

## Electronic Supplementary Information

### **Coordination polymerization of nitrogen-rich linkers and dicyanamide anions toward energetic coordination polymers with low sensitivities**

Hao-Hui Xie,<sup>[a]</sup> Qin Wang,<sup>[a]</sup> Jiao-Lin Weng,<sup>[a]</sup> Yun-Fan Yan,<sup>[b]</sup> Hong-Yi Bian,<sup>[b]</sup>

Ying Huang,<sup>[a]</sup> Fa-Kun Zheng,<sup>[b,c]</sup> Ren-Hui Qiu,<sup>[a]\*</sup> Jian-Gang Xu<sup>[a,b,c]\*</sup>

<sup>a</sup> College of Material Engineering, Fujian Agriculture and Forestry University, Fuzhou 350108, China

<sup>b</sup> State Key Laboratory of Structural Chemistry, Fujian Institute of Research on the Structure of Matter, Chinese Academy of Sciences, Fuzhou, Fujian 350002, P. R. China

<sup>c</sup> Fujian Science & Technology Innovation Laboratory for Optoelectronic Information of China, Fuzhou, Fujian 350108, PR China

E-mail: renhuiqiu@fafu.edu.cn; jgxu@fafu.edu.cn

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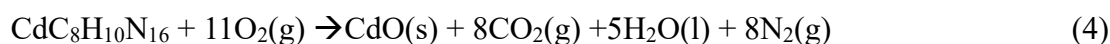
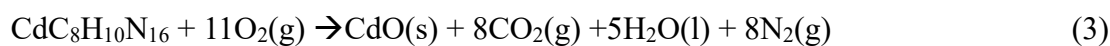
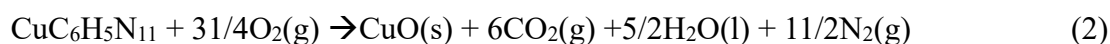
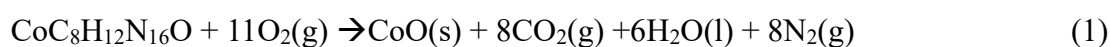
# 1. Experimental details

## 1.1 Heat of combustion

The constant-volume combustion energies of the compounds were determined by a precise oxygen bomb calorimetry (5E-AC8018, Changsha Kaiyuan Instruments, China). The correct value of the heat exchange was calculated according to the Linio-Pyfengdelel-Wsava equation.<sup>1</sup>

Firstly, we adopt the certified benzoic acid (about 1.0 g, pellet), which has an isothermal heat of combustion of  $(-26434 \pm 3) \text{ J}\cdot\text{g}^{-1}$  at 298.15 K, by the combustion in an oxygen atmosphere to calibrate the calorimeter. Then, 150 mg of the samples were prepared and mixed with certified benzoic acid, which were pressed to form a pellet to ensure better combustion. Finally, the pellet was placed in combustion pots, which were subsequently burned in an atmosphere of pure oxygen.

The enthalpies of formation ( $\Delta_f H$ ) of the compounds were back calculated by the enthalpy of combustion ( $\Delta_c H$ ). The  $\Delta_c H$  values were calculated from  $\Delta_c U$  with a gas volume correction:  $\Delta_c H = \Delta_c U + \Delta nRT$ , where  $\Delta n$  is the change of about molar amount of gases in the reaction process,  $R = 8.314 \text{ J}\cdot\text{mol}^{-1}\cdot\text{K}^{-1}$  and  $T = 298.15 \text{ K}$ . The constant-volume combustion heat ( $\Delta_c U$ ) **1**, **2**, **3**, and **4** is 13.490, 12.143, 12.695, and 11.308  $\text{kJ}\cdot\text{g}^{-1}$ , respectively, measured by the oxygen bomb calorimetry. The combustion reactions are based on Eqs. 1–4 as follows:



The **1–4**  $\Delta_c H$  values are determined to be  $-13.460$ ,  $-12.111$ ,  $-12.667$ , and  $-11.280$   $\text{kJ}\cdot\text{g}^{-1}$ , respectively. The  $\Delta_f H^\circ$  value of **1–4** was calculated from Hess's law to be  $0.935$ ,  $1.150$ ,  $1.745$ , and  $0.358$   $\text{kJ}\cdot\text{g}^{-1}$ , respectively, based on the known enthalpies of CuO (s,

$-155.2 \text{ kJ}\cdot\text{mol}^{-1}$ ),  $\text{CoO}$  (s,  $-237.9 \text{ kJ}\cdot\text{mol}^{-1}$ ),  $\text{CdO}$  (s,  $-258.35 \text{ kJ}\cdot\text{mol}^{-1}$ ),  $\text{CO}_2$  (g,  $-393.51 \text{ kJ}\cdot\text{mol}^{-1}$ ) and  $\text{H}_2\text{O}$  (l,  $-285.83 \text{ kJ}\cdot\text{mol}^{-1}$ ).

$$\Delta_f H^\circ[\mathbf{1},\text{s}] = \Delta_f H^\circ[\text{CoO},\text{s}] + 8\Delta_f H^\circ[\text{CO}_2,\text{g}] + 6\Delta_f H^\circ[\text{H}_2\text{O},\text{l}] - \Delta_c H[\mathbf{1},\text{s}] \quad (5)$$

$$\Delta_f H^\circ[\mathbf{2},\text{s}] = \Delta_f H^\circ[\text{CuO},\text{s}] + 6\Delta_f H^\circ[\text{CO}_2,\text{g}] + 5/2\Delta_f H^\circ[\text{H}_2\text{O},\text{l}] - \Delta_c H[\mathbf{2},\text{s}] \quad (6)$$

$$\Delta_f H^\circ[\mathbf{3},\text{s}] = \Delta_f H^\circ[\text{CdO},\text{s}] + 8\Delta_f H^\circ[\text{CO}_2,\text{g}] + 5\Delta_f H^\circ[\text{H}_2\text{O},\text{l}] - \Delta_c H[\mathbf{3},\text{s}] \quad (7)$$

$$\Delta_f H^\circ[\mathbf{4},\text{s}] = \Delta_f H^\circ[\text{CdO},\text{s}] + 8\Delta_f H^\circ[\text{CO}_2,\text{g}] + 5\Delta_f H^\circ[\text{H}_2\text{O},\text{l}] - \Delta_c H[\mathbf{4},\text{s}] \quad (8)$$

## 1.2 Detonation properties

Owing to that the explosion parameter calculation software EXPLO 5 cannot calculate the Cd and Co element, we selected the developed empirical Kamlet formula by Pang<sup>4</sup> to investigate the detonation properties of the metal-based EMs. Detonation performance of the related energetic materials here was evaluated by the developed method based on the empirical Kamlet formula as follows.

$$D = 1.01 \Phi^{1/2} (1 + 1.30\rho) \quad (9)$$

$$P = 1.558 \Phi\rho^2 \quad (10)$$

$$\Phi = 31.68 N(MQ)^{1/2} \quad (11)$$

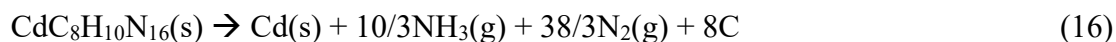
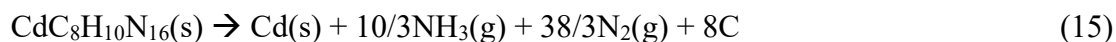
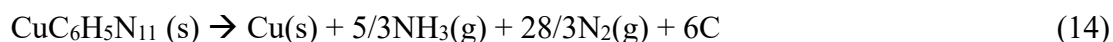
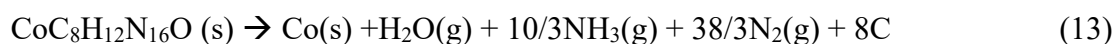
$$Q = -[\Delta H_f(\text{denotation products}) - \Delta H_f(\text{explosive})]/\text{formula weight of explosive} \quad (12)$$

Where  $D$  represents detonation velocity ( $\text{km}\cdot\text{s}^{-1}$ ) and  $P$  is detonation pressure (Gpa),  $\rho$  is the density of explosive ( $\text{g}\cdot\text{cm}^{-3}$ ).  $\Phi$ ,  $N$ ,  $M$ , and  $Q$  are the characteristic parameters of an explosive.  $N$  is the moles of detonation gases per gram of explosive,  $M$  is the average molecular weight of these gases, and  $Q$  is the heat of detonation ( $\text{kcal}\cdot\text{g}^{-1}$ ).

When the K-J (Kamlet-Jacobos) equation is employed, the overall calculation process can be described as follows: for the explosives composed of C, H, N, and O elements, all N atoms are converted to  $\text{N}_2$ ; O atoms form  $\text{H}_2\text{O}$  with H atoms first and then form

CO<sub>2</sub> with C atoms; the remaining C atoms are retained in solid state; if there are O atoms left, they will form O<sub>2</sub>. To preserve Kamlet's method, the developed theory is employed to determine the detonation products from metal-containing explosives. In most cases, metal atoms are converted to their oxidation states, emitting more heat after detonation. Otherwise, metal atoms can be treated as their reduction states, if the heat of formation (HOF) of metallic oxides is higher than that of H<sub>2</sub>O, or there is no O atom in the molecule. Besides, O atoms form H<sub>2</sub>O with H atoms first and the remaining ones then form CO<sub>2</sub> with C atoms. However, if the amount of O atoms is not sufficient to oxidize all H atoms, the remaining H atoms can produce NH<sub>3</sub> with N atoms, and the rest of the N atoms are released as N<sub>2</sub> gas. On the other hand, the remaining C atoms are retained in the solid state if they are not completely oxidized by O atoms. If there are redundant O atoms, however, they can be expelled as O<sub>2</sub>. The complete detonation reactions are described by Equations 4 and 5. The formation of metal as solid was assumed to be governed by the deficiency of oxygen.

The  $\Delta H_{det}$  value of **1–4** was calculated to be 1.654, 1.410, 2.091, and 0.704 kJ·g<sup>-1</sup>, respectively. On the basis of Equation 12 with the known  $\Delta_f H^\circ$ , Co, Cu, Cd, NH<sub>3</sub> (g, -46 kJ·mol<sup>-1</sup>), H<sub>2</sub>O (g, -241.8 kJ·mol<sup>-1</sup>), N<sub>2</sub>, C, and the above experimentally determined  $\Delta_f H^\circ$  values of **1–4**.



For **1**

$$\rho = 1.668 \text{ g}\cdot\text{cm}^{-3}$$

$$Q = \Delta H_{det} = 1.654 \text{ kJ}\cdot\text{g}^{-1} = 0.397 \text{ kcal}\cdot\text{g}^{-1}$$

$$N = 17/407.27 = 0.042 \text{ mol}\cdot\text{g}^{-1}$$

$$M = (18.015 \times 1 + 17.03 \times 10/3 + 28.01 \times 38/3) / 17 = 25.39 \text{ g} \cdot \text{mol}^{-1}$$

$$P = 1.558 \times (1.668)^2 \times [31.68 \times 0.042 \times (25.39 \times 0.397)^{1/2}] = 1.558 \times (1.668)^2 \times 4.196 = 18.19$$

GPa

$$D = 1.01 \times (4.196)^{1/2} \times (1 + 1.30 \times 1.668) = 6.555 \text{ km} \cdot \text{s}^{-1}$$

**For 2**

$$\rho = 1.811 \text{ g} \cdot \text{cm}^{-3}$$

$$Q = \Delta H_{det} = 1.410 \text{ kJ} \cdot \text{g}^{-1} = 0.338 \text{ kcal} \cdot \text{g}^{-1}$$

$$N = 11/294.75 = 0.037 \text{ mol} \cdot \text{g}^{-1}$$

$$M = (17.03 \times 10/3 + 28.01 \times 38/3) / 11 = 29.12 \text{ g} \cdot \text{mol}^{-1}$$

$$P = 1.558 \times (1.811)^2 \times [31.68 \times 0.037 \times (29.12 \times 0.338)^{1/2}] = 1.558 \times (1.811)^2 \times 3.710 = 18.96$$

GPa

$$D = 1.01 \times (3.710)^{1/2} \times (1 + 1.30 \times 1.811) = 6.526 \text{ km} \cdot \text{s}^{-1}$$

**For 3**

$$\rho = 1.822 \text{ g} \cdot \text{cm}^{-3}$$

$$Q = \Delta H_{det} = 2.091 \text{ kJ} \cdot \text{g}^{-1} = 0.501 \text{ kcal} \cdot \text{g}^{-1}$$

$$N = 16/442.72 = 0.036 \text{ mol} \cdot \text{g}^{-1}$$

$$M = (17.03 \times 10/3 + 28.01 \times 38/3) / 16 = 25.85 \text{ g} \cdot \text{mol}^{-1}$$

$$P = 1.558 \times (1.882)^2 \times [31.68 \times 0.036 \times (25.85 \times 0.501)^{1/2}] = 1.558 \times (1.882)^2 \times 4.122 = 21.32$$

GPa

$$D = 1.01 \times (4.122)^{1/2} \times (1 + 1.30 \times 1.822) = 6.908 \text{ km} \cdot \text{s}^{-1}$$

**For 4**

$$\rho = 1.777 \text{ g} \cdot \text{cm}^{-3}$$

$$Q = \Delta H_{det} = 0.704 \text{ kJ} \cdot \text{g}^{-1} = 0.169 \text{ kcal} \cdot \text{g}^{-1}$$

$$N = 16/442.73 = 0.036 \text{ mol}\cdot\text{g}^{-1}$$

$$M = (17.03 \times 10/3 + 28.01 \times 38/3)/16 = 25.85 \text{ g}\cdot\text{mol}^{-1}$$

$$P = 1.558 \times (1.777)^2 \times [31.68 \times 0.036 \times (25.85 \times 0.169)^{1/2}] = 1.558 \times (1.777)^2 \times 2.392 = 11.77 \text{ GPa}$$

$$D = 1.01 \times (2.392)^{1/2} \times (1 + 1.30 \times 1.777) = 5.171 \text{ km}\cdot\text{s}^{-1}$$

### 1.3 Sensitivity Test

The sensitivities of the compounds were determined according to the BAM (German: Bundesanstalt für Materialforschung und Prüfung) standard for friction and impact. The classification of the tested compounds results from the ‘UN Recommendations on the Transport of Dangerous Goods’.

**Impact sensitivity:** The impact sensitivities of **1–4** were tested on a BAM fall hammer produced by OZM Research Impact sensitivity tests according to STANAG 4489. A 5 kg weight was dropped from a set height onto a 10 mg sample placed on a copper cap. The test results showed that the explosion happened with approximate 50% initiation probability. Impact sensitivity of **1–4** were observed to be > 40, > 25, > 40, and > 40 J, respectively.<sup>2</sup>

**Friction sensitivity:** The friction sensitivity was determined using a FSKM-10 BAM friction apparatus produced by OZM Research on the basis of STANAG 4487. Friction sensitivity of **1-4** were observed to be > 360, > 360, > 360, and 360 N, respectively.<sup>2</sup>

### 1.4 Specific impulse and thrust coefficient

Specific impulse and thrust coefficient are crucial parameters to assess propellant performance. Specific impulse represents the duration of per unit propellant producing the same thrust and thrust coefficient ( $C_F$ ) represents the ratio of actual thrust to

isentropic expansion flow. It is calculated by equations  $C_F = I_{sp} \cdot g \cdot c^{*-1}$ , where  $g = 9.8 \text{ m} \cdot \text{s}^{-2}$ ,  $c^*$  is effective velocity calculated by software.

In this work, the theoretical specific impulse is calculated by chemical equilibrium application (CEA) codes and reported by NASA researchers.<sup>3</sup> In the entire calculation, the chemical formula of fuels and oxidizer ( $\text{HNO}_3$ ), heat of formation ( $\Delta_f H^\circ = 339 \text{ kJ} \cdot \text{mol}^{-1}$ ), ambient temperature ( $T_a = 298.15 \text{ K}$ ), fuel-to-oxidizer ratio ( $\text{O/F} = 1.0\text{--}4.0$ ), chamber pressure ( $P_c = 25 \text{ atm}$ ), ambient pressure ( $P_e = 1 \text{ atm}$ ), expansion ratio (exit-to-throat area ratio,  $A_e/A_t = 2\text{--}5$ ), freezing flow conditions during expansion also considered. The best thrust is collected at  $\text{O/F} = 4.0$ ,  $A_e/A_t = 4.836$  with  $I_{sp} = 217 \text{ s}$  and  $C_F = 1.478$ .



## 2. Tables

**Table S1.** Selected bond distances (Å) and bond angles (°).

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Compound 1			
Co(1)–N(14)	2.126(2)	Co(1)–N(11)#2	2.088(2)
Co(1)–N(26)	2.142(2)	Co(1)–N(13)	2.109(2)
Co(1)–N(16)#1	2.148(2)	Co(1)–N(21)	2.139(2)
N(14)–Co(1)–N(26)	91.59(7)	N(11)#2–Co(1)–N(21)	92.60(8)
N(14)–Co(1)–N(16)#1	90.41(8)	N(13)–Co(1)–N(14)	177.85(8)
N(14)–Co(1)–N(21)	87.54(7)	N(13)–Co(1)–N(26)	90.27(8)
N(26)–Co(1)–N(16)#1	85.56(8)	N(13)–Co(1)–N(16)#1	88.65(8)
N(11)#2–Co(1)–N(14)	89.04(8)	N(13)–Co(1)–N(21)	90.47(8)
N(11)#2–Co(1)–N(26)	95.46(8)	N(21)–Co(1)–N(26)	171.88(8)
N(11)#2–Co(1)–N(16)#1	178.85(8)	N(21)–Co(1)–N(16)#1	86.37(8)
Compound 2			
Cu(1)–N(21)	2.221(3)	Cu(1)–N(13)	1.997(3)
Cu(1)–N(16)#1	1.981(3)	Cu(1)–N(14)	1.962(2)
Cu(1)–N(11)#2	1.995(3)		
N(16)#1–Cu(1)–N(21)	98.83(10)	N(14)–Cu(1)–N(21)	93.19(12)
N(16)#1–Cu(1)–N(11)#2	161.52(11)	N(14)–Cu(1)–N(16)#1	91.48(10)
N(13)–Cu(1)–N(21)	94.84(11)	N(14)–Cu(1)–N(13)	171.71(13)
N(13)–Cu(1)–N(16)#1	89.35(10)	N(14)–Cu(1)–N(11)#2	89.29(11)
N(13)–Cu(1)–N(11)#2	87.33(10)	N(11)#2–Cu(1)–N(21)	99.56(10)
Compound 3			
Cd(1)–N(21)#1	2.3288(16)	Cd(1)–N(13)	2.3527(18)
Cd(1)–N(21)	2.3288(16)	Cd(1)–N(11)#2	2.346(2)
Cd(1)–N(13)#1	2.3527(18)	Cd(1)–N(11)#3	2.346(2)

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N(21)#1–Cd(1)–N(21)	180.0	N(21)–Cd(1)–N(11)#3	89.22(7)
N(21)#1–Cd(1)–N(13)	86.42(6)	N(13)–Cd(1)–N(13)#1	180.0
N(21)#1–Cd(1)–N(13)#1	93.58(6)	N(11)#3–Cd(1)–N(13)#1	94.54(7)
N(21)–Cd(1)–N(13)#1	86.42(6)	N(11)#3–Cd(1)–N(13)	85.46(7)
N(21)–Cd(1)–N(13)	93.58(6)	N(11)#2–Cd(1)–N(13)	94.54(7)
N(21)#1–Cd(1)–N(11)#2	89.22(7)	N(11)#2–Cd(1)–N(13)#1	85.46(7)
N(21)–Cd(1)–N(11)#2	90.78(7)	N(11)#2–Cd(1)–N(11)#3	180.0
N(21)#1–Cd(1)–N(11)#3	90.78(7)		
<b>Compound 4</b>			
Cd(2)–N(21)	2.355(2)	Cd(1)–N(11)#4	2.365(2)
Cd(2)–N(21)#1	2.355(2)	Cd(1)–N(11)	2.365(2)
Cd(2)–N(43)#2	2.320(2)	Cd(1)–N(33)#5	2.338(2)
Cd(2)–N(43)#3	2.320(2)	Cd(1)–N(33)#6	2.338(2)
Cd(2)–N(41)	2.312(2)	Cd(1)–N(31)#4	2.314(2)
Cd(2)–N(41)#1	2.312(2)	Cd(1)–N(31)	2.314(2)
N(31)#4–Cd(1)–N(11)	86.24(9)	N(31)–Cd(1)–N(33)#6	94.61(9)
N(31)–Cd(1)–N(11)#4	86.23(9)	N(31)#4–Cd(1)–N(33)#5	94.61(9)
N(31)–Cd(1)–N(11)	93.77(9)	N(31)#4–Cd(1)–N(31)	180.0
N(31)#4–Cd(1)–N(11)#4	93.76(9)	N(31)#4–Cd(1)–N(11)	86.24(9)
N(31)#4–Cd(1)–N(33)#6	85.39(9)	N(31)–Cd(1)–N(11)#4	86.23(9)
N(31)–Cd(1)–N(33)#5	85.39(10)	N(31)–Cd(1)–N(11)	93.77(9)
N(31)–Cd(1)–N(33)#6	94.61(9)	N(31)#4–Cd(1)–N(11)	86.24(9)
N(31)#4–Cd(1)–N(33)#5	94.61(9)	N(31)–Cd(1)–N(11)#4	86.23(9)
N(31)#4–Cd(1)–N(31)	180.0	N(31)–Cd(1)–N(11)	93.77(9)
N(31)#4–Cd(1)–N(11)	86.24(9)	N(31)#4–Cd(1)–N(11)#4	93.76(9)
N(31)–Cd(1)–N(11)#4	86.23(9)	N(31)#4–Cd(1)–N(33)#6	85.39(9)
N(31)–Cd(1)–N(11)	93.77(9)	N(31)–Cd(1)–N(33)#5	85.39(10)
N(31)#4–Cd(1)–N(11)#4	93.76(9)	N(31)–Cd(1)–N(33)#6	94.61(9)
N(31)#4–Cd(1)–N(33)#6	85.39(9)	N(31)#4–Cd(1)–N(33)#5	94.61(9)
N(31)–Cd(1)–N(33)#5	85.39(10)	N(31)#4–Cd(1)–N(31)	180.0

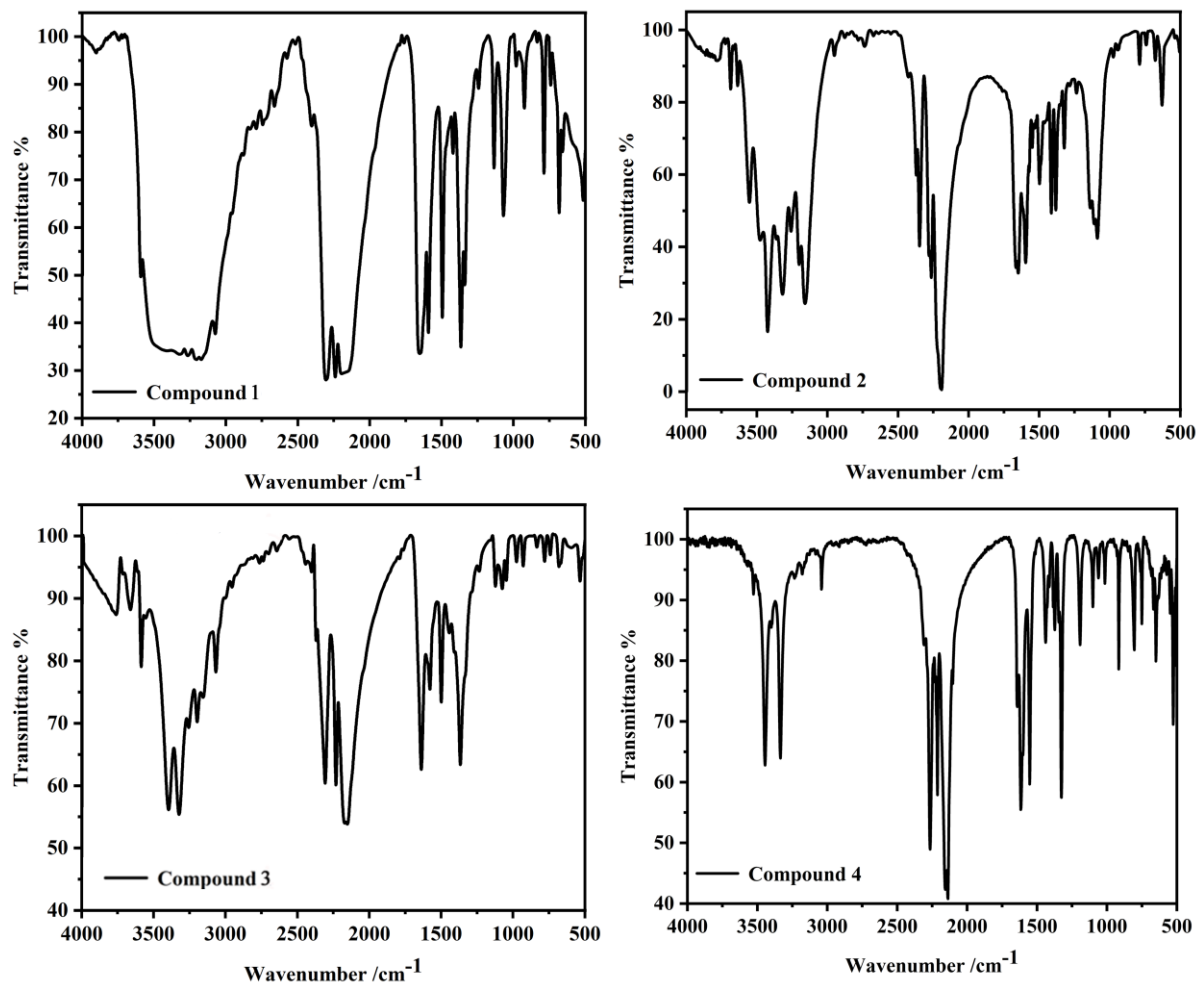
Symmetry codes for the compounds **1**, **2**, **3** and **4**. For **1**, #1  $-1 + x, y, z$ .; #2  $1 + x, y, z$ . For **2**, #1  $x, 3/2 - y, -1/2 + z$ .; #2  $-x, -y, 1 - z$ .; #3  $x, 3/2 - y, 1/2 + z$ . For **3**, #1  $2 - x, 1 - y, 1 - z$ .; #2  $x, 3/2 - y, 1/2 + z$ .; #3  $2 - x, -1/2 + y, 1/2 - z$ .; #4  $2 - x, 1/2 + y, 1/2 - z$ . For **4**, #1  $1 - x, 2 - y, -z$ .; #2  $-x, 2 - y, -z$ .; #3  $1 + x, y, z$ .; #4  $1 - x, -y, 1 - z$ .; #5  $2 - x, -y, 1 - z$ .; #6  $-1 + x, y, z$ .

**Table S2.** Hydrogen bond distances (Å) and bond angles (°).

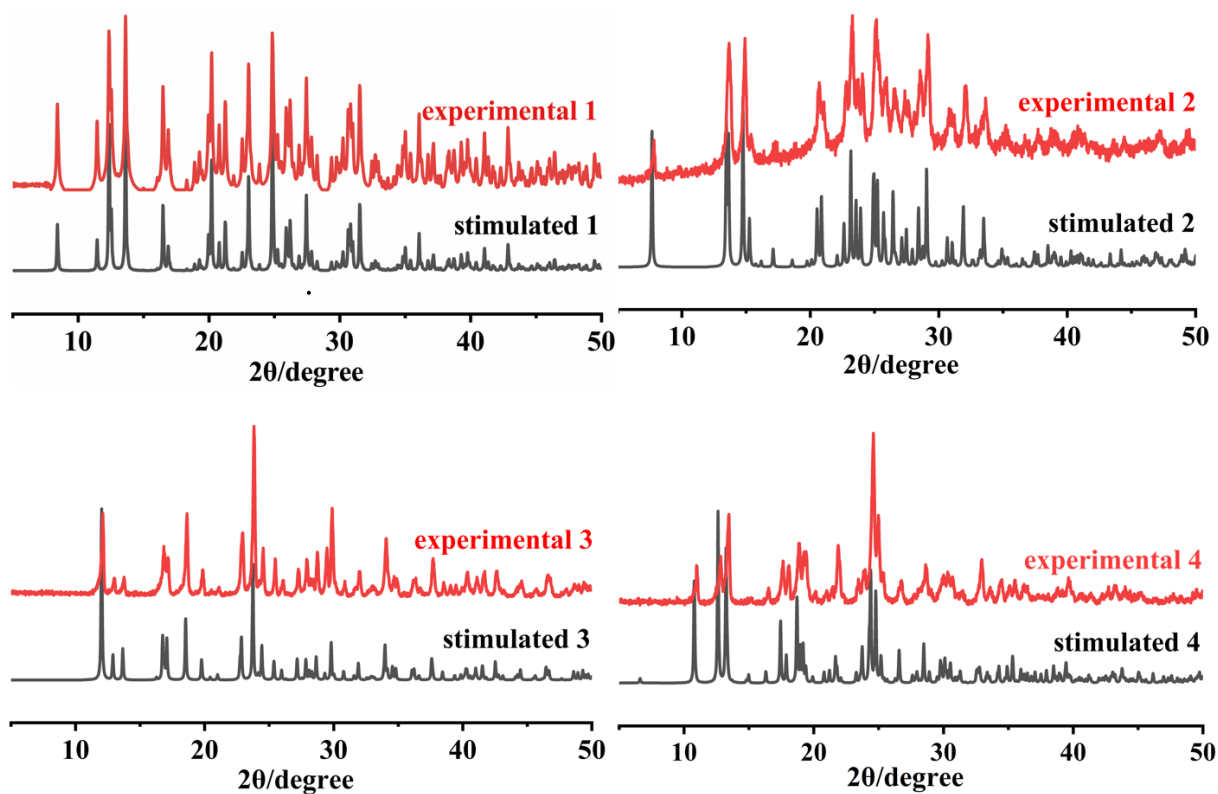
Donor–H···Acceptor	d(D–H)	d(H···A)	d(D···A)	∠D---H···A
<b>Compound 1</b>				
O(1W)–H(1WA)···N(15)#4	0.71(5)	2.23(5)	2.929(3)	169
O(1W)–H(1WB)···N(27)#2	0.82(4)	2.14(4)	2.918(3)	159
N(25)–H(25A)···N(11)#2	0.88	2.80	3.440(3)	130
N(30)–H(30B)···N(22)#6	0.88	2.14	2.982(3)	160
<b>Compound 2</b>				
N(25)–H(25A)···N(22)#9	0.86	2.17	3.005(4)	164
<b>Compound 3</b>				
N(25)–H(25A)···N(11)#1	0.86	2.29	3.059(3)	150
N(25)–H(25B)···N(13)#2	0.86	2.45	3.135(3)	138
<b>Compound 4</b>				
N(15)–H(15A)···N(33)#7	0.86	2.39	3.218(4)	162
N(15)–H(15B)···N(22)#6	0.86	2.41	3.255(3)	168
N(25)–H(25A)···N(14)	0.86	2.33	3.217(4)	154
N(25)–H(25B)···N(43)#8	0.86	2.53	3.330(4)	154

Symmetry codes: #1  $x, 3/2 - y, 1/2 + z$ ; #2  $1 - x, 1 - y, 1 - z$ ; #3  $x, 3/2 - y, 1/2 + z$ ; #4  $-1/2 + x, 3/2 - y, 1/2 + z$ ; #5  $2 - x, 1 - y, -z$ ; #6  $1 - x, 1 - y, -z$ ; #7  $2 - x, 1 - y, 1 - z$ ; #8  $1 + x, y, z$ ; #9  $x, 1/2 - y, -1/2 + z$ .

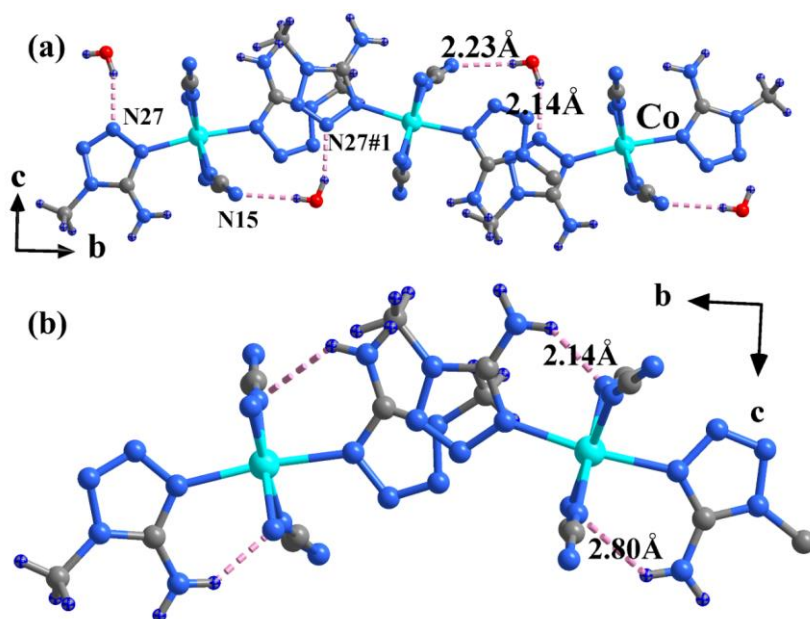
### 3. Graphics



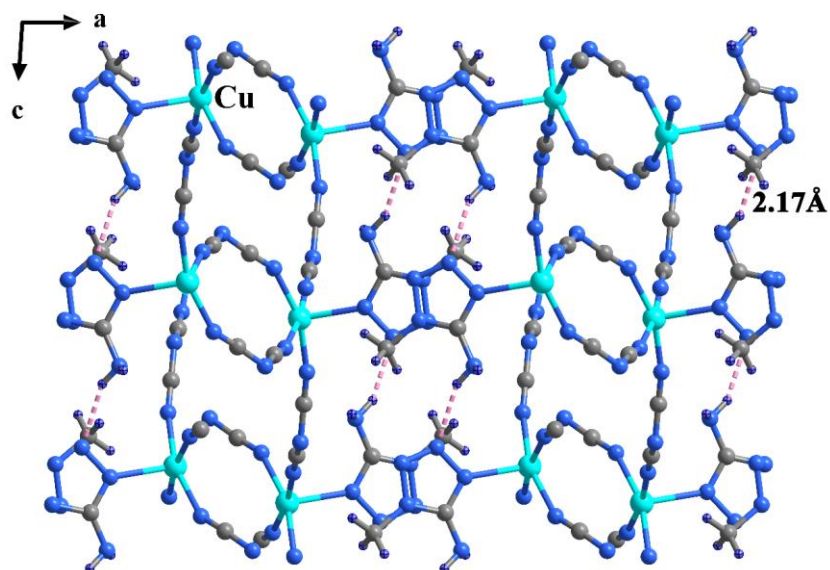
**Fig. S1** Fourier transform infrared (FT-IR) spectra of the compounds 1–4.



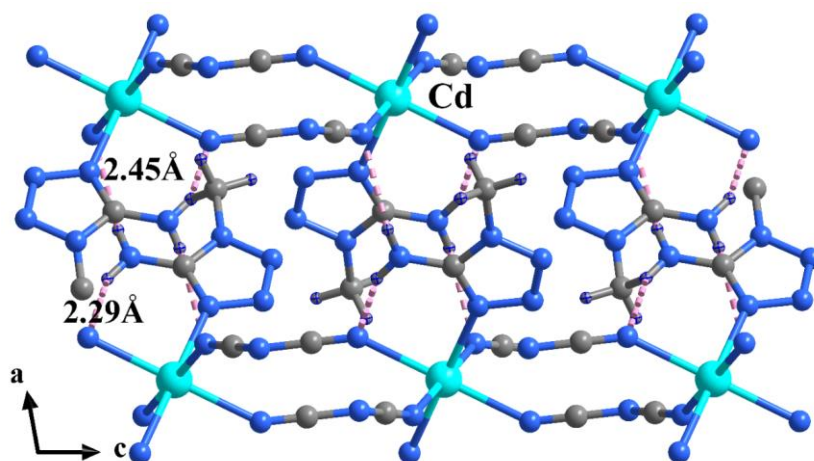
**Fig. S2** Powdered X-ray diffraction (PXRD) patterns of the compounds **1–4**.



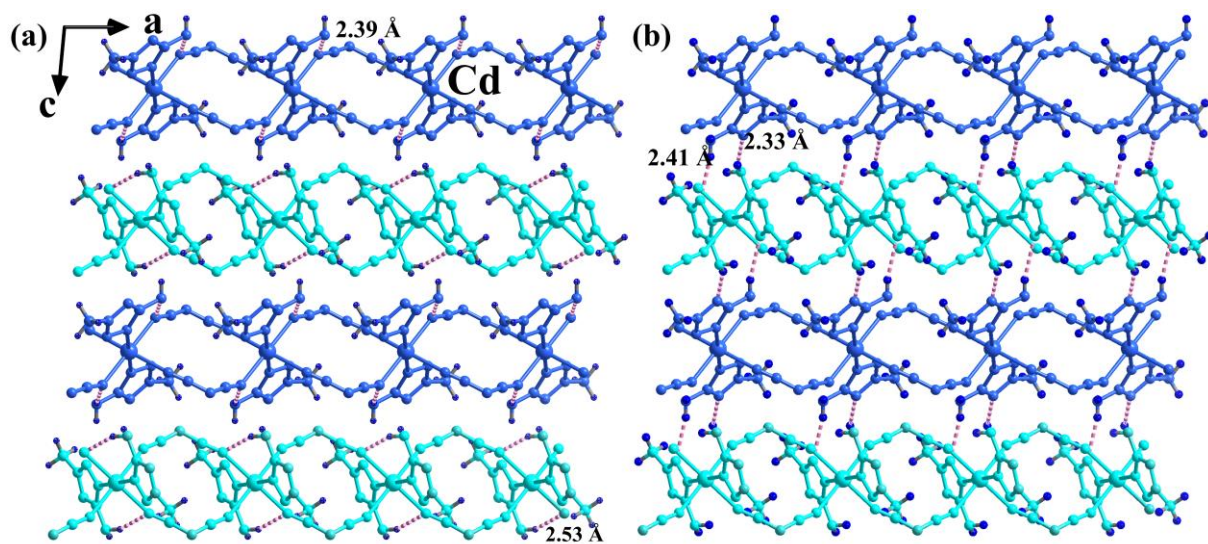
**Fig. S3** Hydrogen bonds of the compound **1** generated by (a) water molecules and (b) adjacent nitrogen atoms.



**Fig. S4** Hydrogen bonds of the compound **2** running along *c* direction.



**Fig. S5** Hydrogen bonds of the compound **3** running along *c* direction.



**Fig. S6** Hydrogen bonds of the compound **4** (a) between single-chain ending-on  $\text{DCA}^-$  anions and the amine group of 2-MAT ligand and (b) interleaved chains.



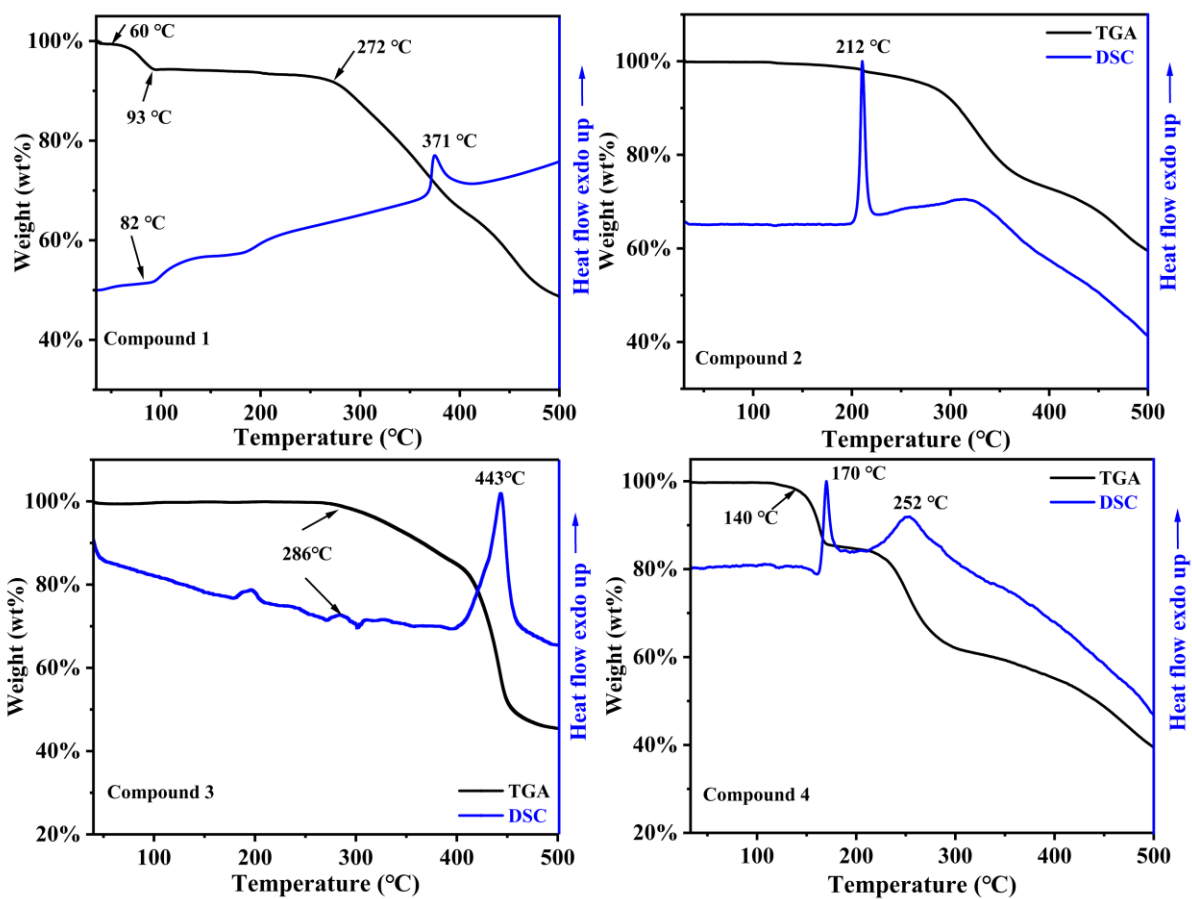
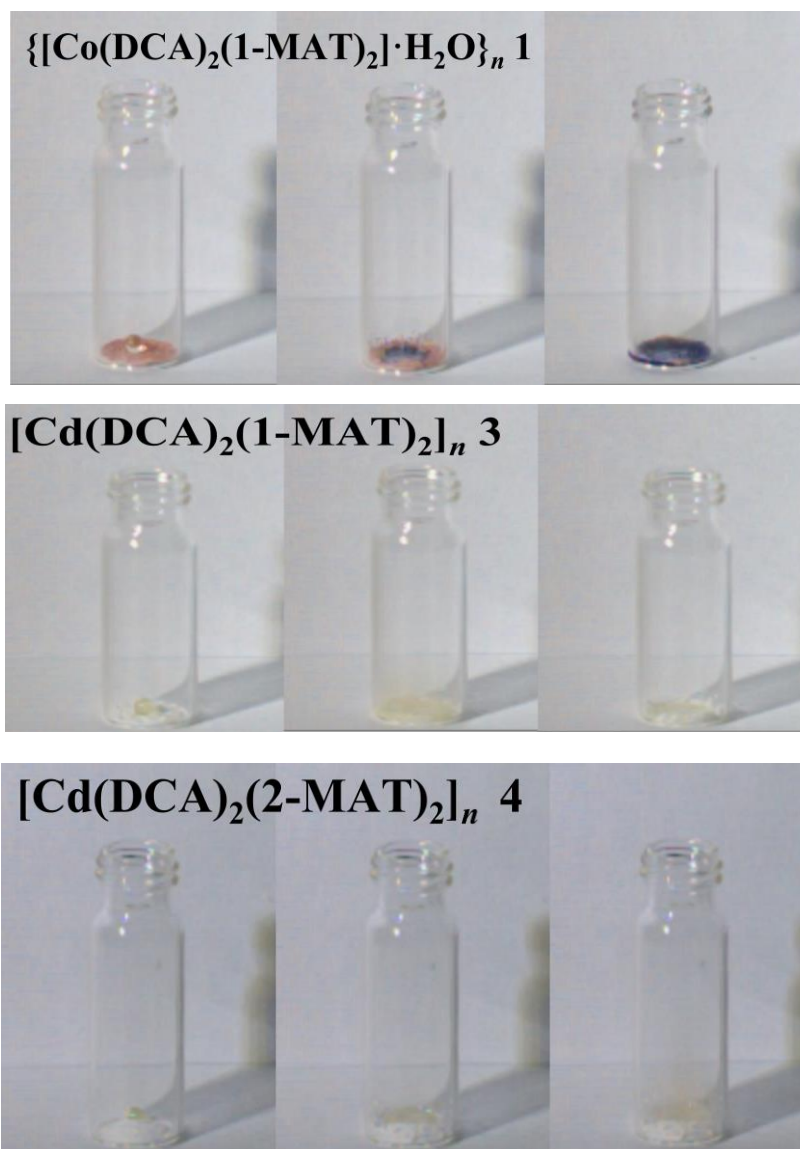


Fig. S7 DSC-TGA curves of 1-4.



**Fig. S8** Hypergolicity drop tests of the compounds **1**, **3** and **4**.

## 4. References

- [1] Popov, M. M. Thermometry and Calorimetry; Moscow University Publishing House: Moscow. **1954**, 382.
- [2] Impact: insensitive  $> 40$  J, less sensitive  $\geq 35$  J, sensitive  $\geq 4$  J, very sensitive  $\leq 3$  J; Friction: insensitive  $> 360$  N, less sensitive  $= 360$  N,  $80$  N  $<$  sensitive  $< 360$  N, very sensitive  $\leq 80$  N, extremely sensitive  $\leq 10$  N.
- [3] G.S. McBride BJ, Computer Program for Calculation of Complex Chemical Equilibrium Compositions and Applications II. Users Manual and Program Description, NASA Ref. Publ. 1311, NASA Lewis Research Center Cleveland, Ohio 44135; 1996.
- [4] Y. Wang, J.-C. Zhang, H. Su, S.-H. Li, S.-W. Zhang, and S.-P. Pang, *J. Phys. Chem. A*, 2014, **118**, 4575-4581.