Supplementary Information

Continuous flow hydrogenolysis of 5-hydroxymethylfurfural into 2,5-dimethylfuran over alumina-supported nickel-iron alloy catalysts

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5-HMF 2.5-DMF Т Time Р Catalyst **Reactor type** vield Solvent conv. Ref. (%) (°C) (h) (%) (bar) CuNi/Biochar THF 100 93.5 1 Batch reactor 220 6 40 2 FeCoNi/h-BN THF 180 Batch reactor 4.5 20 100 94 3 Co-CoO_x-FeNiCo/y-Al₂O₃ Batch reactor THF 190 10 100 99.9 4 4 Ni/ZrP Batch reactor THF 240 5 50 100 68.1 Ni₂In/MgO-Al₂O₃ 5 Batch reactor THF 200 10 10 100 93.2 NiCo THF 200 5 100 80.1 6 Batch reactor 4 7 Ni/WO₃ 180 >99 Batch reactor Water 6 10 96 8 NiZnAl Batch reactor 1,4-dioxane 180 12 15 100 93.6 NiZn 180 9 Batch reactor 2-propanol 20 100 99 4 10 NiFe/TiO₂ Batch reactor 1.4-dioxane 220 30 100 75 1 11 NiFe/CNT Batch reactor 1-butanol 200 3 30 100 91.3 Continuous fixed-bed reactor 12 $NiCu/ZrO_2$ (Gas phase) 1-butanol 275 WHSV=0.15 h⁻¹ 100 70 15 Continuous fixed-bed reactor 13 NiCu/Carbon WHSV=0.15 h⁻¹ (Gas phase) 1-butanol 275 15 100 45 Continuous fixed-bed reactor 14 THF NiCo/Carbon (Liquid phases) 130 WHSV=3.3 h⁻¹ 10 100 >90 Continuous fixed-bed reactor Ni_{0.74}Fe_{0.97}Al (Liquid phases) Ethanol 160 WHSV=0.3 h⁻¹ 40 100 90.5 This work

Table S1 Comparison of the catalytic performance for the hydrogenolysis of 5-HMF to 2,5-DMF over the Ni-based catalysts in batch and continuous operations

Catalysts	Weak acidic sites	Strong acidic sites		
	(mmol NH ₃ /g _{cat})	(mmol NH ₃ /g _{cat})		
Al ₂ O ₃	0.62	1.03		
FeAl	0.12	0.55		
Ni _{0.74} Fe _{0.97} Al	0.27	1.20		
NiAl	0.41	1.46		

 Table S2 Number of acidic sites obtained from the NH₃-TPD profiles of the reduced catalysts

Table S3 Elemental composition and physical properties of the fresh and spent $Ni_{0.74}Fe_{0.97}Al$ catalysts

Sample	Elemental c	ompositi	on (%) ^(a)	$S_{BET}^{}\left(b ight)$	$V_{p}^{(c)}$	$D_p^{(d)}$
	Fe	Ni	Al ₂ O ₃	$(m^2 g^{-1})$	$(cm^3 g^{-1})$	(nm)
Fresh Ni _{0.74} Fe _{0.97} Al	11.9	9.5	78.6	164.2	0.37	9.2
Spent Ni _{0.74} Fe _{0.97} Al	11.1	9.0	79.9	157.2	0.35	9.2

^a Elemental composition obtained from XRF measurement.

 $^{\text{b}}$ S_{BET} obtained from the adsorption branch of the N_2 isotherm.

 $^{\rm c}$ V_p calculated from N_2 adsorption at a relative pressure of ~0.99.

 d D_{p} obtained from the desorption branch using the BJH method.



Figure S1. N₂ (A) adsorption and (B) desorption isotherms of FeA1, (b) $Ni_{0.33}Fe_{1.02}A1$, (c) $Ni_{0.56}Fe_{1.03}A1$, (d) $Ni_{0.74}Fe_{0.97}A1$, (e) $Ni_{1.04}Fe_{0.98}A1$, and (f) NiAl catalysts



Figure S2. XPS survey of the reduced and passivated (a) NiA1, (b) FeA1, and (c) $Ni_{0.74}Fe_{0.97}A1$ catalysts



Figure S3. 5-HMF conversion and product yields on time-on-stream over $Ni_{0.74}Fe_{0.97}Al$ catalyst at a reaction temperature of 160 °C, H₂ pressure of 30 bar, and WHSV of 0.3 h⁻¹. The mole ratio of H₂ to 5-HMF was fixed at 1: 25.



Figure S4. XRD patterns of the (a) reduced and (b) spent $Ni_{0.74}Fe_{0.97}Al$ catalysts after a reaction temperature of 160 °C, H₂ pressure of 30 bar, WHSV of 0.3 h⁻¹, and 12 h time-on-stream.



Figure S5. Typical TEM images of the (a) reduced and (b) spent $Ni_{0.74}Fe_{0.97}Al$ catalysts after a reaction temperature of 160 °C, H₂ pressure of 30 bar, WHSV of 0.3 h⁻¹, and 12 h time-on-stream.



Figure S6. TGA profiles of the reduced and spent $Ni_{0.74}Fe_{0.97}Al$ catalysts after a reaction temperature of 160 °C, H₂ pressure of 30 bar, WHSV of 0.3 h⁻¹, and 12 h time-on-stream.

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