

A synergistic approach to achieve high thermoelectric performance of La-doped SnTe using resonance state and partial band convergence

Srikanth Mandava^a, Ranita Basu^{b,*}, B. Khasimsaheb^c, Sivaiah Bathula^d, Sai Muthukumar V^e,
Ajay Singh^b, S. Neeleshwar^{a,*}

^aGuru Gobind Singh Indraprastha University, Delhi-110078, India

^bTechnical Physics Division, Bhabha Atomic Research Centre, Mumbai-400085, India

^cInstitute of Physics, Academia Sinica, Taipei, Taiwan - 11529.

^dDivision of Advanced Materials and Devices Metrology, CSIR-National Physical Laboratory, Dr. K. S. Krishnan Marg, New Delhi 110012, India & School of Minerals, Metallurgical and Materials Engineering, IIT Bhubaneswar-752050, Odisha, India

Supplementary Information

S1: EDS spectra and corresponding quantitative analysis results for all La-doped SnTe samples

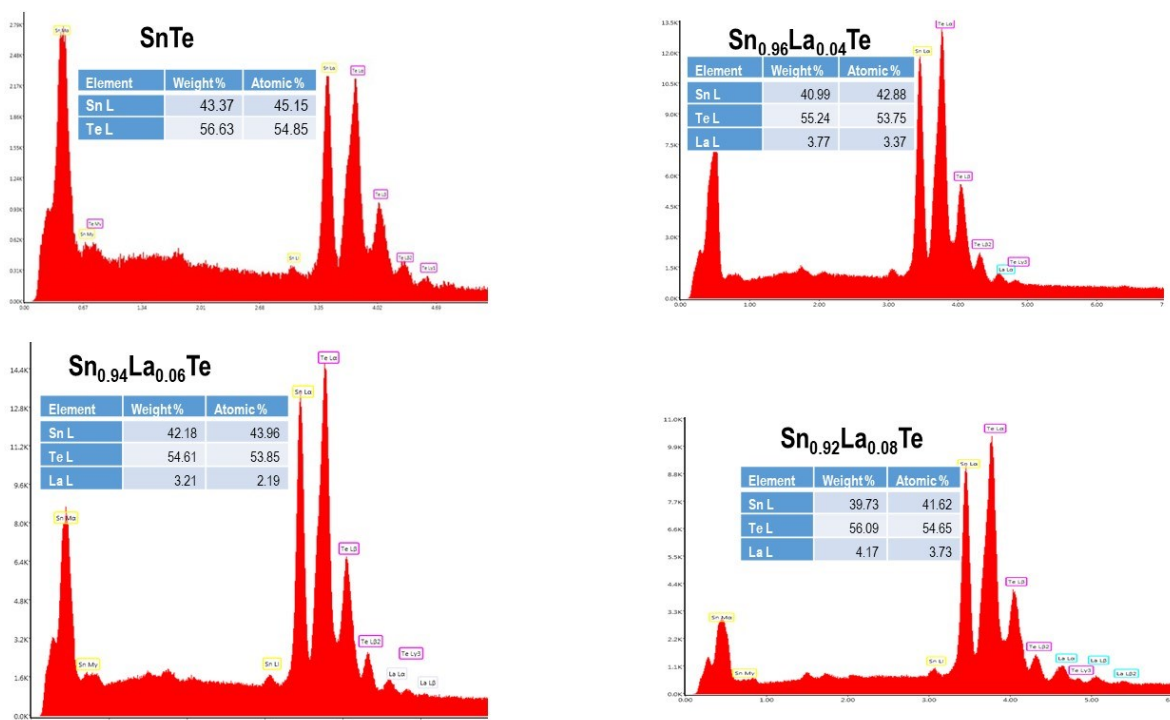


Figure S1: EDS spectra of Sn_{1-x}La_xTe (x=0, 0.04, 0.06, 0.08) for quantitative analysis.

S2: Point scan of $\text{Sn}_{0.92}\text{La}_{0.08}\text{Te}$ to show the precipitation of La when the concentration (x) is 8 at%.

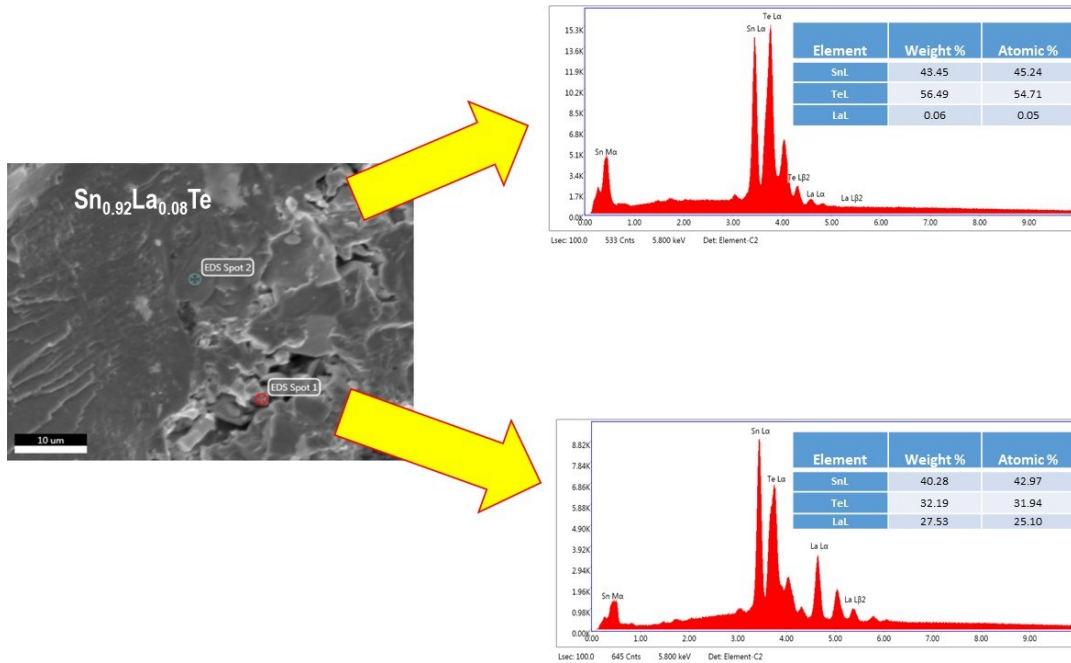


Figure S2: EDS spectra of point scan of $\text{Sn}_{0.92}\text{La}_{0.08}\text{Te}$ to show La-precipitation

S3: Band gap variation for $\text{SnTe} + x\% \text{La}$. The behaviors for both band gap variation and change of lattice parameter indicates a $\sim 6\% \text{La}$ solubility in SnTe

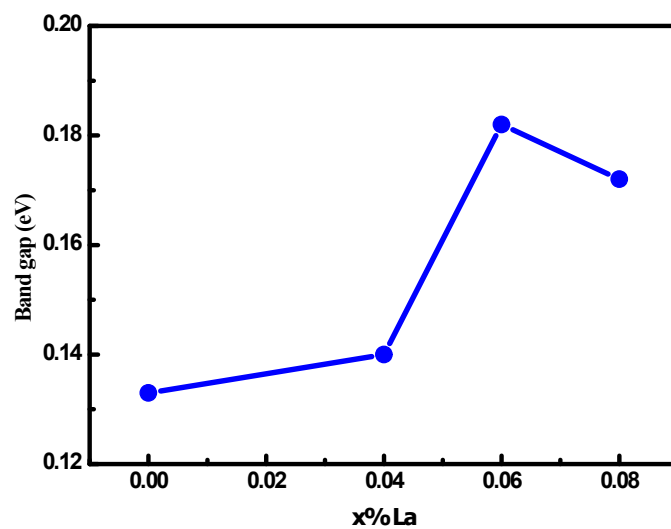
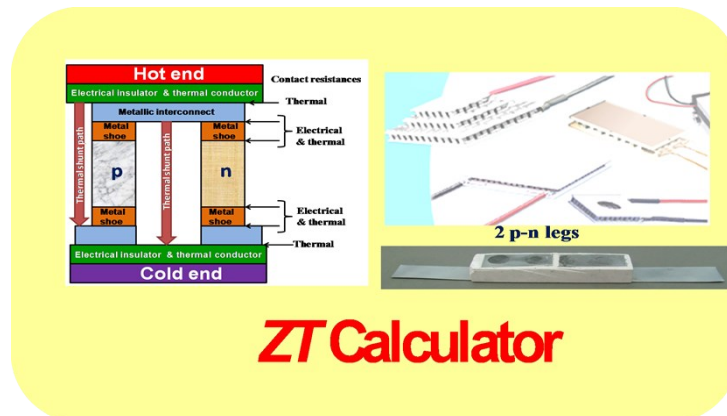


Figure S3: Band gap variation for $\text{SnTe} + x\% \text{La}$.

S4: Calculation of maximum efficiency



ZT Calculator

Although there is no analytic expression for Z , it can be calculated to any desired accuracy numerically with a simple procedure which can be done on a spreadsheet. To calculate the maximum efficiency Z and ZT follow these steps:

(1) Paste the temperature dependent $S(T)$, $\rho(T)$, and $\kappa(T)$ into the T , S , ρ , and κ columns – the 4 columns in the table are shaded blue. The cold side temperature for the calculation is the first temperature, 300 K. We shall use 800 K for hot side temperature for the example in Table 1. As per the literature, 25 K temperature intervals were maintained between data points, but that can vary. Smaller temperature steps give more accurate calculations.

(2) The first entry of the relative current value u is to be optimized. The values for u at higher temperature will adjust accordingly. This is similar to setting the electrical current (or load resistance) through the device. The power and therefore efficiency will be low at low values of u because little electrical current will be flowing through the device and low at high values of u because the output voltage will drop at high currents (and even becomes negative). For good efficiency the u values should be close to the compatibility factor s in the column next to u . Calculation for $u = 0$ is to be avoided as some calculations become undefined, but u arbitrarily small is fine (e.g. $u = 0.001$).

The efficiency of this thermoelectric leg is given in the efficiency column. The calculation assumes the first row (300 K in the Table) is the cold side. For 800 K hot side we should optimize the efficiency of the last row. MS Excel has a solver add-in that makes this easy, but other methods or adjusting by hand also works.

(3) The device ZT is calculated from the maximum efficiency value found by optimizing cold

side u value and the eqn. is given by

$$ZT = \left(\frac{T_h - T_c(1 - \eta)}{T_h(1 - \eta) - T_c} \right)^2 - 1$$

S.4.1 Spreadsheet for the calculation of ZT for SnTe

| T (C) | Material | T (K) | Seebeck ($\mu\text{V/K}$) | resistivity (10-3 Ω cm) | thermal cond (W/m K) | zT | max red eff | s (1/V) | u (1/V) | red eff | Φ (V) | efficiency | ZT |
|----------|----------|----------|--------------------------------|-----------------------------------|-------------------------|------|-------------|------------|------------|---------|---------------|------------|------|
| 27 | SnTe | 300 | 34 | 0.13 | 7.35 | 0.04 | 0.9% | 1.76 | 1.6072 | 0.9% | 0.632 | | |
| 52 | SnTe | 325 | 35 | 0.14 | 7.16 | 0.04 | 1.0% | 1.73 | 1.6093 | 1.0% | 0.633 | 0.1% | 0.04 |
| 77 | SnTe | 350 | 36 | 0.15 | 6.97 | 0.04 | 1.1% | 1.70 | 1.6115 | 1.1% | 0.633 | 0.1% | 0.04 |
| 102 | SnTe | 375 | 38 | 0.16 | 6.78 | 0.05 | 1.2% | 1.67 | 1.6139 | 1.2% | 0.634 | 0.2% | 0.04 |
| 127 | SnTe | 400 | 39 | 0.18 | 6.59 | 0.05 | 1.3% | 1.64 | 1.6166 | 1.3% | 0.634 | 0.3% | 0.04 |
| 152 | SnTe | 425 | 41 | 0.19 | 6.41 | 0.06 | 1.4% | 1.62 | 1.6196 | 1.4% | 0.635 | 0.4% | 0.05 |
| 177 | SnTe | 450 | 42 | 0.21 | 6.23 | 0.06 | 1.5% | 1.60 | 1.6229 | 1.5% | 0.635 | 0.5% | 0.05 |
| 202 | SnTe | 475 | 44 | 0.23 | 6.04 | 0.07 | 1.6% | 1.59 | 1.6266 | 1.6% | 0.636 | 0.6% | 0.05 |
| 227 | SnTe | 500 | 46 | 0.25 | 5.86 | 0.07 | 1.8% | 1.58 | 1.6308 | 1.8% | 0.636 | 0.6% | 0.05 |
| 252 | SnTe | 525 | 49 | 0.26 | 5.68 | 0.08 | 2.0% | 1.58 | 1.6354 | 2.0% | 0.637 | 0.7% | 0.06 |
| 277 | SnTe | 550 | 51 | 0.28 | 5.51 | 0.09 | 2.2% | 1.59 | 1.6406 | 2.2% | 0.638 | 0.8% | 0.06 |
| 302 | SnTe | 575 | 54 | 0.31 | 5.33 | 0.10 | 2.4% | 1.61 | 1.6465 | 2.4% | 0.638 | 0.9% | 0.06 |
| 327 | SnTe | 600 | 57 | 0.33 | 5.15 | 0.11 | 2.7% | 1.63 | 1.6530 | 2.7% | 0.639 | 1.0% | 0.06 |
| 352 | SnTe | 625 | 60 | 0.35 | 4.98 | 0.13 | 3.0% | 1.66 | 1.6604 | 3.0% | 0.640 | 1.2% | 0.07 |
| 377 | SnTe | 650 | 63 | 0.37 | 4.80 | 0.14 | 3.4% | 1.70 | 1.6686 | 3.4% | 0.640 | 1.3% | 0.07 |
| 402 | SnTe | 675 | 67 | 0.40 | 4.63 | 0.16 | 3.8% | 1.75 | 1.6779 | 3.8% | 0.641 | 1.4% | 0.08 |
| 427 | SnTe | 700 | 71 | 0.43 | 4.45 | 0.19 | 4.3% | 1.80 | 1.6882 | 4.3% | 0.642 | 1.6% | 0.08 |
| 452 | SnTe | 725 | 76 | 0.45 | 4.28 | 0.22 | 4.9% | 1.86 | 1.6998 | 4.8% | 0.643 | 1.7% | 0.09 |
| 477 | SnTe | 750 | 81 | 0.48 | 4.10 | 0.25 | 5.5% | 1.93 | 1.7128 | 5.5% | 0.644 | 1.9% | 0.09 |
| 502 | SnTe | 775 | 86 | 0.51 | 3.93 | 0.29 | 6.3% | 2.00 | 1.7274 | 6.2% | 0.646 | 2.1% | 0.10 |

S.4.2 Spreadsheet for the calculation of ZT for Sn_{0.96}La_{0.04}Te

| T (C) | Material | T (K) | Seebeck ($\mu\text{V/K}$) | resistivity (10-3 Ω cm) | thermal cond (W/m K) | zT | max red eff | s (1/V) | u (1/V) | red eff | Φ (V) | efficiency | ZT |
|----------|--|----------|--------------------------------|-----------------------------------|-------------------------|------|-------------|------------|------------|---------|---------------|------------|------|
| 27 | Sn _{0.96} La _{0.04} Te | 300 | 41 | 0.17 | 5.53 | 0.05 | 1.3% | 2.15 | 2.1237 | 1.3% | 0.483 | | |
| 52 | Sn _{0.96} La _{0.04} Te | 325 | 42 | 0.18 | 5.39 | 0.06 | 1.5% | 2.16 | 2.1281 | 1.5% | 0.484 | 0.1% | 0.06 |
| 77 | Sn _{0.96} La _{0.04} Te | 350 | 44 | 0.19 | 5.26 | 0.07 | 1.6% | 2.15 | 2.1328 | 1.6% | 0.484 | 0.2% | 0.06 |
| 102 | Sn _{0.96} La _{0.04} Te | 375 | 46 | 0.20 | 5.13 | 0.07 | 1.8% | 2.16 | 2.1380 | 1.8% | 0.485 | 0.3% | 0.06 |
| 127 | Sn _{0.96} La _{0.04} Te | 400 | 47 | 0.21 | 5.01 | 0.08 | 2.0% | 2.16 | 2.1438 | 2.0% | 0.485 | 0.5% | 0.07 |
| 152 | Sn _{0.96} La _{0.04} Te | 425 | 49 | 0.23 | 4.88 | 0.09 | 2.2% | 2.16 | 2.1501 | 2.2% | 0.486 | 0.6% | 0.07 |
| 177 | Sn _{0.96} La _{0.04} Te | 450 | 51 | 0.24 | 4.75 | 0.10 | 2.4% | 2.16 | 2.1571 | 2.4% | 0.487 | 0.7% | 0.08 |
| 202 | Sn _{0.96} La _{0.04} Te | 475 | 53 | 0.26 | 4.62 | 0.11 | 2.7% | 2.17 | 2.1648 | 2.7% | 0.487 | 0.9% | 0.08 |
| 227 | Sn _{0.96} La _{0.04} Te | 500 | 56 | 0.28 | 4.50 | 0.12 | 2.9% | 2.17 | 2.1732 | 2.9% | 0.488 | 1.0% | 0.08 |
| 252 | Sn _{0.96} La _{0.04} Te | 525 | 58 | 0.30 | 4.38 | 0.14 | 3.2% | 2.17 | 2.1824 | 3.2% | 0.489 | 1.2% | 0.09 |
| 277 | Sn _{0.96} La _{0.04} Te | 550 | 61 | 0.32 | 4.26 | 0.15 | 3.5% | 2.17 | 2.1925 | 3.5% | 0.490 | 1.3% | 0.09 |
| 302 | Sn _{0.96} La _{0.04} Te | 575 | 63 | 0.34 | 4.15 | 0.16 | 3.8% | 2.16 | 2.2035 | 3.8% | 0.490 | 1.5% | 0.10 |
| 327 | Sn _{0.96} La _{0.04} Te | 600 | 66 | 0.37 | 4.02 | 0.18 | 4.1% | 2.16 | 2.2155 | 4.1% | 0.491 | 1.6% | 0.10 |
| 352 | Sn _{0.96} La _{0.04} Te | 625 | 69 | 0.39 | 3.90 | 0.20 | 4.5% | 2.16 | 2.2286 | 4.5% | 0.492 | 1.8% | 0.11 |
| 377 | Sn _{0.96} La _{0.04} Te | 650 | 72 | 0.42 | 3.79 | 0.21 | 4.8% | 2.15 | 2.2428 | 4.8% | 0.493 | 2.0% | 0.11 |
| 402 | Sn _{0.96} La _{0.04} Te | 675 | 76 | 0.45 | 3.68 | 0.23 | 5.2% | 2.15 | 2.2582 | 5.2% | 0.494 | 2.2% | 0.12 |
| 427 | Sn _{0.96} La _{0.04} Te | 700 | 79 | 0.49 | 3.57 | 0.25 | 5.6% | 2.14 | 2.2750 | 5.6% | 0.495 | 2.4% | 0.13 |
| 452 | Sn _{0.96} La _{0.04} Te | 725 | 82 | 0.52 | 3.46 | 0.27 | 6.0% | 2.13 | 2.2932 | 6.0% | 0.496 | 2.6% | 0.13 |
| 477 | Sn _{0.96} La _{0.04} Te | 750 | 86 | 0.56 | 3.36 | 0.29 | 6.4% | 2.13 | 2.3130 | 6.4% | 0.497 | 2.8% | 0.14 |
| 502 | Sn _{0.96} La _{0.04} Te | 775 | 90 | 0.61 | 3.25 | 0.31 | 6.8% | 2.11 | 2.3345 | 6.8% | 0.498 | 3.0% | 0.15 |

S.4.3 Spreadsheet for the calculation of ZT for Sn_{0.96}La_{0.04}Te

| <i>T</i> (C) | Material | <i>T</i> (K) | Seebeck (μV/K) | resistivity (10 ⁻³ Ω cm) | thermal cond (W/m K) | <i>zT</i> | max red eff | <i>s</i> (1/V) | <i>u</i> (1/V) | red eff | Φ (V) | efficiency | ZT |
|-----------------|--|-----------------|-------------------|--|-------------------------|-----------|-------------|-------------------|-------------------|---------|----------|------------|------|
| 27 | Sn _{0.94} La _{0.06} Te | 300 | 43 | 0.16 | 6.16 | 0.06 | 1.4% | 2.13 | 2.0457 | 1.3% | 0.502 | | |
| 52 | Sn _{0.94} La _{0.06} Te | 325 | 44 | 0.17 | 5.95 | 0.06 | 1.5% | 2.12 | 2.0492 | 1.5% | 0.502 | 0.1% | 0.06 |
| 77 | Sn _{0.94} La _{0.06} Te | 350 | 45 | 0.18 | 5.75 | 0.07 | 1.6% | 2.09 | 2.0531 | 1.6% | 0.503 | 0.2% | 0.06 |
| 102 | Sn _{0.94} La _{0.06} Te | 375 | 46 | 0.20 | 5.55 | 0.07 | 1.8% | 2.07 | 2.0575 | 1.8% | 0.503 | 0.3% | 0.06 |
| 127 | Sn _{0.94} La _{0.06} Te | 400 | 48 | 0.21 | 5.36 | 0.08 | 1.9% | 2.06 | 2.0625 | 1.9% | 0.504 | 0.5% | 0.07 |
| 152 | Sn _{0.94} La _{0.06} Te | 425 | 50 | 0.23 | 5.17 | 0.09 | 2.1% | 2.05 | 2.0682 | 2.1% | 0.505 | 0.6% | 0.07 |
| 177 | Sn _{0.94} La _{0.06} Te | 450 | 52 | 0.25 | 4.98 | 0.10 | 2.3% | 2.05 | 2.0747 | 2.3% | 0.505 | 0.7% | 0.07 |
| 202 | Sn _{0.94} La _{0.06} Te | 475 | 54 | 0.27 | 4.79 | 0.11 | 2.6% | 2.06 | 2.0820 | 2.6% | 0.506 | 0.8% | 0.08 |
| 227 | Sn _{0.94} La _{0.06} Te | 500 | 56 | 0.29 | 4.62 | 0.12 | 2.8% | 2.06 | 2.0902 | 2.8% | 0.507 | 1.0% | 0.08 |
| 252 | Sn _{0.94} La _{0.06} Te | 525 | 59 | 0.31 | 4.45 | 0.13 | 3.1% | 2.07 | 2.0993 | 3.1% | 0.507 | 1.1% | 0.09 |
| 277 | Sn _{0.94} La _{0.06} Te | 550 | 62 | 0.34 | 4.28 | 0.15 | 3.4% | 2.08 | 2.1096 | 3.4% | 0.508 | 1.3% | 0.09 |
| 302 | Sn _{0.94} La _{0.06} Te | 575 | 65 | 0.36 | 4.12 | 0.16 | 3.8% | 2.10 | 2.1210 | 3.8% | 0.509 | 1.4% | 0.10 |
| 327 | Sn _{0.94} La _{0.06} Te | 600 | 69 | 0.39 | 3.96 | 0.18 | 4.2% | 2.13 | 2.1336 | 4.2% | 0.510 | 1.6% | 0.10 |
| 352 | Sn _{0.94} La _{0.06} Te | 625 | 72 | 0.42 | 3.80 | 0.20 | 4.6% | 2.16 | 2.1476 | 4.6% | 0.511 | 1.8% | 0.11 |
| 377 | Sn _{0.94} La _{0.06} Te | 650 | 76 | 0.45 | 3.66 | 0.23 | 5.2% | 2.20 | 2.1630 | 5.2% | 0.512 | 2.0% | 0.11 |
| 402 | Sn _{0.94} La _{0.06} Te | 675 | 80 | 0.48 | 3.52 | 0.26 | 5.7% | 2.25 | 2.1799 | 5.7% | 0.513 | 2.2% | 0.12 |
| 427 | Sn _{0.94} La _{0.06} Te | 700 | 84 | 0.51 | 3.39 | 0.29 | 6.4% | 2.31 | 2.1985 | 6.4% | 0.514 | 2.4% | 0.13 |
| 452 | Sn _{0.94} La _{0.06} Te | 725 | 89 | 0.53 | 3.26 | 0.33 | 7.1% | 2.38 | 2.2188 | 7.1% | 0.515 | 2.6% | 0.14 |
| 477 | Sn _{0.94} La _{0.06} Te | 750 | 94 | 0.56 | 3.13 | 0.38 | 8.0% | 2.47 | 2.2410 | 7.9% | 0.516 | 2.9% | 0.15 |
| 502 | Sn _{0.94} La _{0.06} Te | 775 | 99 | 0.59 | 3.01 | 0.43 | 8.9% | 2.55 | 2.2652 | 8.8% | 0.518 | 3.1% | 0.15 |
| 527 | Sn _{0.94} La _{0.06} Te | 800 | 105 | 0.62 | 2.90 | 0.49 | 9.9% | 2.64 | 2.2946 | 9.8% | 0.519 | 3.4% | 0.17 |
| 552 | Sn _{0.94} La _{0.06} Te | 825 | 110 | 0.65 | 2.79 | 0.55 | 10.98% | 2.71 | 2.3249 | 10.79% | 0.52108 | 3.72% | 0.18 |

S.4.4 Spreadsheet for the calculation of ZT for Sn_{0.92}La_{0.08}Te

| T (C) | Material | T (K) | Seebeck ($\mu\text{V/K}$) | resistivity ($10^{-3} \Omega \text{ cm}$) | thermal cond (W/m K) | zT | max red eff | s ($1/\text{V}$) | u ($1/\text{V}$) | red eff | Φ (V) | efficiency | ZT |
|------------|----------------|------------|--------------------------------|--|------------------------------------|------|-------------|-------------------------|-------------------------|---------|---------------|------------|------|
| 27 | Sn0.92La0.08Te | 300 | 41 | 0.16 | 5.67 | 0.06 | 1.4% | 2.27 | 2.2220 | 1.4% | 0.462 | | |
| 52 | Sn0.92La0.08Te | 325 | 43 | 0.17 | 5.50 | 0.06 | 1.6% | 2.27 | 2.2266 | 1.6% | 0.463 | 0.1% | 0.06 |
| 77 | Sn0.92La0.08Te | 350 | 44 | 0.18 | 5.35 | 0.07 | 1.7% | 2.25 | 2.2316 | 1.7% | 0.464 | 0.2% | 0.06 |
| 102 | Sn0.92La0.08Te | 375 | 46 | 0.19 | 5.19 | 0.08 | 1.9% | 2.25 | 2.2371 | 1.9% | 0.464 | 0.4% | 0.07 |
| 127 | Sn0.92La0.08Te | 400 | 47 | 0.21 | 5.04 | 0.09 | 2.1% | 2.24 | 2.2434 | 2.1% | 0.465 | 0.5% | 0.07 |
| 152 | Sn0.92La0.08Te | 425 | 49 | 0.22 | 4.90 | 0.10 | 2.3% | 2.24 | 2.2503 | 2.3% | 0.465 | 0.6% | 0.08 |
| 177 | Sn0.92La0.08Te | 450 | 51 | 0.24 | 4.74 | 0.11 | 2.5% | 2.25 | 2.2581 | 2.5% | 0.466 | 0.8% | 0.08 |
| 202 | Sn0.92La0.08Te | 475 | 54 | 0.25 | 4.59 | 0.12 | 2.8% | 2.26 | 2.2668 | 2.8% | 0.467 | 0.9% | 0.08 |
| 227 | Sn0.92La0.08Te | 500 | 56 | 0.27 | 4.45 | 0.13 | 3.1% | 2.26 | 2.2764 | 3.1% | 0.467 | 1.1% | 0.09 |
| 252 | Sn0.92La0.08Te | 525 | 59 | 0.29 | 4.31 | 0.15 | 3.4% | 2.27 | 2.2870 | 3.4% | 0.468 | 1.2% | 0.09 |
| 277 | Sn0.92La0.08Te | 550 | 62 | 0.31 | 4.17 | 0.16 | 3.7% | 2.28 | 2.2988 | 3.7% | 0.469 | 1.4% | 0.10 |
| 302 | Sn0.92La0.08Te | 575 | 65 | 0.34 | 4.04 | 0.18 | 4.1% | 2.29 | 2.3117 | 4.1% | 0.470 | 1.5% | 0.10 |
| 327 | Sn0.92La0.08Te | 600 | 68 | 0.36 | 3.90 | 0.20 | 4.5% | 2.31 | 2.3260 | 4.5% | 0.471 | 1.7% | 0.11 |
| 352 | Sn0.92La0.08Te | 625 | 71 | 0.39 | 3.76 | 0.22 | 4.9% | 2.33 | 2.3417 | 4.9% | 0.471 | 1.9% | 0.12 |
| 377 | Sn0.92La0.08Te | 650 | 75 | 0.41 | 3.63 | 0.24 | 5.4% | 2.35 | 2.3588 | 5.4% | 0.472 | 2.1% | 0.12 |
| 402 | Sn0.92La0.08Te | 675 | 78 | 0.44 | 3.51 | 0.27 | 5.9% | 2.38 | 2.3776 | 5.9% | 0.473 | 2.3% | 0.13 |
| 427 | Sn0.92La0.08Te | 700 | 82 | 0.47 | 3.39 | 0.30 | 6.5% | 2.41 | 2.3981 | 6.5% | 0.475 | 2.5% | 0.14 |
| 452 | Sn0.92La0.08Te | 725 | 86 | 0.50 | 3.27 | 0.33 | 7.1% | 2.45 | 2.4205 | 7.1% | 0.476 | 2.8% | 0.15 |
| 477 | Sn0.92La0.08Te | 750 | 90 | 0.53 | 3.15 | 0.37 | 7.8% | 2.51 | 2.4448 | 7.8% | 0.477 | 3.0% | 0.15 |
| 502 | Sn0.92La0.08Te | 775 | 95 | 0.55 | 3.03 | 0.41 | 8.6% | 2.58 | 2.4713 | 8.6% | 0.478 | 3.3% | 0.16 |
| 527 | Sn0.92La0.08Te | 800 | 99 | 0.58 | 2.92 | 0.47 | 9.6% | 2.66 | 2.5000 | 9.5% | 0.480 | 3.6% | 0.17 |
| 552 | Sn0.92La0.08Te | 825 | 104 | 0.60 | 2.81 | 0.53 | 10.63% | 2.77 | 2.5312 | 10.57% | 0.48103 | 3.86% | 0.18 |