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Supporting Information for

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Adsorption removal Mn^{2+} and NH_4^+-N from electrolytic manganese metal

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wastewater by modified phosphate ore flotation tailings

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1 Calculation formula

2 The calculation formula for the adsorption capacity at equilibrium (q_e , mg/g) and the adsorption
3 capacity at different time “ t ” (q_t , mg/g) are as follows:

$$q_e = \frac{(C_0 - C_e) \times V}{m}$$

(1)

$$q_t = \frac{(C_0 - C_t) \times V}{m}$$

(2)

7 Where C_0 , C_e and C_t are the initial, equilibrium concentration (mg/L) of $\text{NH}_4^+\text{-N}$ and the
8 concentration of $\text{NH}_4^+\text{-N}$ at different time “ t ”, respectively. V is the volume of the EMMW (L), and
9 m is the mass of the MPOFTs (g).

10 Analysis methods

11 The concentrations of Mn^{2+} and other heavy metals were determined by Atomic Absorption
12 Spectrophotometry (AAS) (HITACHI 180/80, Japan) in flame. The concentration of $\text{NH}_4^+\text{-N}$ was
13 determined via Nessler’s Reagent spectrophotometry. The pH of the solution was measured by using
14 ultra-microvolume pH electrodes (PHS-3C, Shanghai, China). The precipitates composition and
15 properties were analyzed via X-ray diffraction instrument (XRD; JapanD/maxIII A), Scanning
16 Electron Microscope (SEM; Sigma 300) and X-ray fluorescence (XRF; PANalytical B.V., Axios;
17 Netherlands). The Magna 550II FTIR Spectrometer (Perkin Elmer Frontier) was used to obtain the
18 FT-IR spectra of the sample via the KBr particle method. According to the extraction procedure of
19 solid waste, the toxic leaching method of horizontal vibration was selected (HJ 557-2010)

20 S1 Equilibrium adsorption isotherms

21 The equilibrium adsorption isotherm is an important data model that can reflect the surface
22 properties and adsorption behavior of adsorbents. It can be fitted by Langmuir model and Freundlich
23 model and expressed as an equation in linear form.

$$\text{Langmuir model: } \frac{C_e}{q_e} = \frac{1}{K_L q_m} + \frac{C_e}{q_m}$$

(1)

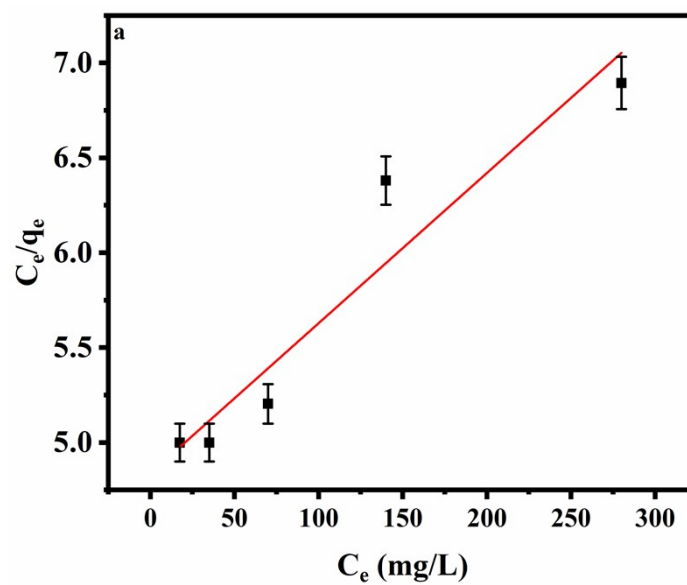
26 Where K_L is the adsorption equilibrium constant (L/ mg), q_m is the maximum monolayer

- 1 adsorption capacity, and q_e is the amount adsorbed on a unit mass of the adsorbent (mg/g) when
 2 the equilibrium concentration is C_e (mg/L).

3 Freundlich model:
$$\ln q_e = \frac{\ln C_e}{n} + \ln K_F \quad (2)$$

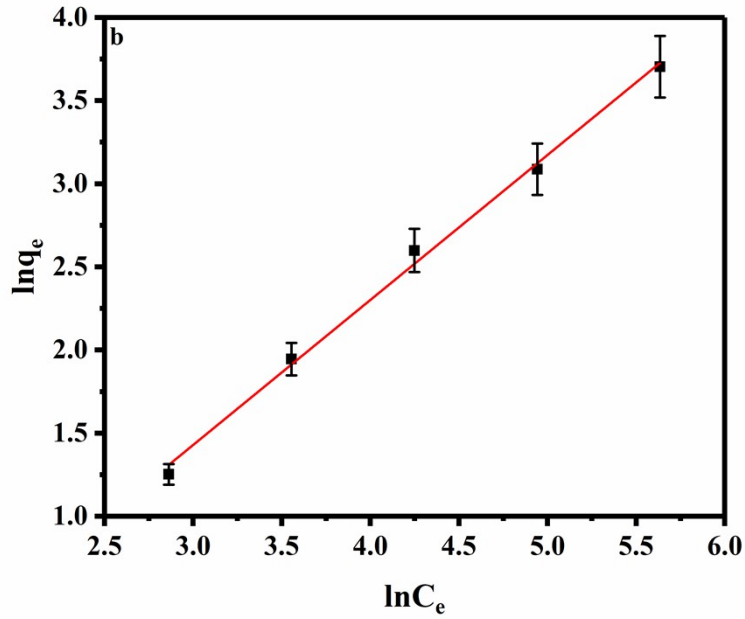
- 4 where K_F ((mg/g) (L/g)ⁿ) and n are Freundlich constants related to sorption capacity and
 5 sorption intensity of adsorbents.

6 **Fig.S1a**



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8 **Fig.S1b**



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2 S2 Adsorption kinetics

3 Adsorption kinetics is composed of pseudo-first-order and pseudo-second-order kinetic
 4 models. They were analyzed to test the experimental data. These two models can be expressed in a
 5 linear form as Eqs. (3) and (4), respectively.

6 The pseudo-first-order kinetic model: $\ln (q_e - q_t) = \ln q_e - K_1 t$ (3)

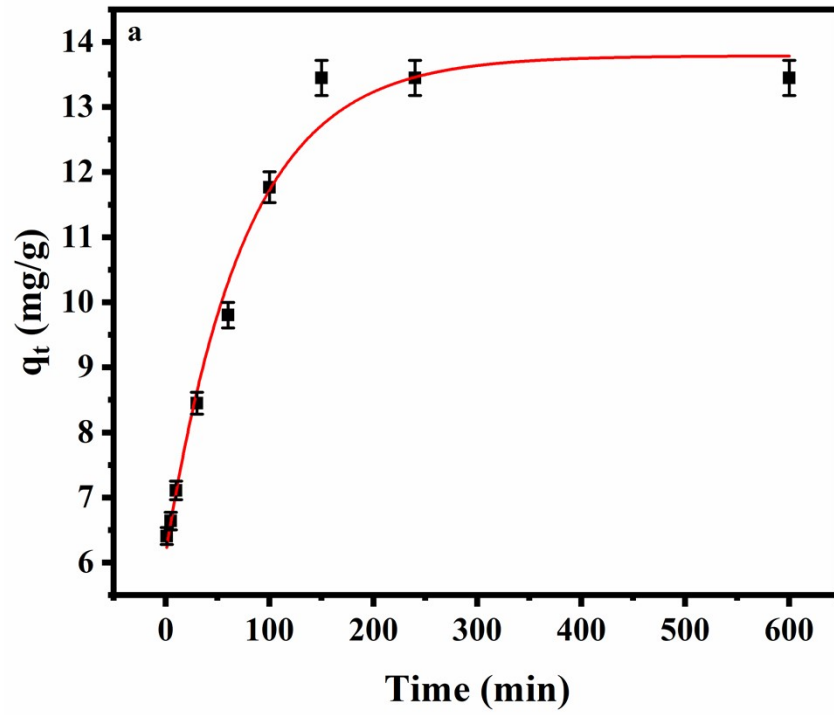
7 The pseudo-second-order kinetic model: $\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e}$ (4)

8 The steps of adsorption process were studied with Weber's intraparticle diffusion model. It can
 9 be expressed as Eq.(5).

10 Weber's intraparticle diffusion model: $q_t = K_i t^{\frac{1}{2}} + C$ (5)

11 where k_i (mg/g/min^{1/2}) is the intraparticle diffusion rate constant and C (mg/g) represents the
 12 intercept.

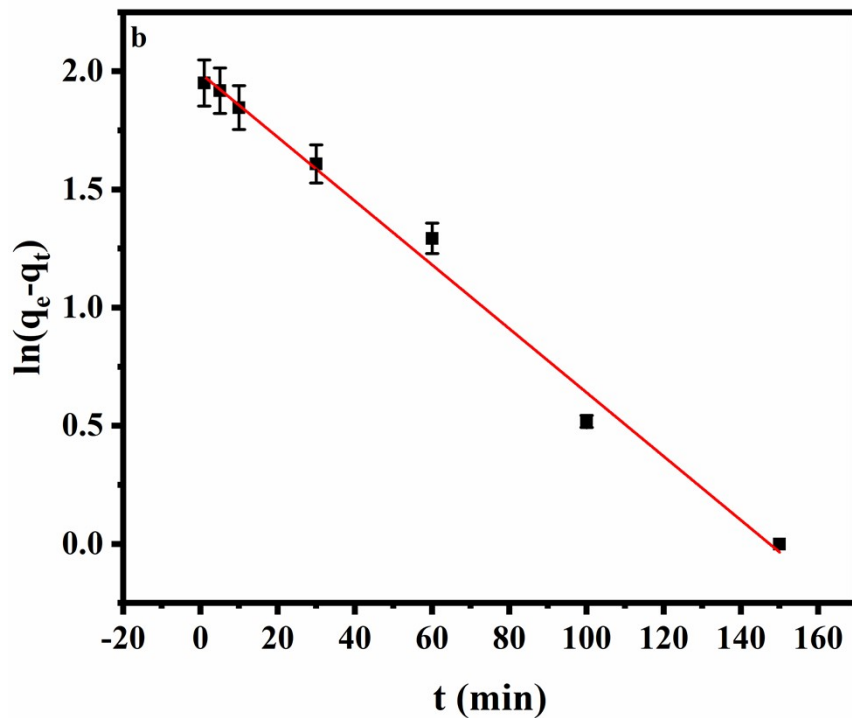
13 **Fig.S2a**



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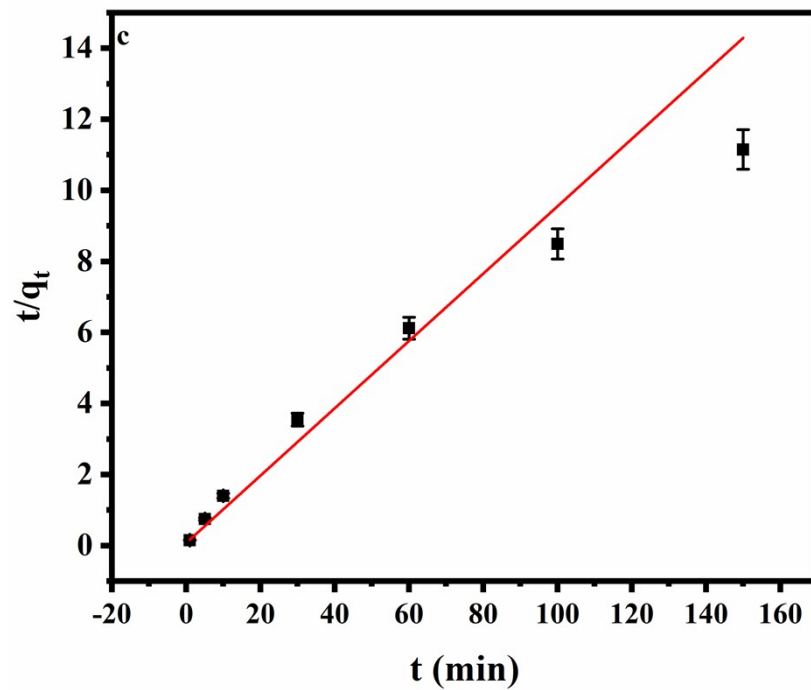
1 Fig.S2b



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4 Fig.S2c

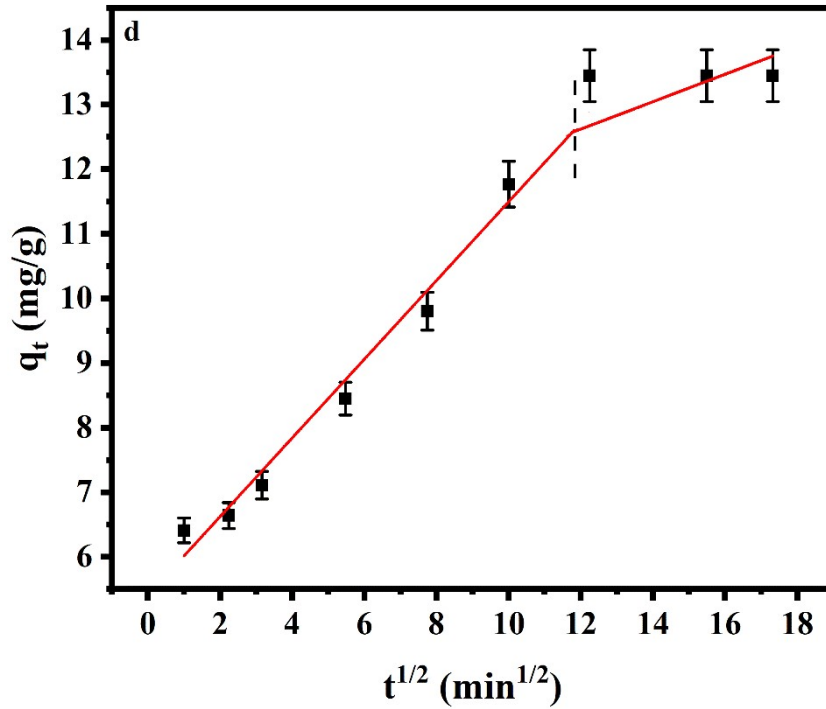


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1 **Fig.S2d**



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3 **S3 Adsorption thermodynamics**

4 Adsorption thermodynamics will explore the enthalpy change (ΔH^0) and Gibbs free energy
5 change (ΔG^0) generated during the adsorption process. The enthalpy change data will be obtained
6 by fitting the Clausius-clapeyron model. Gibbs free energy change will be derived from the Gibbs
7 equation.

8 Clausius-clapeyron model:
$$\ln C_e = \frac{\Delta H}{RT} + C \quad (6)$$

9 Gibbs equation:
$$\Delta G = -RT \ln K_L \quad (7)$$

10 Where K_L is the Langmuir equilibrium constant (L/mol); R and T represent the universal gas
11 constant (8.314 J/K/mol) and the system temperature (K), respectively.

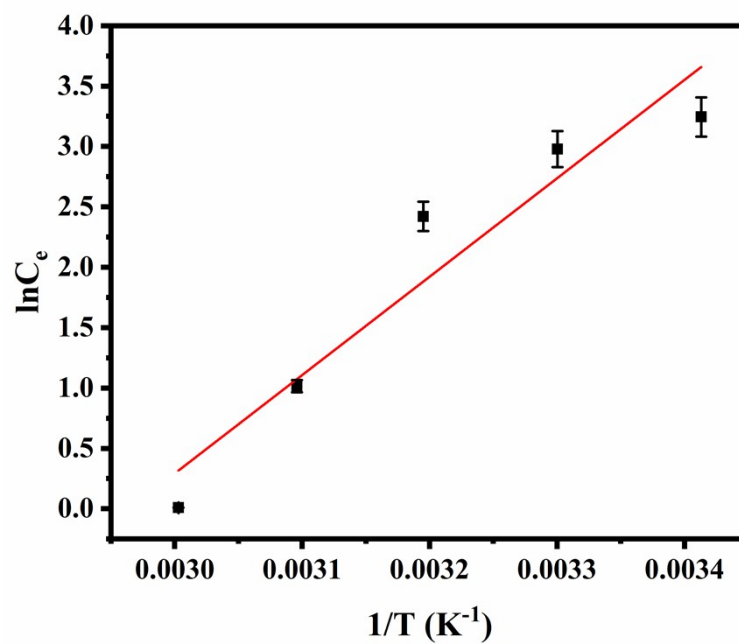
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2 **Fig.S3**



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Table S1 Adsorption free energy change

Adsorption free energy change	
T (K)	ΔG (J/mol)
293	-2793.36
303	-2888.70
313	-2984.04
323	-3079.37
333	-3174.71
343	-3270.05

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Table S2 XRF analysis of the POFTs and MPOFTs

	Parameter	CaO	MgO	P ₂ O ₅	SO ₃	SiO ₂	F	Fe ₂ O ₃	Al ₂ O ₃	MnO	K ₂ O	Na ₂ O	SrO	TiO ₂	ZnO
POFTs	Percentage (%)	57.26	16.89	9.78	8.16	3.53	1.70	1.06	0.81	0.29	0.19	0.07	0.05	0.05	0.04
MPOFTs	Percentage (%)	64.13	22.14	6.52	0.73	3.15	0.31	1.67	0.89	0.48	0.20	/	0.04	/	0.05

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Table S3 Surface areas of the POFTs and MPOFTs

Samples	POFTs	MPOFTs
BET surface area (m²/g)	2.2956	6.5239
BJH desorption pore volume (cm³/g)	0.0049524	0.038057

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2 **Table S4** ICP analysis of leachates (mg/L) (1#: POFTs, 2#:MPOFTs, 3#: EMMW,4#: MPOFTs

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after adsorption).

	NH ₄ ⁺ -N	Mg ²⁺	Mn ²⁺	Ca ²⁺	Zn ²⁺	Sb ²⁺	Co ²⁺
1#	/	22.38	0.03	3.03	/	/	/
2#	/	108.32	/	0.01	/	/	/
3#	70.00	45.00	165.00	9.00	0.06	0.03	0.01
4#	1.73	78.47	0.001	5.85	/	/	/

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