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**Electronic Supplementary Information** 

## Unavoidable but Minimizable Microdefects in a Polycrystalline Zeolite Membrane: Its Remarkable Performance for Wet CO<sub>2</sub>/CH<sub>4</sub> Separations

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#### **S1. Experimental procedures**

#### S1.1. Synthesis of heterogeneous particles

SSZ-13 particles (S-P, where S and P indicate SSZ-13 zeolites and the form of particles, respectively) were synthesized and further calcined based on detailed experimental procedures reported in our previous study.<sup>1</sup> The average size of S-P was ~230 nm. Subsequently, calcined S-P particles were hydrothermally grown with a synthetic precursor that enabled the synthesis of ZSM-58 zeolites; that is, the growth of calcined S-P particles with the ZSM-58 synthetic precursor containing methyltropinium iodide (MTI) as an organic structure directing agent (OSDA) according to a previously reported method.<sup>2</sup> The final molar composition of the ZSM-58 synthetic precursor was 23 NaOH: 70 SiO<sub>2</sub>: 2800 H<sub>2</sub>O: 17.5 MTI. For seeded growth,  $\sim 0.03$  g of calcined S-P was added to  $\sim 30$  mL of the prepared ZSM-58 synthetic precursor, and the mixture was sealed in a Teflon lined stainless-steel autoclave. Subsequently, a hydrothermal reaction was carried out in a preheated oven (PL HV 250, Pluskolab, South Korea) at 130 °C for 10 d while the mixture was rotated at ~45 rpm. The autoclave was then quenched with tap water to stop the reaction. The resulting suspension was transferred to a conical centrifuge tube (Falcon, 50 mL) with deionized (DI) water. Subsequently, the suspension was centrifuged (Combi-514R, Hanil Science Industrial, South Korea) for 20 min. The aqueous part, expect for the white solid in the conical centrifuge tube, was discarded. Fresh DI water was replenished in the conical centrifuge tube. This process was repeated five times to wash the particles thoroughly. The solid particles were recovered and dried in an oven (HB-502M, Pluskolab, South Korea) at 70 °C. For convenience, these dried particles are considered as assynthesized and referred to as SZ-P, where Z indicates the ZSM-58 zeolite used for seeded growth.

#### S1.2. Synthesis of heteroepitaxially grown zeolite films

First, calcined S-P particles were deposited on a porous  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> disc to form a uniform seed layer. Approximately 30 mL of the ZSM-58 synthetic precursor used to synthesize SZ-P was added to a Teflon liner, wherein the calcined seed layer was placed in a tilted position with the seeded side facing downward. Subsequently, the liner was sealed in a stainless-steel autoclave, which was transferred to a preheated 130 °C oven (PL\_HV\_250, Pluskolab, South Korea), and the hydrothermal reaction was conducted under static conditions for 10 d. Detailed information regarding the preparation of the S-P seed layer and the heteroepitaxially grown zeolite film can be found in a previous study.<sup>1</sup> For convenience, the resulting, dried heteroepitaxially grown zeolite film is considered as as-synthesized and referred to as SZ, where S and Z are identical to those in SZ-P except that SZ is a film made on the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> disc.

#### S1.3. Heterogeneous particles and films calcined under various conditions

The SZ-P and SZ samples were calcined under three different conditions. First, the SZ-P and SZ samples were calcined at 550 °C for 12 h in air flowing at 200 mL·min<sup>-1</sup> in a box furnace (CRF-M20-UP, Pluskolab, South Korea). For convenience, the calcined SZ-P and SZ samples are referred to as SZ-P\_air and SZ\_air, respectively, where the calcination environment (here, air) is appended. Second, the SZ-P and SZ samples were calcined at 450 °C for 80 h in oxygen (O<sub>2</sub>) flowing at 200 mL·min<sup>-1</sup> in the box furnace. For convenience, the resulting samples are referred to as SZ-P\_O<sub>2</sub> and SZ\_O<sub>2</sub>, respectively, where the calcination environment (or  $O_2$  is appended. Finally, the SZ-P and SZ samples were calcined at 250 °C for 40 h in ozone (O<sub>3</sub>) in a tubular furnace (a quartz tube with an outer diameter of 50 mm and a wall thickness of 2 mm was used). For convenience, the resulting SZ-P and SZ samples are referred to as SZ-P\_O<sub>3</sub> and SZ\_O<sub>3</sub>, respectively, where O<sub>3</sub> is appended to represent the ozone calcination condition. For the ozone-based calcination, a 5 vol% ozone flow was generated by flowing pure O<sub>2</sub> (99.9%) at 1,000 mL·min<sup>-1</sup> through an ozone generator (OZE-020, Ozone Engineering Co., Ltd., South Korea). The particle and film samples were heated at 1 and 0.2 °C·min<sup>-1</sup>, respectively. For convenience, the calcined SZ particles and SZ membranes (SZ-P\_x and SZ\_x; x = air, O<sub>2</sub>, and O<sub>3</sub>) are called as the SZ-P particle and SZ membrane series, respectively.

#### **S1.4.** Separation performance measurements

The CO<sub>2</sub>/CH<sub>4</sub> and CO<sub>2</sub>/N<sub>2</sub> separation performances of the SZ membrane series were measured using the Wicke-Kallenbach method, wherein the total pressures on both the feed and permeate sides were maintained at ~1 atm. The partial pressures of the equimolar CO<sub>2</sub>/CH<sub>4</sub> and CO<sub>2</sub>/N<sub>2</sub> binary mixtures were approximately 51:51 (kPa/kPa) under dry conditions (referred to as DRY CO<sub>2</sub>:CH<sub>4</sub> = 50:50 and DRY CO<sub>2</sub>:N<sub>2</sub> = 50:50, respectively). In addition, under wet conditions, the partial pressures of the CO<sub>2</sub>/CH<sub>4</sub> and CO<sub>2</sub>/N<sub>2</sub> binary mixtures and water vapor were ca. 49:49:3 (kPa/kPa/kPa) (referred to as WET CO<sub>2</sub>:CH<sub>4</sub> = 50:50 and WET CO<sub>2</sub>:N<sub>2</sub> = 50:50, respectively). Furthermore, a flue gas showing a composition similar to that produced in coal-fired power plants<sup>3-6</sup> was simulated and employed to evaluate the CO<sub>2</sub>/N<sub>2</sub> binary mixture were approximately 15:86 (kPa/kPa) under dry conditions (referred to as DRY CO<sub>2</sub>:N<sub>2</sub> = 15:85). Under wet conditions, the partial pressures of the CO<sub>2</sub>/N<sub>2</sub> mixture and water vapor were ca. 15:84:3 (kPa/kPa) (referred to as WET CO<sub>2</sub>:N<sub>2</sub> = 15:85). In addition, the separation performances were measured for equimolar CO<sub>2</sub>/CH<sub>4</sub> mixture and CO<sub>2</sub>/N<sub>2</sub> binary mixture composed of 15% CO<sub>2</sub> and 85% N<sub>2</sub> while varying the relative humidities of the water vapor. Gas chromatographs (GCs) were used to analyze the molar fluxes of the mixtures for the SZ membrane series. Two GCs of YL 6500 (Young In Chromass, South Korea) and YL 6100 (Young In Chromass, South Korea) were used to measure the  $CO_2/CH_4$  and  $CO_2/N_2$  separation performances, respectively.

#### S1.5. Fluorescence confocal optical microscopy analysis

The defect structures in SZ\_x (x = air, O<sub>2</sub>, or O<sub>3</sub>) were investigated using fluorescence confocal optical microscopy (FCOM). Specifically, the FCOM images were acquired using a ZEISS LSM 700 confocal microscope with a solid-state laser operating at a 555-nm wavelength. For the FCOM images, fluorescein sodium salt (F6377, Sigma-Aldrich), with molecular size of approximately 1 nm,<sup>7</sup> was used for dyeing the SZ membrane series because the dye molecule is smaller than the defect sizes in the zeolite membranes and larger than the pores in the DDR zeolite (0.36 × 0.44 nm<sup>2</sup>).<sup>8</sup> In preparation for the FCOM analysis, SZ\_x (x = air, O<sub>2</sub>, or O<sub>3</sub>) was dyed with the 1 mM fluorescein sodium salt solution. Specifically, the membrane surface was contacted with the dye solution for 4 d to allow sufficient penetration of the dye molecules into the membrane. The detailed dyeing procedure based on an osmosis-type module is described in a previous study.<sup>9</sup> Then, top view FCOM images of the dyed SZ membrane series were obtained from the membrane outer surface to the interface between the membrane and the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> support at an interval of ~0.25 µm.

The resulting FCOM images were further used to quantitatively estimate the properties (mainly the area fraction and tortuosity) of the defect structures by image processing. In addition, the quantitative properties of the defect structures were complemented with unidimensional permeation modeling. This combination yielded the porosity (or density) and size (or width) of the defects. Simultaneously, we could attribute the contributions of the defective and zeolitic parts to the final molar flux of the CO<sub>2</sub> molecules. Detailed information regarding the quantitative analysis of the defects and the contributions of the defective and zeolitic parts to the final CO<sub>2</sub> molar flux has been provided in previous studies.<sup>10, 11</sup> In addition, to estimate the rates of CO<sub>2</sub> permeation inhibited by the adsorbed water molecules, we considered the linear combination of permeations by water-molecule-induced defect blockage and outer and inner surface inhibitions can be found elsewhere.<sup>12</sup> In this study, we further decoupled the surface inhibitions by considering the water-molecule-induced permeation resistance on the membrane outer surface (called the outer surface inhibition) and on the inner micropore surface inside the zeolite membrane (called the inner surface inhibition). For this, we estimated the two surface inhibitions according to the Boltzmann-equation-based statistical approach as follows:

$$y = \frac{A_1 - A_2}{1 + e^{(x - x_0)/dx}} + A_2.$$

For simplicity, we assumed that the  $CO_2$  permeation reduced by the outer surface inhibition was determined at a very low water vapor pressure (i.e., the *y*-axis intercept) and that reduced  $CO_2$  permeation rate because of inner surface inhibition gradually increased with the increasing content of water molecules adsorbed inside the micropores.

#### **S1.6.** Characterization

Scanning electron microscopy (SEM) images and energy dispersive X-ray spectroscopy (EDX) results were obtained using a Hitachi S-4800 field emission-scanning electron microscope (FE-SEM). In addition, SEM images of calcined S-P were obtained using a Hitachi S-4300 FE-SEM. For the SEM images, the particle and membrane samples were precoated with platinum by a Hitachi-1045 ion sputter. A Rigaku Model D/Max-2500V/PC diffractometer equipped with a Cu K<sub>a</sub> radiation source ( $\lambda = 0.154$  nm) was used to obtain the X-ray diffraction (XRD) patterns of the particle and membrane samples. For comparison, the simulated XRD patterns of the all-silica CHA and DDR zeolites were acquired using Mercury software (Cambridge Crystallographic Data Centre; CCDC). The corresponding crystallographic information files (CIFs) were downloaded from the International Zeolite Association (IZA) website (http://www.izaonline.org). Thermogravimetric analysis (TGA) results were obtained using a Q50 (TA Instruments, USA) in air and O<sub>2</sub>. Weight loss percentage after calcination of SZ-P in air, O<sub>2</sub>, and O<sub>3</sub> was obtained by the batch-wise calcination in box (calcination in air and  $O_2$ ) and tubular (calcination in  $O_3$ ) furnaces for different durations. First, a weight of SZ-P (approximately 0.1 g) was measured and then placed in a porcelain holder. The porcelain holder was transferred to the box or tubular furnace. Temperature was increased at a heating ramp rate of 10 °C·min<sup>-1</sup> to a target temperature. After reaching the target temperature, it was held at 550 °C for up to 12 h under air, at 450 °C for up to 80 h under O<sub>2</sub>, and at 250 °C for up to 80 h under O<sub>3</sub>. Finally, the final weight of calcined SZ-P was measured again after different durations to calculate the weight loss percentage. Fourier transform infrared (FT-IR) spectroscopy (Nicolet<sup>TM</sup> iS50, Thermo Scientific<sup>TM</sup>, USA) was used to verify the presence of OSDAs in the particle and membrane samples. The FT-IR spectra of the particle and membrane samples were acquired in the transmittance and attenuated total reflectance (ATR) modes, respectively. Specifically, the SZ-P particle series were pelletized for the FT-IR measurements and mounted in an *in-situ* cell. Subsequently, the *in*situ cell was heated at 200 °C for 12 h to remove any residual moisture and was then cooled to 150 °C under vacuum before starting the measurements. An ASAP 2020 (Micromeritics Instruments Corporation,

USA) was used to measure the adsorption isotherms of  $CO_2$ ,  $CH_4$ , and  $N_2$  in SZ-P\_air at 30, 50, and 75 °C for the  $CO_2$  and  $CH_4$  molecules and at 10, 20, and 30 °C for the  $N_2$  molecules. In addition, the Ar physisorption isotherms at 87 K for the SZ-P particle series were obtained using the ASAP 2020. In addition, the water vapor adsorption isotherms were measured using a vapor sorption analyzer (DVS Vacuum, Surface Measurement Systems, England) at 50 °C for the SZ-P particle series. To investigate the hydrophobicity of the SZ membrane series, the contact angles of water droplets on the membrane surfaces were obtained using a contact angle analyzer (Phoenix-300, Surface Electro Optics, South Korea).

#### S2. Supplemental results and discussion

#### S2.1. Properties of the SZ particle series

Fig. S2a and b reveals the changes in weight of SZ-P at ca. 260 °C in air and at ca. 240 °C in O<sub>2</sub>. The TGA result obtained for MTI in air indicates that MTI was oxidized at approximately 310 °C (Fig. S2c). Thus, it is reasonable to accept that the changes in weight observed in Fig. S2a and b were associated with the removal of MTI from the outer surface of SZ-P not from inside. To accurately measure the MTI content inside SZ-P, the sample was heated again at 300 °C for 3 h to remove any external residual MTI (Fig. S2d). Accordingly, the weight of MTI inside SZ-P was ~12 wt%, which was in good agreement with ca. 12 wt% of MTI inside the ZSM-58 zeolites.<sup>2, 13</sup> This strongly indicates that the DDR zeolites are a major constituent of SZ-P.

#### S2.2. Properties of the SZ membrane series

We investigated the membrane properties of SZ and SZ\_x (x = air, O<sub>2</sub>, and O<sub>3</sub>). The top and crosssectional view SEM images and water contact angles are shown in Fig. S6. In the top view SEM images in Fig. S6a1-d1, the shapes and sizes of the grains among SZ and SZ\_x (x = air, O<sub>2</sub>, and O<sub>3</sub>) were indistinguishable, indicating that the membrane constituents were negligibly affected by the different calcination methods. The EDX results of the Si and Al atoms shown in Fig. S6a2-d2 indicate the plausible high hydrophobicity of all the SZ membrane series. The SZ membrane series were ~7 µm thick, which is in good agreement with previously reported membrane thickness.<sup>1</sup> In addition, although some Al atoms leached from the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> discs during the secondary growth can be incorporated into some parts near the interface,<sup>14, 15</sup> the majority of the membrane constituents in the SZ membrane series were highly siliceous and plausibly hydrophobic, provided that they were fully calcined (Fig. S6b2-d2). Along with the EDX result, the water droplet contact angles shown in Fig. S6b3-d3 confirm the high hydrophobicity of the SZ membrane series. In contrast, the as-synthesized SZ film exhibited some hydrophilic properties (Fig. S6a3), which could be related to the water-soluble MTI included in the ZSM-58 precursor. Furthermore, the XRD patterns of SZ\_x (x = air, O<sub>2</sub>, and O<sub>3</sub>) shown in Fig. S7 reveal that the major constituent of the hybrid membrane was the DDR zeolite, while the SSZ-13 zeolite originating from the seed layer was a minor constituent.

#### S2.3. CO<sub>2</sub>/N<sub>2</sub> separation performances of the SZ membrane series

The CO<sub>2</sub>/N<sub>2</sub> separation performances of the SZ membrane series under both dry and wet conditions are shown in Fig. S9. Specifically, the maximum CO<sub>2</sub>/N<sub>2</sub> SFs were 16.2 ± 1.2 for SZ\_air (Fig. S9a1), 18.0 ± 2.5 for SZ\_O<sub>2</sub> (Fig. S9b1), and 29.2 ± 0.1 for SZ\_O<sub>3</sub> (Fig. S9c1) at 30 °C under dry conditions. However, the CO<sub>2</sub>/N<sub>2</sub> SFs at 50 °C (a representative temperature of the flue gas emitted from coal-fired power plants) under wet conditions were 14.4 ± 4.0 for SZ\_air (Fig. S9a2), 17.9 ± 4.2 for SZ\_O<sub>2</sub> (Fig. S9b2), and 14.7 ± 2.4 for SZ\_O<sub>3</sub> (Fig. S9c2). In general, the trends of the CO<sub>2</sub> and N<sub>2</sub> permeances observed under dry and wet conditions were similar to those observed for the equimolar CO<sub>2</sub>/CH<sub>4</sub> mixtures (Fig. 2a2-c2). However, although the kinetic diameter of CH<sub>4</sub> (0.38 nm) is slightly larger than that of N<sub>2</sub> (0.364 nm), it is relatively much larger than the 8-MR channels in the DDR zeolite ( $0.36 \times 0.44$  nm<sup>2</sup>). Therefore, the molecular sieve effect was more pronounced for the CO<sub>2</sub>/CH<sub>4</sub> mixtures than for the CO<sub>2</sub>/N<sub>2</sub> ones, thereby resulting in the extremely high CO<sub>2</sub>/CH<sub>4</sub> SFs for the SZ membrane series (~285-673 at 30 °C).

In addition, we carried out  $CO_2/N_2$  permeation tests of the SZ membrane series for a simulated flue gas composition (Fig. S10). For the simulation, we considered the compositions of the main components (15%  $CO_2$  and 85%  $N_2$ ) and the third most abundant component, water vapor.<sup>3-6</sup> The resulting maximum  $CO_2/N_2$  SFs at 30 °C under dry conditions were 16.2 ± 2.0 for SZ\_air (Fig. S10a1), 18.2 ± 1.2 for SZ\_O<sub>2</sub> (Fig. S10b1), and 28.6 ± 4.7 for SZ\_O<sub>3</sub> (Fig. S10c1). This trend would reflect the degree of defects in the SZ membrane series, which plausibly decreased in the order SZ\_air, SZ\_O<sub>2</sub>, and SZ\_O<sub>3</sub>. Notably, these values were close to those observed for the equimolar  $CO_2/N_2$  mixtures (Fig. S9a1-c1). This was attributable to the almost linear behaviors of both the  $CO_2$  and  $N_2$  molecules in SZ-P\_air up to ~1 bar at 30 °C (Fig. S15). In addition, introducing the water vapor to the dry feed similarly reduced the  $CO_2/N_2$  permeances and, thus, the  $CO_2/N_2$  SFs at 30 °C were comparable, except for that of SZ\_O<sub>3</sub>, which showed a more pronounced reduction in the  $CO_2$  permeance and, accordingly, a very low  $CO_2/N_2$  SF at 30 °C. Nevertheless, the  $CO_2/N_2$  SFs at 50 °C under wet conditions were as high as 19.6 ± 1.3 for SZ\_air (Fig. S10a2), 22.8 ± 2.6 for SZ\_O<sub>2</sub> (Fig. S10b2), and 17.2 ± 3.5 for SZ\_O<sub>3</sub> (Fig. S10c2). Despite the high

 $CO_2/N_2$  SFs at 50 °C, the  $CO_2$  permeances through SZ\_O<sub>3</sub> drastically decreased, plausibly because of the hydrophilicity of the residual MTI inside the DDR zeolite: ~9 × 10<sup>-9</sup> mol·m<sup>-2</sup>·s<sup>-1</sup>·Pa<sup>-1</sup> for SZ\_O<sub>3</sub> was much lower than those of both SZ\_air and SZ\_O<sub>2</sub> (~3.1-3.2 × 10<sup>-8</sup> mol·m<sup>-2</sup>·s<sup>-1</sup>·Pa<sup>-1</sup> at 50 °C).

In addition to the  $CO_2/N_2$  separation performance plotted as a function of temperature (Fig. S9 and S10), the relative humidity of the water vapor was systematically increased from 0% through 26% and 60% to 100% at 50 °C to determine its effect on the  $CO_2/N_2$  separation performance (Fig. S11a1-c1). As the relative humidity was increased, the  $CO_2$  and  $N_2$  permeances decreased monotonically. Interestingly, the degree of the decreased permeance was comparable for both  $CO_2$  and  $N_2$ , as mentioned above for both SZ\_air and SZ\_O<sub>2</sub> shown in Fig. S10a1-a2 and b1-b2. Accordingly, the comparable  $CO_2/N_2$  SFs were maintained up to 100% relative humidity. However, the effect of the water vapor on the rates of  $CO_2/N_2$  permeation through SZ\_O<sub>3</sub> was distinct; that is, the degree of  $CO_2$  permeance became increasingly pronounced with increasing relative humidity, thus resulting in the monotonically decreasing  $CO_2/N_2$  SFs. Although the apparently defect-free SZ\_O<sub>3</sub> achieved the highest  $CO_2/N_2$  SF under dry conditions, it showed rather weak resistance against water vapor, seemingly because of the aforementioned hydrophilicity. This indicates the importance of maximizing hydrophobicity to achieve high  $CO_2$  permeate after removing the water vapor from the feed indicates the robustness of the inorganic zeolite membranes.

By determining the effect of the water vapor on the  $CO_2/N_2$  separation performance, we further confirmed the long-term stabilities of the SZ membrane series at 100% relative humidity and 50 °C (Fig. S11a2-c2). For both SZ\_air and SZ\_O<sub>2</sub>, the  $CO_2/N_2$  SF increased from 15 and 15.6 under dry conditions to 16.2 and 22.8, respectively, at the 100% relative humidity at the expense of the reduced  $CO_2$ permeance (Fig. S11a1-b1 and a2-b2). However, gradually adding the water vapor to the feed monotonically decreased the  $CO_2/N_2$  SF of SZ\_O<sub>3</sub> (Fig. S11c1 and c2) from 23.5 under dry conditions to 7.3 at 100% relative humidity. Fig. S11a2-c2 reveals that the hydrophobic SZ membranes (i.e., SZ\_air and SZ\_O<sub>2</sub>) could preserve the high  $CO_2/N_2$  SFs (~16-23) without showing any noticeable performance degradation, whereas SZ\_O<sub>3</sub> could not feasibly maintain the original high  $CO_2/N_2$  SF under dry conditions at 100% relative humidity. This strongly supports the desirable hydrophobicity of the zeolite membrane to ensure high  $CO_2$  permselectivities under wet conditions. Despite the intentionally interposed hydrothermal treatment at 200 °C in Fig. S11a2-c2, the SZ membrane series could provide steady  $CO_2$ permselectivities, thereby supporting the application of zeolite membranes.

# S2.4. Comparison of the $CO_2/N_2$ separation performances of the SZ membrane series and other membranes

We noticed that the  $CO_2/N_2$  separation performance of the entire SZ membrane series measured at 50 °C could not overcome the Robeson upper bound limit under both dry and wet conditions (Fig. S21a).<sup>16</sup> Nevertheless, SZ O<sub>2</sub> still exhibited very good CO<sub>2</sub>/N<sub>2</sub> SFs (ca. 22.8) at the saturated water vapor pressure of 12.3 kPa at 50 °C. Likewise, the SZ membranes series showed the high CO<sub>2</sub>/N<sub>2</sub> separation performances under both dry and wet conditions, as compared to those of other zeolite membranes; (1) DDR type: ZSM-5817 and c-oriented DDR,18 (2) CHA type: SSZ-13,19,20 dye-post-treated SSZ-13,10 RTPtreated SSZ-13,12 CHA,21 CVD-treated CHA,22 and SDA-free CHA,23 and (3) faujasite24 zeolites (Fig. S21b). SZ air, which comprises the majority of the ZSM-58 zeolites, showed good CO<sub>2</sub>/N<sub>2</sub> separation performances comparable to those of the homogeneous ZSM-58 membrane<sup>17</sup> under both dry and wet conditions. Furthermore, defect-free SZ O<sub>3</sub> showed a very high CO<sub>2</sub>/N<sub>2</sub> SF (ca. 23.5) under dry conditions, whereas SZ\_air and SZ\_O<sub>2</sub> showed the CO<sub>2</sub>/N<sub>2</sub> SFs (ca. 14.9-17.2) comparable or superior to those of intact or post-treated CHA type membranes. However, adding the water vapor to the feed resulted in good CO<sub>2</sub>/N<sub>2</sub> SFs (ca. 22.8) for SZ O<sub>2</sub>. In particular, the hydrophobicity of a zeolite membrane constituent was required for achieving high CO<sub>2</sub> permselectivities under wet conditions, as reflected by the SZ\_O<sub>2</sub> performance and the significant performance deterioration in the hydrophilic membrane.24 faujasite zeolite

Adsorbed gas	Temp. (°C)	$Q_{sat}^{A}$ (mol·kg <sup>-1</sup> )	$\frac{K^A}{(\text{kPa}^{-1}) \times 10^3}$	$-\Delta H_{ads}{}^A$ (kJ·mol <sup>-1</sup> )	$Q_{sat}^{B}$ (mol·kg <sup>-1</sup> )	$\frac{K^B}{(\mathrm{kPa}^{-1})\times 10^3}$	$-\Delta H_{ads}{}^B$ (kJ·mol <sup>-1</sup> )
CO <sub>2</sub>	30	$0.15 \pm 0.01$	33,000 ± 7,580	69.4 ± 13.3	$2.69\pm0.06$	$11.9 \pm 0.48$	$33.4\pm0.47$
	50		$3,290 \pm 486$			$5.34 \pm 0.18$	
	75		$922 \pm 3$			$2.14 \pm 0.07$	
N <sub>2</sub>	10	$0.94\pm0.01$	$3.51\pm0.07$	$26.4 \pm 1.8$			
	20		$2.50 \pm 0.04$				
	30		$1.68 \pm 0.03$				
	50		0.89 <sup>a</sup>				
CH <sub>4</sub>	30	$1.27 \pm 0.03$	$4.14 \pm 0.12$	$30.2 \pm 1.8$			
	50		$2.13 \pm 0.05$				
	75		$0.88\pm0.02$				

**Table S1** Dual-site Langmuir adsorption constants and saturation capacities estimated from  $CO_2$  adsorption isotherms in SZ\_air and single-siteLangmuir adsorption constants and saturation capacities estimated from  $N_2$  and  $CH_4$  adsorption isotherms in SZ\_air.<sup>25, 26</sup>

<sup>a</sup> Estimated based on the values measured at 10, 20, and 30 °C.

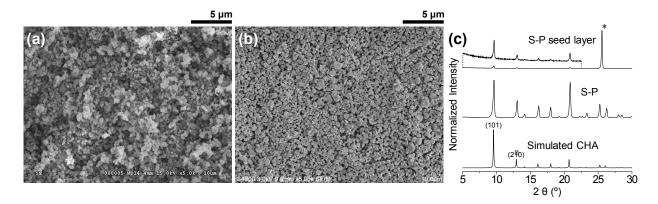
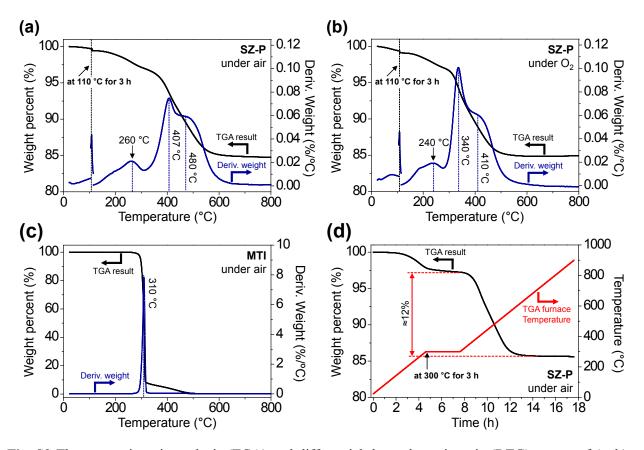
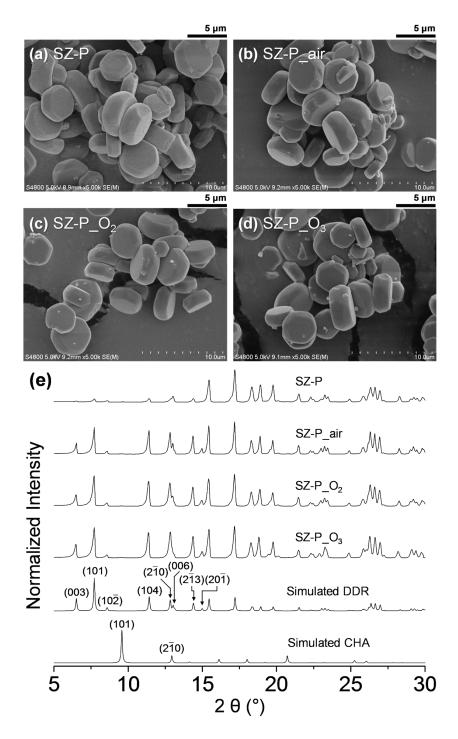


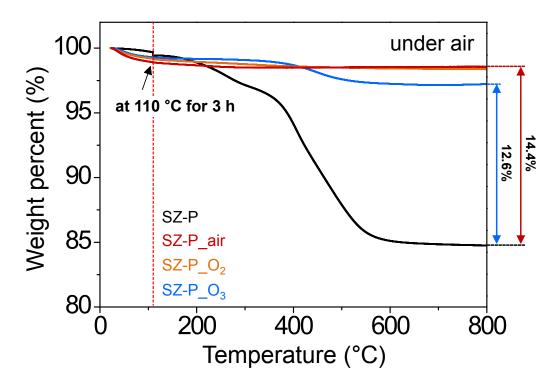
Fig. S1 SEM images of (a) calcined S-P particles and (b) a calcined seed layer comprising the S-P particles shown in (a) along with (c) the corresponding XRD patterns. A magnified XRD pattern of the S-P seed layer is shown above the normalized XRD pattern. In addition, the simulated XRD pattern of all-silica CHA zeolite is added at bottom. Finally, an asterisk (\*) denotes a XRD peak originating from an  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> disc.



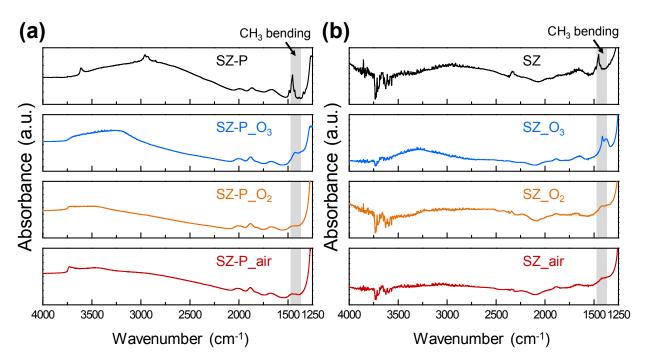
**Fig. S2** Thermogravimetric analysis (TGA) and differential thermal gravimetric (DTG) curves of (a, b) SZ-P and (c) MTI in (a, c) air and (b)  $O_2$  plotted as a function of temperature up to 800 °C. In (a, b), a black dashed line indicates heat treatment at 110 °C for 3 h to remove weakly adsorbed molecules (e.g., water molecules) from SZ-P. (d) TGA results of SZ-P in air with respect to a temperature profile (marked in red). In (a-c), the samples were heated at 1 °C·min<sup>-1</sup> and blue dashed lines indicate peak positions of derivative weight loss curves.



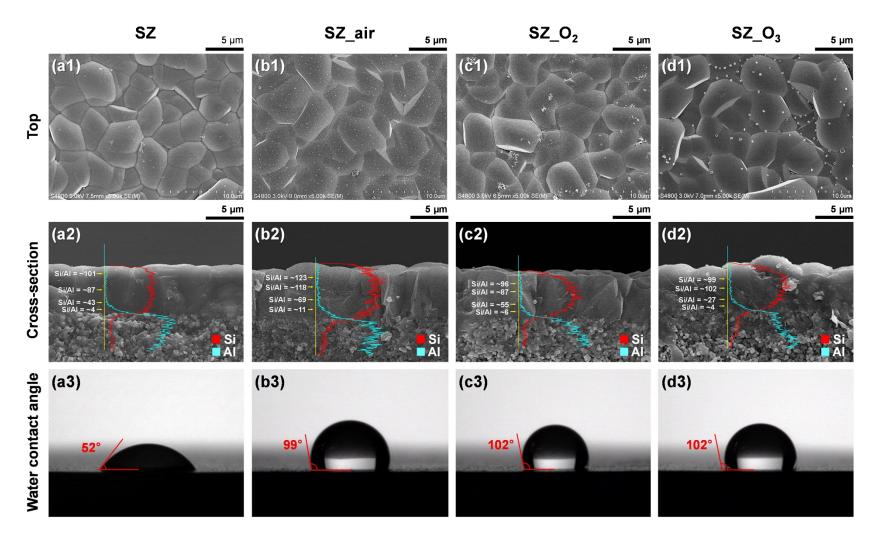
**Fig. S3** SEM images of (a) SZ-P, (b) SZ-P\_air, (c) SZ-P\_O<sub>2</sub>, and (d) SZ-P\_O<sub>3</sub> along with (e) the corresponding XRD patterns. In (e), the simulated XRD patterns of all-silica CHA and DDR zeolites are provided.



**Fig. S4** TGA results of SZ-P (*black*), SZ-P\_air (*red*), SZ-P\_O<sub>2</sub> (*orange*), and SZ-P\_O<sub>3</sub> (*blue*). TGA was measured as a function of temperature up to 800 °C at a ramp rate of 1 °C·min<sup>-1</sup>. For the removal of weakly adsorbed molecules, heat treatment at 110 °C for 3 h was conducted (indicated by a red dashed line). In addition, weight loss percentage at 800 °C was calculated by setting the weight percent to 100% after the heat treatment at 100 °C (indicated by the red vertical dashed line).



**Fig. S5** FT-IR spectra of (a) SZ-P and SZ-P\_x (x = air, O<sub>2</sub>, and O<sub>3</sub>) obtained in the transmission mode and (b) SZ and SZ\_x (x = air, O<sub>2</sub>, and O<sub>3</sub>) obtained in the attenuated total reflection (ATR) mode. IR peak ranges due to the CH<sub>3</sub> bending are marked by shaded areas.



**Fig. S6** (a1-d1) Top view SEM images and (a2-d2) cross-sectional view SEM images along with the EDX results for Si (*red*) and Al (*cyan*) of SZ and SZ\_x (x = air, O<sub>2</sub>, and O<sub>3</sub>). (a3-d3) Images of contact angles measured immediately after dropping water onto membrane surfaces. (a1-a3) SZ, (b1-b3) SZ\_air, (c1-c3) SZ\_O<sub>2</sub>, and (d1-d3) SZ\_O<sub>3</sub>. For better understanding, in (a2-d2), the values of Si/Al ratios estimated from the EDX results are displayed at four points (*indicated by yellow arrows*) of the cross-sectional view SEM images.

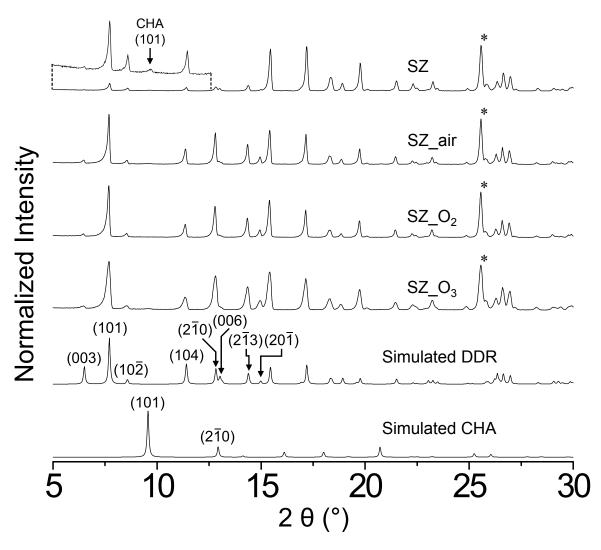
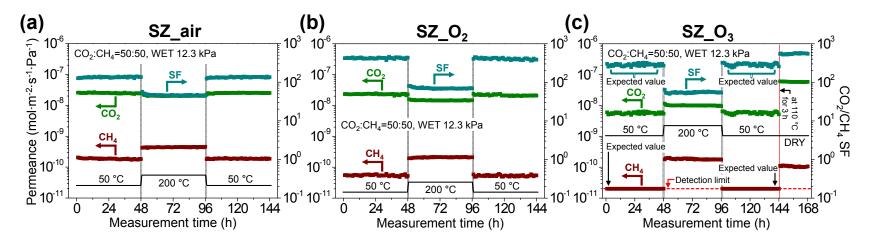
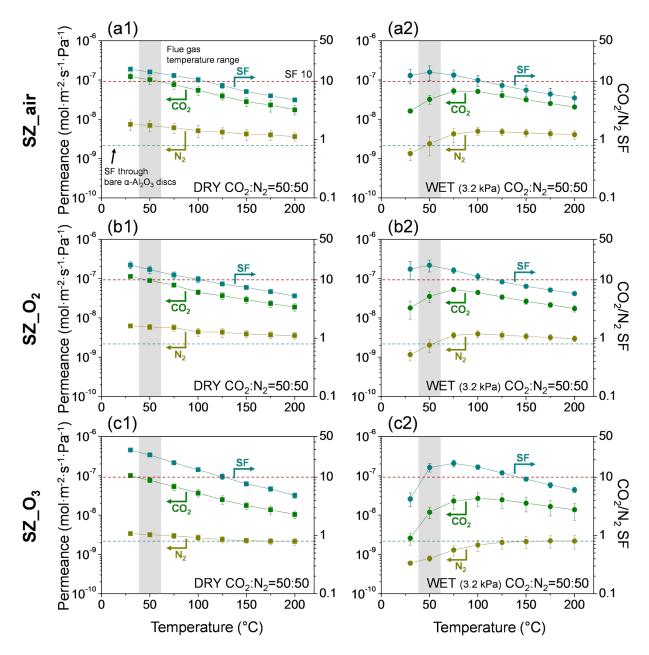


Fig. S7 XRD patterns of SZ, SZ\_air, SZ\_O<sub>2</sub>, and SZ\_O<sub>3</sub>. For clarity, the magnified XRD pattern of SZ is shown above its normalized one. The simulated XRD patterns of the all-silica CHA and DDR zeolites are added at bottom. Asterisks (\*) denote the XRD peaks originating from the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> disc.



**Fig. S8** Long-term stability tests of (a) SZ\_air, (b) SZ\_O<sub>2</sub>, and (c) SZ\_O<sub>3</sub> conducted at 50 °C up to 4 d to separate equimolar  $CO_2/CH_4$  binary mixture feed containing water vapor (12.3 kPa). Harsh conditions at 200 °C for 2 d were intentionally interposed to simulate long-term use. In (c), after long-term stability test of SZ\_O<sub>3</sub> at 12.3 kPa under wet conditions, SZ\_O<sub>3</sub> was heated at 110 °C for 3 h and then separation performance was measured at 50 °C under dry conditions.



**Fig. S9** CO<sub>2</sub>/N<sub>2</sub> permeances and SFs of (a1, a2) SZ\_air, (b1, b2) SZ\_O<sub>2</sub>, and (c1, c2) SZ\_O<sub>3</sub> measured under both (a1-c1) dry and (a2-c2) wet conditions. Separation performances of the SZ membrane series are plotted as a function of temperature up to 200 °C for equimolar CO<sub>2</sub>/N<sub>2</sub> binary mixture feed. Red and cyan dashed lines indicate the CO<sub>2</sub>/N<sub>2</sub> SFs of 10 and 0.8 (the SF value through a bare  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> disc), respectively. For clarity, temperature ranges of flue gases emitted from coal-fired power plants are shaded.

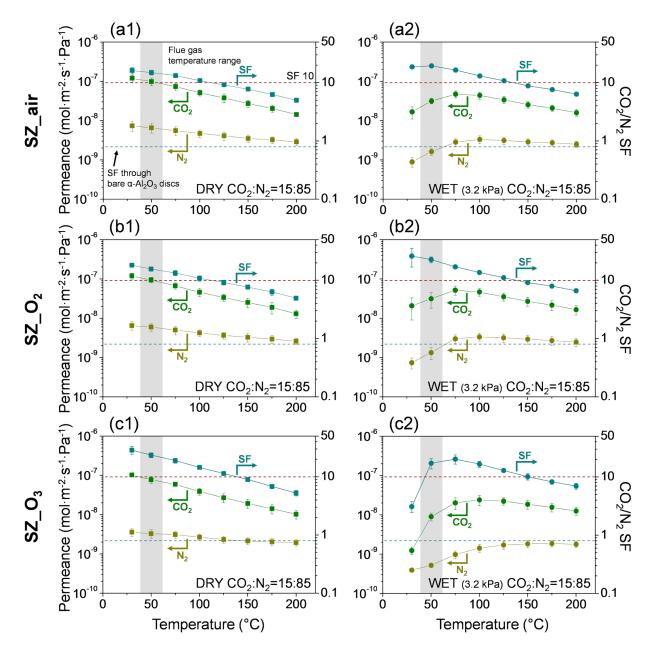
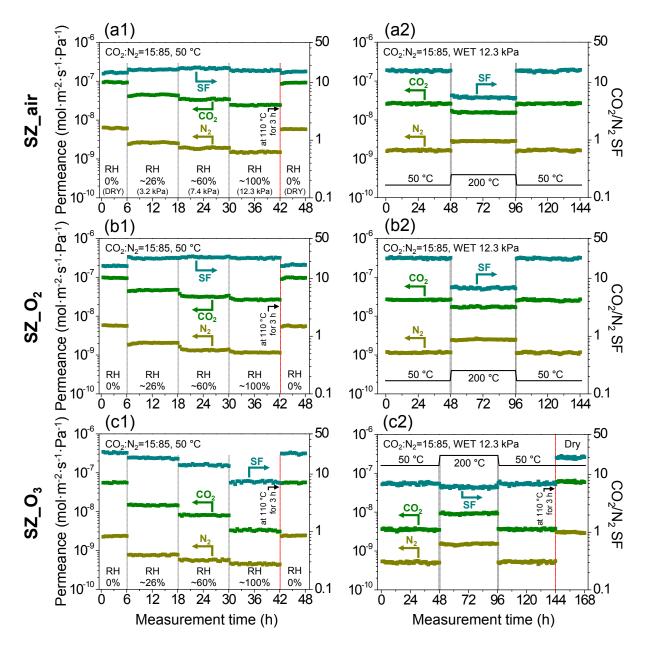
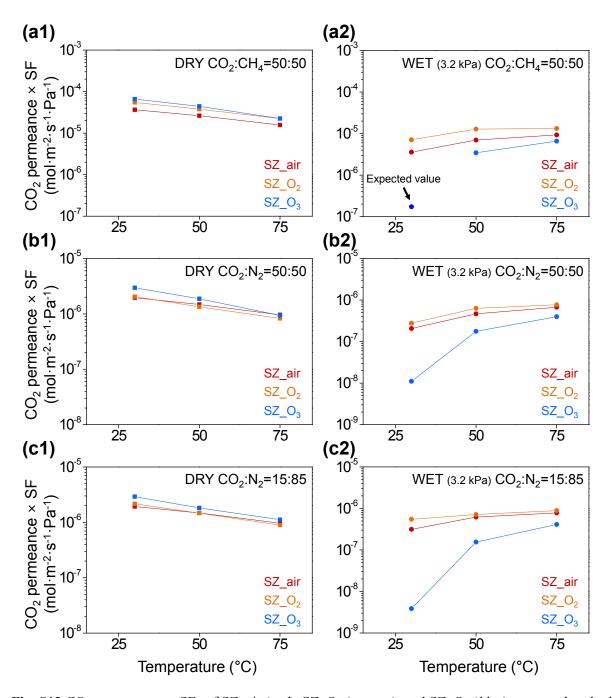


Fig. S10 CO<sub>2</sub>/N<sub>2</sub> permeances and SFs of (a1, a2) SZ\_air, (b1, b2) SZ\_O<sub>2</sub>, and (c1, c2) SZ\_O<sub>3</sub> measured under both (a1-c1) dry and (a2-c2) wet conditions. Separation performances of SZ membrane series are plotted as a function of temperature up to 200 °C for binary mixture feed composed of 15% CO<sub>2</sub> and 85% N<sub>2</sub>. Red and cyan dashed lines indicate the CO<sub>2</sub>/N<sub>2</sub> SFs of 10 and 0.8 (the SF value through a bare  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> disc), respectively. For clarity, temperature ranges of flue gases emitted from coal-fired power plants are shaded.



**Fig. S11** Stability tests of (a1) SZ\_air, (b1) SZ\_O<sub>2</sub>, and (c1) SZ\_O<sub>3</sub> for various humidities. Relative humidity was changed from 0% through ~26% and ~60% to ~100% (corresponding to H<sub>2</sub>O partial pressures of 0, 3.2, 7.4, and 12.3 kPa, respectively) at 50 °C in CO<sub>2</sub>/N<sub>2</sub> binary mixture feed composed of 15% CO<sub>2</sub> and 85% N<sub>2</sub>. Long-term stability tests of (a2) SZ\_air, (b2) SZ\_O<sub>2</sub>, and (c2) SZ\_O<sub>3</sub> conducted at 50 °C up to 4 d in CO<sub>2</sub>/N<sub>2</sub> binary mixture feed composed of 15% CO<sub>2</sub> and 85% N<sub>2</sub> containing water vapor (12.3 kPa). Harsh conditions at 200 °C for 2 d were intentionally interposed to simulate long-term use. After (a1-c1) relative humidity and (c2) long-term stability tests at 12.3 kPa under wet conditions, samples were heated at 110 °C for 3 h and then separation performances were measured at 50 °C under dry conditions.



**Fig. S12** CO<sub>2</sub> permeances × SFs of SZ\_air (*red*), SZ\_O<sub>2</sub> (*orange*), and SZ\_O<sub>3</sub> (*blue*) measured under both dry (*left*) and wet (*right*) conditions and plotted with respect to the relevant temperature ranges for equimolar (a1, a2) CO<sub>2</sub>/CH<sub>4</sub> and (b1, b2) CO<sub>2</sub>/N<sub>2</sub> binary mixture feeds and (c1, c2) CO<sub>2</sub>/N<sub>2</sub> binary mixture feed composed of 15% CO<sub>2</sub> and 85% N<sub>2</sub>.

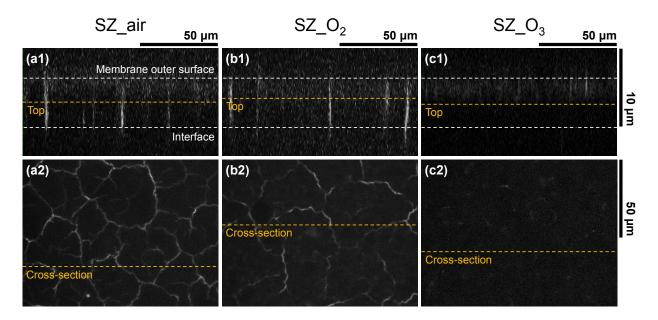
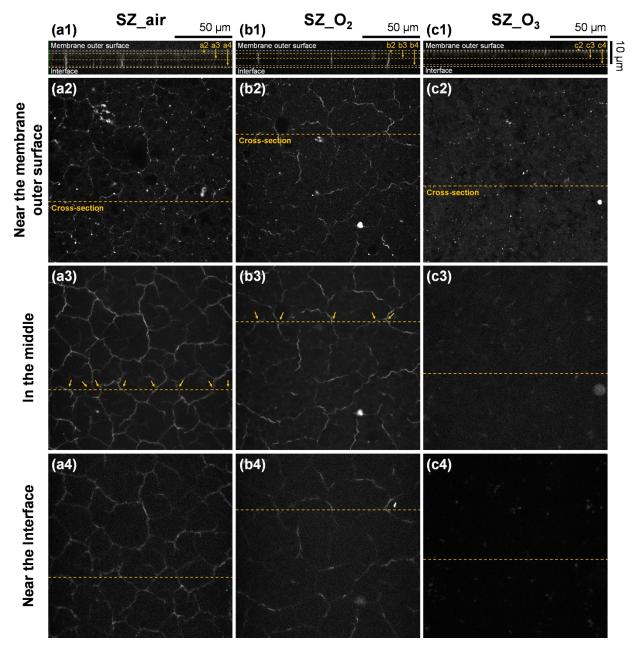
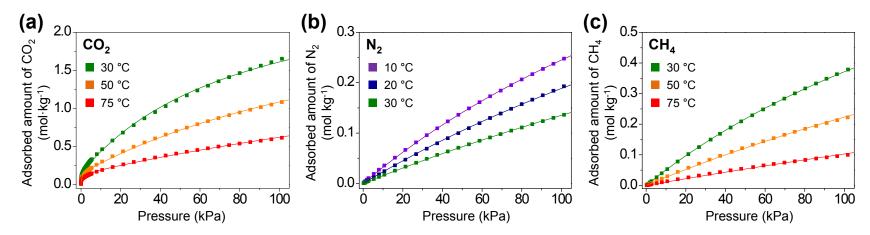


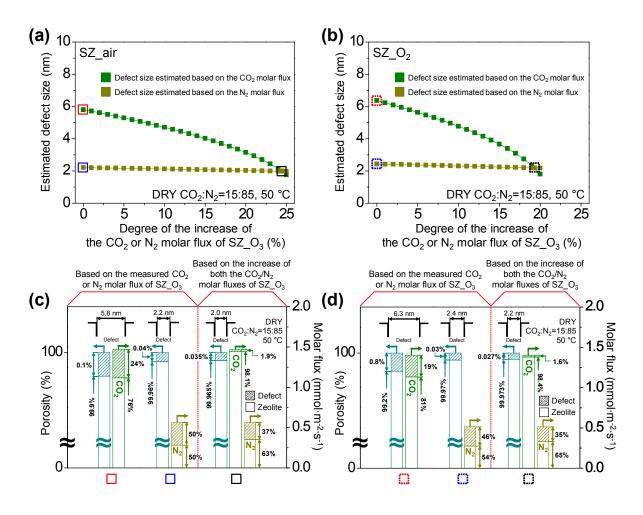
Fig. S13 (a1-c1) Cross-sectional view and (a2-c2) top view FCOM images of (a1-a2) SZ\_air, (b1-b2) SZ\_O<sub>2</sub>, and (c1-c2) SZ\_O<sub>3</sub>. These images are identical to those shown in Fig. 3, while information of where the images were obtained is given here. In particular, orange dashed lines in (a1-c1) indicate the positions where the top view FCOM images in (a2-c2) were obtained. Likewise, orange dashed lines in (a2-c2) indicate the positions where the cross-sectional view FCOM images in (a1-c1) were obtained. For clarity, white dashed lines in (a1-c1) are added to indicate membrane outer surface (*upper*) and interface between the membrane and  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> disc (*lower*).



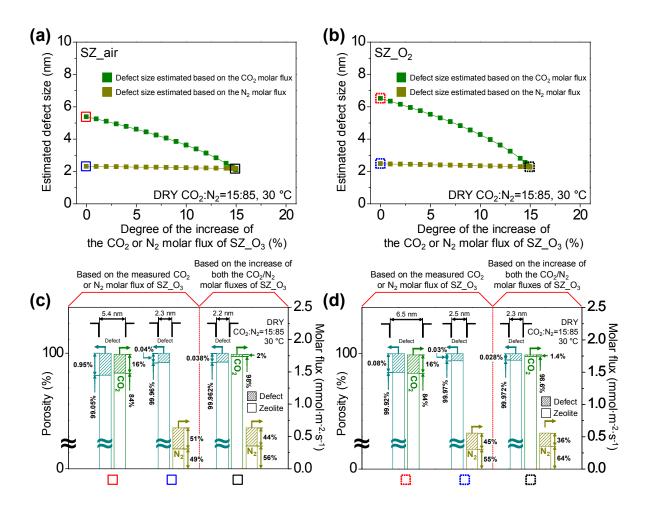
**Fig. S14** FCOM images of (a1-a4) SZ\_air, (b1-b4) SZ\_O<sub>2</sub>, and (c1-c4) SZ\_O<sub>3</sub>. Each membrane sample was dyed with 1 mM fluorescein sodium salt solution for 4 d. First row shows cross-sectional view FCOM images and second to fourth rows show top view FCOM images obtained (a2-c2) near the membrane outer surface, (a3-c3) in the middle, and (a4-c4) near the interface between the membrane and  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> disc. Cross-sectional view FCOM images were obtained at areas indicated by orange dashed lines in top view FCOM images. Orange dashed lines in cross-sectional view FCOM images in (a1-c1) indicate positions of top view FCOM images shown in (y2-y4), where y = a, b, and c. White dashed lines in cross-sectional view FCOM images in (a1-c1) indicate the membrane outer surface and interface. For convenience, cracks shown in (a1, b1) are indicated by orange arrows in (a3, b3).



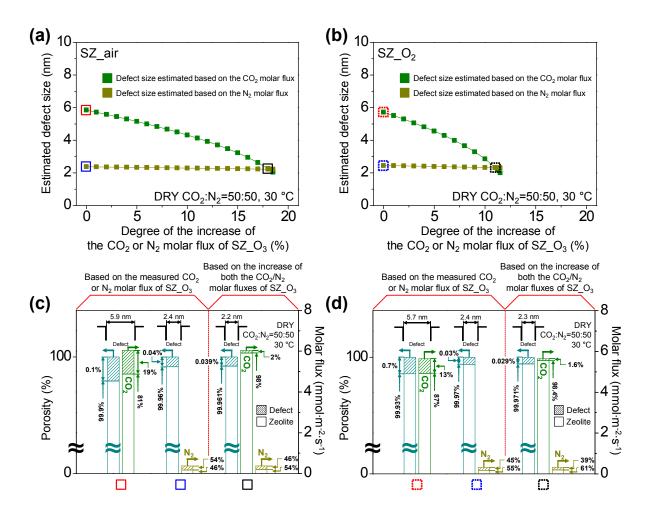
**Fig. S15** Adsorption isotherms of (a)  $CO_2$ , (b)  $N_2$ , and (c)  $CH_4$  in SZ-P\_air. Adsorption isotherms of  $CO_2$  and  $CH_4$  in (a, c) were measured at 30, 50, and 75 °C, while that of  $N_2$  in (b) was measured at 10, 20, and 30 °C. The fitted curves based on the parameters given in Table S1 are displayed as well.



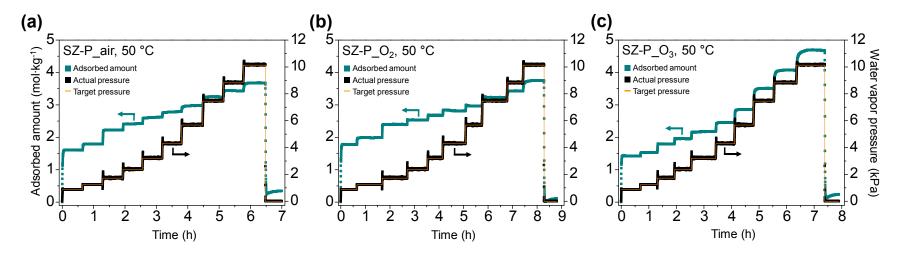
**Fig. S16** Defect sizes for (a) SZ\_air and (b) SZ\_O<sub>2</sub> estimated by combining quantitative properties extracted from the FCOM images and unidimensional permeation modeling. To simulate intrinsic membrane performance, the CO<sub>2</sub> and N<sub>2</sub> molar fluxes of defect-free SZ\_O<sub>3</sub> were equally increased, while preserving the corresponding CO<sub>2</sub>/N<sub>2</sub> SF. (c, d) Porosities of defective and zeolitic parts and their corresponding contributions to the total CO<sub>2</sub> and N<sub>2</sub> molar fluxes of (c) SZ\_air and (d) SZ\_O<sub>2</sub> for CO<sub>2</sub>/N<sub>2</sub> binary mixture feed composed of 15% CO<sub>2</sub> and 85% N<sub>2</sub> at 50 °C. Results corresponding to points marked by red, blue, and black boxes in (a) and dashed boxes in (b) are displayed in (c, d), respectively.



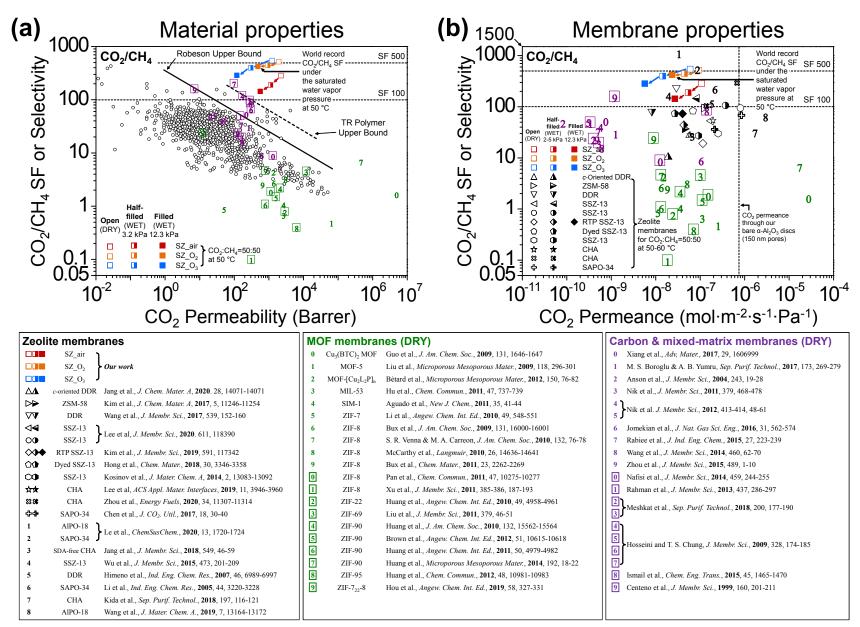
**Fig. S17** Defect sizes for (a) SZ\_air and (b) SZ\_O<sub>2</sub> estimated by combining quantitative properties extracted from the FCOM images and unidimensional permeation modeling. To simulate intrinsic membrane performance, the CO<sub>2</sub> and N<sub>2</sub> molar fluxes of defect-free SZ\_O<sub>3</sub> were equally increased, while preserving the corresponding CO<sub>2</sub>/N<sub>2</sub> SF. (c, d) Porosities of defective and zeolitic parts and their corresponding contributions to the total CO<sub>2</sub> and N<sub>2</sub> molar fluxes of (c) SZ\_air and (d) SZ\_O<sub>2</sub> for CO<sub>2</sub>/N<sub>2</sub> binary mixture feed composed of 15% CO<sub>2</sub> and 85% N<sub>2</sub> at 30 °C. Results corresponding to points marked by red, blue, and black boxes in (a) and dashed boxes in (b) are displayed in (c, d), respectively.



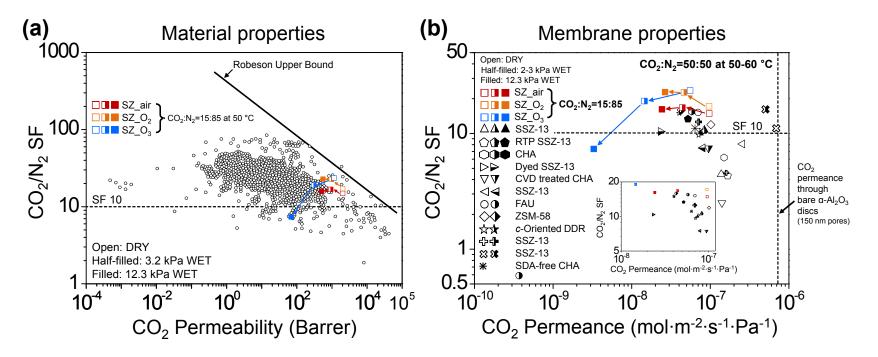
**Fig. S18** Defect sizes for (a) SZ\_air and (b) SZ\_O<sub>2</sub> estimated by combining quantitative properties extracted from the FCOM images and unidimensional permeation modeling. To simulate intrinsic membrane performance, the CO<sub>2</sub> and N<sub>2</sub> molar fluxes of defect-free SZ\_O<sub>3</sub> were equally increased, while preserving the corresponding CO<sub>2</sub>/N<sub>2</sub> SF. (c, d) Porosities of defective and zeolitic parts and their corresponding contributions to the total CO<sub>2</sub> and N<sub>2</sub> molar fluxes of (c) SZ\_air and (d) SZ\_O<sub>2</sub> for equimolar CO<sub>2</sub>/N<sub>2</sub> binary mixture feed at 30 °C. Results corresponding to points marked by red, blue, and black boxes in (a) and dashed boxes in (b) are displayed in (c, d), respectively.



**Fig. S19** Water vapor uptakes (*cyan*) in (a) SZ-P\_air, (b) SZ-P\_O<sub>2</sub>, and (c) SZ-P\_O<sub>3</sub> measured at different water vapor pressures (0.9, 1.2, 1.7, 2.3, 3.2, 4.2, 5.7, 7.4, 8.8, and 12.3 kPa) and 50 °C. In (a-c), target (*orange*) and actual (*black*) water vapor pressures are also displayed.



**Fig. S20** (a) CO<sub>2</sub>/CH<sub>4</sub> SFs (or selectivities) vs. CO<sub>2</sub> permeabilities of SZ\_air (*red*), SZ\_O<sub>2</sub> (*orange*), and SZ\_O<sub>3</sub> (*blue*) under dry conditions (*open*) and wet conditions (ca. 3.2 kPa (*half-filled*) and 12.3 kPa (*filled*)) at 50 °C. For comparison, the performances of polymeric ( $\odot$ ),<sup>16</sup> metal organic framework (MOF) (*green*),<sup>27.46</sup> and carbon & mixed-matrix (*purple*)<sup>47.61</sup> membranes under dry conditions are included. In addition, Robeson and thermally rearranged (TR) polymer upper bounds are denoted by black solid and dashed lines, respectively.<sup>16</sup> (b) CO<sub>2</sub>/CH<sub>4</sub> SFs (or selectivities) vs. CO<sub>2</sub> permeances of the SZ membrane series and other zeolite membranes (*marked by symbol*)<sup>10, 12, 17-21, 62-64</sup> measured at 50-60 °C under dry conditions (*open for symbols*) and wet conditions (ca. 2-5 kPa (*half-filled*) and 12.3 kPa (*filled*)). For comparison, the performances of additional zeolite (*numbered*),<sup>23, 65-70</sup> MOF (*green*),<sup>27.46</sup> and carbon & mixed-matrix (*purple*)<sup>47-49, 51-58, 60, 61</sup> membranes under dry conditions are included. Horizontal dashed lines in (a, b) indicate CO<sub>2</sub>/CH<sub>4</sub> SFs of 100 and 500. A vertical dashed line in (b) indicates CO<sub>2</sub> permeance estimated through Knudsen diffusion of a bare α-Al<sub>2</sub>O<sub>3</sub> disc having 150 nm pores. Detailed information about the membranes used for the graphs is described below.



**Fig. S21** (a)  $CO_2/N_2$  SFs vs.  $CO_2$  permeabilities of SZ\_air (*red*), SZ\_O<sub>2</sub> (*orange*), and SZ\_O<sub>3</sub> (*blue*) under dry conditions (*open*) and wet conditions (ca. 3.2 kPa (*half-filled*) and 12.3 kPa (*filled*)) at 50 °C. In (a), for comparison, the performances of polymeric membranes (*open dots*) and Robeson upper bound is denoted by the black line.<sup>16</sup> (b)  $CO_2/N_2$  SFs vs.  $CO_2$  permeances of the SZ membrane series and other zeolite membranes<sup>10, 12, 17-24</sup> measured at 50-60 °C under dry conditions (*open*) and wet conditions (ca. 2-3 kPa (*half-filled*) and 12.3 kPa (*filled*)). In (b), for clarity, the concentrated part of separation performances is illustrated in the inset graph. Horizontal dashed lines in (a, b) indicate the  $CO_2/N_2$  SF of 10, while a vertical dashed line in (b) indicates  $CO_2$  permeance through Knudsen diffusion of a bare  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> disc having 150 nm pores.

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