

Supporting Information

Coupling of water-splitting mechanism and doping-mixture to design a novel Cr-perovskite for rapid and efficient solar thermochemical H₂ production

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Experimental Section

The experimental setup of the thermochemical reaction is shown in the Fig. S1. In the redox process, the main equipment includes a tubular furnace with a corundum reaction chamber, a syringe pump to inject water, a steam generator to evaporate the injected water, and a gas chromatograph to analyze the concentration of H₂ and O₂. The experimental setting parameters of equipment are listed in the Table 1.

Table S1. Experimental details

Equipment	Setting Parameters
Tubular furnace (SK-G05163)	Heating rate: 10 °C/min, $T = 0 \sim 1600$ °C
Syringe pump	water injection velocity: $0 \sim 1$ ml min ⁻¹
Steam generator (FD-HG)	Evaporation temperature: 100 ~ 150 °C
Gas chromatograph (GC-2014C)	Tracer gas: H ₂ , O ₂

There are three parts of experimental system. The first part is the gas pipeline, with heat tracing device (130 °C), to deliver the inert gas (argon) and water vapor into the reaction chamber. The carriers of analyzing O₂ and H₂ is Argon gas. In the reduction process, argon with the rate of 200 ml min⁻¹ flows into reaction chamber to provide an inert environment, and in the oxidation process, the mixing gas (vapor-argon) flows into the chamber to react with the sample powder hold in a corundum crucible. The water injection rate is controlled at 0.5 ml min⁻¹. This part of the system is the reaction region. After the redox reaction, the produced gas flows through a gas-liquid separator to remove water vapor and then the produced H₂ is analyzed by the gas chromatograph.

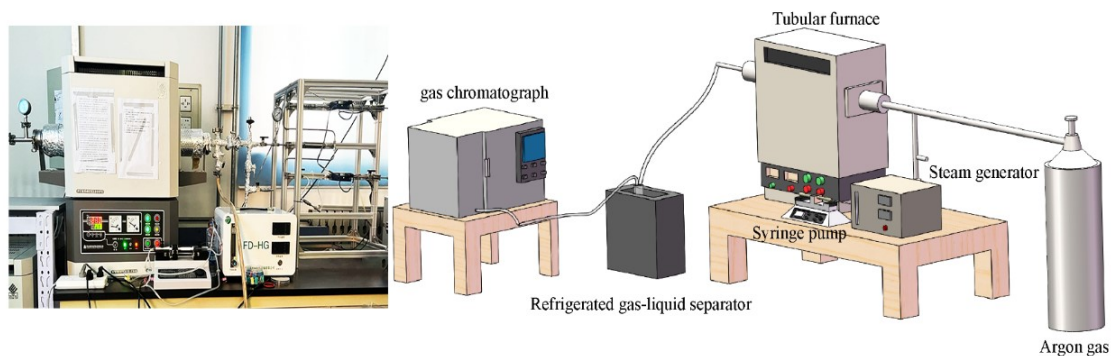


Fig. S1 Experimental setup of the redox reaction and gas detection process.

XRD result

Fig. S2 shows the XRD results of CeO_2 before and after the thermochemical H_2 production cycles. CeO_2 remains the stable lattice structure after experiments. A good fit of the synthesized materials with the PDF graph of CeO_2 (PDF #81-0792) has been obtained in this part.

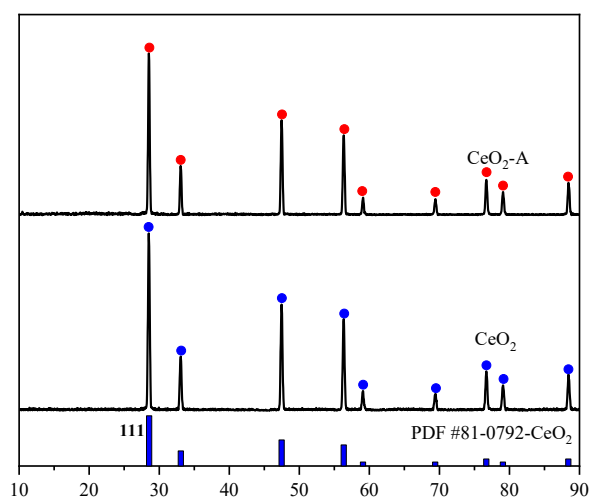


Fig. S2 XRD patterns of the ready-made Ceria (A indicates the results after experiments)

As shown in Fig. S3, the Bragg peaks of CeO_2 appear in the XRD graph of $\text{YCr}_{0.75}\text{Zr}_{0.25}\text{O}_3$ -25wt% CeO_2 after experiments. The mixing of CeO_2 causes the downshift of the main peak (111) because of the large ionic radius of Ce^{4+} (0.87 Å). The calculated lattice structures and parameters are listed in Table S2.

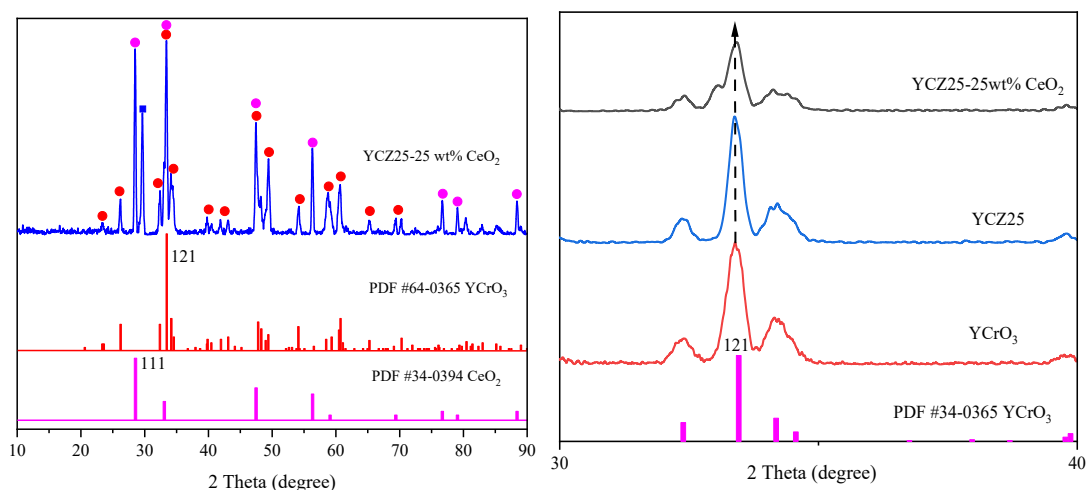


Fig. S3 XRD patterns of the mixed $\text{YCr}_{0.75}\text{Zr}_{0.25}\text{O}_3\text{-25wt\% CeO}_2$ after experimental process.

Table S2. XRD calculation results of $\text{YCr}_{0.75}\text{Zr}_{0.25}\text{O}_3\text{-25wt\% CeO}_2$

Samples	Lattice constants and angles	Crystalline size(nm)	d (1 2 1) (Å)
$\text{YCZ25-25wt\% CeO}_2$	$a=5.517 \text{ \AA}$, $b=7.54 \text{ \AA}$, $c=5.26 \text{ \AA}$, $\alpha=\beta=\gamma=90^\circ$	28.0	2.681

SEM result

Fig. S4 shows the SEM graphs of $\text{YCr}_{0.75}\text{Zr}_{0.25}\text{O}_3\text{-25 wt\% CeO}_2$ after the thermochemical reactions, which shows a multi-porous structure..

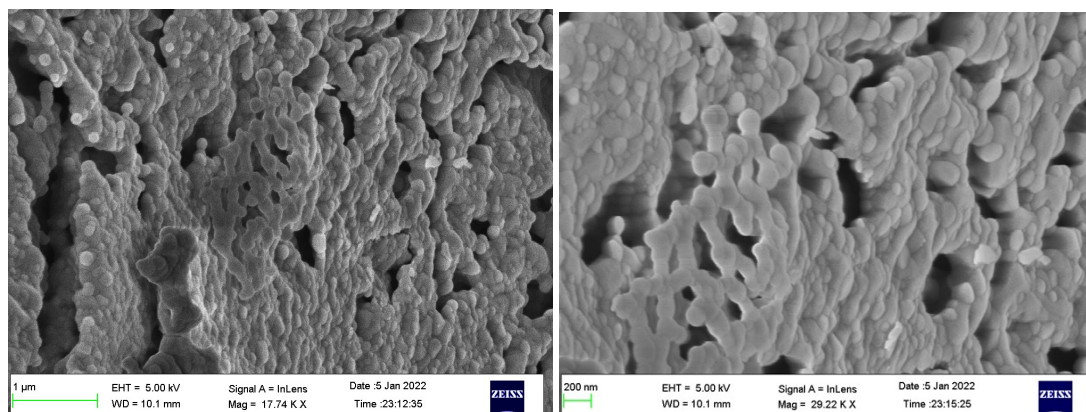


Fig. S4 SEM graphs of $\text{YCr}_{0.75}\text{Zr}_{0.25}\text{O}_3\text{-25 wt\% CeO}_2$

EDX result

Fig. S5 indicates the EDX result of elemental composition of the synthesized material $\text{YCr}_{0.75}\text{Zr}_{0.25}\text{O}_3$.

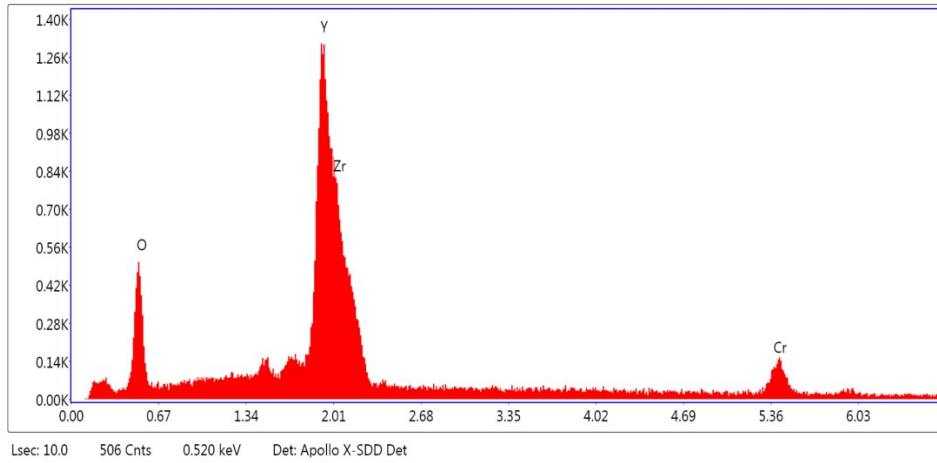


Fig. S5 EDX mapping of the Y, Cr and Zr distribution in the $\text{YCr}_{0.75}\text{Zr}_{0.25}\text{O}_{3-\delta}$ sample

Zr doping ratio

Fig. S6 shows the H_2 production capacity under different Zr doping ratios (10, 25, 40 mol%).

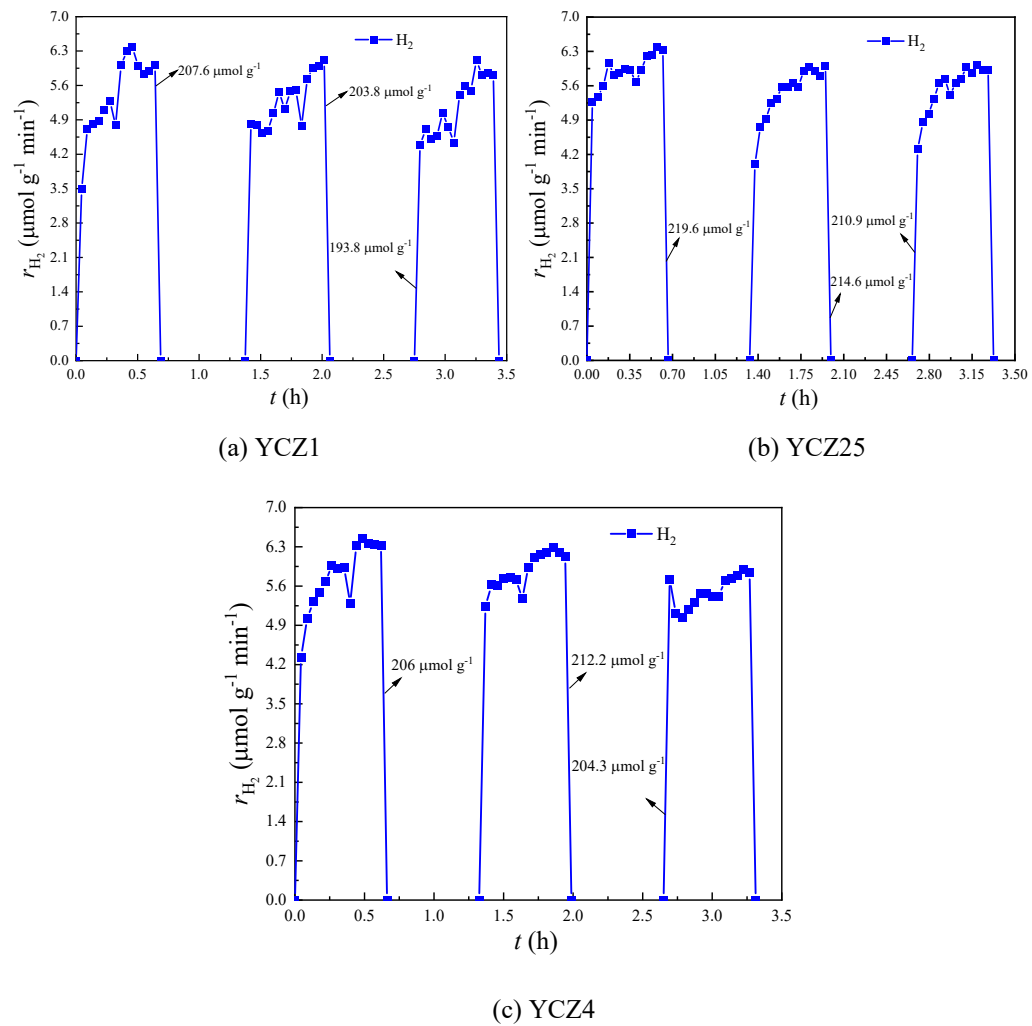


Fig. S6 The H_2 rate under different Zr doping ratios (10, 25, 40 mol%). Materials were reduced at 1400

°C (heated at 10 °C/min) and oxidized at 1300 °C (cooled at 30 °C/min) in the 40 min water-splitting process

The comparison of H₂ yield of three Zr doping ratios

To determine the optimum doping ratio of Zr, the STWS performance of three Zr doping ratios (10, 25, 40 mol%) are compared in the Fig. S7. Based on the comparison results of different Zr doping ratios, the doping of Zr at 25 mol% presents the favorable H₂ yield ($Y_{H_2}=219.6 \mu\text{mol g}^{-1}$). On the whole, H₂ yield of multiple cycles under the three Zr doping ratios show a gradual decrease trend except a slight increase of YCZ4, which may be caused by the remove of impurities contained in the parent and the release of excess oxygen have limited H₂ production ability of the first STWS cycle. By comparing H₂ yield loss of different Zr doping ratios, YCZ1 shows the most considerable decrease of H₂ production capacity and YCZ25 has the lowest rate of decline. As for the whole H₂ production performance of the three cycles, the Y_{H_2} of YCZ25 is higher than the value of YCZ1 and YCZ4. From the above analysis, the setting of Zr doping ratio at 25 mol% can achieve the favorable performance of H₂ production.

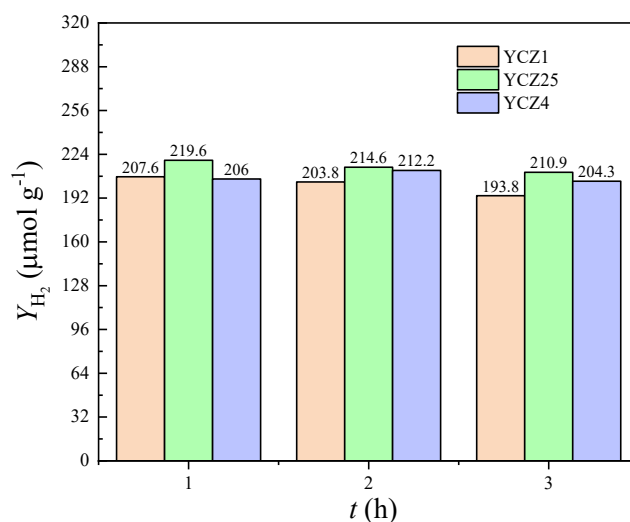


Fig. S7 The H₂ yield per mass and rate per minute of YCZ1, YCZ25 and YCZ4. Materials were reduced at 1400 °C (heated at 10 °C/min) and oxidized at 1300 °C (cooled at 30 °C/min) in the 40 min water-splitting process

Ceria mixing ratio

After the determination of Zr doping ratio, we try to mix ceria in 25 mol% Zr doped YCrO₃

materials to improve the water-splitting kinetic performance. Fig. S8 shows the H₂ production performance of three STWS cycles under different ceria mixing ratios. The ceria mixing ratio of 25 wt% shows a favorable H₂ production performance compared with the ceria ratio of 10 wt% and 50 wt%.

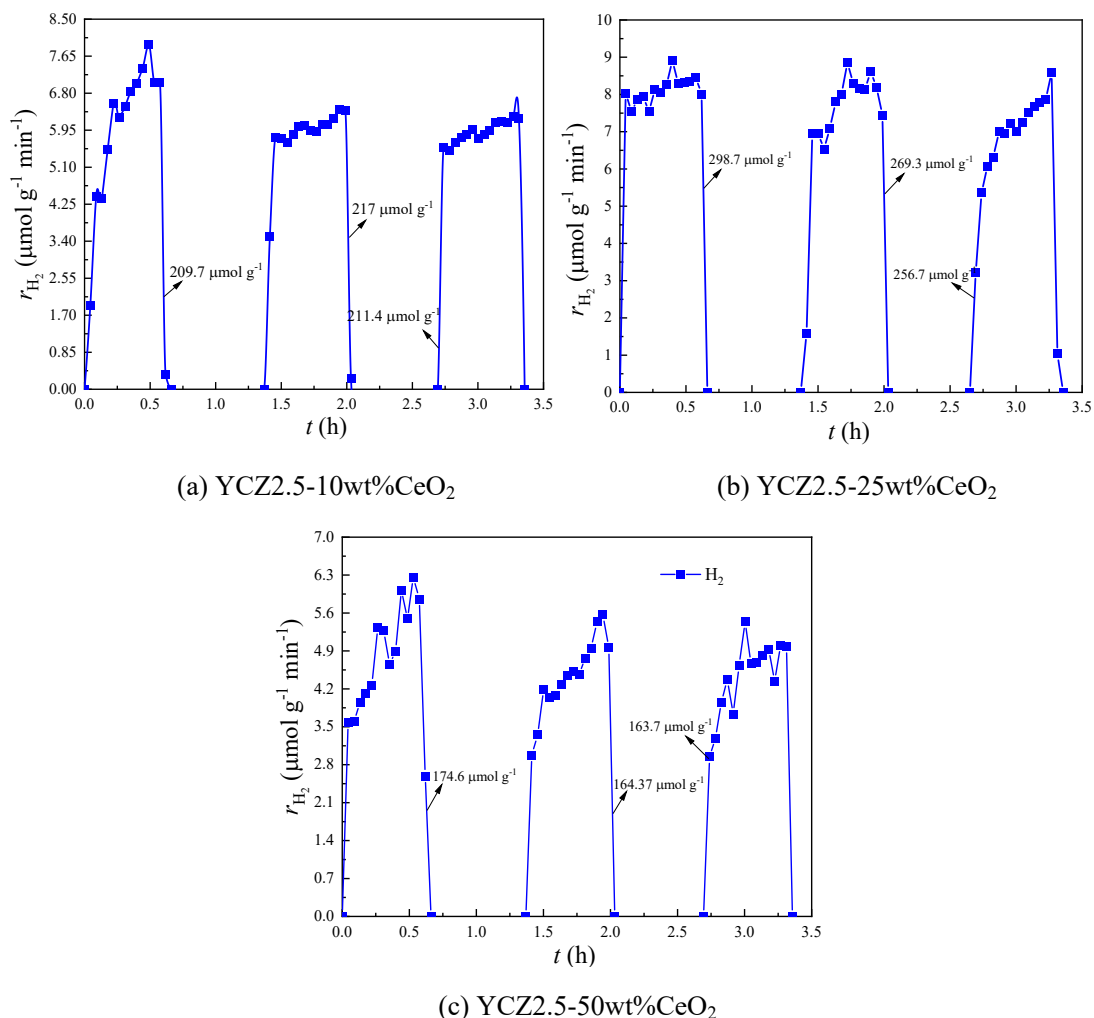


Fig. S8 Hydrogen production under different ceria mixing ratios (10, 25, 50 wt% CeO₂). Materials were reduced at 1400 °C (heated at 10 °C/min) and oxidized at 1300 °C (cooled at 30 °C/min) in the 40 min water-splitting process

The comparison of H₂ yields of three ceria mixing ratios

The comparison of H₂ yield of three ceria mixing conditions (10, 25 and 50 wt%) are shown in the Fig. S9. In the multiple cycles, the H₂ yields of mixture materials indicated a slight decrease trend, the maximum variation of H₂ yields was 9.8% and the minimum change was 0.4%. In the STWS cycles, the ceria mixture ratio of 25 wt% performs the optimum performance, and the average

H₂ yield of this condition is 274.9 μmol g⁻¹. The average H₂ yields of YCZ25-10wt%CeO₂ and YCZ25-50wt%CeO₂ are 22.7% and 39.1% lower than YCZ25-25wt%CeO₂. From the above analysis, the suitable ceria mixing ratio can stimulate water splitting in the STWS process and the excess of ceria influences the H₂ yields because of the weakness of reduction capacity. On the basis of the determined Zr doping ratio, ceria mixing ratio at 25% can further lead to 27.8% increase of H₂ yield.

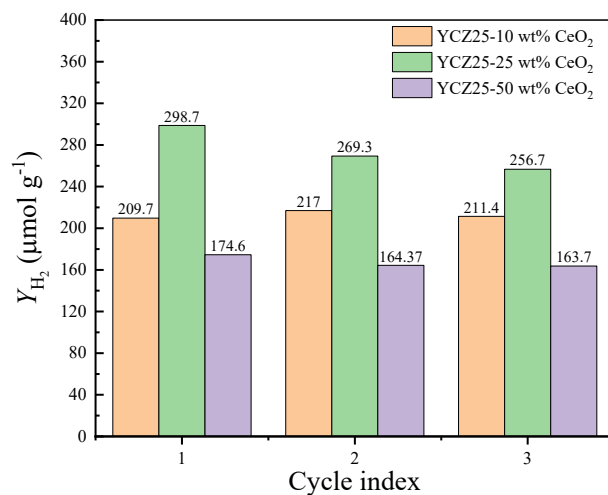


Fig. S9 The H₂ yield of YCZ25-10 wt%CeO₂, YCZ25-25wt%CeO₂ and YCZ25-50wt%CeO₂. Materials were reduced at 1400 °C (heated at 10 °C/min) and oxidized at 1300 °C (cooled at 30 °C/min) in the 40 min water-splitting process