

1 This supplemental information file covers: (1) Contribution analysis results for the laboratory-scale  
2 perovskite tandems; (2) Contribution analysis results for the commercial-scale perovskite tandems; (3)  
3 Resistivity test results; (4) Short current density, open circuit voltage, and fill factor of perovskite-perovskite  
4 tandem; (5) Transmittance; (6) Scanning Electron Microscopy; (7) Normalized photoluminescence (PL)  
5 intensity and PL quantum efficiency (PLQE); (8) Solar cell stability test; (9) Cumulative energy yield; (10)  
6 Doctor blading v.s. solvent dissolution method; (11) Techno-economic analysis for the recovery process  
7 with sensitivity analysis; (12) Impact of module shipping; (13) Sensitivity analysis of EROI on insolation  
8 condition; (14) Impact of PCE threshold on perovskite-perovskite tandem module replacement; (15)  
9 Material and energy inventory; (16) Supplemental references.

10

## 11 **Supplemental items**

### 12 **Contribution analysis results for the laboratory-scale perovskite tandems**

13 Two representative perovskite tandem architectures that have the potential to be implemented on a  
14 commercial scale are investigated. Identifying the energy and environmental hotspots from the prototypical  
15 tandem architectures through contribution analysis is important and guides material and processing step  
16 replacement toward industry-relevant tandem stacks. The results of the “cradle-to-grave” contribution  
17 analysis would inform the components worth recycling and guide the experimental investigation of the  
18 recycling process at the laboratory scale. The “cradle-to-grave” system boundary comprises four life cycle  
19 stages, including raw material acquisition, device fabrication, electricity generation, and end-of-life disposal.  
20 The landfill of used photovoltaic (PV) modules is selected as the end-of-life scenario method following the  
21 existing literature. The Product Environmental Footprint (PEF) approach is selected to unmask the full  
22 spectrum environmental profiles of the investigated perovskite tandem modules.<sup>1</sup> There is a total of 17  
23 midpoint indicators, including climate change; ozone depletion; human toxicity, cancer effects; human  
24 toxicity, non-cancer effects; particulate matter/respiratory effects; ionizing radiation, human health;  
25 photochemical ozone formation; acidification; eutrophication, terrestrial; eutrophication, freshwater;  
26 eutrophication, marine; ecotoxicity, freshwater; land use; resource depletion, water; resource depletion,  
27 mineral, fossil, renewable; cumulative energy demand (CED), renewable; and CED, non-renewable.

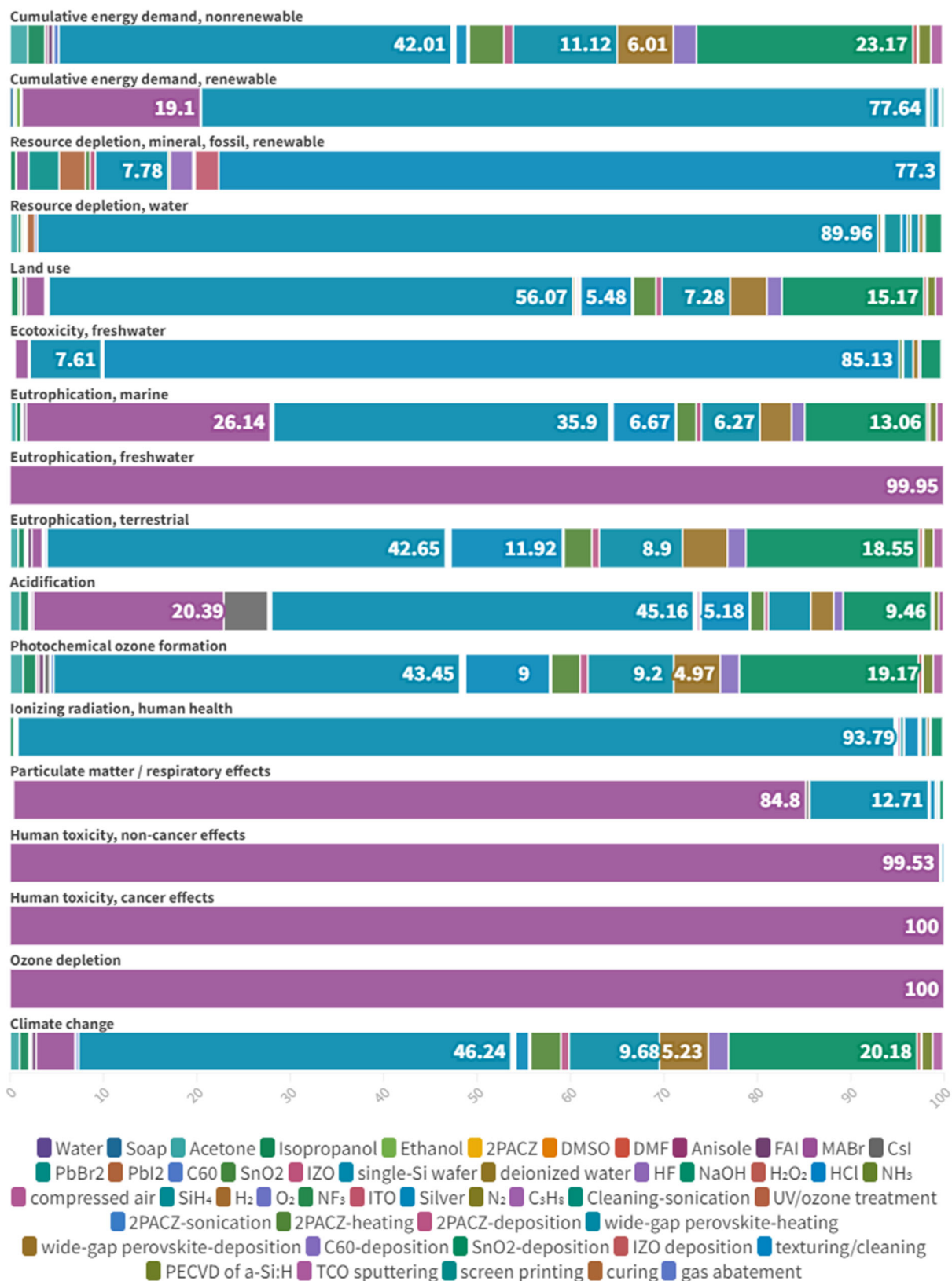
28



30 Figure S1. Contribution analysis results for the laboratory-scale perovskite-perovskite tandem with a  
31 “cradle-to-grave” system boundary.

32  
33 Figure S1 depicts the environmental profile of the laboratory-scale perovskite-perovskite tandem for  
34 the explored midpoint impact categories according to the PEF method. The environmental impacts are  
35 divided by different material and energy inputs for each impact category. We note that gold and atomic  
36 layer deposition (ALD) of the SnO<sub>2</sub> layer are identified as the predominant contributors to cumulative energy  
37 demand and climate change. The ALD of the SnO<sub>2</sub> layer is regarded as the primary contributor due to  
38 intensive energy consumption, accounting for 31.8% of the total energy consumption.

39



41 Figure S2. Contribution analysis results for the laboratory-scale perovskite-silicon tandem with a “cradle-to-  
42 grave” system boundary.

43  
44 Figure S2 depicts the full-spectrum environmental profile for the laboratory-scale perovskite-silicon  
45 tandem. We note that for most of the impact categories, heating processes, silicon wafers, and ALD of  
46 SnO<sub>2</sub> are the significant contributors. In addition, the use of silver contributes up to 80% of the indicator  
47 regarding resource depletion and freshwater ecotoxicity. The use of even small quantities of the precious  
48 metal dominates certain impact categories for perovskite tandems. The impact of MABr is the most  
49 pronounced for human toxicity and ozone depletion.

50

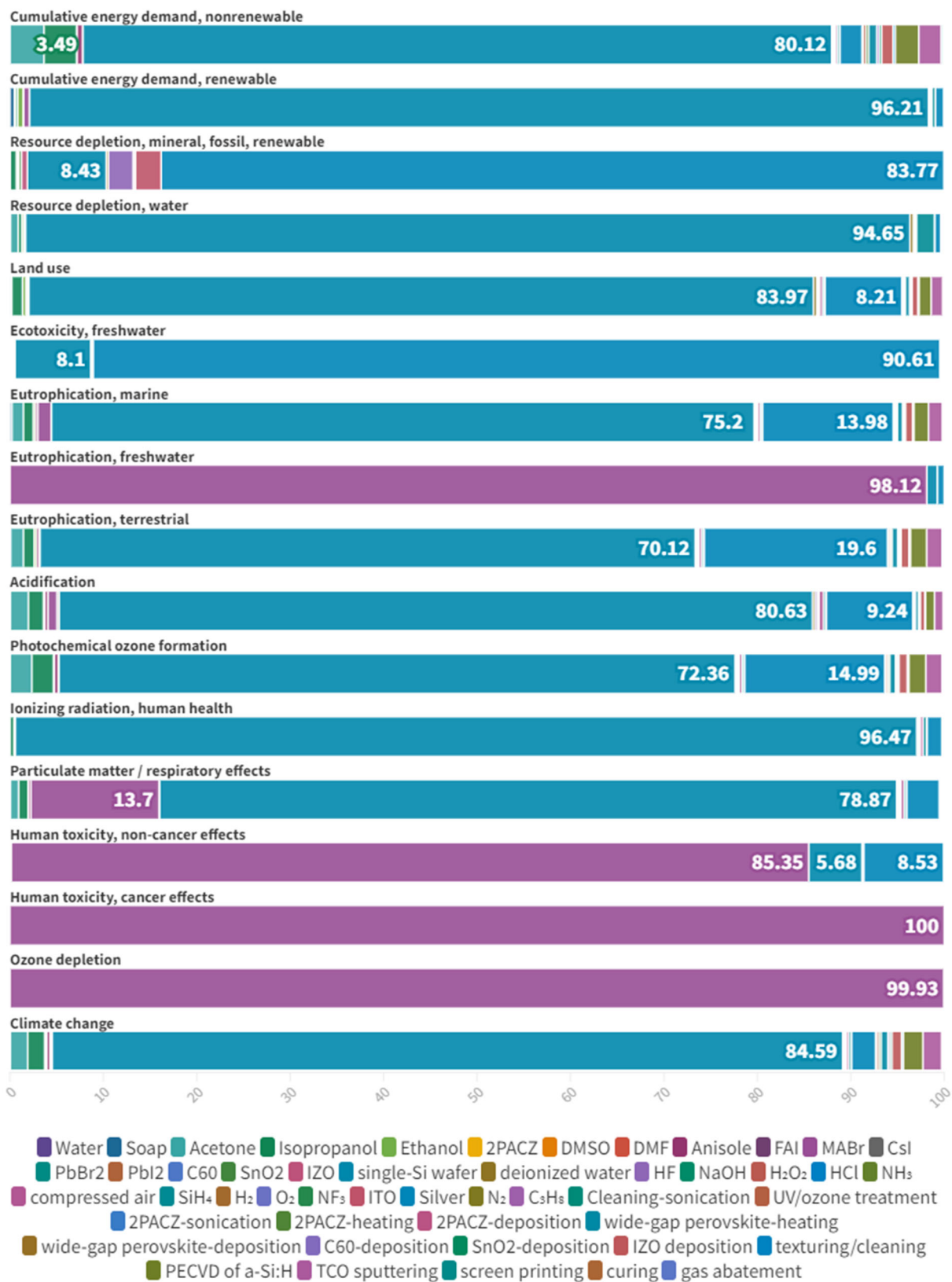
51 **Contribution analysis results for the commercial-scale perovskite tandems**



54 Figure S3. Contribution analysis results for the commercial-scale perovskite-perovskite tandem with a  
55 “cradle-to-grave” system boundary.

56

57 To explicitly consider scalable fabrication of the investigated perovskite tandems, we use two tandem  
58 architectures in existing literature<sup>2, 3</sup> as references while substituting the materials and processing steps  
59 used for depositing specific layers with scalable alternatives.<sup>4</sup> Specifically, spin coating is replaced with  
60 screen printing, which is compatible with large-scale and high-throughput manufacturing.<sup>5</sup> The energy-  
61 intensive ALD of tin dioxide is replaced with sputtering. Although the industry-relevant ALD process, such  
62 as spatial atmospheric ALD,<sup>6</sup> is two times faster than the laboratory-scale counterpart and thus consumes  
63 less energy, it is still energy-intensive in terms of absolute energy consumption.



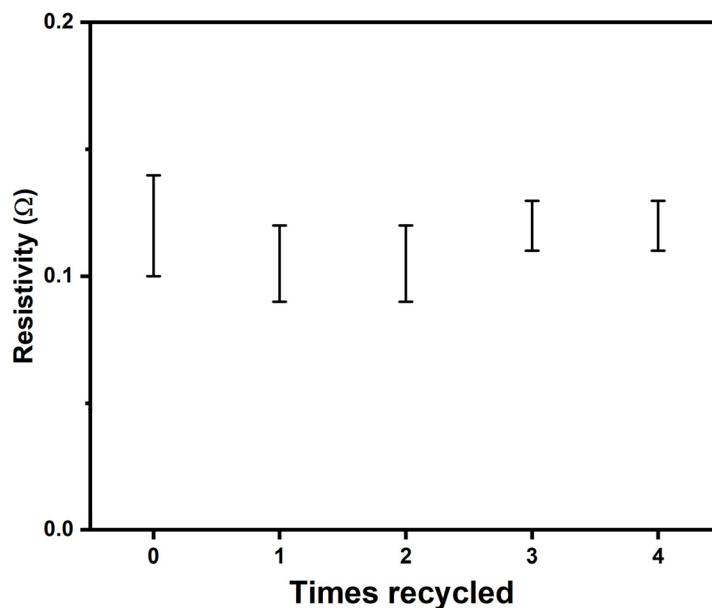


65 Figure S4. Contribution analysis results for the commercial-scale perovskite-silicon tandem with a “cradle-  
66 to-grave” system boundary.

67  
68 As shown in our previous study,<sup>7</sup> organic solvents would induce substantial environmental impacts if  
69 they are not recycled at the EOL or merely incinerated as hazardous waste. To this end, for commercial-  
70 scale processes, organic solvents, such as acetone and isopropanol, are considered to be effectively  
71 recovered and re-used with an efficiency of approximately 90%, according to the existing literature.<sup>8, 9</sup>  
72 Figure S3 and Figure S4 show the environmental profiles of the commercial-scale perovskite-perovskite  
73 and perovskite-silicon tandems for the explored midpoint impact categories according to the PEF method,  
74 respectively. We note that the overall environmental profile of the commercial-scale perovskite-perovskite  
75 tandem looks more dynamic, i.e., the percentage share of each material and processing step is more evenly  
76 distributed. The contributions from the identified hotspot material and processing steps are drastically  
77 reduced compared to the environmental profiles of the laboratory-scale tandems.

## 78 79 **Resistivity test**

80 The resistivity of the ITO substrates was measured using a four-point probe setup consisting of a 2450  
81 Keithley SourceMeter and a four-point collinear probe.

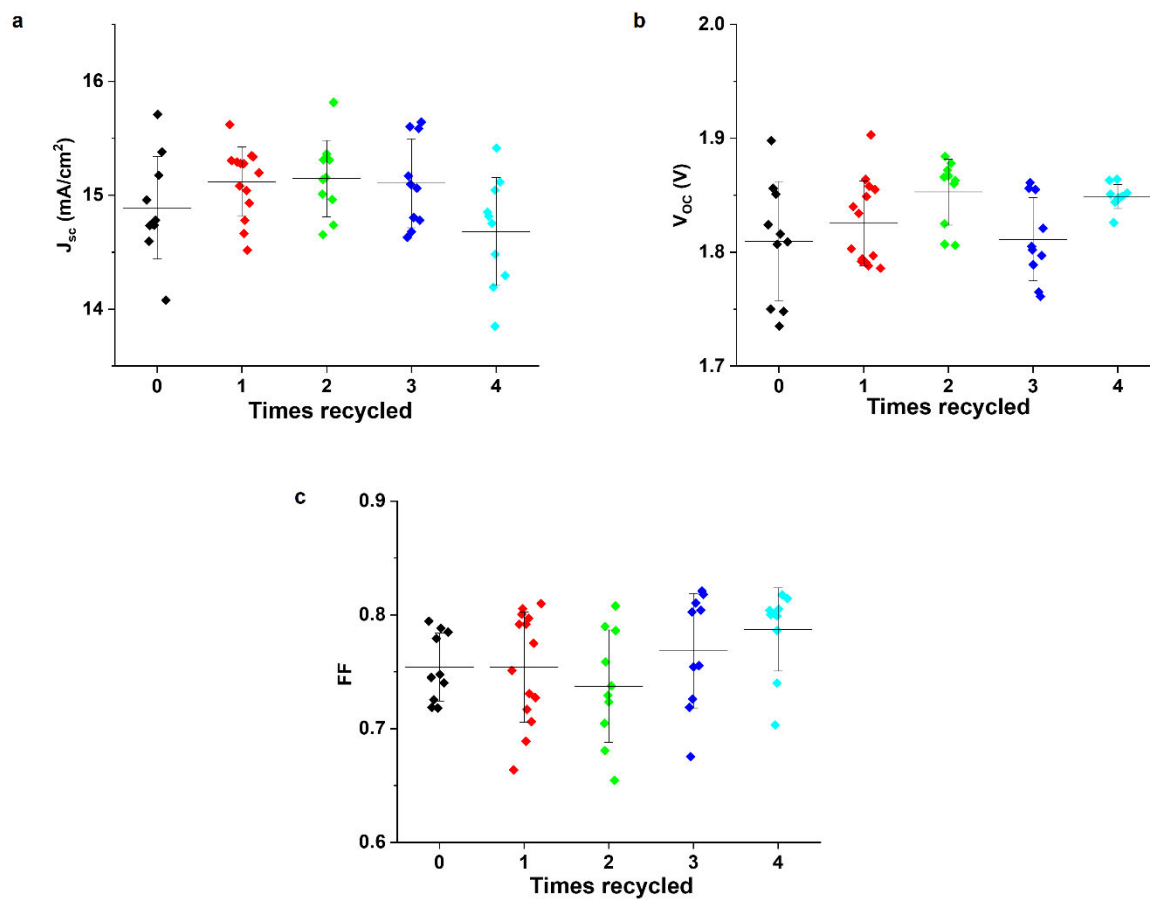


82  
83 Figure S5. Resistivity test of the pristine and recycled ITO substrates.

## 84 85 **Short current density (Jsc), open circuit voltage (Voc), and fill factor (FF) of** 86 **perovskite-perovskite tandem**

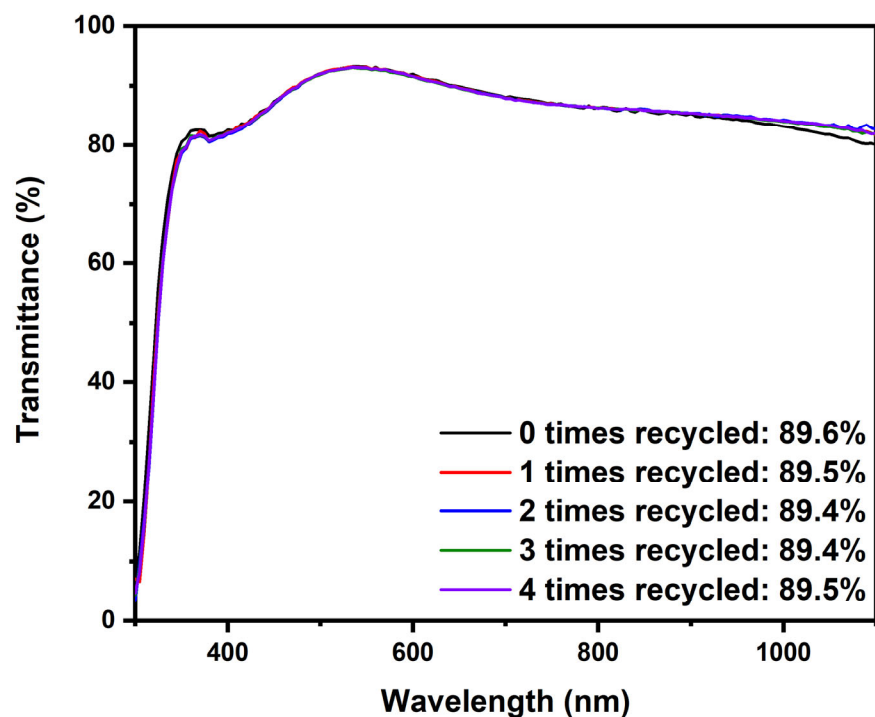
87 Figure S6 shows the short current density, open circuit voltage, and fill factor of perovskite-perovskite

88 tandem, as a function of times recycled.



89  
90 Figure S6. **a**, Short current density ( $J_{sc}$ ) as a function of times recycled. **b**, Open circuit voltage ( $V_{oc}$ ) as a  
91 function of times recycled. **c**, Fill factor (FF) as a function of times recycled.  
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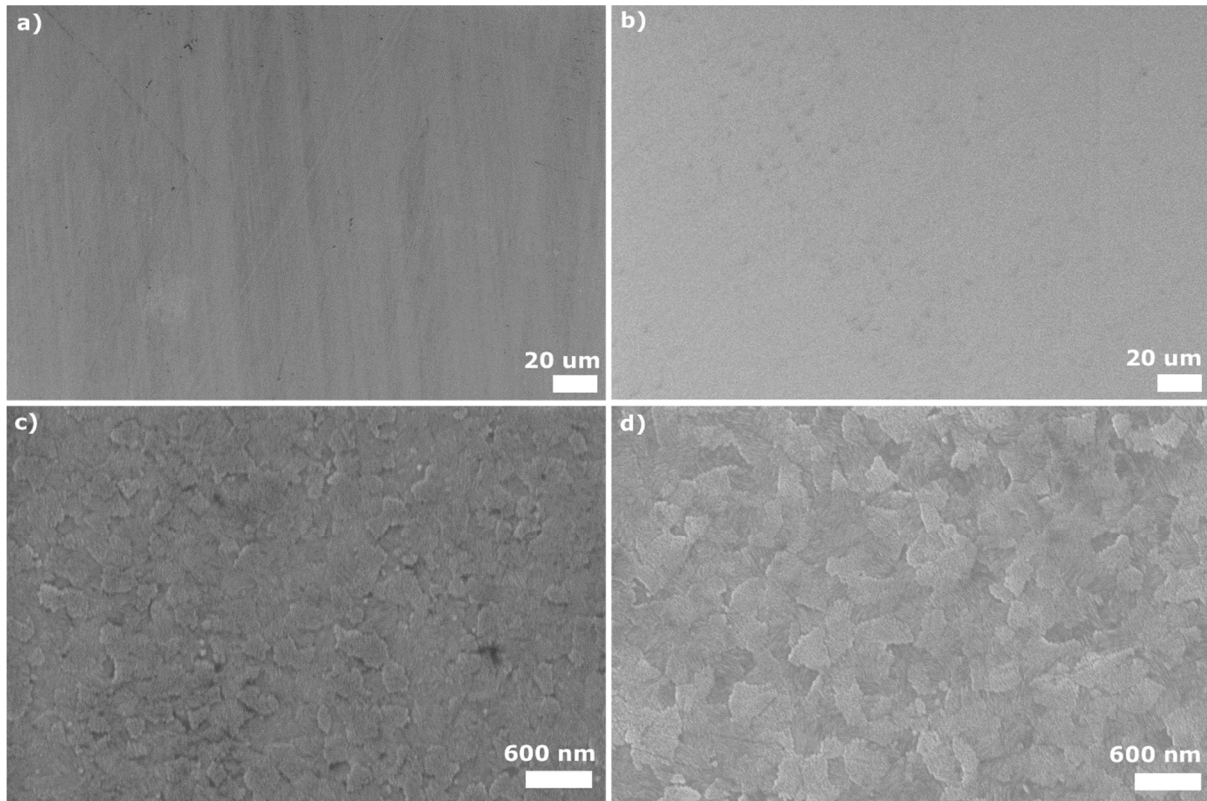
93 **Transmittance**



94  
95 Figure S7. Optical transmittance of substrates before and after recycling. The percentages shown refer to  
96 the transmittance of AM1.5G illumination. Loss of transmittance mainly occurs in the 300-400nm range,  
97 this is attributed to SnO<sub>x</sub> deposition on the front of the substrate during atomic layer deposition. This can  
98 likely be prevented in an industrial setting, but even here the overall reduction in transmittance is negligible.  
99

100 Transmittance was measured using a Bentham PVE300 system in transformer mode. A dual xenon  
101 short-arc lamp and a quartz halogen lamp were utilized as the light source, with a swing-away mirror set to  
102 750 nm. A 10 × 10 mm Si reference diode was used as the detector. Transmittance was calculated by  
103 dividing the diode response in the presence of a substrate by the diode response without substrate.  
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105 **Scanning electron microscopy**



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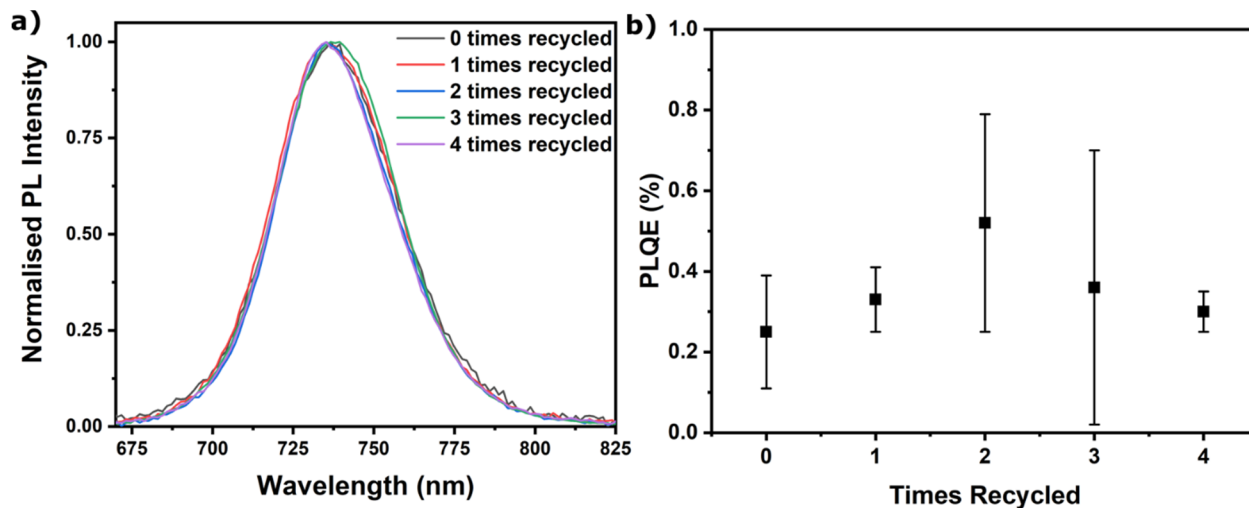
107 Figure S8. Scanning electron microscope images at 1000X (a,b) and 50000X (c,d) magnification of  
108 new (a,c) and recycled substrates (b,d). There are no traces of leftover perovskite on the recycled  
109 substrates, showing that the recycling strategy effectively removes all materials from the substrate.

110

111 Scanning electron microscopy was performed using a Zeiss LEO 1550 FE-SEM with a field emission  
112 source operating at 2 kV acceleration voltage in the InLens mode.

113

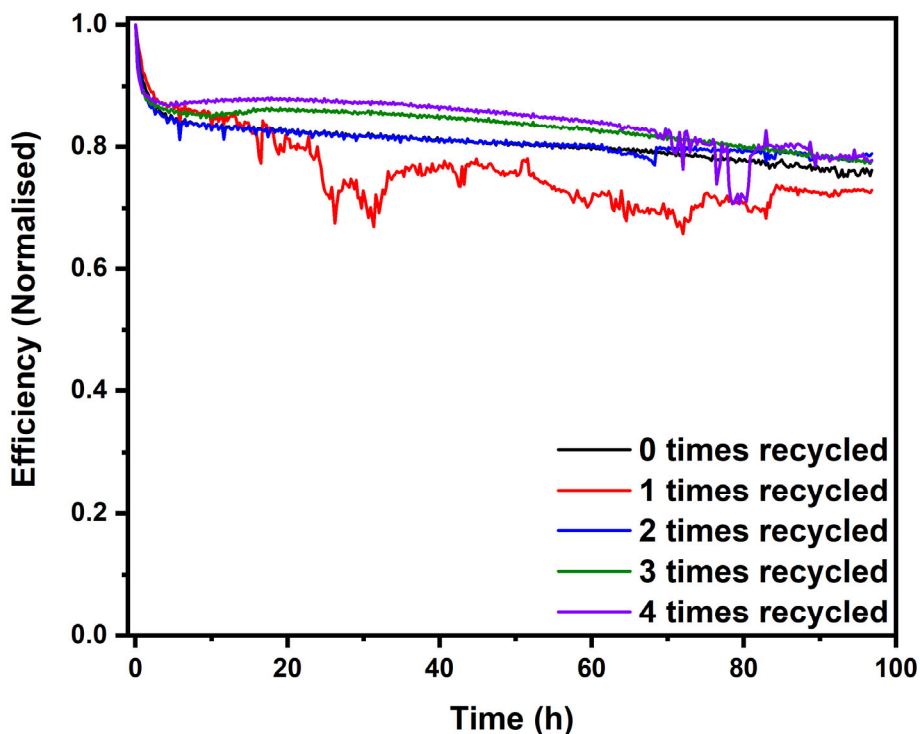
114 **Normalized photoluminescence (PL) intensity and PL quantum efficiency (PLQE)**



115  
116 Figure S9. Normalized photoluminescence (PL) intensity (Figure a) and corresponding PL quantum  
117 efficiency (Figure b, values are averages for five individual measurements for each recycling frequency) of  
118  $\text{Cs}_{0.25}\text{FA}_{0.75}\text{PbI}_{2.1}\text{Br}_{0.9}$  perovskite deposited on fresh and recycled substrates. There is no obvious change  
119 in peak position and width, or in the PLQE values, indicating that the perovskite quality is not significantly  
120 affected by using recycled substrates.

121  
122 PL and PLQE measurements were recorded using an integrating sphere, following the three-  
123 measurement approach of de Mello et al.<sup>10</sup> In both PL and PLQE measurements, a continuous wave  
124 temperature-controlled Thorlabs 520 nm laser was used to photoexcite samples. Excitation intensity was  
125 varied with an optical filter wheel. The emission was recorded using an Andor IDus DU420A silicon detector.  
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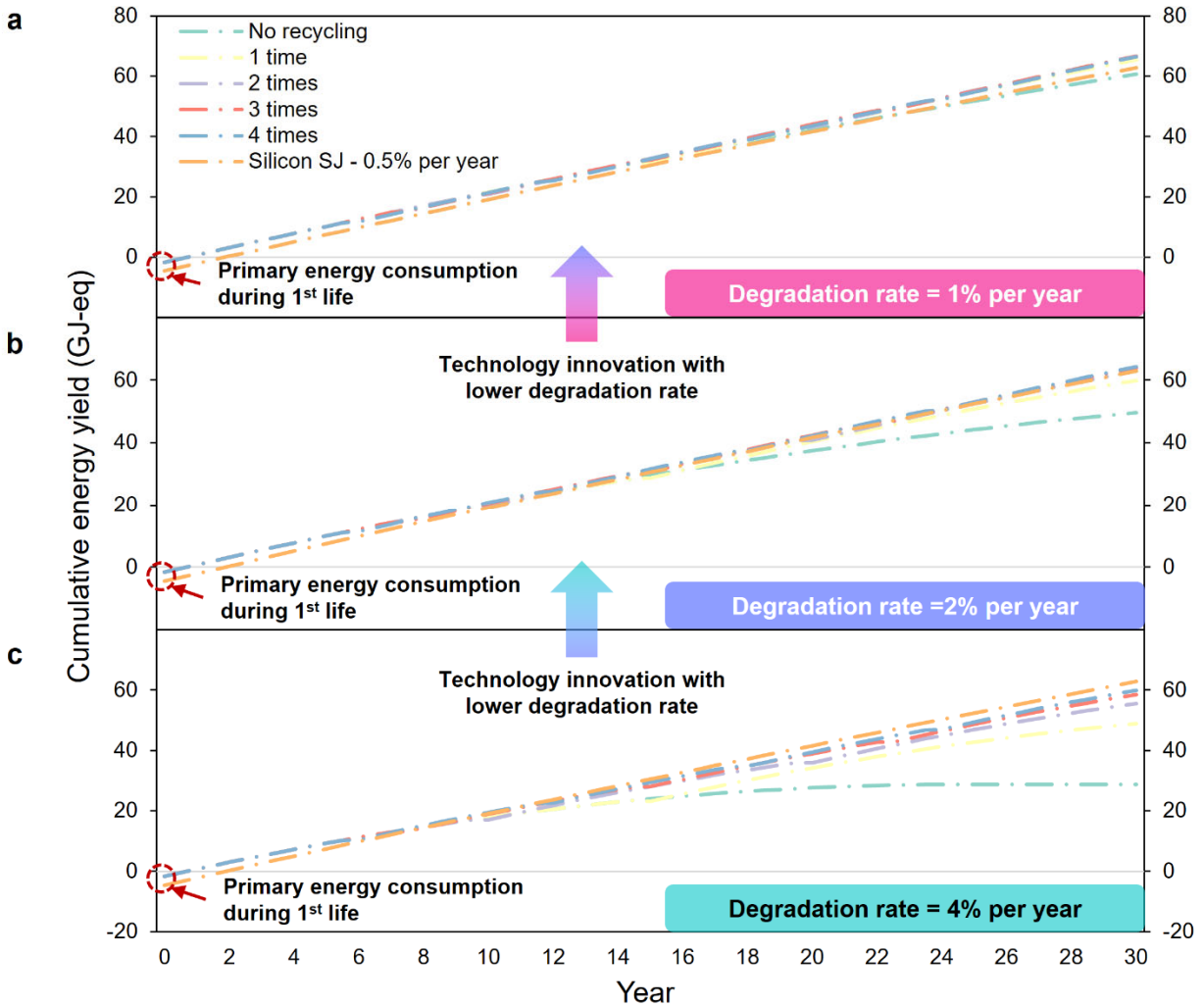
127 **Solar cell stability test**



128  
129 Figure S10. Normalized efficiency of perovskite-perovskite tandem solar cells deposited on fresh and  
130 recycled substrates.

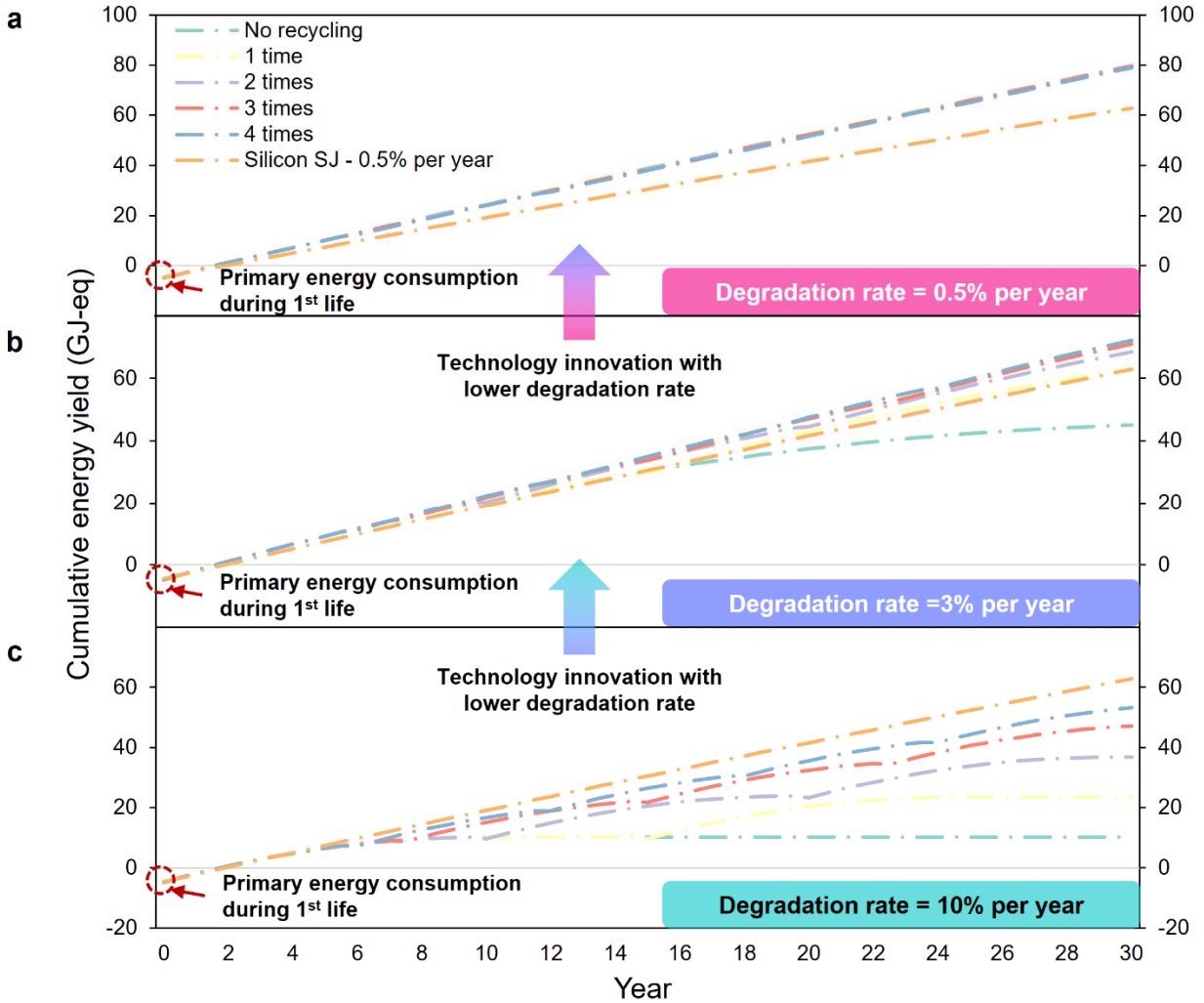
131  
132 A 100-hour maximum power point tracking stability test of fresh and recycled substrates shows that  
133 there is no significant change in degradation rate when recycled substrates are used. Although we do not  
134 observe any adverse effects of the recycling process on stability on the timescales we have studied, multi-  
135 year testing would be required to ensure that the recycling process does not affect stability on the timescales  
136 of operation in real-world applications. Each curve is the average of five devices. Devices were  
137 encapsulated using glass and UV-curable epoxy glue immediately after fabrication. Stability measurements  
138 were carried out under an inert atmosphere and AM1.5G illumination generated by a G2V Base-UV  
139 Sunbrick. Maximum power point traces were collected using a 32-channel Arkeo setup (Cicci Research).  
140 Further optimization of the layers will improve their absolute stability, but the focus of this study is to  
141 demonstrate that the stability remains comparable when considering various numbers of recycling steps.  
142

143 **Cumulative energy yield**



144  
 145 Figure S11. Cumulative energy yield for perovskite-perovskite tandems considering degradation rates of  
 146 1%, 2%, and 4% per year. **a**, Cumulative energy yield for perovskite-silicon tandems with different recycling  
 147 frequencies (from no recycling to four times over the system lifetime) under 1% per year degradation, and  
 148 compared to the silicon PVs (0.5% per year degradation). **b**, Cumulative energy yield for perovskite-silicon  
 149 tandems with different recycling frequencies (from no recycling to four times over the system lifetime) under  
 150 2% per year degradation and compared to the silicon PVs (0.5% per year degradation). **c**, Cumulative  
 151 energy yield for perovskite-silicon tandems with different recycling frequencies (from no recycling to four  
 152 times over the system lifetime) under 4% per year degradation, and compared to the silicon PVs (0.5% per  
 153 year degradation). The cumulative energy yields initiate as negative values (year zero), which are equal to  
 154 the initial primary energy consumption.

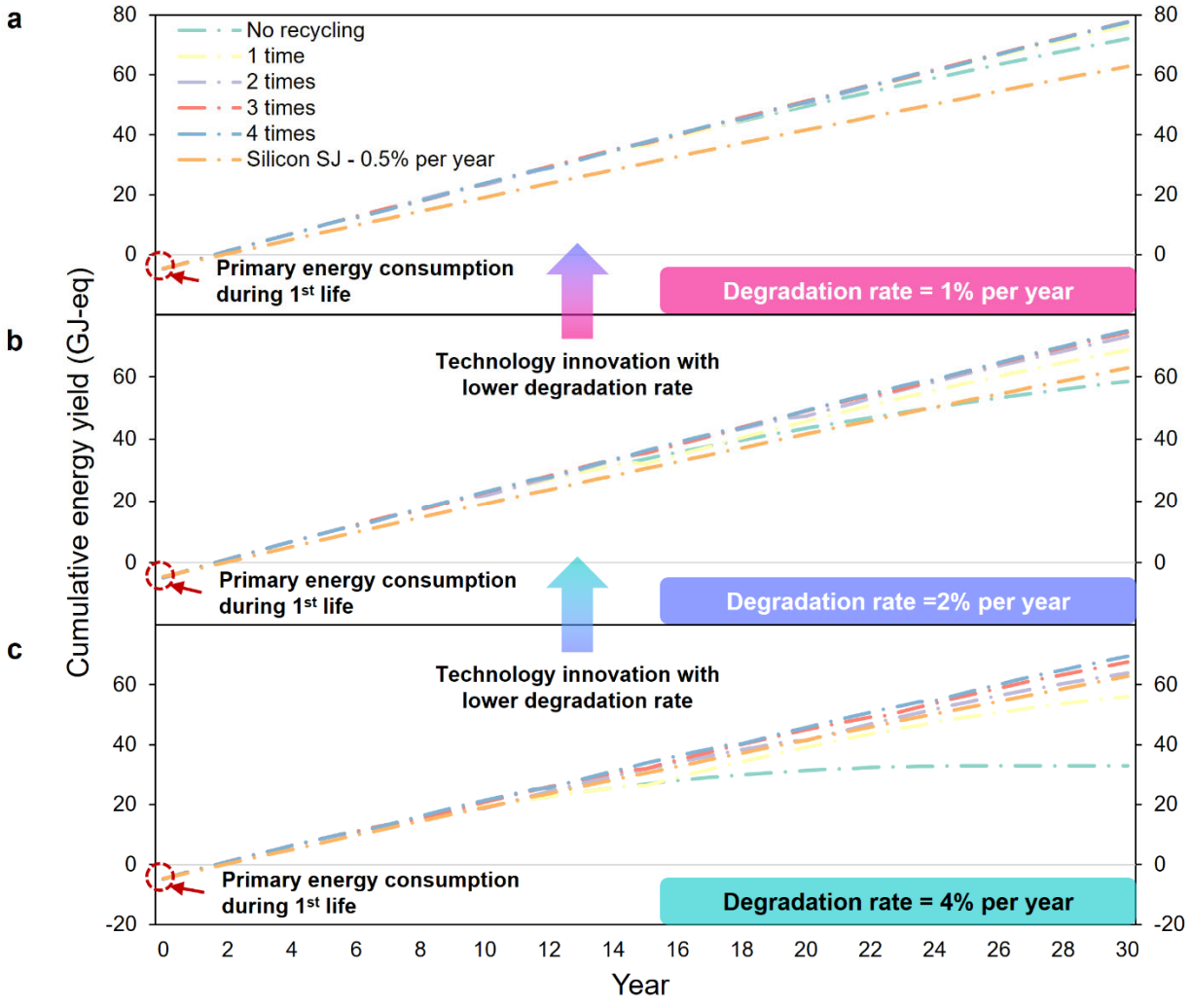
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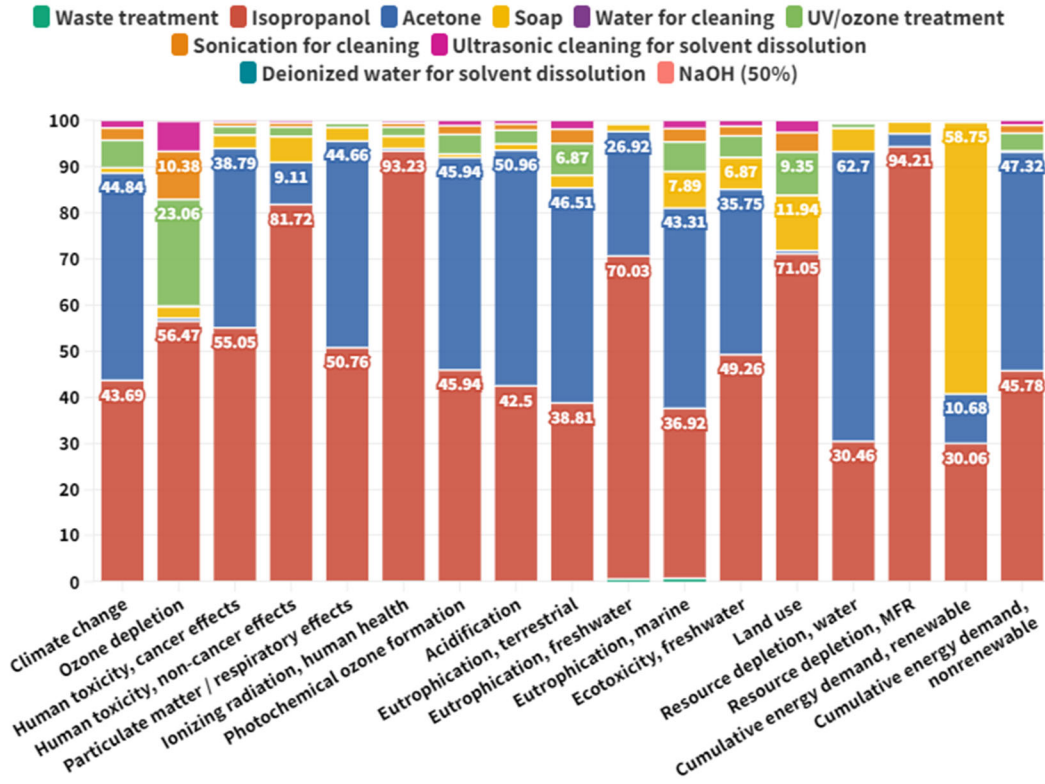
Figure S12. Cumulative energy yield for perovskite-silicon tandems considering degradation rates of 0.5%, 3%, and 10% per year. **a**, Cumulative energy yield for perovskite-silicon tandems with different recycling frequencies (from no recycling to four times over the system lifetime) under 0.5% per year degradation, and compared to the silicon PVs (0.5% per year degradation). **b**, Cumulative energy yield for perovskite-silicon tandems with different recycling frequencies (from no recycling to four times over the system lifetime) under 3% per year degradation and compared to the silicon PVs (0.5% per year degradation). **c**, Cumulative energy yield for perovskite-silicon tandems with different recycling frequencies (from no recycling to four times over the system lifetime) under 10% per year degradation, and compared to the silicon PVs (0.5% per year degradation). The cumulative energy yields initiate as negative values (year zero), which are equal to the initial primary energy consumption.



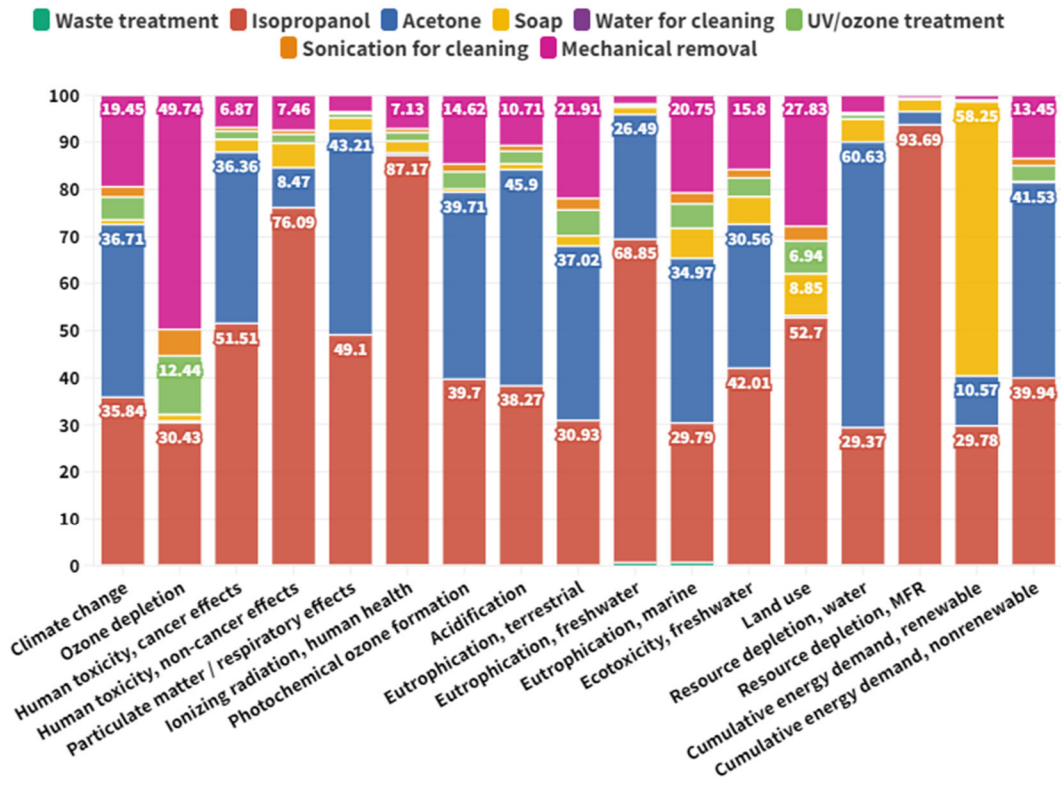


168  
 169 Figure S13. Cumulative energy yield for perovskite-silicon tandems considering degradation rates of 1%,  
 170 2%, and 4% per year. **a**, Cumulative energy yield for perovskite-silicon tandems with different recycling  
 171 frequencies (from no recycling to four times over the system lifetime) under 1% per year degradation, and  
 172 compared to the silicon PVs (0.5% per year degradation). **b**, Cumulative energy yield for perovskite-silicon  
 173 tandems with different recycling frequencies (from no recycling to four times over the system lifetime) under  
 174 2% per year degradation and compared to the silicon PVs (0.5% per year degradation). **c**, Cumulative  
 175 energy yield for perovskite-silicon tandems with different recycling frequencies (from no recycling to four  
 176 times over the system lifetime) under 4% per year degradation, and compared to the silicon PVs (0.5% per  
 177 year degradation). The cumulative energy yields initiate as negative values (year zero), which are equal to  
 178 the initial primary energy consumption.  
 179

180 Doctor blading v.s. solvent dissolution method



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182  
183 Figure S14. Environmental profile for recycling process based on the solvent dissolution method.

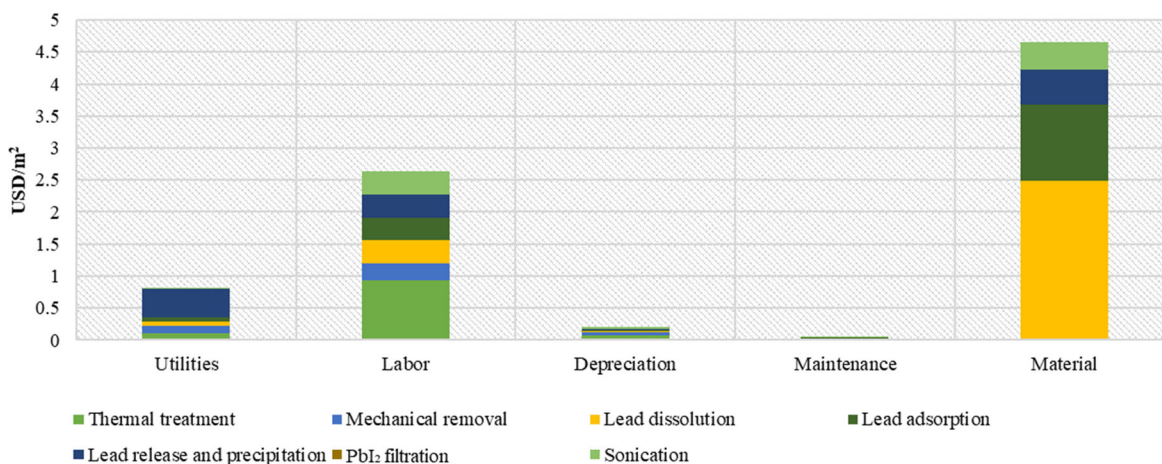


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185 Figure S15. Environmental profile for recycling process based on the blade-scratching method.

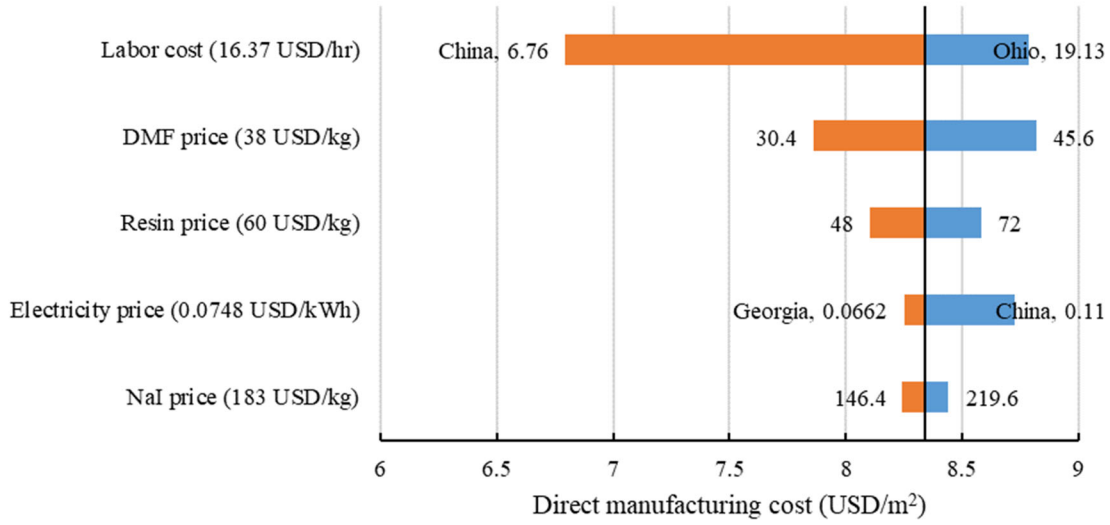
186  
187 Figure S14 and Figure S15 show the environmental profiles for the recycling process based on the solvent  
188 dissolution method and the blade-scratching method, respectively. Note that the subsequent cleaning  
189 processes are the same for either the solvent dissolution method or the blade-scratching method. Overall,  
190 the environmental impact of mechanical removal is more pronounced than solvent dissolution.  
191

## 192 Techno-economic analysis for the recovery process with sensitivity analysis



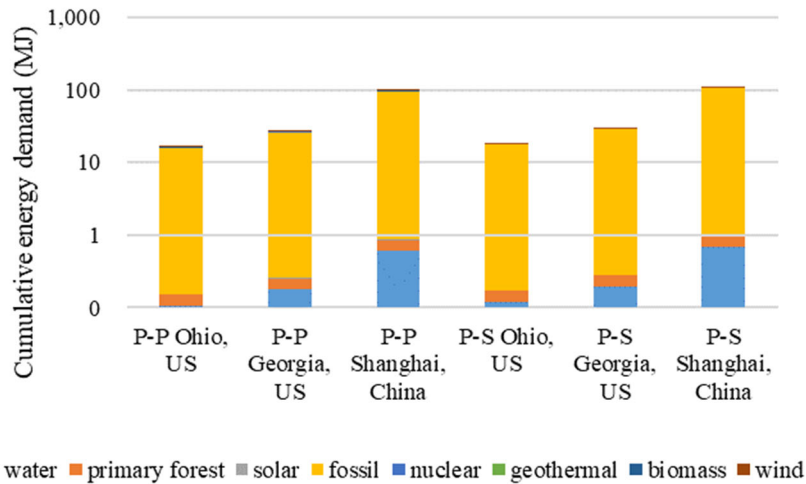
193 Figure S16. Techno-economic analysis for the recycling process of perovskite-perovskite tandem modules.

194  
195  
196 Figure S16 shows the techno-economic analysis results for the recycling process of the perovskite-  
197 perovskite tandem modules. The results show that the costs in the recovery process of the perovskite-  
198 perovskite tandem are dominated by labor (31.6%) and material costs (55.8%), and the total recycling cost  
199 is \$ 8.3 / m<sup>2</sup> of the tandem module. A sensitivity analysis is also performed to capture the impact of key  
200 parameter variations, including labor cost, electricity price, and other material prices, due to the uncertainty  
201 of the recycling process on an industrial scale, as shown in Figure S17. The equipment cost, electricity  
202 usage, process throughput, and associated labor cost used for the techno-economic analysis are extracted  
203 from existing literature.<sup>11, 12</sup> The maintenance costs for the facilities are assumed to be 20% of the annual  
204 equipment depreciation.<sup>13</sup> Material costs are estimated based on recycling process of lead and transparent  
205 conductors from perovskite solar modules by Chen et al.<sup>14</sup>  
206

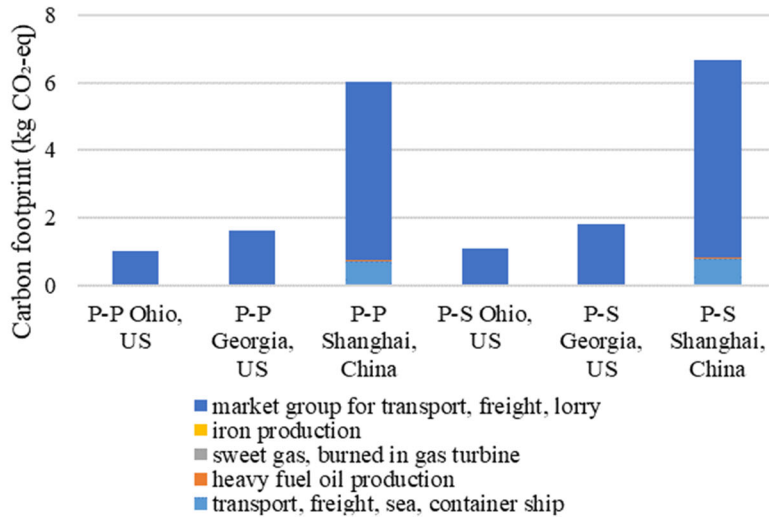


207  
208 Figure S17. Sensitivity analysis for the recycling cost of perovskite-perovskite tandem modules.

209 **Impact of module shipping**



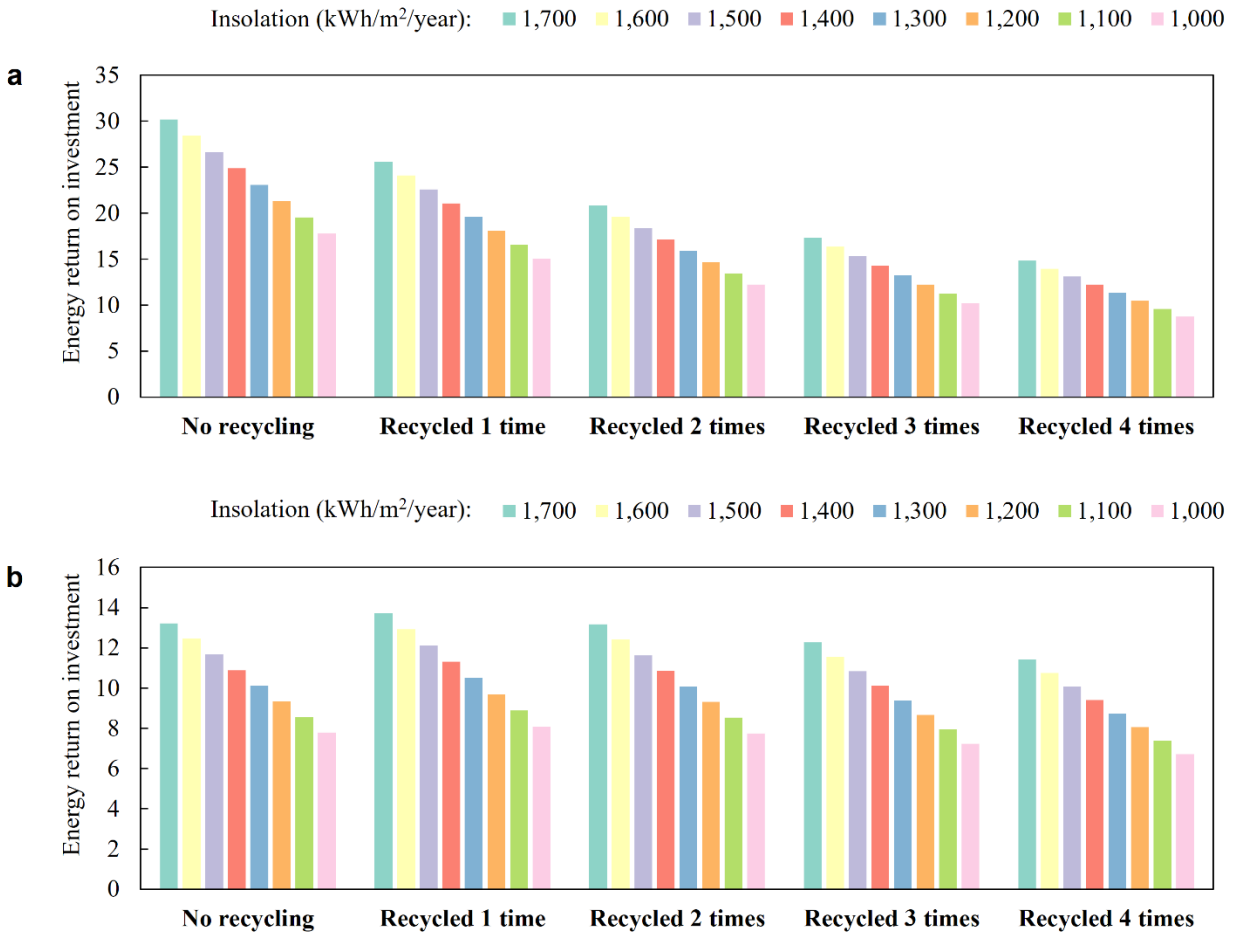
210  
211 Figure S18. Cumulative energy demand for international and domestic module shipping for the perovskite-  
212 perovskite (P-P) and perovskite-silicon (P-S) tandems.  
213



214  
 215 Figure S19. The carbon footprint for international and domestic module shipping for the perovskite-  
 216 perovskite (P-P) and perovskite-silicon (P-S) tandems.  
 217

218 Figure S18 and Figure S19 show the cumulative energy demand and carbon footprint associated with  
 219 international and domestic module shipping for the perovskite-perovskite and perovskite-silicon tandems.  
 220 Specifically, we compare the cumulative energy demand and carbon footprint for three scenarios by  
 221 assuming that the modules are produced in Ohio State, Georgia State, and Shanghai, China, respectively,  
 222 and then transported to and installed in New York State, US. The energy cost and GHG emissions are  
 223 quantified in terms of primary energy forms and involved activities, respectively. The shipping impacts for  
 224 modules produced and installed in other regions or countries could be estimated in the same way.  
 225

226 **Sensitivity analysis of EROI on insolation condition**



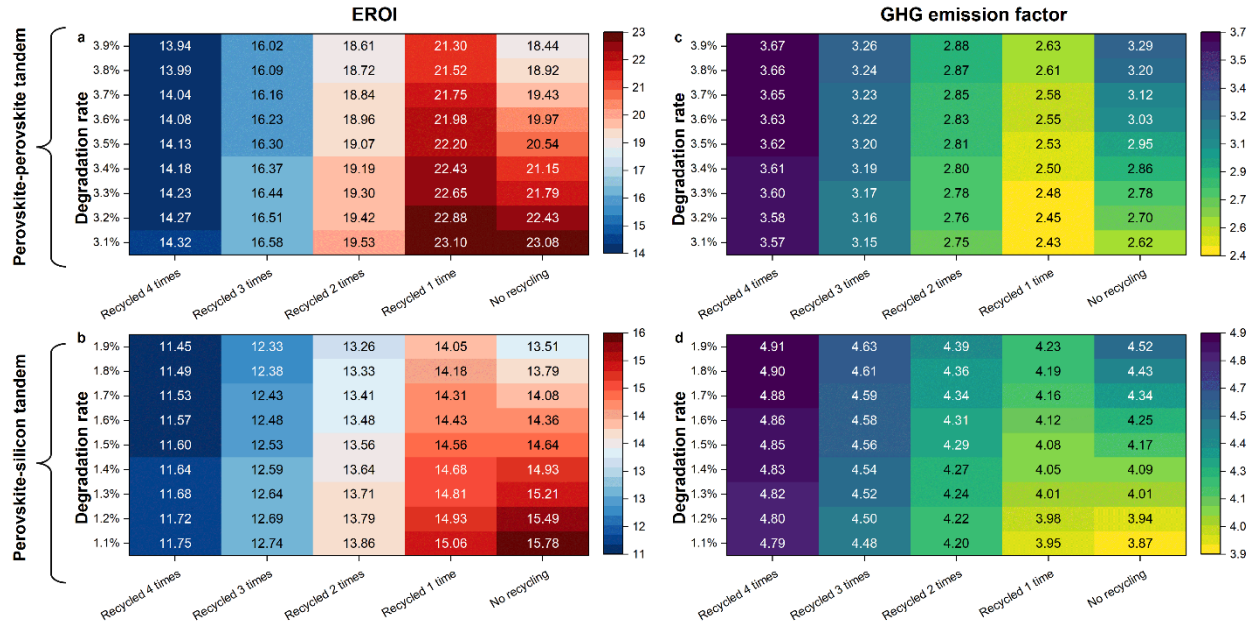
227

228 Figure S20. Impact of insolation condition on energy return on investment for perovskite tandems under 2%  
 229 per year degradation. **a**, Sensitivity of energy return on investment for perovskite-perovskite tandem with a  
 230 spectrum of insolation conditions, ranging from 1,000 to 1,700 kWh/m<sup>2</sup> per year. **b**, Sensitivity of energy  
 231 return on investment for perovskite-silicon tandem with a spectrum of insolation conditions, ranging from  
 232 1,000 to 1,700 kWh/m<sup>2</sup> per year. The default insolation condition is 1,700 kWh/m<sup>2</sup> per year, and we explore  
 233 how energy return on investment results would change if worse insolation conditions were assumed.

234

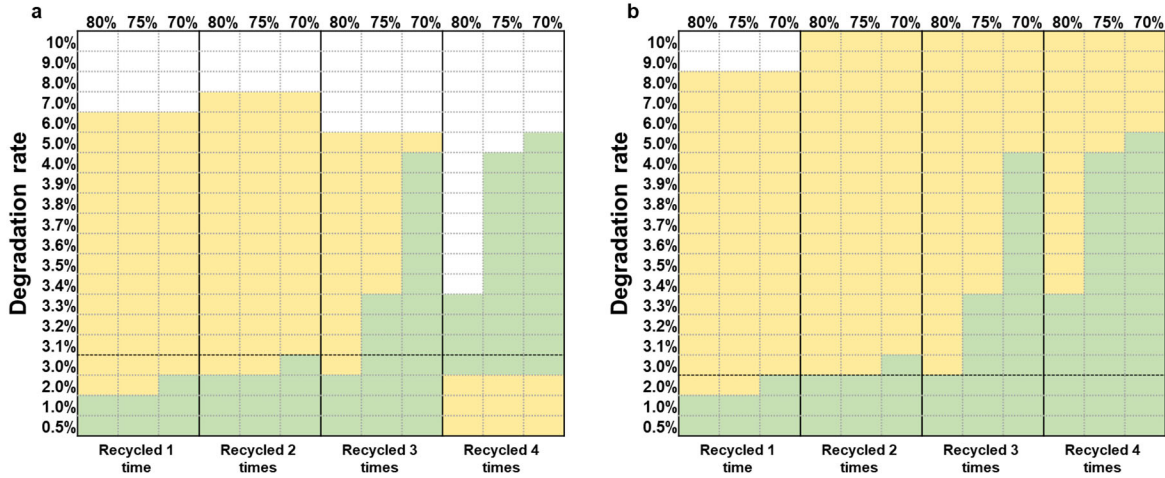
235 In this study, nominal insolation of 1,700 kWh/m<sup>2</sup> per year is assumed in the calculation of energy yield  
 236 potential, energy return on investment (EROI), and greenhouse gas (GHG) emission factor, compliant with  
 237 the literature.<sup>15</sup> However, this insolation condition is quite favorable for PV and the results would change  
 238 with different insolation. Figure S20 shows how the EROIs of the explored perovskite tandem stacks with  
 239 different module replacement strategies vary with different insolation. We note that the EROI of the  
 240 perovskite-perovskite tandem becomes less sensitive to the change of insolation as the recycling frequency  
 241 increases, while that of the perovskite-silicon tandem is almost unchanged.

242



243  
 244 Figure S21. **GHG emission factor (g CO<sub>2</sub>-eq/MJ) and EROI for the perovskite-perovskite and**  
 245 **perovskite-silicon tandems with periodic module replacement under different module degradation**  
 246 **scenarios and recycling frequencies.** The GHG emission factor and EROIs for the two investigated  
 247 perovskite tandems are estimated under an insolation level of 1,700 kWh m<sup>-2</sup> per year over a total system  
 248 lifetime of 30 years. Five scenarios with varying recycling frequencies are simulated, considering the  
 249 perovskite tandem modules are recycled zero to four times over a total system lifetime of 30 years. For the  
 250 perovskite-perovskite tandem, the region of interest is from 3.1% to 3.9% per year degradation; for the  
 251 perovskite-silicon tandem, the region of interest is from 1.1% to 1.9% per year degradation. **a**, Heatmap for  
 252 EROI of the perovskite-perovskite tandems. **b**, Heatmap for EROI of the perovskite-silicon tandems. **c**,  
 253 Heatmap for GHG emission factor of the perovskite-perovskite tandems. **d**, Heatmap for GHG emission  
 254 factor of the perovskite-silicon tandems. The GHG emission factor and EROI of the silicon single junction  
 255 at 0.5% per year degradation are estimated to be 4.73 g CO<sub>2</sub>-eq/MJ and 14.8, respectively.  
 256

257 **Impact of PCE threshold on perovskite-perovskite tandem module replacement**



258  
 259 **Figure S22. Impact of PCE threshold on perovskite-perovskite tandem module replacement.** Three  
 260 scenarios are considered when the threshold is assumed to be 80%, 75%, and 70%. The box in yellow  
 261 indicates that the corresponding scenario outperforms the reference case of silicon PV in terms of the  
 262 investigated sustainability metric, namely EROI or GHG emission factor. The box in green represents the  
 263 replacement scenario is viable given the degradation rate, recycling frequency, and PCE threshold for  
 264 replacement (the module PCE would not drop below the threshold before being replaced). The dotted line  
 265 stands for the degradation rate where intermediate recycling is no longer needed. **a**, Feasibility analysis for  
 266 perovskite-perovskite tandem module replacement in terms of EROI. **b**, Feasibility analysis for perovskite-  
 267 perovskite tandem module replacement in terms of GHG emission factor.

268  
 269 Figure S22 demonstrates that the module replacement strategy becomes viable in the EROI terms  
 270 when recycled three times. Specifically, tandem modules with an annual degradation rate of 3.1% to 4.0%  
 271 can still outperform silicon PV if a 70% replacement threshold is applied, whereas the feasible region  
 272 narrows to between 3.1% and 3.3% when using a 75% threshold. In terms of the GHG emission factors, a  
 273 wider region is observed for the perovskite-perovskite tandem to outcompete silicon PV, particularly when  
 274 recycled more than three times over the 30-year period.

275 **Material and energy inventory**

276 Table S1. Material inventory of 1 m<sup>2</sup> of the perovskite-silicon tandem solar cell.

Process	Unit	Value
<b>Silicon bottom cell fabrication</b>		
<b>Wafer production</b>	Single-Si wafer	m <sup>2</sup> 1.00E+00
<b>Texturing/cleaning</b>	Deionized water	kg 3.34E+01
	Hydrogen fluoride	kg 9.50E-02
	Sodium hydroxide	kg 1.56E-01



	Hydrogen peroxide	kg	5.60E-02
	Hydrochloride acid	kg	6.10E-02
	Ammonia	kg	1.10E-02
	Compressed air	m <sup>3</sup>	2.50E-01
<b>PECVD of a-Si:H</b>	Deionized water	kg	3.94E+02
	Silane	kg	1.62E-03
	Hydrogen	kg	2.42E-03
	Oxygen	kg	2.60E-04
	NF <sub>3</sub> (for cleaning)	kg	2.20E-03
<b>TCO sputtering</b>	Deionized water	kg	5.12E+02
	ITO	kg	2.74E-03
<b>Screen printing</b>	Compressed air	m <sup>3</sup>	1.10E+00
	Silver paste	kg	2.96E-02
<b>Gas abatement</b>	Deionized water	kg	1.20E+01
	Oxygen	kg	5.10E-03
	Nitrogen	kg	4.30E-03
	Propane	kg	3.30E-03
	Compressed air	m <sup>3</sup>	1.40E-02
<b>PSC fabrication</b>			
	Water	kg	2.33E+00
	Soap	kg	4.70E-02
	Acetone	kg	1.84E+00
	Isopropanol	kg	1.83E+00
	Ethanol	kg	1.22E-01
	2PACZ	kg	1.33E-06
	DMSO	kg	3.41E-02
	DMF	kg	1.17E-01
	Anisole	kg	3.09E-01
	FAI	kg	6.05E-04
	MABr	kg	1.21E-04
	CsI	kg	6.05E-05
	PbBr <sub>2</sub>	kg	7.34E-04
	PbI <sub>2</sub>	kg	1.15E-03
	C <sub>60</sub>	kg	4.40E-05
	TDMASn	kg	8.69E-04
	IZO	kg	6.99E-04
<b>Encapsulation</b>			

	Solar glass	kg	8.53E+00
	PET	kg	7.28E-02
	Adhesive	kg	5.06E-02
	<b>Landfill</b>	kg	9.60E+00

277

278 Table S2. Energy inventory of 1 m<sup>2</sup> of the perovskite-silicon tandem solar cell.

Process	Electricity (kWh)
<b>SHJ cell fabrication</b>	
Texturing/cleaning	6.47E-01
PECVD of a-Si:H	6.59E+00
TCO sputter	6.30E+00
Screen printing	5.24E-01
Curing	3.10E-01
Gas abatement	4.50E-02
<b>PSC fabrication</b>	
Cleaning-sonication	3.49E-01
UV/ozone treatment	7.75E-01
2PACZ deposition-sonication	7.75E-03
2PACZ deposition-heating	7.50E-01
2PACZ deposition-screen printing	1.07E-02
wide-gap perovskite-heating	2.25E+00
wide-gap perovskite-screen printing	1.07E-02
C <sub>60</sub> -deposition	6.82E-01
SnO <sub>2</sub> -deposition	7.02E-01
IZO-deposition	3.21E+00
<b>Encapsulation</b>	6.68E-03
<b>Mechanical removal</b>	3.10E+00
<b>Total</b>	<b>26.3</b>

279

280 Table S1 and Table S2 summarize the material and energy inventory for fabricating 1 m<sup>2</sup> of the  
281 perovskite-silicon tandem solar cell, respectively. Specifically, the material and energy inventory for  
282 depositing the silicon bottom cell (silicon heterojunction solar cell) in the tandem stack is retrieved from the  
283 literature.<sup>16</sup> The detailed mass and energy balances for perovskite sub-cell deposition are derived based  
284 on the data generated at the laboratory scale. Our estimates of energy inputs during the recycling process  
285 (based on a roll-to-roll blade coater with 10-second operations for active layer removal)<sup>17</sup> serve as the upper  
286 bound for the real-world application as we are not recuperating much of the end-of-life tandem modules  
287 (merely re-using ITO-coated glass), and the energy consumption is scaled based on the “best available”

288 data obtained at laboratory scale. All devices used for assembling the perovskite-silicon solar cells were  
289 driven by electricity, and the amount of electricity consumption in each procedure was evaluated based on  
290 power and corresponding operational time. Electricity consumption for manufacturing and recycling 1 m<sup>2</sup> of  
291 the perovskite-silicon tandem amounted to 26.3 kWh.  
292

293 Table S3. Material inventory of 1 m<sup>2</sup> of the perovskite-perovskite tandem solar cell.

Process	Unit	Value
ITO glass	m <sup>2</sup>	1.00E+00
Water	kg	2.33E+00
Soap	kg	4.70E-02
Acetone	kg	1.84E+00
Isopropanol	kg	1.83E+00
Ethanol	kg	1.22E-01
2PACZ	kg	1.33E-06
DMSO	kg	4.26E-02
DMF	kg	1.10E-01
Methyl acetate	kg	2.90E-01
FAI	kg	5.57E-04
CsI	kg	2.82E-04
PbBr <sub>2</sub>	kg	7.14E-04
PbI <sub>2</sub>	kg	1.11E-03
C <sub>60</sub>	kg	4.40E-05
SnO <sub>2</sub>	kg	8.69E-04
Gold	kg	2.57E-05
Methanol	kg	1.84E-01
Water	kg	7.75E-02
PEDOT:PSS	kg	4.24E-05
DMSO	kg	4.26E-02
DMF	kg	1.10E-01
Anisole	kg	3.09E-01
FAI	kg	1.29E-03
CsI	kg	3.46E-04
PbI <sub>2</sub>	kg	2.04E-03
SnI <sub>2</sub>	kg	1.65E-03
C <sub>60</sub>	kg	4.40E-05
BCP	kg	1.12E-05
Cu	kg	1.40E-03
<b>Encapsulation</b>		
Solar glass	kg	8.53E+00
PET	kg	7.28E-02
Adhesive	kg	5.06E-02
<b>Landfill</b>	kg	8.66E+00

294 Table S4. Energy inventory of 1 m<sup>2</sup> of the perovskite-perovskite tandem solar cell.

Process	Electricity (kWh)
<b>Fabrication</b>	
Cleaning-sonication	3.49E-01
UV/ozone treatment	7.75E-01
2PACZ deposition-sonication	7.75E-03
2PACZ deposition-heating	7.50E-01
2PACZ deposition-screen printing	1.07E-02
Wide-gap perovskite-heating	2.25E+00
Wide-gap perovskite-screen printing	1.07E-02
C <sub>60</sub> -deposition	1.36E+00
SnO <sub>2</sub> -deposition	7.02E-01
Gold-deposition	3.55E-01
PEDOT:PSS-heating	1.35E+00
PEDOT:PSS-screen printing	1.07E-02
Low-gap perovskite-heating	7.50E-01
Low-gap perovskite-screen printing	1.07E-02
BCP-deposition	2.47E-01
Copper-deposition	5.71E+00
<b>Encapsulation</b>	6.68E-03
<b>Mechanical removal</b>	3.10E+00
<b>Total</b>	<b>17.8</b>

295  
 296 Table S3 and Table S4 summarize the material and energy inventory for fabricating 1 m<sup>2</sup> of the  
 297 perovskite-perovskite tandem solar cell, respectively. The detailed mass and energy balances for wide-gap  
 298 perovskite sub-cell and low-gap perovskite sub-cell deposition are derived based on the data generated at  
 299 the laboratory scale. Electricity consumption for manufacturing and recycling 1 m<sup>2</sup> of the perovskite-  
 300 perovskite tandem amounted to 17.8 kWh.

301

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