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2	SUPPLEMENTARY INFORMATION
3	for
4	Integrated Low Carbon H ₂ Conversion with In-Situ Carbon
5	Mineralization from Aqueous Biomass Oxygenate Precursors by
6	Tuning Reactive Multiphase Chemical Interactions
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8	Prince Ochonma, ¹ Christopher Noe, ² Akanksh Mamidala, ³ Sohaib Mohammed, ³
9	and Greeshma Gadikota ^{1,3*}
10	
11	¹ Robert Frederick Smith School of Chemical and Biomolecular Engineering, Cornell
12	University, 113 Ho Plaza, Ithaca, NY 14853
13	² Department of Chemistry, College of Art and Science, Stony Brook University, Stony Brook,
14	NY 11790
15	³ School of Civil and Environmental Engineering, Cornell University, 527 College Avenue,
16	117 Hollister Hall, Ithaca, NY 14853

^{*} Corresponding Author. Phone: +1 607-255-4796. E-mail: gg464@cornell.edu

1 Extent of carbon mineralization

In this study, the estimation of the extent of carbonation was done using both TGA (Thermo 2 3 Gravimetric Analysis) and TCA (Total Carbon Analysis). The TGA method provided an insight 4 into the presence of different solid phases (e.g., carbonate and hydrate phases as well as organic 5 carbon with distinct decomposition temperature) and the quantification of each phase in the analyzed sample. The TGA technique can be difficult for samples with overlapping weight drop 6 7 curves. Thus, the TGA method should be used for samples with clear distinction between weight drop curves, and this was the case for carbonated samples in this study. The total carbon reported 8 from the TCA [g of C/g of carbonated solids] was converted into the extent of carbonation by 9 10 comparing the TCA data with the theoretical carbon capture capacity of the minerals.

The determination of the extent of the carbon mineralization with the ladle slag was challenged by 11 the heterogeneous compositions of slag samples. Thus, the extent of mineral carbonation is 12 13 calculated and estimated based on a careful determination of the chemical phases. First, only Caand Mg- based oxides and silicates which make up > 65 wt.% of NuLD (**Table 1**) are considered 14 15 to react and produce Ca- and Mg-carbonates, while other metals such as Fe and Al are considered 16 unlikely to dissolve at pH greater than 7.5 and react to produce respective carbonates. For example, Iron oxides can react with CO₂ to form siderite (FeCO₃), however, it has been reported that the 17 formation of siderite is inhibited by the low solubility of iron oxide .⁴³ Second, only non-18 19 carbonated Ca and Mg species are considered for carbon mineralization. The pH of NuLD in 20 solution used in this study was measured to be 12.17. Dissolution of solid calcium and magnesium carbonate at pH greater than 7.5 in material systems bearing alkaline industrial residues and 21 22 solvents is negligible.⁴⁰ Based on the above assumptions, the extent of carbon mineralization was

calculated. Where the TGA method was used to analyze the carbonated solids, Eq. (2) was used to
 determine the extent of carbon mineralization. On the other hand, Eq. (3) was used when TCA was
 used for the solid analysis.

4 Extent of carbon mineralization (%) =
$$\frac{\frac{TGA}{(1-TGA)}}{\text{theoretical maximum CO2 storage capacity}} x100(\%)$$
 (S1)

5 Extent of carbon mineralization (%) =
$$\frac{\frac{3.67*TCA}{(1-3.67*TCA)}}{\text{theoretical maximum CO2 storage capacity}} x100(\%)$$
 (S2)

TGA in Eq. (S1) represents the percent weight change of the carbonated solid at its calcination temperature, and TCA in Eq. (S2) represents the weight fraction of carbon in the carbonated sample with a unit of (weight of carbon/ weight of sample). The coefficient 3.67 is introduced into Eq. (S2) to account for the ratio of the molecular weights of CO₂ to carbon. In reactions where ladle slag was used as the alkaline sorbent, the theoretical maximum CO₂ capacity was calculated after subtracting the initial amount of residual CO₂ which was estimated to be 0.02 g (\pm 2%) CO₂ per g of NuLD.

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- **Table S1.** Reactions involved with complete conversions of various biomass oxygenates with
- 2 and without an alkaline sorbent. *M represents either Ca or Mg metal.*

Biomass Oxygenates	Reaction stoichiometry
Methanol (CH ₃ OH)	$CH_4O_{(aq)} + H_2O_{(l)} \rightarrow CO_{2(g)} + 3H_{2(g)}$
Ethylene glycol (C ₂ H ₆ O ₂)	$C_2H_6O_{2(aq)}+2H_2O_{(l)} \rightarrow 2CO_{2(g)} + 5H_{2(g)}$
Glycerol (C ₃ H ₈ O ₃)	$C_3H_8O_{3(aq)} + 3H_2O_{(l)} \rightarrow 3CO_{2(g)} + 7H_{2(g)}$
Acetate Sodium (C ₂ H ₃ O ₂ Na)	$C_2H_3O_2Na_{(aq)} + 3H_2O_{(l)} \rightarrow CO_{2(g)} + 4H_{2(g)} + NaHCO_{3(aq)}$
Formate (CH ₂ O ₂ Na)	$CHO_2Na_{(aq)} + H_2O_{(l)} \rightarrow H_{2(g)} + NaHCO_{3(aq)}$

Biomass Oxygenates	Reaction stoichiometry with in-situ CO ₂ capture
Methanol (CH ₃ OH)	$CH_4O_{(aq)} + M(OH)_{2(aq)} \rightarrow MCO_{3(s)} + 3H_{2(g)}$
Ethylene glycol (C ₂ H ₆ O ₂)	$C_2H_6O_{2(aq)} + 2M(OH)_{2(aq)} \rightarrow 2MCO_{3(s)} + 5H_{2(g)}$
Glycerol (C ₃ H ₈ O ₃)	$C_3H_8O_{3(aq)} + 3M(OH)_{2(aq)} \rightarrow 3MCO_{3(s)} + 7H_{2(g)}$
Acetate Sodium (C ₂ H ₃ O ₂ Na)	$C_2H_3O_2Na_{(aq)} + 2M(OH)_{2(aq)} + H_2O_{(l)} \rightarrow 2MCO_{3(s)} + 4H_{2(g)} + NaOH_{(aq)}$
Formate (CH ₂ O ₂ Na)	$CHO_2Na_{(aq)} + M(OH)_{2(aq)} \rightarrow MCO_{3(s)} + H_{2(g)} + NaOH_{(aq)}$
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 Oxygenate	Catalyst	Reactor	Time	Yield	Yield	Yield	Yield	Yield
		Mode	(hours)	H_2	CO ₂	CH ₄	СО	MCO ₃
 Methanol	No Catalyst	NA	1	0.05(±0.01)	0.1(±0.01)	0.0(±0.0)	0.00(±0.00)	0.00(±0.00)
Methanol	No Catalyst	NA	3	0.41(±0.05)	0.97(±0.11)	0.0(±0.0)	0.00(±0.00)	0.00(±0.00)
Methanol	No Catalyst	NA	6	0.97(±0.10)	2.39(±0.25)	0.0(±0.0)	0.00(±0.00)	0.00(±0.00)
Methanol	No Catalyst	M1	1	0.31(±0.05)	$0.00(\pm 0.00)$	0.0(±0.0)	0.00(±0.00)	5.35(±1.13)
Methanol	No Catalyst	M1	3	0.88(±0.09)	0.01(±0.01)	0.0(±0.0)	0.00(±0.00)	5.89(±1.82)
Methanol	No Catalyst	M1	6	3.21(±0.35)	$0.00(\pm 0.00)$	0.0(±0.0)	0.00(±0.00)	10.91(±0.68)
Methanol	No Catalyst	M2	1	0.11(±0.01)	$0.00(\pm 0.00)$	0.0(±0.0)	0.00(±0.00)	4.79(±0.64)
Methanol	No Catalyst	M2	3	3.45(±0.39)	$0.00(\pm 0.00)$	0.0(±0.0)	0.00(±0.00)	5.35(±1.40)
Methanol	No Catalyst	M2	6	4.82(±0.54)	$0.40(\pm 0.07)$	0.0(±0.0)	0.00(±0.00)	10.58(±4.33)
Methanol	Pt/Al ₂ O ₃	NA	1	54.80(±8.08)	61.16(±8.53)	0.99(±0.14)	0.00(±0.00)	0.00(±0.00)
Methanol	Pt/Al ₂ O ₃	NA	3	56.85(±6.76)	59.00(±6.98)	1.08(±0.13)	0.00(±0.00)	0.00(±0.00)
Methanol	Pt/Al ₂ O ₃	NA	6	64.49(±6.92)	70.42(±7.49)	1.33(±0.14)	0.54(±0.69)	0.00(±0.00)
Methanol	Pt/Al ₂ O ₃	M1	1	67.97(±7.40)	0.03(±0.01)	$0.04(\pm 0.08)$	0.00(±0.00)	77.35(±8.30)
Methanol	Pt/Al ₂ O ₃	M1	3	73.06(±8.48)	0.04(±0.01)	0.13(±0.01)	0.00(±0.00)	77.19(±8.49)
Methanol	Pt/Al ₂ O ₃	M1	6	76.23(±8.20)	0.11(±0.02)	0.19(±0.02)	0.00(±0.00)	88.37(±7.24)
Methanol	Pt/Al ₂ O ₃	M2	1	35.03(±3.94)	7.28(±2.41)	0.83(±0.10)	0.00(±0.00)	24.71(±2.10)
Methanol	Pt/Al ₂ O ₃	M2	3	70.96(±8.82)	2.51(±0.55)	0.44(±0.05)	0.00(±0.00)	62.83(±10.07)
Methanol	Pt/Al ₂ O ₃	M2	6	71.34(±6.07)	2.83(±1.67)	0.44(±0.02)	0.00(±0.00)	81.89(±1.35)

Table S2. Gas product yields for hydrothermal conversion of biomass oxygenates with and without an alkaline sorbent.

Methanol	Ni/Al ₂ O ₃	NA	1	18.31(±1.95)	32.26(±4.13)	20.79(±2.21)	0.00(±0.00)	0.00(±0.00)
Methanol	Ni/Al ₂ O ₃	NA	3	16.27(±2.59)	45.18(±6.23)	50.46(±7.38)	0.00(±0.00)	0.00(±0.00)
Methanol	Ni/Al ₂ O ₃	NA	6	12.59(±1.81)	44.15(±5.88)	57.89(±8.43)	0.00(±0.00)	0.00(±0.00)
Methanol	Ni/Al ₂ O ₃	M 1	1	56.43(±6.11)	0.02(±0.01)	5.63(±0.64)	0.00(±0.00)	73.09(±4.74)
Methanol	Ni/Al ₂ O ₃	M 1	3	59.47(±6.24)	0.02(±0.00)	5.43(±0.56)	0.00(±0.00)	78.86(±7.89)
Methanol	Ni/Al ₂ O ₃	M 1	6	57.04(±6.08)	0.50(±0.16)	6.78(±1.41)	0.00(±0.00)	72.40(±11.41)
Methanol	Ni/Al ₂ O ₃	M2	1	20.88(±2.23)	1.16(±0.30)	3.95(±0.46)	0.00(±0.00)	60.93(±1.45)
Methanol	Ni/Al ₂ O ₃	M2	3	48.58(±4.84)	0.09(±0.01)	5.01(±0.46)	0.00(±0.00)	65.00(±2.08)
Methanol	Ni/Al ₂ O ₃	M2	6	74.77(±7.54)	0.59(±0.17)	2.95(±0.31)	0.00(±0.00)	79.98(±10.05)
Formate	Ni/Al ₂ O ₃	NA	3	44.74(±9.05)	7.14(±0.78)	4.50(±1.02)	0.00(±0.00)	0.00(±0.00)
Formate	Ni/Al ₂ O ₃	M2	3	65.21(±3.86)	0.04(±0.04)	1.15(±0.06)	0.00(±0.00)	63.52(±0.34)
Formate	Pt/Al ₂ O ₃	NA	3	71.36(±4.02)	15.11(±1.02)	0.22(±0.02)	0.00(±0.00)	0.00(±0.00)
Formate	Pt/Al ₂ O ₃	M2	3	73.05(±4.54)	2.26(±1.54)	0.2(±0.02)	0.00(±0.00)	72.28(±2.38)
Acetate	Ni/Al ₂ O ₃	NA	3	2.14(±0.57)	1.88(±0.32)	0.71(±0.21)	0.00(±0.00)	0.00(±0.00)
Acetate	Ni/Al ₂ O ₃	M2	3	8.34(±0.78)	1.14(±0.17)	13.83(±1.20)	0.00(±0.00)	19.55(±2.21)
Acetate	Pt/Al ₂ O ₃	NA	3	3.25(±0.30)	12.31(±1.05)	33.47(±2.96)	0.00(±0.00)	0.00(±0.00)
Acetate	Pt/Al ₂ O ₃	M2	3	9.34(±0.91)	0.83(±0.22)	13.57(±1.17)	0.00(±0.00)	36.52(±2.29)
Glycerol	Ni/Al ₂ O ₃	NA	3	15.15(±0.19)	44.11(±1.99)	32.14(±1.28)	0.00(±0.00)	$0.00(\pm 0.00)$
Glycerol	Ni/Al ₂ O ₃	M2	3	73.38(±3.29)	0.12(±0.01)	7.09(±0.41)	0.00(±0.00)	73.94(±9.59)
Glycerol	Pt/Al ₂ O ₃	NA	3	49.88(±0.29)	61.89(±1.05)	15.74(±0.03)	0.00(±0.00)	0.00(±0.00)
Glycerol	Pt/Al ₂ O ₃	M2	3	68.59(±0.43)	1.86(±0.09)	$6.64(\pm 0.05)$	0.00(±0.00)	77.06(±11.86)
Ethylene Glycol	Ni/Al ₂ O ₃	NA	3	19.16(±0.23)	46.33(±2.09)	30.18(±0.18)	0.00(±0.00)	0.00(±0.00)

E	Ethylene Glycol	Ni/Al ₂ O ₃	M2	3	90.90(±0.02)	0.48(±0.01)	3.68(±0.02)	0.00(±0.00)	85.27(±2.44)
E	Ethylene Glycol	Pt/Al ₂ O ₃	NA	3	79.48(±1.12)	90.32(±1.28)	2.11(±0.04)	0.00(±0.00)	0.00(±0.00)
E	Ethylene Glycol	Pt/Al ₂ O ₃	M2	3	85.50(±0.72)	1.10(±0.18)	0.43(±0.01)	0.00(±0.00)	97.52(±1.15)

Phenomena	Reactions	Equilibrium Constant
Water dissociation	$H_2O_{(l)} \longrightarrow H^+_{(aq)} + OH^{(aq)}$	$Kw = 10^{-13.997}$
	$CO_{2(aq)} + H_2O_{(l)} \rightarrow H_2CO_3*_{(aq)}$	$k_1 = 10^{-1.46}$
CO ₂ hydration	$H_2CO_3*_{(aq)} \rightarrow HCO_3^{(aq)} + H^+_{(aq)}$	$k_2 = 10^{-6.33}$
	$HCO_3^{(aq)} \rightarrow CO_3^{2-}_{(aq)} + H^+_{(aq)}$	$k_3 = 10^{-10.33}$

Table S3. Summary of the Reactions Representing water dissociation and CO₂ hydration

To calculate the partial pressure of CO_2 in this systems, the maximum possible concentration of CO₂ was obtained by assuming complete conversion of methanol in Reaction 1, S.I Table 1. The concentrations of carbonic acid, bicarbonate (HCO³⁻), and carbonate (CO₃²⁻) species at total carbon supply between 0 – 1.05 M was computed using the equations below and the distribution is shown in S.I Figure 1.

 $[HCO_{3}(aq)] = ([H_{2}CO_{3}(aq)] * k_{2})/[H^{+}(aq)]$ (S.I 1)

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$$[CO_3^{2-}(aq)] = ([HCO_3^{-}(aq)] * k_3) / [H^+(aq)]$$
 (S.I 2)

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$$C_{TOT} = [H_2CO_3^*(aq)] + [HCO_3^-(aq)] + [CO_3^{2-}(aq)]$$
 (S.I 3)

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$$[H_2CO_3^*_{(aq)}] = C_{TOT} / (1 + (k_2 / [H^+_{(aq)}]) + ((k_2 * k_3) / ([H^+_{(aq)}]^2))$$
(S.I 4)

Phenomena	pH of feedstock solution without	pH of feedstock solution with		
	Ca(OH) ₂ in aqueous phase	Ca(OH) ₂ in aqueous phase		
Methanol (CH ₃ OH)	6.43	12.27		
Ethylene glycol (C ₂ H ₆ O ₂)	4.88	12.25		
Glycerol (C ₃ H ₈ O ₃)	5.09	12.25		
Acetate Sodium (C ₂ H ₃ O ₂ Na)	7.67	12.27		
Formate (CH ₂ O ₂ Na)	7.56	12.29		

Table S4. pH distribution of solutions.



Figure S1. XPS survey scan for a) Pt/Al₂O₃, and b) Ni/Al₂O₃.



2 Figure S2. a) FTIR spectra of 3wt% methanol, formate glycerol, ethylene glycol and acetate

3 feedstocks.) NMR spectra of 3wt% methanol, formate glycerol, ethylene glycol and acetate

4 feedstocks.



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Figure S3. Volume weighted particle size distributions for: (a) Ladle Slag before and after reaction using 3wt% model oxygenate bearing wastewater as feedstock, (b) Pt/Al₂O₃, catalyst before and after reaction using 3wt% methanol as feedstock in the absence of an alkaline sorbent, (c) Ni/Al₂O₃ catalyst before and after reaction using 3wt% methanol as feedstock in the absence of an alkaline sorbent, and (d) Ca(OH)₂ before and after reaction using 3wt% methanol as feedstock. Reactions were carried out at 50 bar and temperatures of 240 °C.





3 a closed system at maximum CO_2 concentration of ~ 1M.





Figure S5. NMR analysis for liquid product from reforming 3wt% methanol without a catalyst a) no catalyst and no alkaline sorbent, b) no catalyst with an alkaline sorbent using the mode 2 configuration. Reactions were carried out at 50 bar, and temperatures of 240°C.



Figure S6. NMR analysis for liquid product from reforming 3wt% methanol in the presence of a catalyst a) reforming was carried out over Pt/Al₂O₃ catalyst without an alkaline sorbent. b) reforming was carried out using Pt/Al₂O₃ catalyst with an alkaline sorbent using the mode 1 configuration c) reforming was carried out using Pt/Al₂O₃ catalyst with an alkaline sorbent using the mode 2 configuration. d) reforming was carried out over Ni/Al₂O₃ catalyst without an alkaline sorbent, e) reforming was carried out using Ni/Al₂O₃ catalyst with an alkaline sorbent using the mode 1 configuration f) reforming was carried out using Ni/Al₂O₃ catalyst with an alkaline sorbent using the mode 2 configuration Reactions were carried out at 50 bar, and temperatures of 240^oC.

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Figure S7. NMR analysis for liquid product from reforming 3wt% methanol, formate, glycerol, ethylene glycol, and acetate over a catalyst a) reforming was carried out over Ni/Al₂O₃ catalyst without an alkaline sorbent. b) reforming was carried out using Ni/Al₂O₃ catalyst with an alkaline sorbent using the mode 2 configuration. c) reforming was carried out over Pt/Al₂O₃ catalyst without an alkaline sorbent. d) reforming was carried out using Pt/Al₂O₃ catalyst with an alkaline sorbent using the mode 2 configuration.

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Figure S8. a) Number weighted particle size distributions and b) pore size distribution of catalysts
used for experiments.



2 Figure S9. DTG and DSC curve for Ni/Al₂O₃ and Pt/Al₂O₃ catalyst before and after reaction



Figure S10. a) FTIR pattern for Ni/Al₂O₃ and Pt/Al₂O₃ before and after using 3 wt% methanol

- 3 as feedstock.in the absence of an alkaline sorbent. b) XRD pattern for Ni/Al_2O_3 and Pt/Al_2O_3
- 4 before and after using 3wt% methanol as feedstock.in the absence of an alkaline sorbent.