.15×10 <sup>-7</sup>	3.15×10 <sup>-7</sup>
Hetero aggregation rate constant	$k_{het-agg}$	s <sup>-1</sup>	3.44×10 <sup>-5</sup>	-
Concentration of SPM	$C_{SPM}$	1/m <sup>3</sup>	2.88×10 <sup>13</sup>	2.88×10 <sup>13</sup>
Collision rate	$k_{coll}$	m <sup>3</sup> /s	9.95×10 <sup>-17</sup>	9.95×10 <sup>-17</sup>
Settling velocity of nAg	$v_{set}^{nAg}$	m/s	1.31×10 <sup>-8</sup>	1.31×10 <sup>-8</sup>
Settling velocity of SPM	$v_{set}^{SPM}$	m/s	7.29×10 <sup>-7</sup>	7.29×10 <sup>-7</sup>
Sedimentation rate constant	$k_{sed}$	s <sup>-1</sup>	1.09×10 <sup>-8</sup>	6.19×10 <sup>-7</sup>
Advection rate constant	$k_{adv}$	s <sup>-1</sup>	2.05×10 <sup>-8</sup>	2.05×10 <sup>-8</sup>
Removal rate constant for freshwater	$k_{w,w}$	s <sup>-1</sup>	3.48×10 <sup>-5</sup>	9.54×10 <sup>-7</sup>
Fate factor	FF	days	0.33	12

Table S5. List of characterization factors calculated in the current study and the literature values

Reference	Scenarios	XF (%)	FF (days)	EF (PAF.m <sup>3</sup> /kg)	CF (PAF.m <sup>3</sup> .day/kg or CTUe/kg)
(Garvey et al., 2019)	S1	60	30	1.35×10 <sup>4</sup>	2.43×10 <sup>5</sup>
	S2	80	130	2.81×10 <sup>5</sup>	2.92×10 <sup>7</sup>
(Pu, 2017)	-	100	1.36	1.45×10 <sup>4</sup>	1.97×10 <sup>4</sup>
(Miseljic and Olsen, 2014)	-	100	1	8.58×10 <sup>3</sup>	8.58×10 <sup>3</sup>
This study	S1 – Optimistic (regardless of coating)	100	0.33	8.04×10 <sup>3</sup>	2.67×10 <sup>3</sup>
	S1 – Skeptical (regardless of coating)	100	0.33	1.47×10 <sup>4</sup>	4.88×10 <sup>3</sup>
	S2 – Optimistic (regardless of coating)	100	12.13	8.04×10 <sup>3</sup>	9.74×10 <sup>4</sup>
	S2 – Skeptical (regardless of coating)	100	12.13	1.47×10 <sup>4</sup>	1.78×10 <sup>5</sup>
	S1 – Optimistic (PVP coated)	100	0.33	6.58×10 <sup>3</sup>	2.19×10 <sup>3</sup>
	S1 – Skeptical (PVP coated)	100	0.33	1.93×10 <sup>4</sup>	6.42×10 <sup>3</sup>
	S2 – Optimistic (PVP coated)	100	12.13	6.58×10 <sup>3</sup>	7.98×10 <sup>4</sup>
	S2 – Skeptical (PVP coated)	100	12.13	1.93×10 <sup>4</sup>	2.34×10 <sup>5</sup>
USEtox spreadsheet	For ionic silver Ag (I)	41.2	18.1	2.60×10 <sup>4</sup>	1.94×10 <sup>5</sup>

Table S6. Scenario 1: sensitivity factors (SF) based on 20% change of inputs on the rate constants and fate factor. Reported numbers are SFs, where red cells indicate sensitive inputs.

	$d_{nAg}$	$d_{SPM}$	$\rho_{nAg}$	$\alpha_{het-agg}$	$C_{mass,SPM}$	$C_0$	$C_{ions}$	$\rho_{SPM}$
$k_{het-agg}$	-1.67E-01	-4.04E-01	-5.50E-05	1.67E-01	1.67E-01	0.00E+00	0.00E+00	-1.91E-01
$k_{sed}$	3.06E-01	0.00E+00	1.81E-01	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
$k_{diss}$	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	-2.06E-01	1.71E-01	0.00E+00
$k_{adv}$	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
$k_{w,w}$	-1.65E-01	-3.98E-01	1.51E-05	1.65E-01	1.65E-01	-1.55E-03	1.87E-03	-1.89E-01
FF	1.41E-01	2.85E-01	-1.51E-05	-1.98E-01	-1.98E-01	1.54E-03	-1.87E-03	1.59E-01

Table S7. Scenario 1: sensitivity factors (SF) based on 20% change of rate constants on fate factor. Reported numbers are SFs, where red cells indicate sensitive inputs.

	$k_{het-agg}$	$k_{sed}$	$k_{diss}$	$k_{adv}$
$k_{w,w}$	1.65E-01	6.29E-05	1.81E-03	-1.18E-04
FF	-1.98E-01	-6.29E-05	-1.81E-03	-1.18E-04

Table S8. Scenario 2: sensitivity factors (SF) based on 20% change of inputs on the rate constants and fate factor. Reported numbers are SFs, where red cells indicate sensitive inputs.

	$d_{nAg}$	$d_{SPM}$	$\rho_{nAg}$	$\alpha_{het-agg}$	$C_{mass,SPM}$	$C_0$	$C_{ions}$	$\rho_{SPM}$
$k_{sed}$	7.72E-03	3.02E-01	3.89E-03	0.00E+00	0.00E+00	0.00E+00	0.00E+00	3.51E-01
$k_{diss}$	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	-2.06E-01	1.71E-01	0.00E+00
$k_{adv}$	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
$k_{w,w}$	5.02E-03	2.19E-01	2.53E-03	0.00E+00	0.00E+00	-5.96E-02	6.39E-02	2.60E-01
FF	-5.05E-03	-2.80E-01	-2.53E-03	0.00E+00	0.00E+00	5.63E-02	-6.82E-02	-3.51E-01

Table S9. Scenario 2: sensitivity factors (SF) based on 20% change of rate constants on fate factor. Reported numbers are SFs, where red cells indicate sensitive inputs.

	$k_{sed}$	$k_{diss}$	$k_{adv}$
$k_{w,w}$	1.15E-01	6.19E-02	4.28E-03
FF	-1.30E-01	-6.60E-02	-4.30E-03

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