

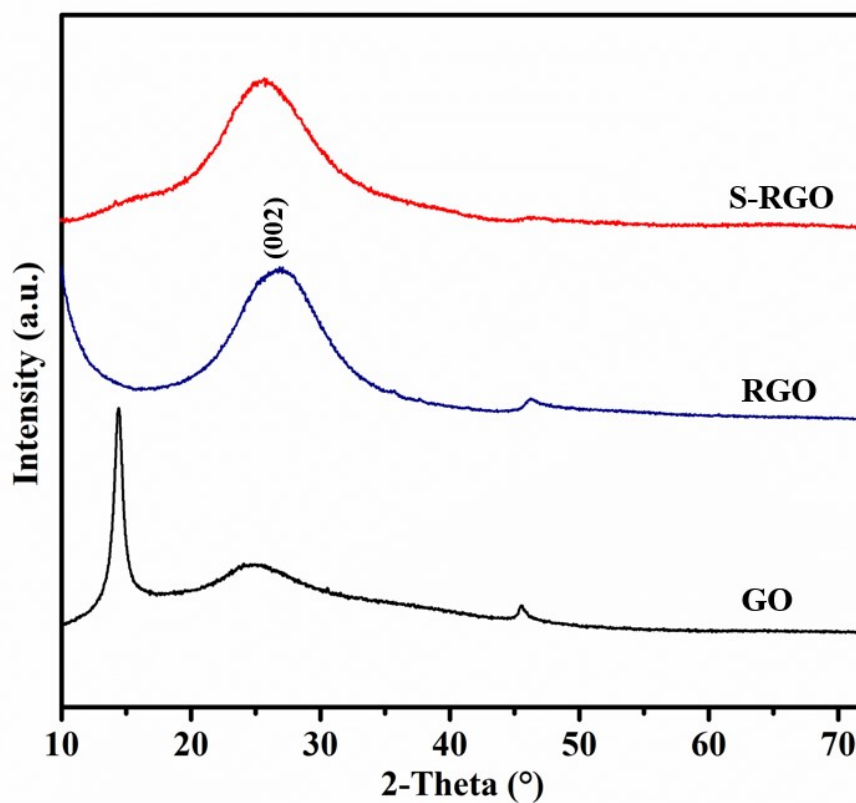
**Facile synthesis of ultralight S-doped Co<sub>3</sub>O<sub>4</sub> microflowers@reduced graphene oxide aerogel with defect and interface engineering for broadband electromagnetic wave absorption**

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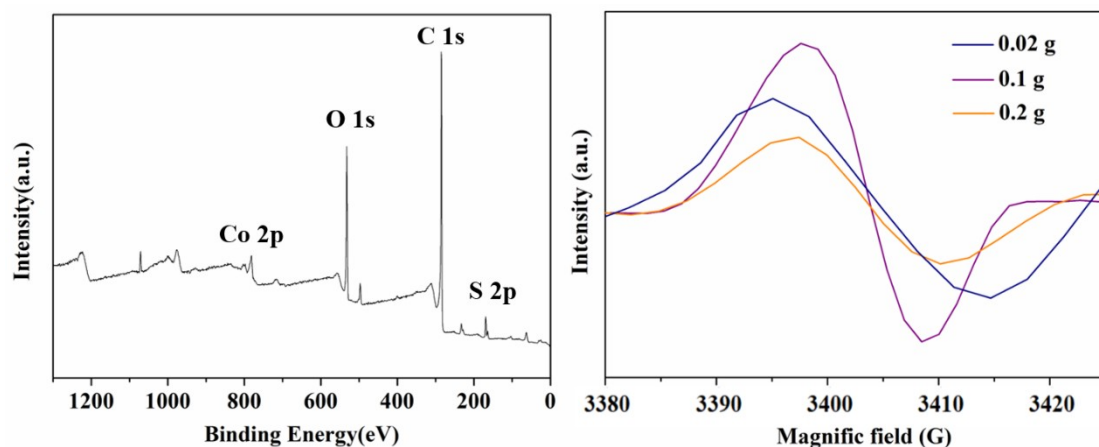
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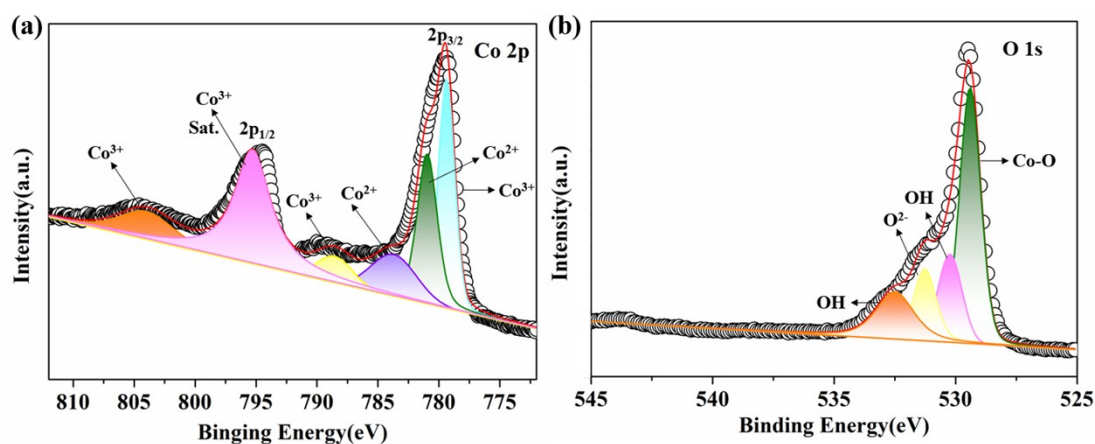
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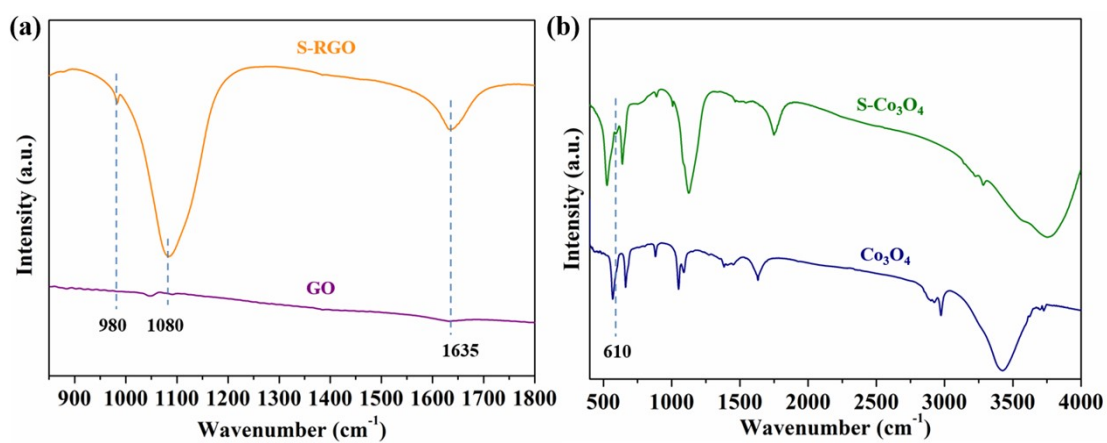
**Fig. S1.** XRD patterns of GO, RGO and S-RGO.



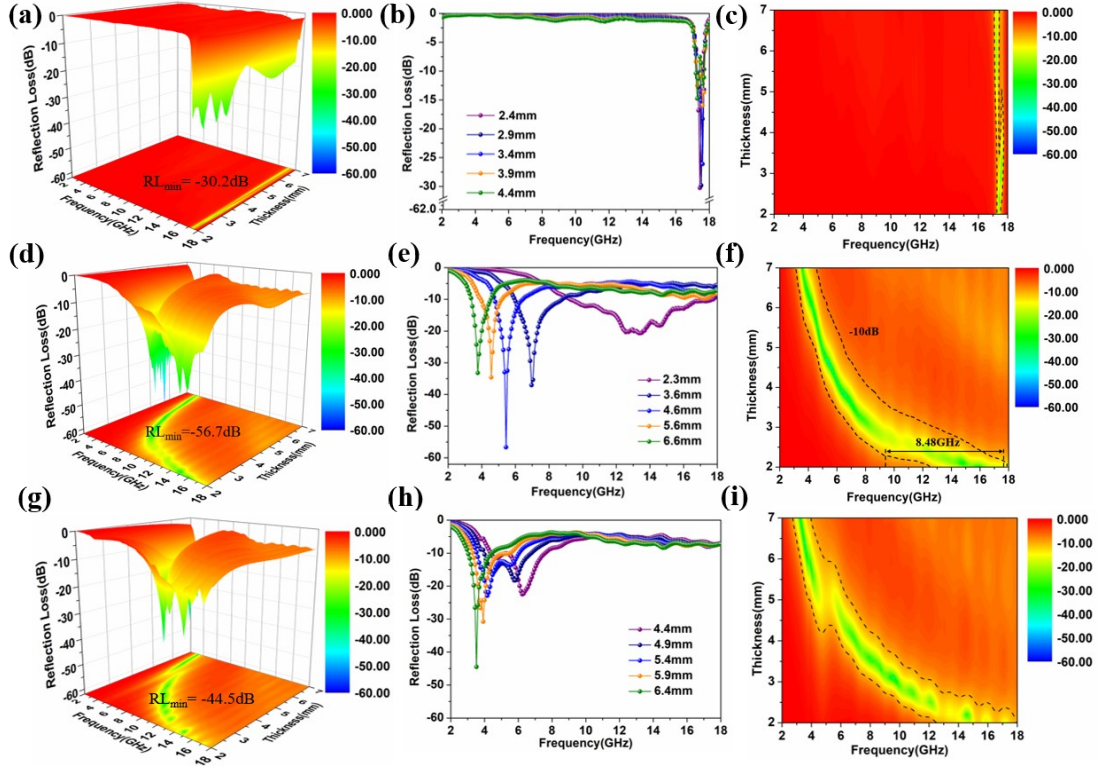
**Fig. S2.** (a) The survey scan spectrum of S-Co<sub>3</sub>O<sub>4</sub>@RGO aerogel, (b) EPR spectra of S-Co<sub>3</sub>O<sub>4</sub>@RGO-2, S-Co<sub>3</sub>O<sub>4</sub>@RGO-10 and S-Co<sub>3</sub>O<sub>4</sub>@RGO-20.



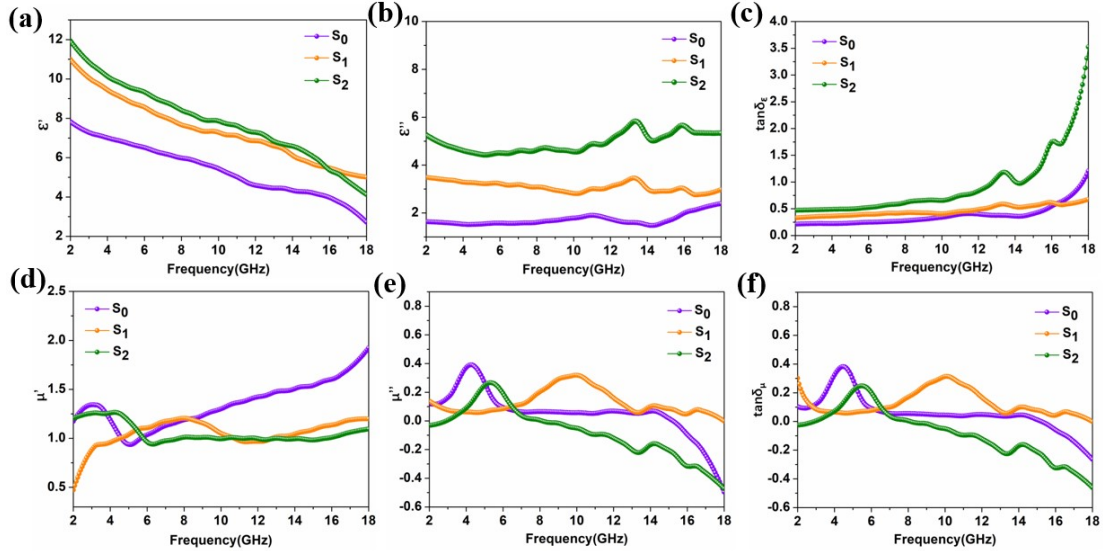
**Fig. S3.** XPS analysis of Co<sub>3</sub>O<sub>4</sub>: (a) Co 2p, (b) O 1s.



**Fig. S4.** FTIR spectra of (a) GO and S-RGO, (b) Co<sub>3</sub>O<sub>4</sub> and S-Co<sub>3</sub>O<sub>4</sub>.



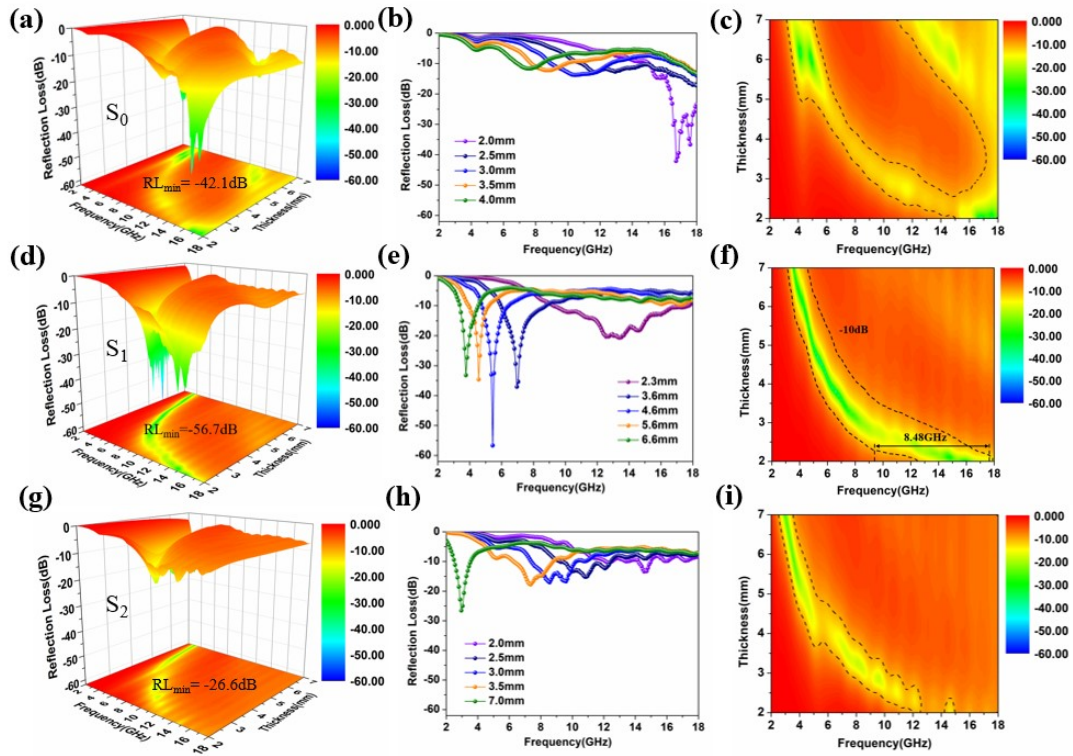
**Fig. S5.** 3D RL projection mappings, RL curves with different thickness and 2D RL contour maps of (a-c) S-Co<sub>3</sub>O<sub>4</sub>@RGO-2, (d-f) S-Co<sub>3</sub>O<sub>4</sub>@RGO-10, (g-i) S-Co<sub>3</sub>O<sub>4</sub>@RGO-20 with filling ratio of 5 wt.%.



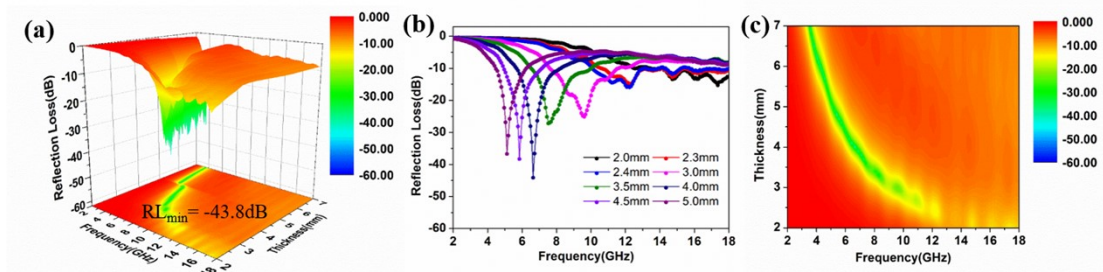
**Fig. S6.** (a, b) the  $\epsilon'$  and  $\epsilon''$  of complex permittivity, (c)  $\tan\delta_\epsilon$ , (d, e) the  $\mu'$  and  $\mu''$  of the complex permeability, (f)  $\tan\delta_\mu$  of S<sub>0</sub>, S<sub>1</sub> and S<sub>2</sub>.

To further investigate the effect of Co<sub>3</sub>O<sub>4</sub> and RGO ratios on the EMA properties,

three types of 3D S-Co<sub>3</sub>O<sub>4</sub>/RGO aerogels with different mass ratios of Co<sub>3</sub>O<sub>4</sub> and RGO (2:1, 1:1, 1:2) are prepared, marked as S<sub>0</sub>, S<sub>1</sub> and S<sub>2</sub>, respectively. As displayed in Fig. S6a-S6f, the  $\epsilon'$  values of S<sub>0</sub>, S<sub>1</sub> and S<sub>2</sub> decrease from 7.8 to 2.7, 11.1 to 5.3 and 12.0 to 4.2, respectively, while the  $\epsilon''$  values of S<sub>0</sub>, S<sub>1</sub> and S<sub>2</sub> maintain at 1.8, 3 and 5 in 2.0-18.0 GHz, respectively. With the increase of RGO mass fraction in the S-Co<sub>3</sub>O<sub>4</sub>@RGO composite, both the  $\epsilon'$  and  $\epsilon''$  values increase, which indicates the enhanced conduction loss and polarization relaxation. However, too excessive dielectric loss brings the mismatching between  $\epsilon_r$  and  $\mu_r$ . Then, EMW cannot enter the absorber, which is not favourable to the EMA. The RL<sub>min</sub> value of S<sub>0</sub> is -42.1 dB at 2.0 mm (Fig. S7a-S7c). As presented in Fig. S7d-S7f, the RL<sub>min</sub> value of S<sub>1</sub> can reach up to -56.7 dB at 5.44 GHz with the matching thickness of 3.6 mm. The RL<sub>min</sub> value of S<sub>2</sub> is -26.6 dB at 7.0 mm (Fig. S7g-S7i). From above discussion, the EMA performance of the S<sub>1</sub> sample is optimal. The 1:1 ratio of RGO/Co<sub>3</sub>O<sub>4</sub> endows the appropriate balance between good impedance matching and strong loss capability.



**Fig. S7.** 3D RL projection mappings, RL curves with different thickness and 2D RL contour maps of (a-c)  $S_0$ , (d-f)  $S_1$ , (g-i)  $S_2$  with filling ratio of 5 wt.%.



**Fig. S8.** (a) 3D RL projection mappings, (b) RL curves with different thickness and (c) 2D RL contour maps of  $R_2$  under 10 wt.% loading.



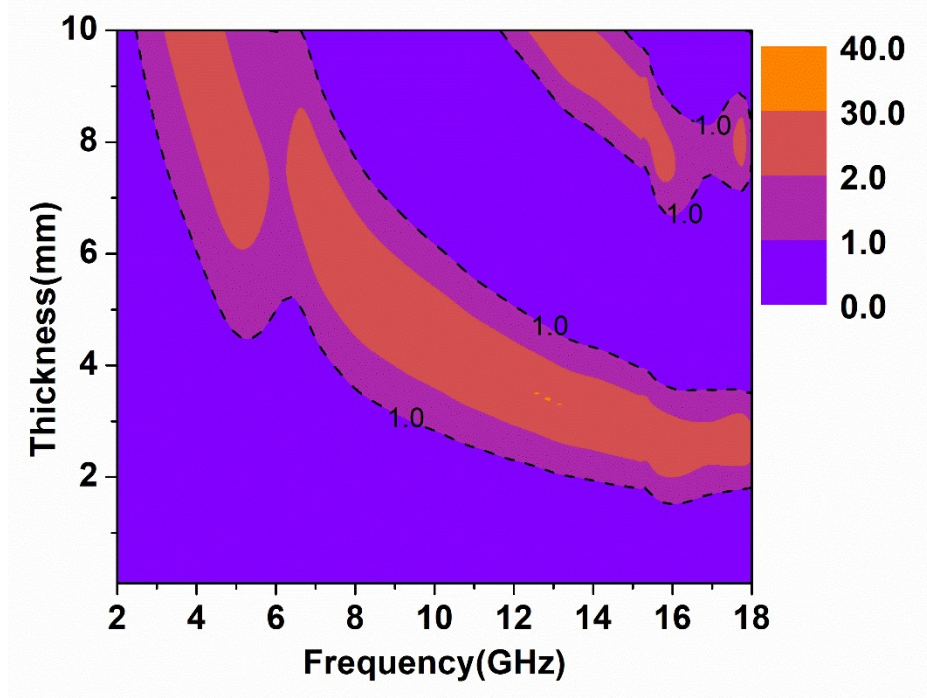


Fig. S9. Two-dimensional contour maps of  $|Z_{in}/Z_0|$  values of  $R_0$

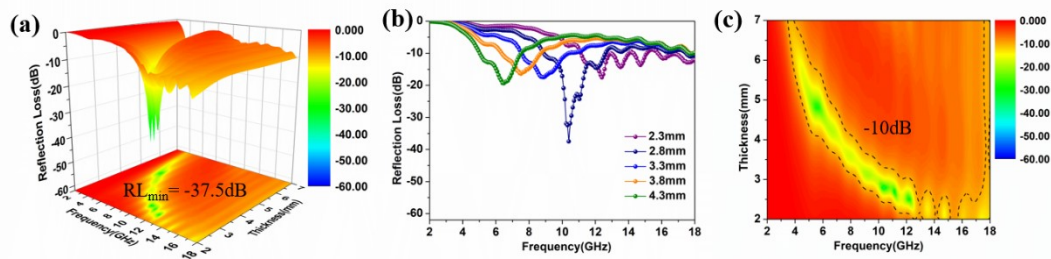


Fig. S10. (a) 3D RL projection mappings, (b) RL curves with different thickness and (c) 2D RL contour maps of  $R_4$  under 5 wt.% loading.

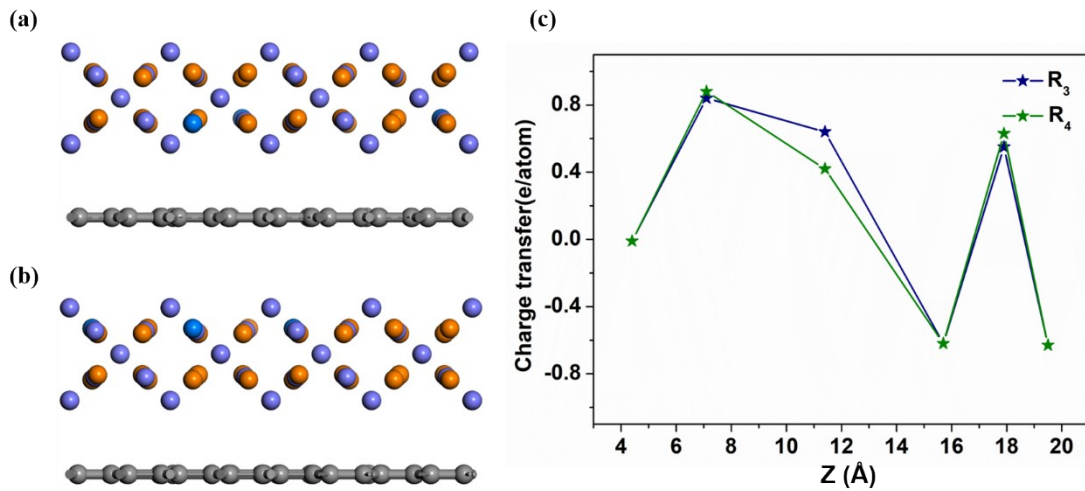
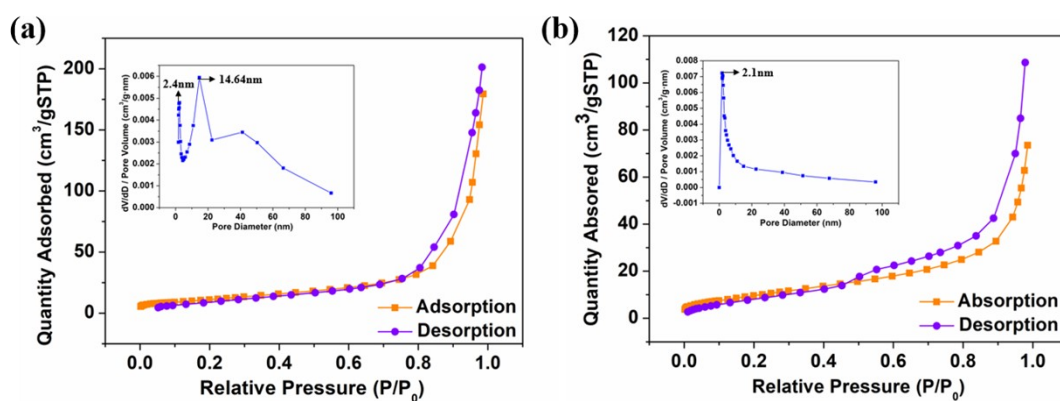


Fig. S11. The crystal structure models of (a)  $R_3$  and (b)  $R_4$ . (c) Charge transfer indicated

by variation of charge in each atomic layer along the z direction for  $R_3$  and  $R_4$  systems.

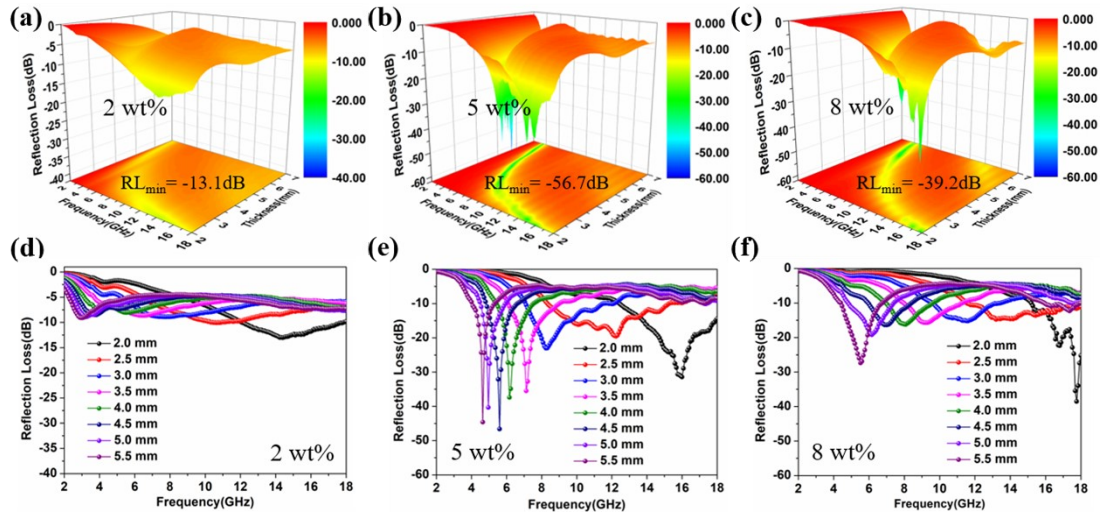
The pore size and surface area are obtained by the  $N_2$  adsorption-desorption isotherms and pore diameters of the synthesized composites. As seen in Fig. S12,  $Co_3O_4$  and  $S-Co_3O_4@RGO$  aerogels display type IV isotherm with an obvious hysteresis loop in the  $P/P_0$  range of 0-1.0, which indicates the presence of mesopores. Besides, the Barrett–Joyner–Halenda (BJH) pore size distribution analysis (the inset in Fig. S12) reveals that the average pore diameter of  $Co_3O_4$  is mainly concentrated in 2.4 nm and 14.64 nm, and the dominant pore size of  $S-Co_3O_4@RGO$  focuses on 2.1 nm. Benefiting from the high porosity, the mesoporous structure and high specific surface area, the 3D aerogel structure improves the reflection of EMW inside the material, and the air entering the pores can modulate the effective permittivity and impedance matching according to the Maxwell-Garnett model<sup>1,2</sup>.



**Fig. S12.**  $N_2$  adsorption (orange)-desorption (purple) isotherms with corresponding pore-size distributions in the inset for (a)  $Co_3O_4$  and (b)  $S-Co_3O_4@RGO$  composites.

To explore the influence of filler loading ratios on the EMW absorption properties, we perform the electromagnetic measurements of the sample of  $S-Co_3O_4@RGO$  with three different filler loading ratios.<sup>3</sup> As shown in the figure below, it can be found that

the values of  $RL_{\min}$  of S-Co<sub>3</sub>O<sub>4</sub>@RGO are -13.1 dB, -56.7 dB and -39.2 dB for the filler loading ratios of 2 wt%, 5 wt% and 8 wt%, respectively. Consequently, the S-Co<sub>3</sub>O<sub>4</sub>@RGO exhibits the optimal EMW absorption performance with the filler loading ratio of 5 wt%.



**Fig. S12.** 3D RL projection mappings of S-Co<sub>3</sub>O<sub>4</sub>@RGO with filling ratio of (a) 2 wt.%, (b) 5 wt.% and (c) 8 wt.%, RL curves with different thickness of S-Co<sub>3</sub>O<sub>4</sub>@RGO with filling ratio of (d) 2 wt.%, (e) 5 wt.% and (f) 8 wt.%.



**Table S1.** Typical EMW absorbers reported in recent literatures.

Samples	Ratios (wt.%)	d (mm)	f (GHz)	RL <sub>min</sub> (dB)	Bandwidth (GHz)	Ref.
Fe <sub>3</sub> O <sub>4</sub> /CNTs	30	3	7.12	-35.9	4.3	4
FeNi/RGO	20	3	11.12	-39.86	4	5
FeNi <sub>3</sub> @RGO/MoS <sub>2</sub>	40	2	14.72	-30.39	4.72	6
Co <sub>3</sub> O <sub>4</sub> Nanosheets/RGO	5	3.6	5.61	-45.15	5.61	7
Co <sub>3</sub> O <sub>4</sub> /Ni Foam	40	2.1	11.2	-41.1	3.46	8
PEDOT/RGO/Co <sub>3</sub> O <sub>4</sub>	50	2	10.7	-51.1	3.1	9
Co/C	40	4	5.8	-35.3	5.8	10
Fe <sub>3</sub> O <sub>4</sub> @SiO <sub>2</sub> /RGO	50	1.5	17.8	-26.4	2.6	11
Ni/RGO	20	9	13	-24.8	6.9	12
ZnFe <sub>2</sub> O <sub>4</sub> /SiO <sub>2</sub> /RGO	33	2.8	13.9	-43.9	6	13
S-Co <sub>3</sub> O <sub>4</sub> @RGO aerogels	5	3.6	5.44	-56.7	8.48	This work

**Table S2.** The binding energy calculation of T<sub>1</sub> and T<sub>2</sub> structures (eV).

Structures	E <sub>total</sub>	E <sub>1</sub>	E <sub>2</sub>	E <sub>b</sub>
T <sub>1</sub>	-102208.43	-10780.75	-15324.80	-76102.88
T <sub>2</sub>	-102212.45	-10780.75	-15324.80	-76106.90

The ease of forming a composite structure is characterized by the binding energy, which is defined as:  $E_b = E_{total} - E_1 - E_2$ , where E<sub>b</sub> is the binding energy, E<sub>1</sub> and E<sub>2</sub> represent the energy of different monomers, and E<sub>total</sub> is the total energy of the composite structure, respectively. The smaller the absolute value of E<sub>b</sub> is, the easier the structure is to form.

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