

Supporting Information

Exploring the effect of acid modulators on MIL-101 (Cr) metal-organic framework catalysed olefin-aldehyde condensation; A sustainable approach for the selective synthesis of nopol

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Figure S1. Pyridine FTIR spectra of MIL-101(Cr) catalysts

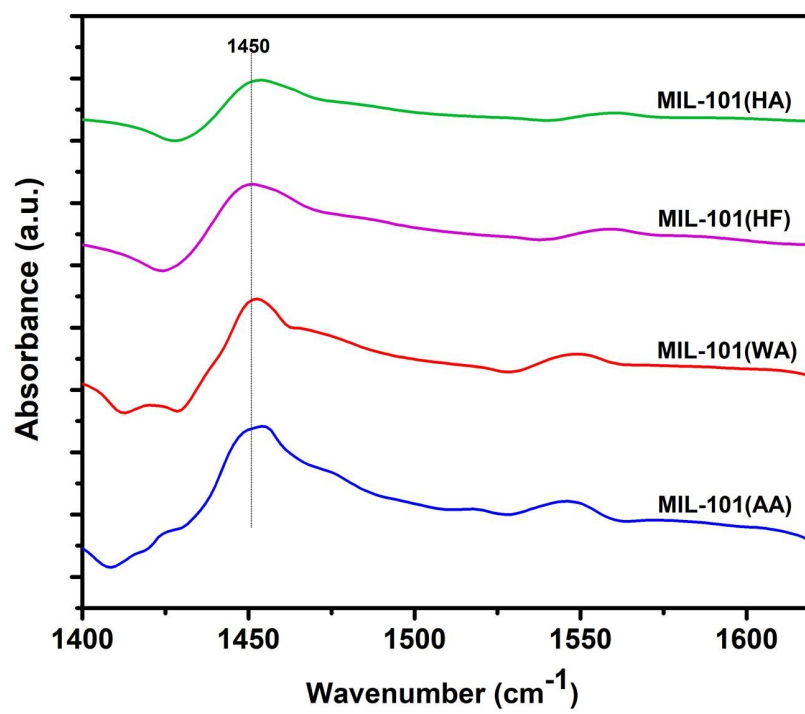


Figure S2. Plausible mechanism for the Prins condensation of β -pinene with p-formaldehyde

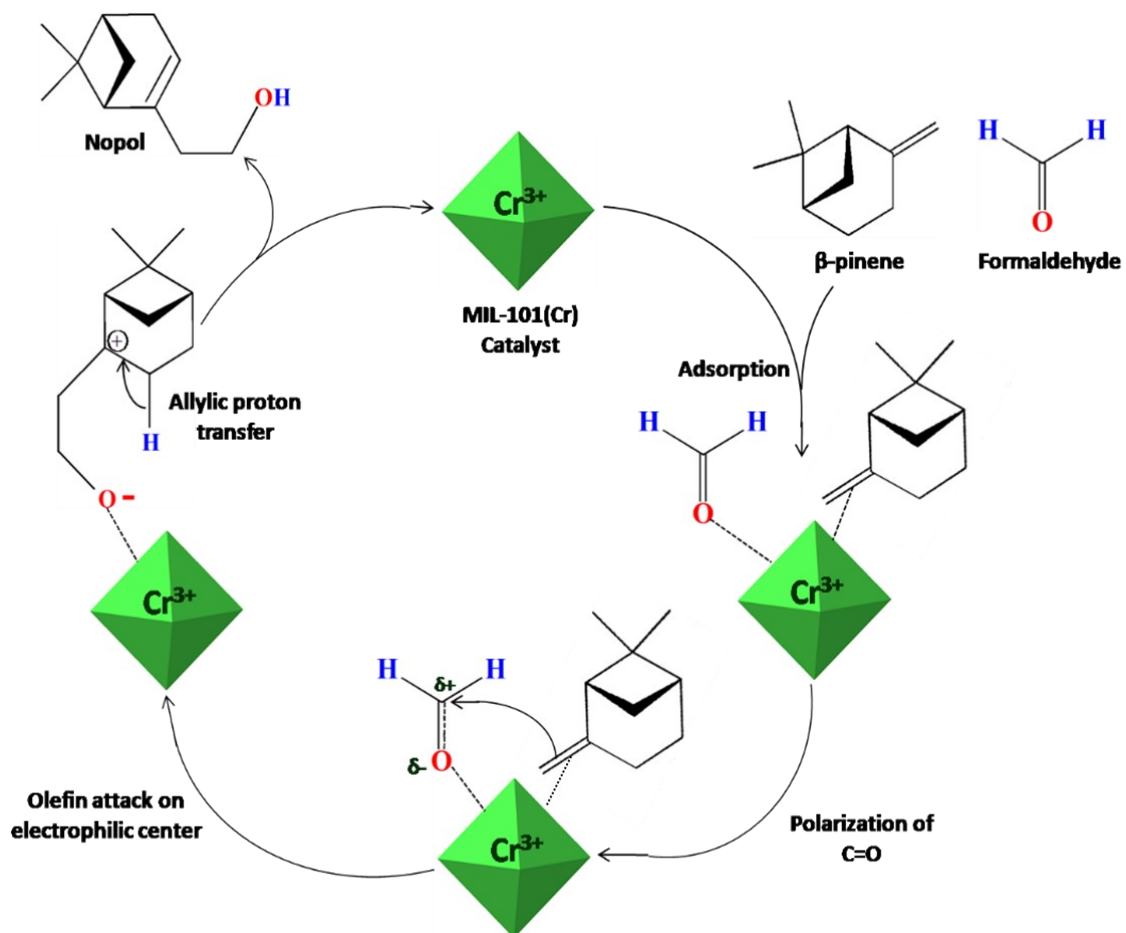


Figure S3. PXRD profile of spent MIL-101(AA) catalyst

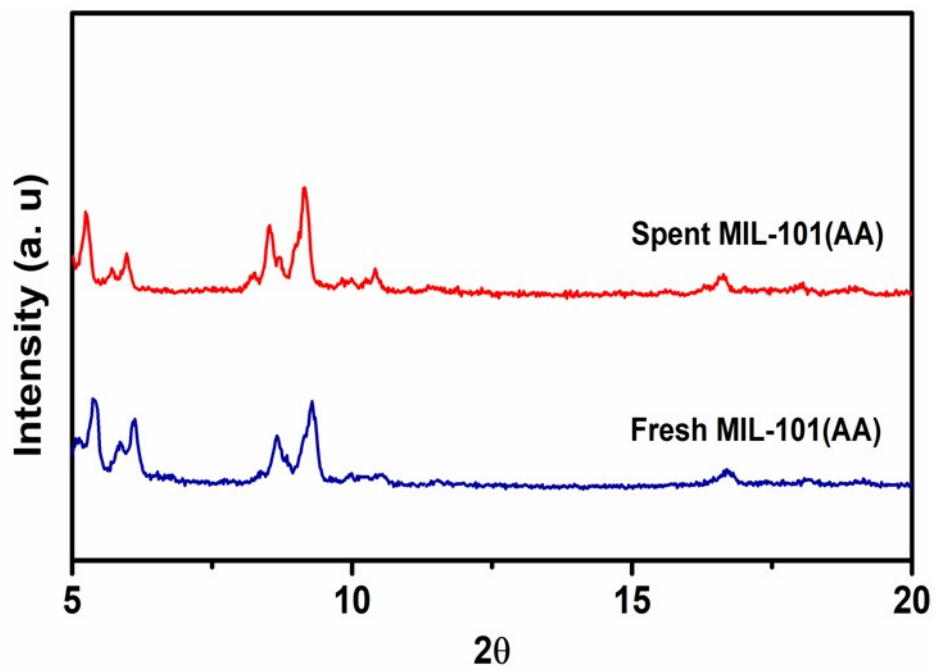


Figure S4. N₂ sorption isotherm of spent MIL-101(AA) catalyst

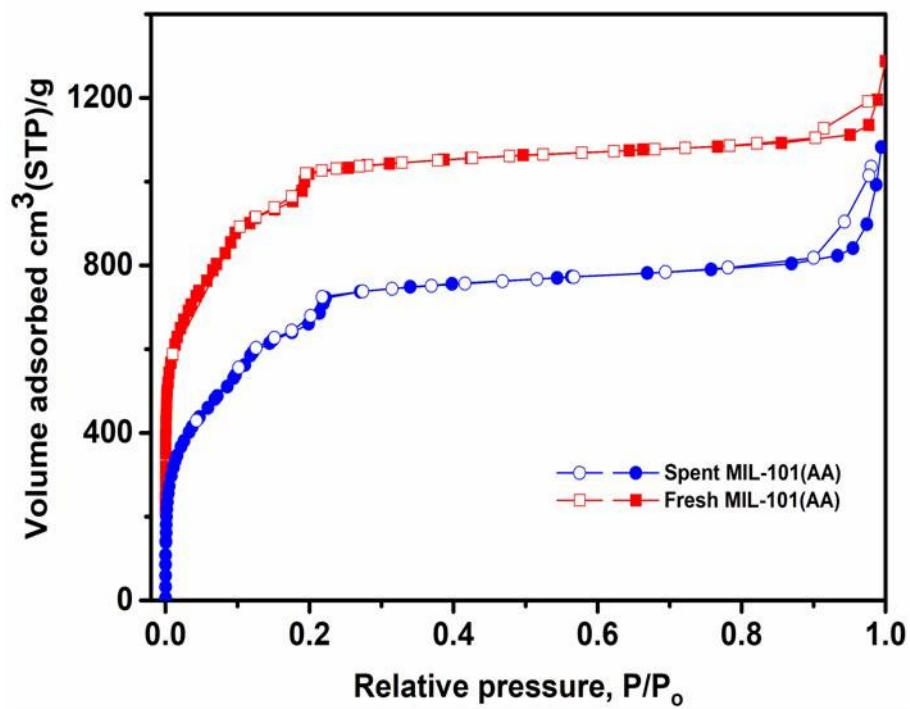


Figure S5. TGA profile of spent MIL-101(AA) catalyst

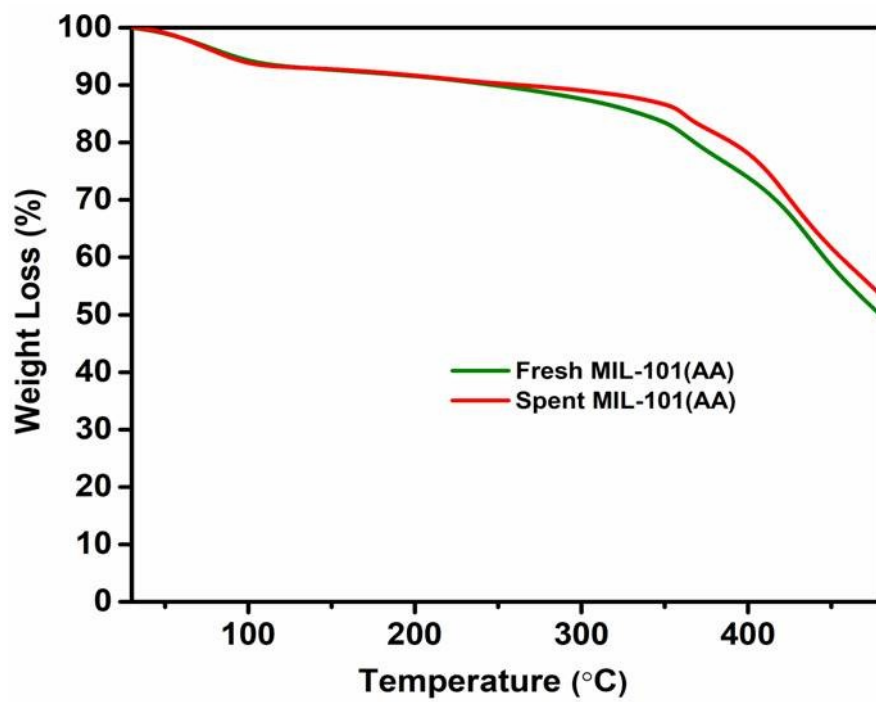


Figure S6. FTIR spectra of spent MIL-101(AA) catalyst

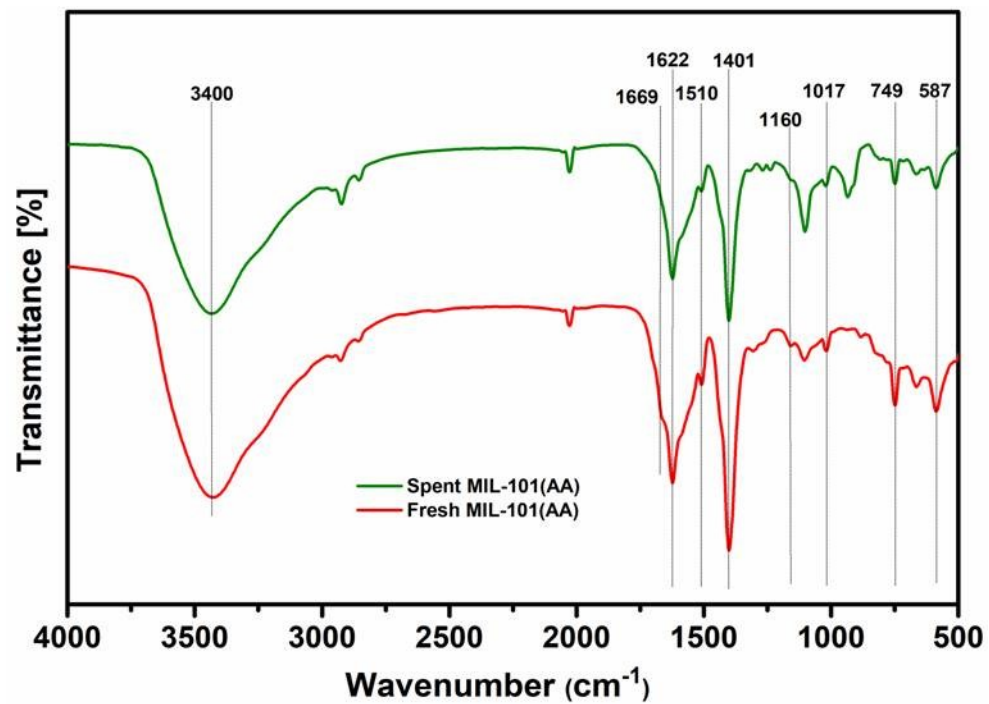


Figure S7. Py-FTIR spectra of spent MIL-101(AA) catalyst

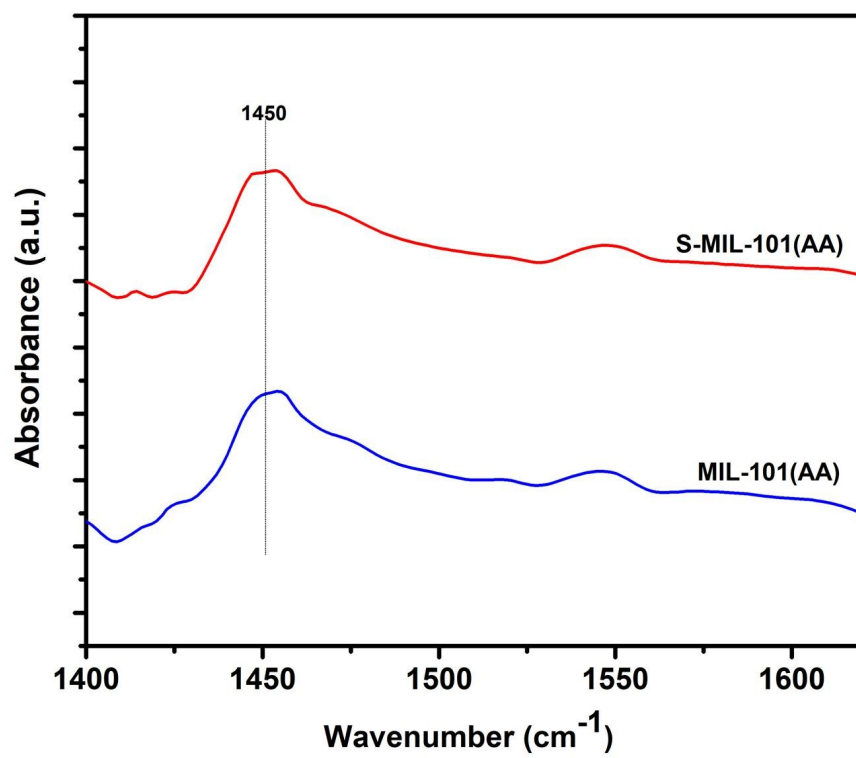


Table S1. Selected literature on the Prins Condensation of β -pinene with p-formaldehyde

| Sl. no. | Catalyst | Cat. (Wt.%) | ^a Mole ratio | Time (h) | Temp. (°C) | Solvent | Conv. (%) | ^b Sel. (%) | TOF | Ref. |
|-----------|---|-------------|-------------------------|------------|-------------|---------------------|-----------|-----------------------|-------------|-----------|
| 1 | MIL-100(Fe) | 25.5 | 2.0 | 5.0 | 80.0 | Acetonitrile | 82 | - | 2.2 | [1] |
| 2 | MIL-100(Fe,Ni) | 9.0 | 1.0 | 10.0 | 80.0 | Acetonitrile | 90 | - | NA | [2] |
| 3 | Fe-BTC | 25.5 | 2.0 | 6.0 | 80.0 | Acetonitrile | 47 | 100 | 0.7 | [3] |
| 4 | 0.94Zr-MCM-41(550) | 25.5 | 2.0 | 6.0 | 90.0 | Toluene | 97 | 90 | 23.1 | [4] |
| 5 | Zn-Al-MCM-41(151) | 143.2 | 1.7 | 6.0 | 90.0 | Toluene | 75 | 94 | 4.9 | [5] |
| 6 | FePO ₄ | 50.9 | 2.0 | 6.0 | 80.0 | Acetonitrile | 82 | 100 | NA | [6] |
| 7 | Fe-Zn-DMC | 10.2 | 2.0 | 12.0 | 80.0 | Toluene | 90 | - | 1.9 | [7] |
| 8 | Sn-MCM-41 | 144.2 | 2.0 | 6.5 | 90.0 | Toluene | 98 | 80 | NA | [8] |
| 9 | Zn-Beta | 20.0 | 2.0 | 10.0 | 90.0 | Benzonitrile | 92 | 85 | 1.2 | [9] |
| 10 | SZF-470 | 12.4 | 3.0 | 12.0 | 95.0 | Toluene | 70 | 88 | 3.8 | [10] |
| 11 | SnMB16 | 50.9 | 2.0 | 1.0 | 90.0 | Toluene | 95 | 79 | 237.1 | [11] |
| 12 | Sn-MCM-41-D1 | 50.9 | 2.0 | 1.0 | 90.0 | Toluene | 99 | 98 | NA | [12] |
| 13 | Sn-SBA-15 | 12.7 | 2.0 | 6.0 | 90.0 | Toluene | 99 | 95 | NA | [13] |
| 14 | SZ-2N | 11.0 | 3.0 | 9.0 | 80.0 | Acetonitrile | 99 | 99 | 3.7 | [14] |
| 15 | SnO ₂ -T-350 | 383.7 | 0.4 | 10.0 | 90.0 | Benzonitrile | 80 | 93 | 0.2 | [15] |
| 16 | Na-ZrO ₂ -ZrP-a-350 | 25.5 | 2.0 | 4.0 | 80.0 | Toluene | 86 | 87 | 11.9 | [16] |
| 17 | 10Zr-208-8 | 25.5 | 2.0 | 6.0 | 80.0 | Toluene | 74 | 100 | 4.8 | [17] |
| 18 | MoO _x / γ -Al ₂ O ₃ | 20.0 | 2.0 | 10.0 | 90.0 | Benzonitrile | 96 | 86 | 2.7 | [18] |
| 19 | SnCl ₂ -I-24 | 24.5 | 2.0 | 3.0 | 90.0 | Toluene | 79 | 86 | NA | [19] |
| 20 | Zn-MMT | 10.2 | 2.0 | 24.0 | 80.0 | Acetonitrile | 75 | 97 | NA | [20] |
| 21 | MIL-101(AA) | 5.0 | 2.0 | 6.0 | 90.0 | Benzonitrile | 98 | >99 | 18.9 | CW |
| 22 | MIL-101(WA) | 5.0 | 2.0 | 6.0 | 90.0 | Benzonitrile | 86 | >99 | 23.2 | CW |
| 23 | MIL-101(HF) | 5.0 | 2.0 | 6.0 | 90.0 | Benzonitrile | 80 | >99 | 24.7 | CW |
| 24 | MIL-101(HA) | 5.0 | 2.0 | 6.0 | 90.0 | Benzonitrile | 58 | >99 | 25.2 | CW |
| 25 | MIL-101(AA) | 5.0 | 2.0 | 3.0 | 90.0 | Benzonitrile | 67 | >99 | 25.9 | CW |

^a- Mole ratio (β -pinene top-formaldehyde)^b- Nopol selectivity

TOF- Turn-over frequency

NA- Not available

CW- Current work

Table S2.Solvent properties

| Solvent | AN | DN | BP (°C) | DC | HSP (MPa)^{1/2} |
|----------------|-----------|-----------|--------------------|-----------|------------------------------------|
| Acetonitrile | 18.9 | 14.1 | 82 | 37.5 | 24.3 |
| Benzonitrile | 15.5 | 11.9 | 191 | 26.0 | 19.9 |
| Nitrobenzene | 14.8 | 4.4 | 210.9 | 34.8 | 22.2 |
| Toluene | 8.2 | 0 | 110.6 | 2.4 | 18.2 |
| Cyclohexane | 0 | 0 | 80.75 | 2.0 | 16.7 |

AN: Acceptor number

DN: Donor number

BP: Boiling point

DC: Dielectric constant

HSP: Hansen's solubility parameter

Table S3. Textural and surface acidic Properties of spent MIL-101(AA) catalyst obtained from N₂ sorption at 77K and NH₃-TPD analysis

| Sample | S_{BET}^a (m² g⁻¹) | V_{total}^b (cm³ g⁻¹) | D_p^c (nm) | Acidity^d (mmol g⁻¹) |
|-------------------|---|--|---|--|
| Fresh MIL-101(AA) | 3014 | 1.75 | 2.32 | 0.88 |
| Spent-MIL-101(AA) | 2867 | 1.62 | 2.34 | 0.78 |

^aS_{BET} is the specific surface area determined by Brunauer-Emmett-Teller (BET) method

^bV_{total} is the total pore volume at $p/p_0 = 0.990$

^cD_p is the mean pore diameter

^dAcidity of the material calculated from NH₃-TPD measurement

Table S4. Comparison of various kinetic models

| No. | Kinetic Model | R^2 | Linearized kinetic parameter equations | R_i^2 |
|-----|--|-------|--|---|
| M1 | $R = \frac{K_s(C_F C_B)}{\{1 + K_F C_F\}}$ | 0.989 | $\ln K_F = \frac{9225.1}{T} - 23.37$ $\ln K_S = \frac{-12317}{T} + 35.747$ | $R_{kf^2}^2 = 0.967$ $R_{ks}^2 = 0.9547$ |
| M2 | $R = \frac{K_s(C_F C_B)}{\{1 + K_F C_F + K_N C_N\}}$ | 0.988 | $\ln K_F = \frac{7167}{T} - 16.53$ $\ln K_n = \frac{3759}{T} - 101.33$ $\ln K_S = \frac{-9693}{T} + 28.96$ | $R_{kf^2}^2 = 0.807$ $R_{kn^2}^2 = 0.7951$ $R_{ks}^2 = 0.9772$ |
| M3 | $R = \frac{K_s(C_F C_B - C_N/K_c)}{\{1 + K_F C_F + K_N C_N\}}$ | 0.988 | $\ln K_F = \frac{13204}{T} - 33.59$ $\ln K_n = \frac{39980}{T} - 108.33$ $\ln K_S = \frac{-8644}{T} + 25.99$ | $R_{kf^2}^2 = 0.9992$ $R_{kn^2}^2 = 0.8229$ $R_{ks}^2 = 0.8892$ |
| M4 | $R = \frac{K_s(C_F C_B)}{\{1 + K_F C_F\}^2}$ | 0.959 | $\ln K_F = \frac{9225.1}{T} - 23.37$ $\ln K_S = \frac{-12'317}{T} + 35.747$ | $R_{kf^2}^2 = 0.967$ $R_{ks}^2 = 0.9547$ |
| M5 | $R = \frac{K_s(C_F C_B)}{\{1 + K_F C_F + K_B C_B + K_N C_N\}^2}$ | 0.989 | $\ln K_F = \frac{9434.7}{T} - 23.91$ $\ln K_B = \frac{14564}{T} - 37.792$ $\ln K_n = \frac{12928}{T} - 33.257$ $\ln K_S = \frac{-12317}{T} + 35.74$ | $R_{kf^2}^2 = 0.9978$ $R_{kB^2}^2 = 0.9314$ $R_{kn^2}^2 = 0.998$ $R_{ks}^2 = 0.9547$ |
| M6 | $R = \frac{K_s(C_F C_B - C_N/K_c)}{\{1 + K_F C_F + K_B C_B + K_N C_N\}^2}$ | 0.991 | $\ln K_F = \frac{8495}{T} - 20.73$ $\ln K_B = \frac{39571}{T} - 106.9$ $\ln K_n = \frac{2558}{T} - 4.332$ $\ln K_S = \frac{-7367.9}{T} + 22.858$ | $R_{kf^2}^2 = 0.991$ $R_{kB^2}^2 = 0.775$ $R_{kn^2}^2 = 0.7033$ $R_{ks}^2 = 0.8892$ |

R^2 : Coefficient of determination between the experimental and simulated model

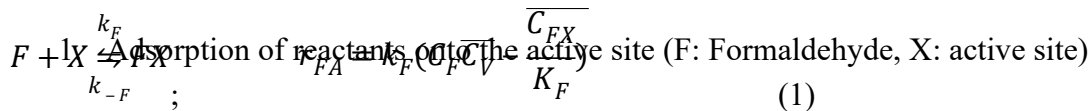
$K_{F,B,N}$: Adsorption constants of formaldehyde, β -Pinene and nopol

K_s : Reaction constant

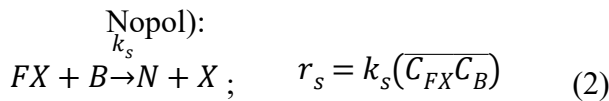
R_i^2 : Coefficient of determination of linear fitting of kinetic parameters; i represents the corresponding subscript used in kinetic constants K_i .

Models M1, M2 and M3 are based on a single site mechanism with the adsorption of formaldehyde onto the active site and its reaction with β -pinene present in the liquid phase. M1 considers the formation of nopol without its adsorption onto the active site, while M2 considers nopol adsorption, and M3 considers nopol adsorption with a possible reversible reaction. Models M4, M5 and M6 are based on a dual site mechanism with the adsorption of formaldehyde and β -pinene onto the active site and their reaction to yield nopol, which later desorbs into the liquid phase. M4 considers the relatively strong adsorption of formaldehyde while M5 considers an irreversible reaction and M6 considers the reversible reaction

M1 Model derivation:



2. Surface reaction on the dual sites and the formation of product (B: β -Pinene, N: Nopol):



Active site balance:

$$\overline{C_V} = \frac{C_{Total}}{1 + K_F C_F + K_B C_B + K_N C_N}$$

$$R = \frac{K(C_F C_B)}{1 + K_F C_F} \quad (K = C_{Total} \times K_F \times K_B) \quad (M1)$$

$$R = \frac{dX}{dt} W_{cat} \quad eqn. 1$$

Mole balance of β -Pinene throughout the reaction is calculated by eqn. 1 and this ode was solved using ode45 solver in MATLAB while the unknown adsorption and reaction constants were estimated using genetic algorithm as an optimization function. The objective function f used to calculate the coefficient of determination eqn 2. was optimized using GA to yield a minimum error. Default parameters of genetic algorithm optimization were used with a

population size of 200.

$$f = \sum_{i=0}^n (C_{B,Exp} - C_{B,Thr})^2 \quad eqn. 2$$

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