

Supplementary Information for

Anodic generation of hydrogen peroxide in continuous flow

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Scheme S1 Scheme for anodic H₂O₂ production in carbonate electrolyte. Carbonate (CO₃²⁻) can be anodically oxidized to peroxodicarbonate (C₂O₆²⁻) species. C₂O₆²⁻ undergoes hydrolysis to form bicarbonate (HCO₃⁻) and hydrogen peroxide (H₂O₂). In alkaline electrolytes, HCO₃⁻ ions are deprotonated to CO₃²⁻, which closes the cycle with a higher concentration of H₂O₂.¹ 8

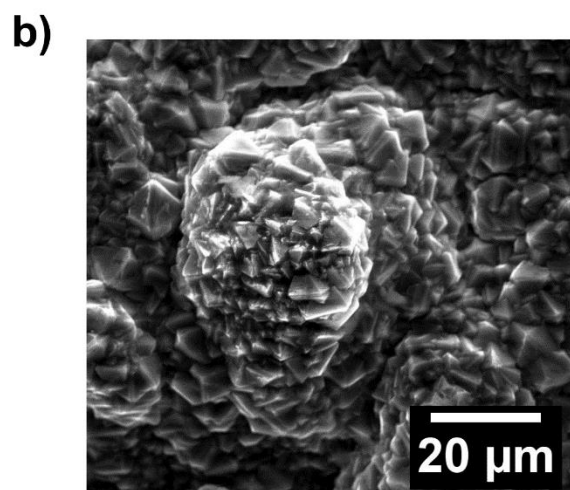
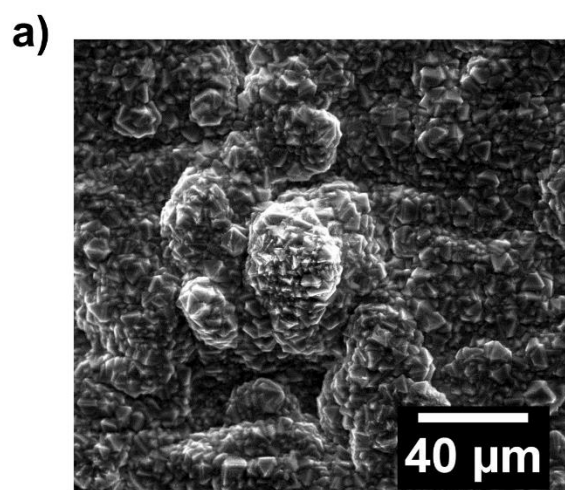


Figure S1 SEM images of used BDD electrode. SEM images of used BDD in this study at different magnification.

The molar fractions for each species were calculated using **Eqs. S2** and **S3**. The experiments were done in highly concentrated electrolytes, which differ from the ideal behavior of diluted electrolytes. As a result, the ion activities ($a_{\text{HCO}_3^-}$ and $a_{\text{CO}_3^{2-}}$) were calculated as shown in **Eqs. S4** and **S5** using the activity coefficient (f_{\pm}) shown in **Eq. S6**, where z_i is the charge of the ion, A is the Debye-Hückel parameter (0.51 $\text{kg}^{1/2} \text{mol}^{-1/2}$, for water at 25 °C), and B is a temperature-dependent parameter. In response to pH changes and carbonate equilibrium, we calculated the activity of HCO_3^- ($a(\text{HCO}_3^-)$) and CO_3^{2-} ($a(\text{CO}_3^{2-})$) ions during electrolysis for each concentration (c) of KHCO_3 .

$$K_{a,i} = 10^{-pK_{a,i}} \quad (\text{S1})$$

$$\alpha_{\text{HCO}_3^-} = \frac{K_{a,1} \cdot [\text{H}^+]}{[\text{H}^+]^2 + K_{a,1} \cdot [\text{H}^+] + K_{a,1} \cdot K_{a,2}} \quad (\text{S2})$$

$$\alpha_{\text{CO}_3^{2-}} = \frac{K_{a,1} \cdot K_{a,2}}{[\text{H}^+]^2 + K_{a,1} \cdot [\text{H}^+] + K_{a,1} \cdot K_{a,2}} \quad (\text{S3})$$

$$a_{\text{HCO}_3^-} = \alpha_{\text{HCO}_3^-} \cdot c_{\text{KHCO}_3} \cdot f_{\pm} \quad (\text{S4})$$

$$a_{\text{CO}_3^{2-}} = \alpha_{\text{CO}_3^{2-}} \cdot c_{\text{KHCO}_3} \cdot f_{\pm} \quad (\text{S5})$$

$$\log f_{\pm} = - \frac{A \cdot z_i^2 \cdot \sqrt{I}}{1 + B \cdot a_i \cdot \sqrt{I}} \quad (\text{S6})$$

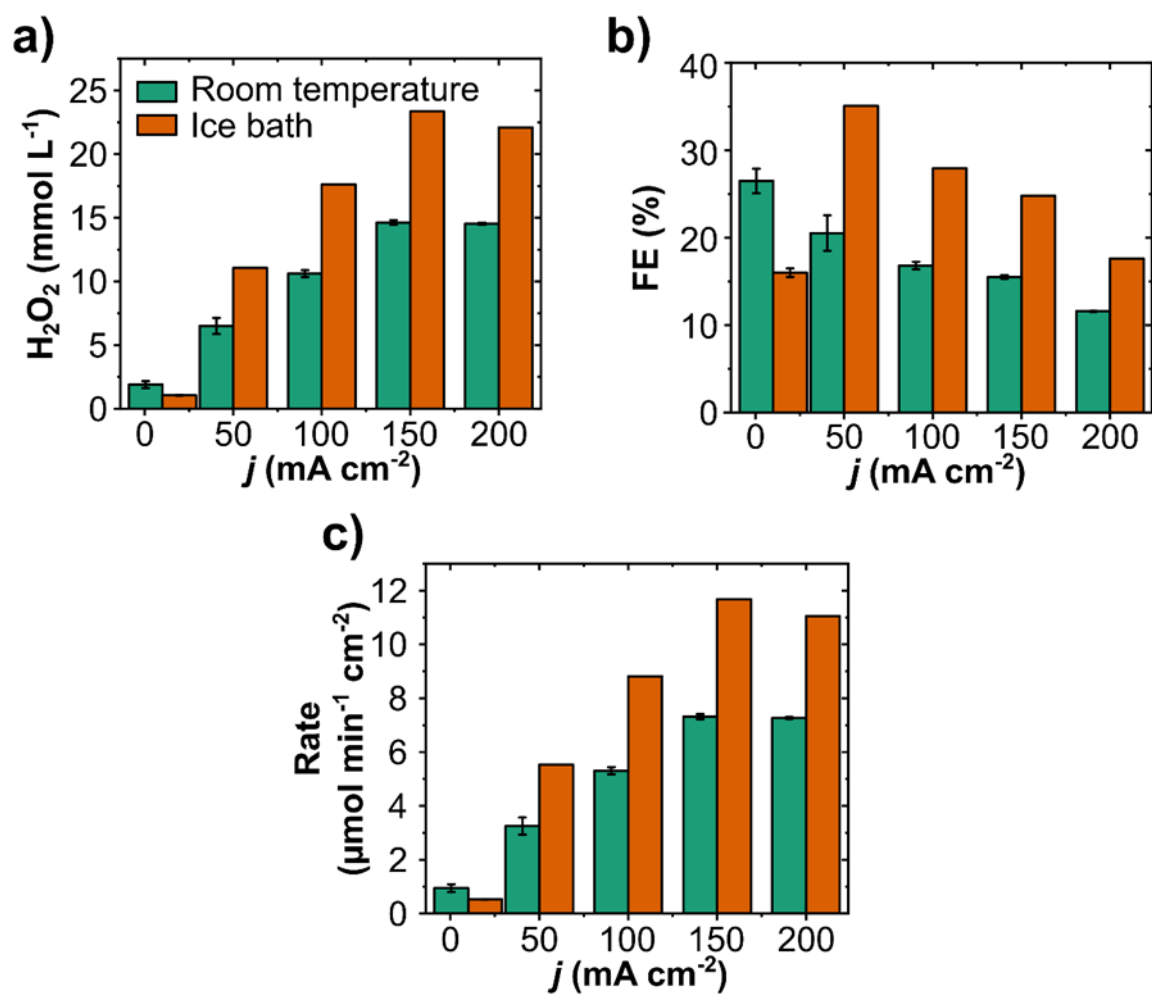


Figure S2 Comparison of electrolyte conditions using BDD as anode. Anodic H_2O_2 (a) concentration (b) FE, and (c) production rate for H_2O_2 production against applied current density during 10 minutes in 25 mL 2 mol L^{-1} KHCO_3 (pH 9) at room temperature and in ice bath using 5 cm^2 BDD as an anode in a two compartment H-cell.

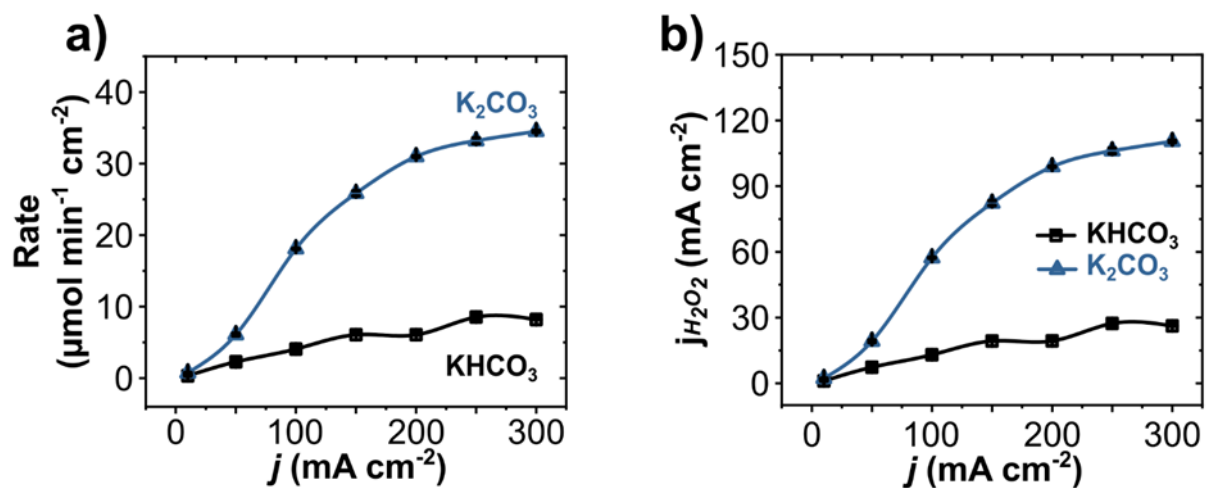
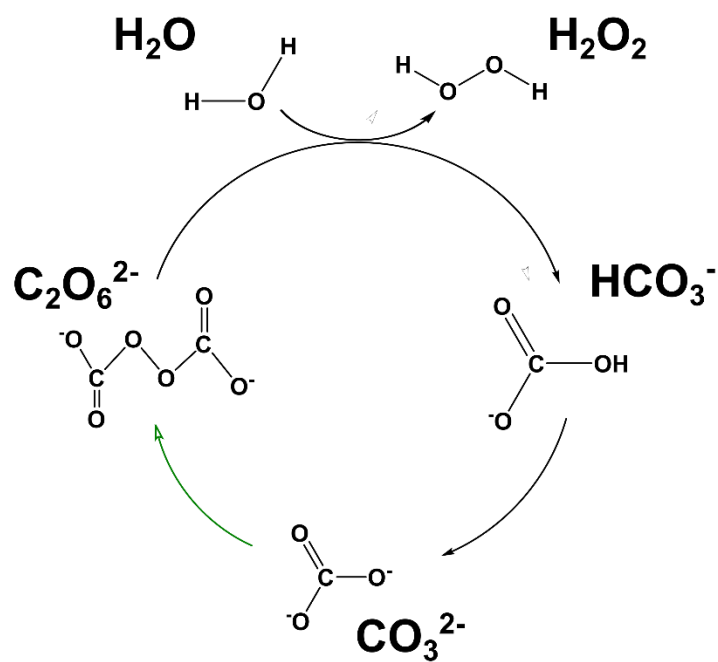


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Scheme S1 Scheme for anodic H_2O_2 production in carbonate electrolyte. Carbonate (CO_3^{2-}) can be anodically oxidized to peroxodicate ($\text{C}_2\text{O}_6^{2-}$) species. $\text{C}_2\text{O}_6^{2-}$ undergoes hydrolysis to form bicarbonate (HCO_3^-) and hydrogen peroxide (H_2O_2). In alkaline electrolytes, HCO_3^- ions are deprotonated to CO_3^{2-} , which closes the cycle with a higher concentration of H_2O_2 .¹

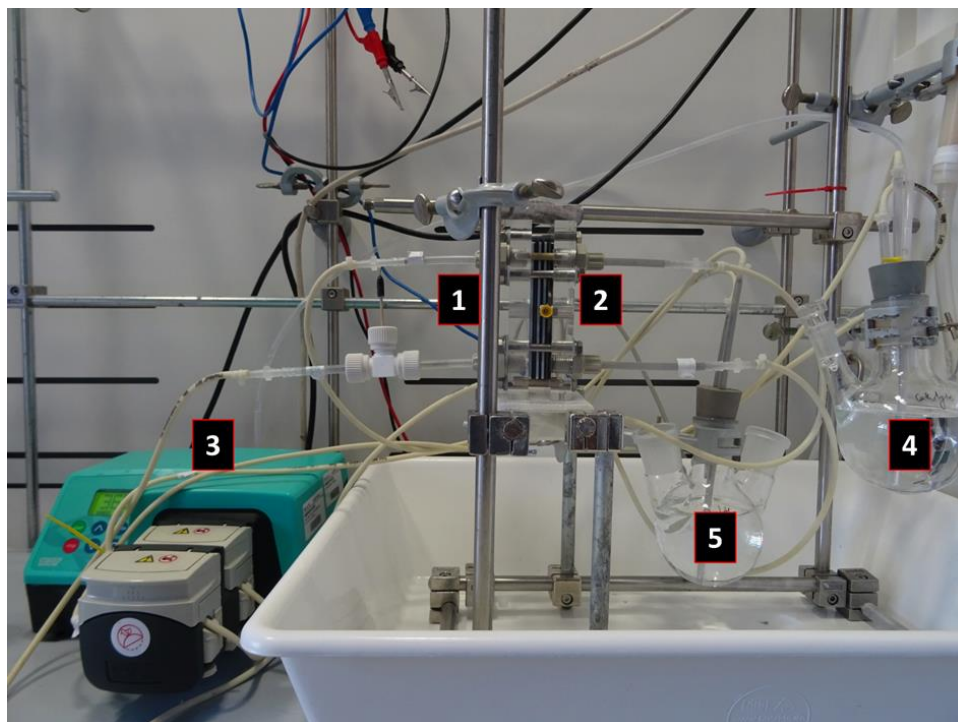


Figure S4 Experimental setup for circular flow. (1) Cathodic compartment, (2) anodic compartment, (3) flow pump, (4) catholyte tank, and (5) anolyte tank. The anolyte collected in (5) is recirculated to the anodic half-cell and the product is collected in the same reservoir.

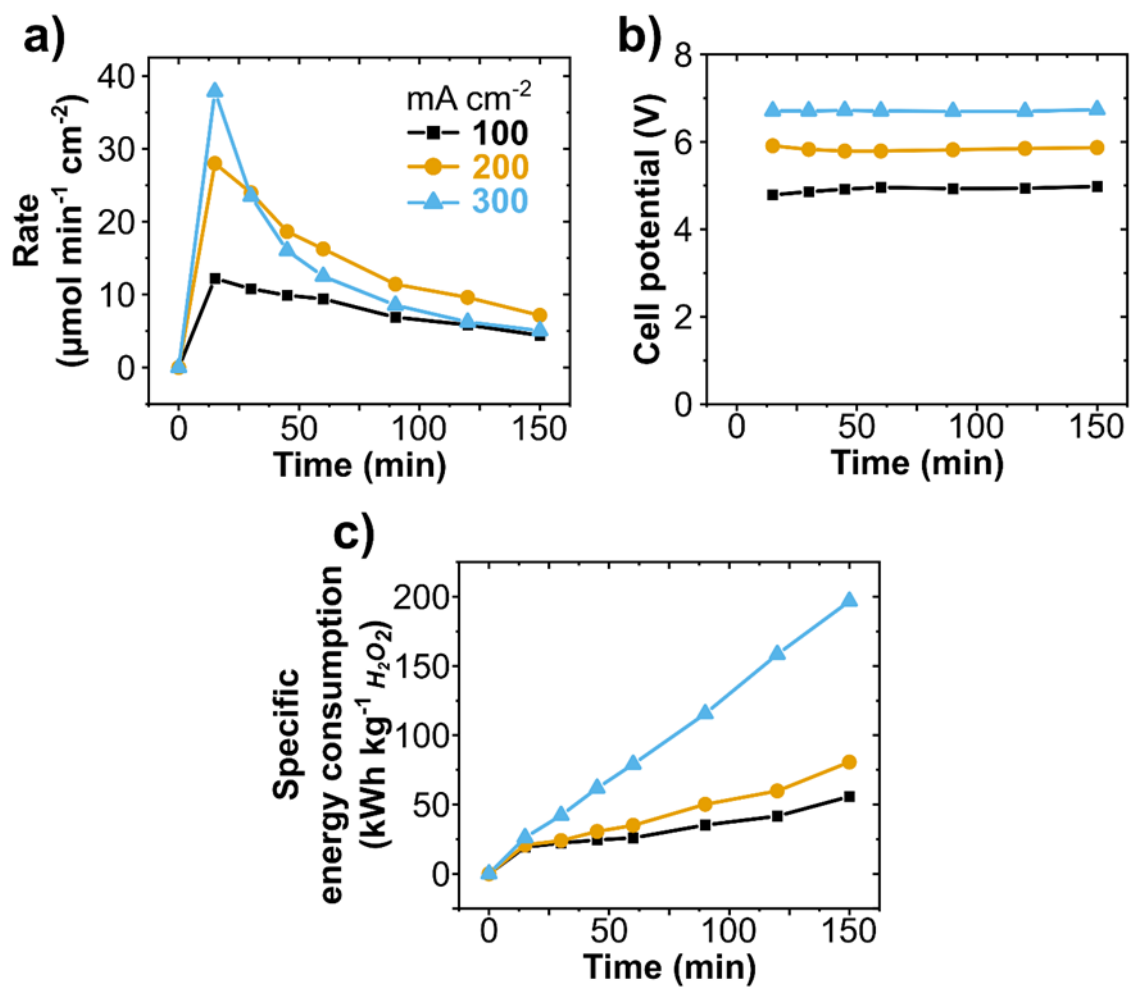


Figure S5 Anodic H₂O₂ production in a circular flow reactor. Anodic H₂O₂ (a) production rate, (b) cell potential, and (c) specific energy consumption to produce 1 kg of H₂O₂ at different current densities using a circular flow system.

Table S1 Anodic H₂O₂ production in a circular flow reactor. Faradaic efficiency and corresponding specific energy consumption to produce 1 kg of H₂O₂ over time at different current densities using a circular flow system.

Time (min)	Faradaic efficiency (%)			Specific energy consumption (kWh ⁻¹ kg ⁻¹)		
	100 <i>mA cm⁻²</i>	200 <i>mA cm⁻²</i>	300 <i>mA cm⁻²</i>	100 <i>mA cm⁻²</i>	200 <i>mA cm⁻²</i>	300 <i>mA cm⁻²</i>
15	39.09	44.86	40.41	0.58	0.62	0.79
30	34.55	38.42	25.08	0.67	0.72	1.27
45	31.72	29.91	17.13	0.73	0.92	1.86
60	30.13	26.09	13.37	0.78	1.05	2.37
90	22.07	18.31	9.14	1.06	1.50	3.47
120	18.70	15.41	6.67	1.25	1.80	4.75
150	14.08	11.48	5.40	1.67	2.42	5.90

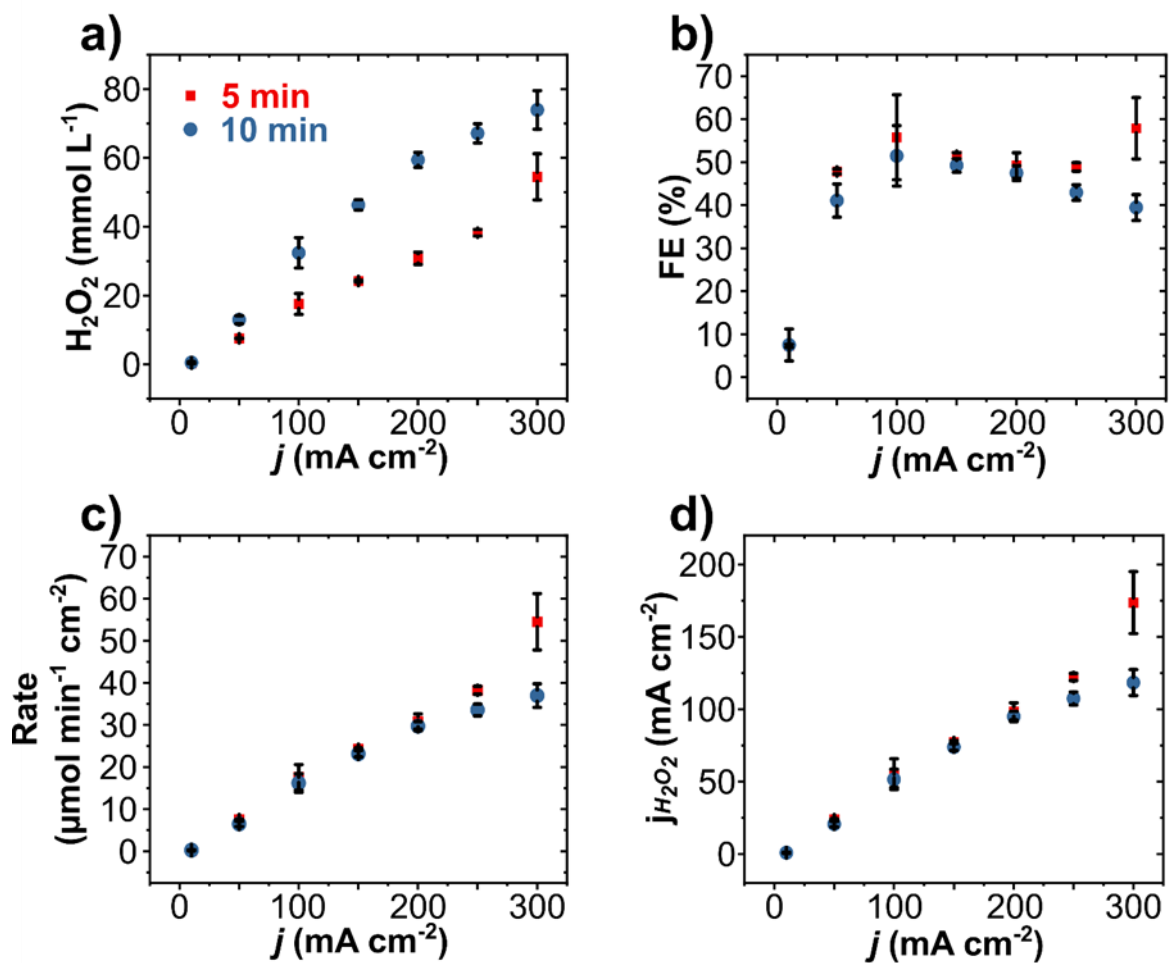


Figure S6 Comparison of the sampling time during electrolysis in H-Cell. (a) Anodic H_2O_2 concentration, **(b)** FE, **(c)** production rate, and **(d)** partial current density at different applied current densities for 5 or 10 minutes. The electrolyte was $2 \text{ mol L}^{-1} \text{ K}_2\text{CO}_3$ at pH 12.6 and the anode a 5 cm^2 BDD.

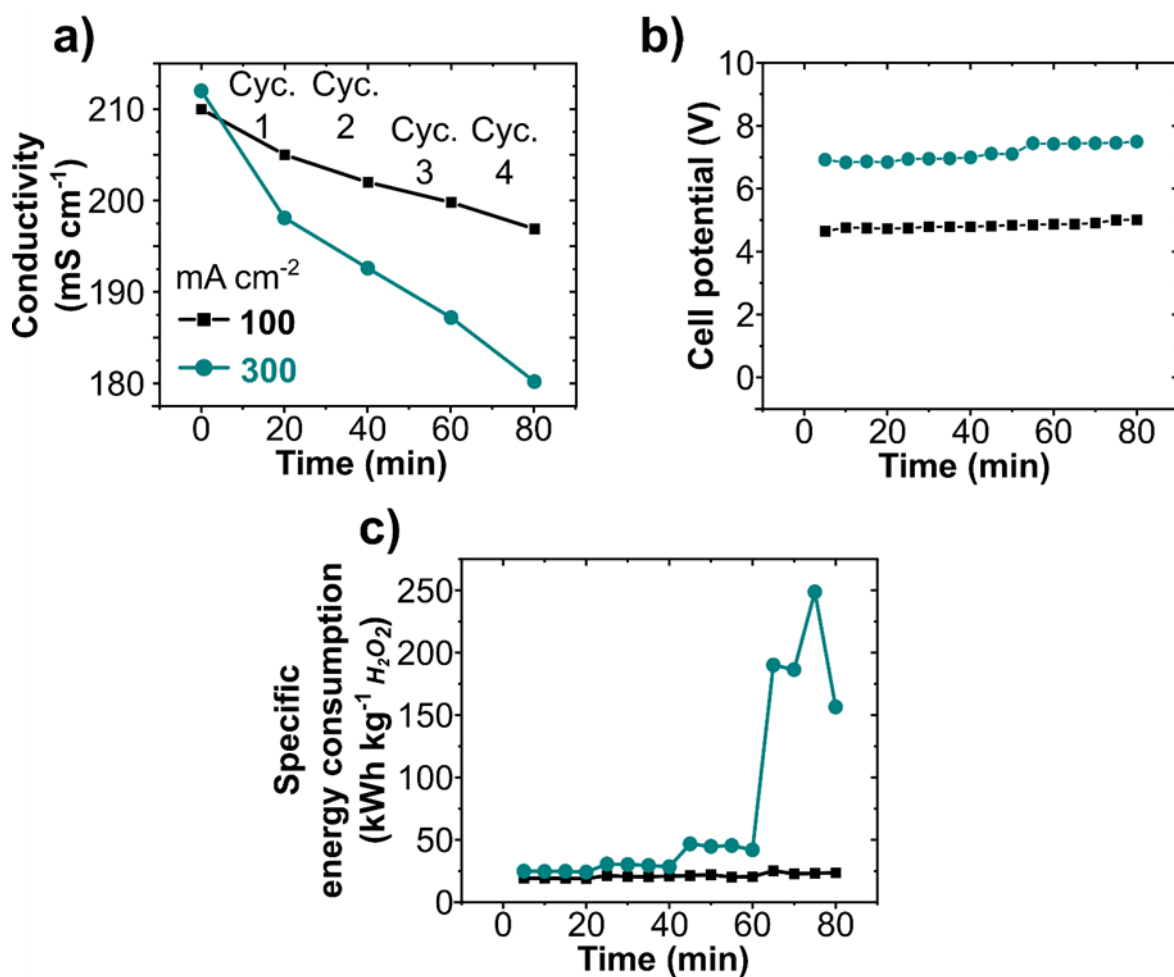


Figure S7 H₂O₂ generation with multiple electrolyte flow cycles. Change in (a) conductivity of the electrolyte, (b) cell potential, and (c) energy consumption against time at a current density of 100 and 300 mA cm⁻² in 2 mol L⁻¹ K₂CO₃ with 90 mmol L⁻¹ Na₂SiO₃ stabilizer using 10 cm² BDD as an anode. The total volume of the electrolyte used for each cycle was 200 mL. Experiments were performed in a single flow system. The volume accumulated in each cycle was reused in the following one.

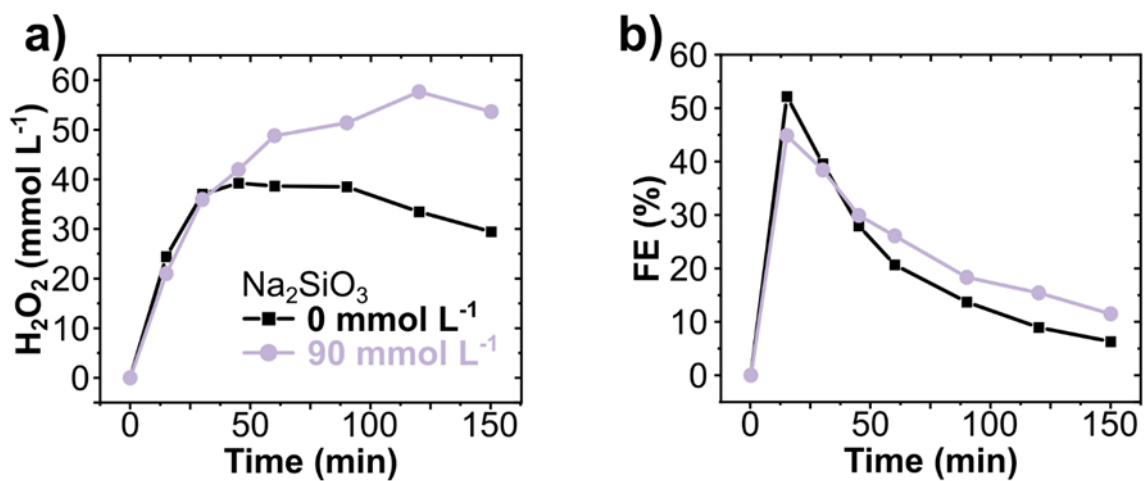


Figure S8 Effect of Na_2SiO_3 stabilizer on H_2O_2 generation in circular flow. Anodic H_2O_2 (a) concentration and (b) FE at current density of 200 mA cm^{-2} with (■) and without (●) 90 mmol L^{-1} Na_2SiO_3 at a controlled pH of 12.6. Each cell compartment contained a reservoir with 200 mL of 2 mol L^{-1} K_2CO_3 electrolyte circulating at 100 mL min^{-1} flow rate.

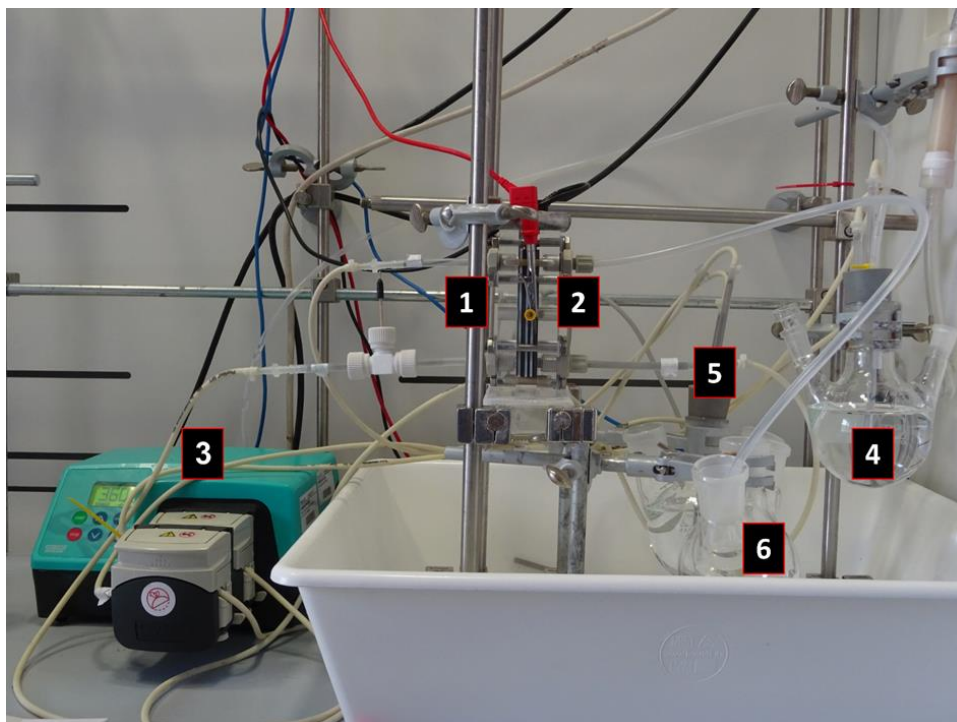


Figure S9 Experimental setup of single-pass flow. (1) Cathodic compartment, (2) anodic compartment, (3) flow pump, (4) catholyte tank, (5) fresh anolyte tank before cell, and (6) collected anolyte containing H_2O_2 after flow cell.

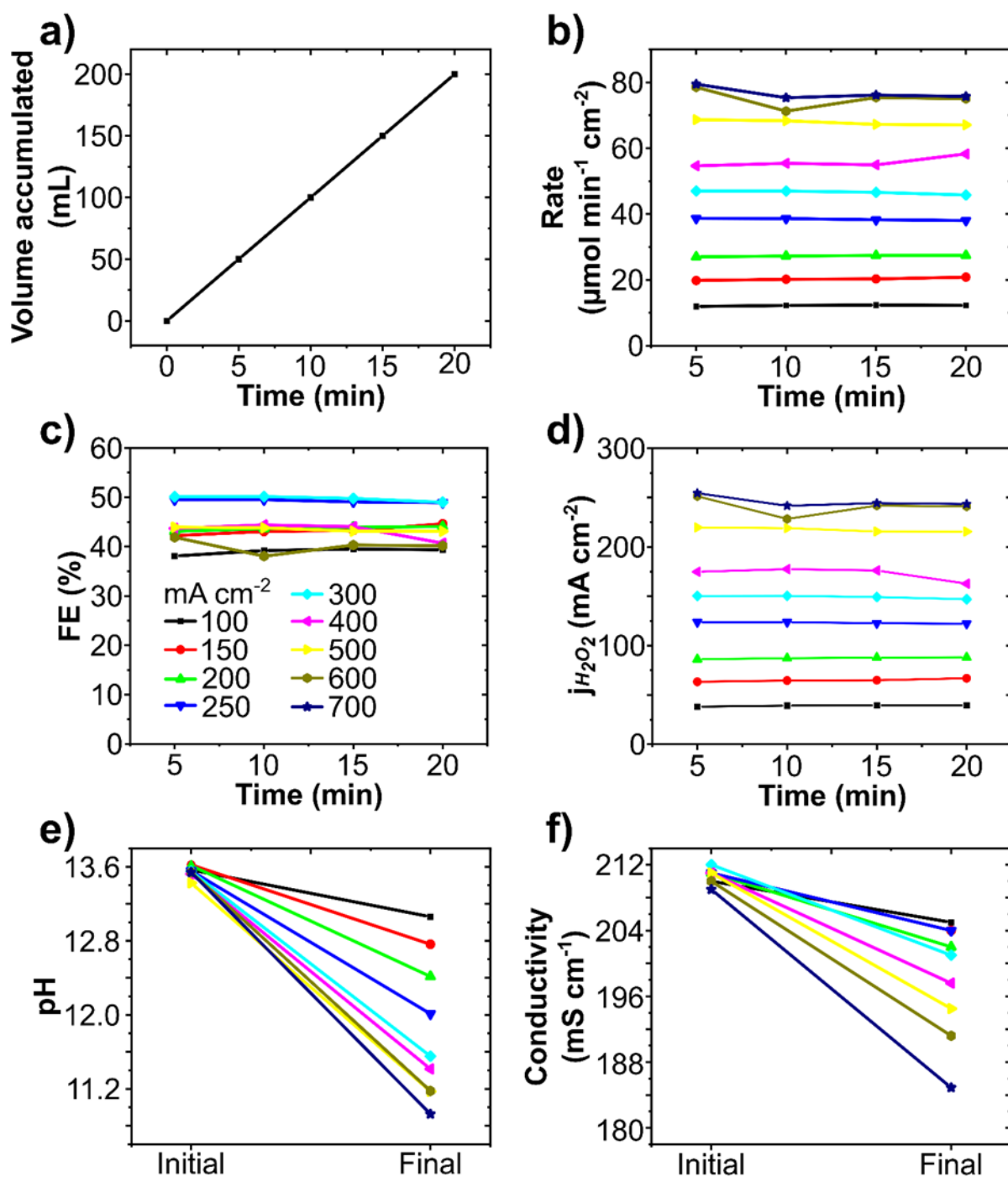


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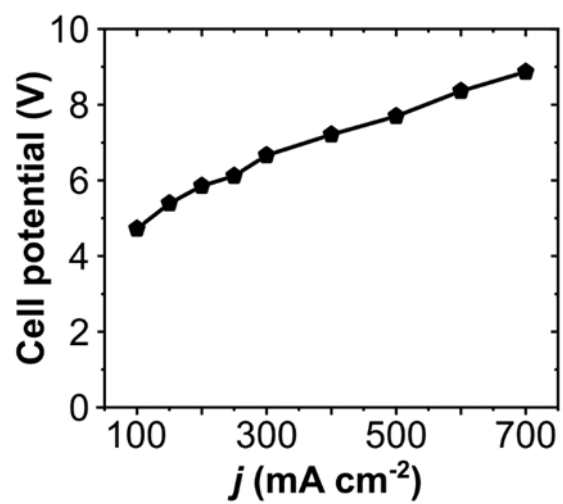


Figure S11 Anodic H_2O_2 production in a single pass mode flow reactor. Cell potential at different current densities using 10 mL min^{-1} flow rate without recirculation in $2 \text{ mol L}^{-1} \text{ K}_2\text{CO}_3 + 90 \text{ mmol L}^{-1} \text{ Na}_2\text{SiO}_3$.

Table S2 A comparison of the reported work on water oxidation to H₂O₂ with our present study.

Electrode	Cell type	Electrolyte	Conditions*							[H ₂ O ₂] _{max}	Production rate	Peak FE	Ref.
			pH	j/P	t	EA	VA	S	mmol L ⁻¹	μmol min ⁻¹ cm ⁻²	%		
PTFE/CFP	H-Cell	1 M Na ₂ CO ₃	12	100	420	0.36	25	~30	3	23.4	66	²	
BDD/Nb			11.9	39.8	10	1.13	8.5	-	-	3.93	31.7	³	
BDD/Ti		2 M KHCO ₃	8	120	5	7.4	25	-	~16	~8	28	⁴	
BDD/Ti			8	295	5	7.4	25	-	29	19.7	~22	⁴	
CaSnO ₃ @CF-2	Undivided	2 M KHCO ₃	~8.3	2.9 V	10	1.3	-	-	-	39.8	90	⁵	
CaSnO ₃ /FTO			8.3	3.2 V	10	-	30	-	-	~4.6	76	⁶	
CaSnO ₃ /FTO		8.3	2.2 V	720	-	30	-	~0.9	-	-	⁶		
BiVO ₄ /FTO		1 M NaHCO ₃	8.3	3.1 V	-	1	20	-	-	5.7	70	⁷	
BDD/Nb	H-Cell	2 M Hybrid	10	300	5	~7	25	-	104.6	76.4	82	⁸	
BDD/Nb		5 M K ₂ CO ₃	>13	100	5	~6	25	-	39	15.6	91.5	⁹	
CFP	Flow-Cell	2 M K ₂ CO ₃	12.6	100	150	10	200	90	33	4.5	14.3	¹	
BDD/Ta				300	40	10	200	90	76	73	78	This work	
				300	80	10	200	90	110	46	50		
				700	20	10	200	90	80	79	35		

*j: Current density (mA cm⁻²), P: Potential applied (V vs. RHE), t: Time (minutes), EA: Electrode geometric area (cm²), VA: Volume of anolyte (mL), S: Stabilizer concentration (mmol L⁻¹ Na₂SiO₃)

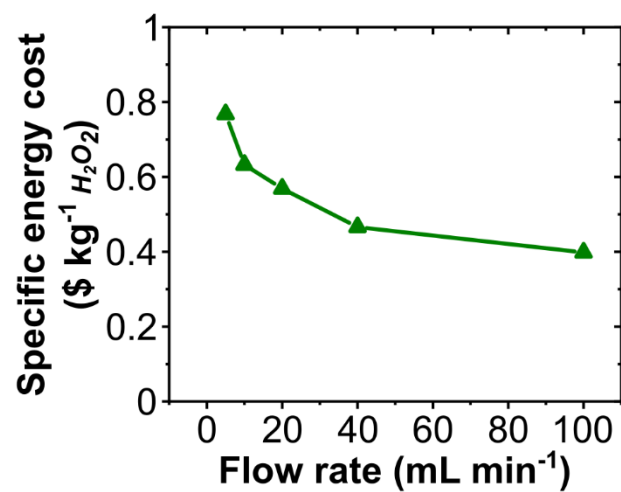


Figure S12 Anodic H₂O₂ generation at different electrolyte flow rates. Specific electricity cost based on energy consumption to produce 1 kg of H₂O₂ at different flow rates. Experiment conditions: Flow cell with 200 mL anolyte at a constant current density (j) of 300 mA cm⁻².

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