# RSM, ANN-GA and ANN-PSO modeling of SDBS removal from greywater in rural areas via $\mathrm{Fe}_{2} \mathrm{O}_{3}$-coated volcanic rocks 

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## Supplementary text

## Text S1 List of chemical reagents

SDBS (AR grade, mixture), ferric chloride $\left(\mathrm{FeCl}_{3} \cdot 6 \mathrm{H}_{2} \mathrm{O}\right)$, cetyltrimethylammonium bromide (CTAB) and sodium salts $\left(\mathrm{NaCl}, \mathrm{Na}_{2} \mathrm{SO}_{4}, \mathrm{NaHCO}_{3}\right.$, $\mathrm{NaNO}_{3}$ ) were all supplied by Aladdin (Shanghai, China). $\mathrm{H}_{2} \mathrm{SO}_{4}$ (98 wt\%), trichloromethane, NaOH ( $96 \mathrm{wt} \%$ ), $\mathrm{HCl}(37 \mathrm{wt} \%$ ), methylene blue and humic acid were purchased from Beijing Yili Fine Chemicals Co., Ltd. (Beijing, China). The SDBS stock was prepared by mixing 1.0 g into 1000 mL of DI water that had been stored at $4^{\circ} \mathrm{C}$.

## Text S2 Preparation of $\mathrm{Fe}_{2} \mathrm{O}_{3}$-coated volcanic rocks ( $\mathrm{Fe}_{2} \mathrm{O}_{3}$-VR)

Modified filter materials were prepared by heating evaporation method. Before coating the VR surface with iron, VR was cleaned a few times with DI water and soaked in 1 N HCl for 12 h to remove its surface impurities. Then, it was rinsed a few times by deionized water until its effluent acidity reached neutral. VR was then dried at $100^{\circ} \mathrm{C}$ for 12 h to remove the remaining water. Different concentrations of $\mathrm{FeCl}_{3}$ solution ( $0.05-0.3 \mathrm{~mol} / \mathrm{L}$ ) were prepared and added into the pretreated modified filter material according to the solid-liquid ratio of 1:3. The modified filter materials were dried at $110^{\circ} \mathrm{C}$ and coated repeatedly for three times with stirring every half an hour during the process. Then put the dried filter materials into a tubular furnace and calcine it for two hours in air atmosphere. The obtained materials were cooled to room temperature and washed by DI water for several times to remove extra iron coated surface that adhered loosely. Finally, the material was dried at $110^{\circ} \mathrm{C}$ and $\mathrm{Fe}_{2} \mathrm{O}_{3}$-coated volcanic rocks $\left(\mathrm{Fe}_{2} \mathrm{O}_{3}\right.$-VR) were obtained.

## Text S3 Characterization of $\mathrm{Fe}_{2} \mathrm{O}_{3}$-coated volcanic rocks ( $\mathrm{Fe}_{2} \mathrm{O}_{3}$-VR)

For observation of volcanic rock morphology and identification of atomic elements and relative concentrations of elements in volcanic rock samples the characterizations of pumice were analyzed using field emission scanning electron microscopy (FE-SEM), together with Energy Dispersive X-Ray Spectroscopy (EDX) analysis (SEM-EDX, SU8020, Japan). The specific surface area of natural and modified
adsorbent was measured using a nitrogen adsorption technique based on the Brunauer-Emmet-Teller isotherm model (Autosorb iQ/Quantachrome). Transmission Fourier Transform Infrared (FTIR) spectra were registered on a Perkin Elmer FTIR spectrometer model Frontier in the range $400-4000 \mathrm{~cm}^{-1}$, using KBr pellets. KBr was ground with a small amount of the solid to be analyzed, and the spectra were collected with a resolution of $4 \mathrm{~cm}^{-1}$ and accumulation of 32 scans. The crystalline structures of the used adsorbents were determined using an X ray diffractometer (XRD) which are collected by means of a D8 Advance with $\mathrm{Cu} \mathrm{K} \alpha$ as radiation (1.54056 $\AA$ ) generated at 40 kV and 40 mA instrument. The diffractograms were obtained with a step width of $0.02^{\circ}(2 \theta)$ and a scan rate of $8 \% \mathrm{~min}$. The surface area, total pore volume and average pore diameter (at $\mathrm{P} / \mathrm{P}_{0}=0.988$ ) were determined using $\mathrm{N}_{2}$ adsorption-desorption isotherm measurements by the standard Brunauer-Emmett-Teller (BET) method.

## Supplementary figures

Fig. S1 SEM images of VR (a, b) and $\mathrm{Fe}_{2} \mathrm{O}_{3}-\mathrm{VR}(\mathbf{c}, \mathrm{d})$
Fig. S2 EDS images of VR (a) and $\mathrm{Fe}_{2} \mathrm{O}_{3}$-VR (b)


Fig. S1 SEM images of VR (a, b) and $\mathrm{Fe}_{2} \mathrm{O}_{3}$-VR (c, d)


Fig. S2 EDS images of VR (a) and $\mathrm{Fe}_{2} \mathrm{O}_{3}-\mathrm{VR}(\mathrm{b})$

## Supplementary tables

Table S1 Experimental ranges and levels of variables
Table S2 RSM and ANN predicted results and errors, along with experimental values of the response

Table S1
Experimental ranges and levels of variables

| Factors | Variables | Unit | Levels |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Low (-1) | Middle (0) | High (+1) |
| A | Contact time | min | 5 | 92.5 | 180 |
| B | pH | / | 2 | 6 | 10 |
| C | SDBS initial concentration | mg/L | 10 | 50 | 90 |
| D | $\mathrm{FeCl}_{3}$ solution concentration | $\mathrm{mol} / \mathrm{L}$ | 0.05 | 0.175 | 0.3 |
| E | Adsorbent dosage | $\mathrm{g} / \mathrm{L}$ | 10 | 60 | 110 |
| F | Calcination temperature |  | 200 | 400 | 600 |

Table S2
RSM and ANN predicted results and errors, along with experimental values of the response

| Run | Variables |  |  |  |  |  | SDBS removal efficiency |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | A | B | C | D | E | F | Experiment | RSM | Error | ANN | Error |
| 1 | 92.5 | 10 | 90 | 0.175 | 110 | 400 | 85.67 | 80.373 | -5.297 | 85.670 | 0.000 |
| 2 | 5 | 2 | 50 | 0.05 | 60 | 400 | 32.96 | 34.421 | 1.461 | 32.960 | 0.000 |
| 3 | 180 | 2 | 50 | 0.3 | 60 | 400 | 75.45 | 77.493 | 2.043 | 75.450 | 0.000 |
| 4 | 92.5 | 2 | 10 | 0.175 | 10 | 400 | 48.34 | 52.407 | 4.067 | 43.991 | -4.349 |
| 5 | 5 | 6 | 50 | 0.3 | 10 | 400 | 37.32 | 32.882 | -4.438 | 37.320 | 0.000 |
| 6 | 92.5 | 10 | 10 | 0.175 | 10 | 400 | 58.39 | 62.187 | 3.797 | 58.390 | 0.000 |
| 7 | 5 | 6 | 50 | 0.05 | 10 | 400 | 27.08 | 23.190 | -3.890 | 27.080 | 0.000 |
| 8 | 5 | 6 | 50 | 0.05 | 110 | 400 | 45.66 | 46.189 | 0.529 | 45.660 | 0.000 |
| 9 | 92.5 | 10 | 90 | 0.175 | 10 | 400 | 45.37 | 46.109 | 0.739 | 45.370 | 0.000 |
| 10 | 92.5 | 6 | 50 | 0.175 | 60 | 400 | 88.34 | 87.333 | 1.953 | 86.776 | 1.396 |
| 11 | 5 | 6 | 90 | 0.175 | 60 | 600 | 47.26 | 50.599 | 3.339 | 47.260 | 0.000 |
| 12 | 92.5 | 10 | 50 | 0.175 | 10 | 200 | 57.32 | 57.749 | 0.429 | 57.320 | 0.000 |
| 13 | 92.5 | 10 | 50 | 0.175 | 110 | 600 | 90.12 | 90.936 | 0.816 | 90.120 | 0.000 |
| 14 | 92.5 | 2 | 10 | 0.175 | 110 | 400 | 73.48 | 73.971 | 0.491 | 73.480 | 0.000 |
| 15 | 92.5 | 6 | 90 | 0.3 | 60 | 200 | 82.59 | 83.064 | 0.474 | 82.590 | 0.000 |
| 16 | 92.5 | 6 | 90 | 0.05 | 60 | 200 | 71.51 | 72.321 | 0.811 | 71.510 | 0.000 |
| 17 | 92.5 | 2 | 50 | 0.175 | 110 | 600 | 80.29 | 78.631 | -1.659 | 75.552 | -4.738 |
| 18 | 92.5 | 6 | 50 | 0.175 | 60 | 400 | 88.34 | 87.333 | 0.763 | 86.776 | 0.206 |
| 19 | 92.5 | 6 | 50 | 0.175 | 60 | 400 | 88.34 | 87.333 | -1.317 | 86.776 | -1.874 |
| 20 | 92.5 | 2 | 50 | 0.175 | 10 | 600 | 52.79 | 52.997 | 0.207 | 52.790 | 0.000 |
| 21 | 92.5 | 2 | 90 | 0.175 | 10 | 400 | 42.47 | 39.794 | -2.676 | 42.470 | 0.000 |
| 22 | 92.5 | 10 | 10 | 0.175 | 110 | 400 | 84.97 | 86.416 | 1.446 | 84.970 | 0.000 |
| 23 | 92.5 | 6 | 10 | 0.05 | 60 | 200 | 82.65 | 82.308 | -0.342 | 83.039 | 0.389 |
| 24 | 5 | 10 | 50 | 0.05 | 60 | 400 | 45.04 | 42.676 | -2.364 | 45.040 | 0.000 |
| 25 | 180 | 6 | 90 | 0.175 | 60 | 600 | 83.73 | 82.573 | -1.157 | 83.730 | 0.000 |
| 26 | 5 | 2 | 50 | 0.3 | 60 | 400 | 42.23 | 43.380 | 1.150 | 42.230 | 0.000 |
| 27 | 5 | 6 | 90 | 0.175 | 60 | 200 | 45.02 | 48.594 | 3.574 | 45.020 | 0.000 |


| 28 | 180 | 2 | 50 | 0.05 | 60 | 400 | 62.63 | 62.796 | 0.166 | 62.630 | 0.000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 29 | 92.5 | 6 | 90 | 0.3 | 60 | 600 | 85.77 | 86.431 | 0.661 | 85.770 | 0.000 |
| 30 | 92.5 | 6 | 50 | 0.175 | 60 | 400 | 88.34 | 87.333 | -2.787 | 86.776 | -3.344 |
| 31 | 180 | 6 | 50 | 0.05 | 10 | 400 | 47.35 | 47.043 | -0.307 | 49.169 | 1.819 |
| 32 | 92.5 | 6 | 10 | 0.3 | 60 | 200 | 94.21 | 93.086 | -1.124 | 94.210 | 0.000 |
| 33 | 92.5 | 6 | 50 | 0.175 | 60 | 400 | 88.34 | 87.333 | 0.013 | 86.776 | -0.544 |
| 34 | 92.5 | 10 | 50 | 0.175 | 110 | 200 | 86.92 | 87.943 | 1.023 | 86.920 | 0.000 |
| 35 | 92.5 | 6 | 10 | 0.05 | 60 | 600 | 84.43 | 83.637 | -0.793 | 90.091 | 5.661 |
| 36 | 92.5 | 2 | 90 | 0.175 | 110 | 400 | 73.96 | 71.393 | -2.567 | 73.960 | 0.000 |
| 37 | 180 | 6 | 50 | 0.3 | 110 | 400 | 91.09 | 95.301 | 4.211 | 91.090 | 0.000 |
| 38 | 180 | 10 | 50 | 0.3 | 60 | 400 | 89.78 | 87.998 | -1.782 | 89.780 | 0.000 |
| 39 | 92.5 | 6 | 90 | 0.05 | 60 | 600 | 73.56 | 75.003 | 1.443 | 77.072 | 3.512 |
| 40 | 92.5 | 2 | 50 | 0.175 | 10 | 200 | 50.88 | 51.294 | 0.414 | 50.880 | 0.000 |
| 41 | 180 | 6 | 50 | 0.05 | 110 | 400 | 78.67 | 82.787 | 4.117 | 80.569 | 1.899 |
| 42 | 180 | 6 | 10 | 0.175 | 60 | 200 | 94.33 | 90.673 | -3.657 | 94.330 | 0.000 |
| 43 | 5 | 6 | 10 | 0.175 | 60 | 200 | 55.62 | 56.459 | 0.839 | 55.620 | 0.000 |
| 44 | 180 | 6 | 90 | 0.175 | 60 | 200 | 77.87 | 78.528 | 0.658 | 77.870 | 0.000 |
| 45 | 180 | 10 | 50 | 0.05 | 60 | 400 | 75.58 | 74.751 | -0.829 | 75.580 | 0.000 |
| 46 | 92.5 | 6 | 50 | 0.175 | 60 | 400 | 88.34 | 87.333 | 1.373 | 86.776 | 0.816 |
| 47 | 92.5 | 2 | 50 | 0.175 | 110 | 200 | 81.92 | 78.823 | -3.097 | 81.920 | 0.000 |
| 48 | 5 | 6 | 50 | 0.3 | 110 | 400 | 52.98 | 52.966 | -0.014 | 52.980 | 0.000 |
| 44 | 180 | 6 | 10 | 0.175 | 60 | 600 | 96.62 | 93.365 | -3.255 | 94.852 | -1.768 |
| 53 | 5 | 6 | 10 | 0.175 | 60 | 600 | 57.45 | 57.111 | -0.339 | 57.450 | 0.000 |
| 52 | 5 | 10 | 50 | 0.3 | 60 | 400 | 50.03 | 50.185 | 0.155 | 51.252 | 1.222 |
| 51 | 92.5 | 6 | 10 | 0.3 | 60 | 600 | 96.23 | 95.101 | -1.129 | 96.230 | 0.000 |
| 52 | 92.5 | 10 | 50 | 0.175 | 10 | 600 | 60.77 | 62.637 | 1.867 | 60.770 | 0.000 |

