Supporting information Monitoring of n-hexane degradation in a plasma reactor by Chemical Ionization Mass Spectrometry

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Figure 1: Energy per pulse deduced from the current and voltage waveforms, for a sample of 1000 HV-pulses, effect of n-hexane on the discharge stability.

For the same parameters values as in figure 2 in the article, plotted in this figure are the values of E_{pulse} measured for a sample of 1000 HV-pulses, the first five hundred being for air whereas the others were captured while the air was rapidly replaced by the mixture containing 100 ppm of n-hexane at the fixed flow rate of 0.5 L/mn. For clean air, the mean energy is 3.90 mJ (with a standard deviation of 0.2 mJ), whereas it is slightly lower for the mixture with n-hexane, 3.75 mJ (with a standard deviation of 0.1 mJ). However, there is a clear effect of the hydrocarbon on energy fluctuation: it is significantly lower when n-hexane is present compared to clean air. In other words, the functioning of the pulsed dielectric barrier discharge is somewhat stabilized by the hydrocarbon. At a given value of the HV-pulse repetition frequency, the amplitude of the current waveform may vary a little bit from pulse to pulse, depending on the applied voltage but above all depending on the gas mixture type, i.e. without ("clean" air) or with the presence of the hydrocarbon molecules. This current fluctuation effect induces a fluctuation of the deposited energy in the plasma from pulse to pulse, as can be seen in the figure 1.



Figure 2: Timing diagram of the BTrap sequence.

Figure 2 shows the operating loop necessary for the real-time analysis of the gas stream:

- 1. The introduction of the precursor molecule $\rm H_2O$ at a pressure of 2.10^{-6} Torr for 10 ms.
- 2. The ionization of the H₂O molecule with a 70 eV electron beam $H_2O + e^- \rightarrow H_2O^+ + 2 e^-$. The generated H_2O^+ ions then need a sufficient amount of time to form the precursor ion H_3O^+ through reactions with H_2O molecules: $H_2O^+ + H_2O \rightarrow H_3O^+ + HO$.
- 3. The ejection of all ions excluding H_3O^+ , these unwanted ions were formed alongside H_3O^+ but are not necessary for the experiment.
- 4. The introduction of the gas sample, proton transfer reaction between the precursor H_3O^+ and the gas sample M takes place during this phase: $H_3O^+ + M \rightarrow H_2O + MH^+$. A delay of about (500 ms) is needed for the complete pumping of the cell to allow the pressure to drop to around 10^{-8} Torr.
- 5. RF excitation and detection of the signal.

Diffuorobenzene is injected at very low pressure (10^{-7} torr) for a few ms at the end of the experimental sequence as a calibrant for better mass identification. The reaction with O_2^+ precursor ion gives $C_6H_4F_2^+$ ion $(m/z \ 114.028)$ and with H_3O^+ ion, $C_6H_4F_2-H^+$ $(m/z \ 115.035)$.

General quantification formula for CI-MS In the data treatment step, we need to determine the intensity of each analyte A_i . If a single analyte A_i reacts with the precursor ion P^+ and shows fragmentation:

$$P^+ + A_i \to F_{ij}^+ \tag{1}$$

with j = 1...f, the intensities of all the fragments issued from A_i have to be summed:

$$I_{F_{i}^{+}} = \sum_{j} I_{F_{ij}^{+}}$$
(2)

For a complex mixture of analytes, most of the F_{ij}^{+} ions appearing in the mass spectrum are common to several analytes. These ions are therefore not characteristic of a single analyte A_i , and the sum of the corresponding $I_{F_{ii}}^{+}$ intensities does not give $I_{F_i}^{+}$.

An alternative solution for obtaining $I_{\mathrm{F_i^+}}$ consists in choosing a single fragment ion $\mathrm{F_{i1}^+}$ characteristic of $\mathrm{A_i}$, and dividing its intensity by the corresponding branching ratio α_{i1} . The products and branching ratios of the CI reaction of $\mathrm{A_i}$ are then supposed to be known, either from literature or better from measurements under the same experimental conditions, as done in the present work.

The molecular formula of F_{i1}^{+} requires a very careful choice, since F_{i1}^{+} must originate from the analyte A_i exclusively, with the highest possible intensity in comparison with the other F_{ij}^{+} fragments.

The absolute ion intensities $I_{F_i^+}$ are divided by I_{sum} , in order to obtain the relative intensities of each ion $[F_i^+]$, where sum represents the sum of the intensities of all detected ions.

The general quantification formula is based on the perfect gas law. At temperature T, it is expressed as follows, k_B being the Boltzmann constant, and $[A_i]$ (ppm) being the mixing ratio of A_i in the gas sample:

$$[A_{i}] = -\frac{ln(P^{+}) \cdot I_{F_{i}^{+}} \cdot k_{B} \cdot T \cdot 10^{6}}{(1 - (P^{+})) \cdot k_{i} \cdot P \cdot t}$$
(3)

For T = 298 K and accounting for unit conversion factors, the quantification formula becomes:

$$[A_{i}] = -\frac{ln(P^{+}) \cdot (F_{i}^{+}) \cdot 10^{6}}{(1 - (P^{+})) \cdot 3.21 \cdot k_{i} \cdot P \cdot t}$$
(4)

Where k_i (10⁻⁹ cm³·s⁻¹) represents the rate coefficient of the CI reaction P⁺ + A_i, an $P \cdot t$ (mbar·ms) represents the sample amount introduced in a gas pulse.

The above relationship can be used either to determine analyte concentrations if the rate constants are known (case of H_3O^+ precursor) or to determine rate constants and branching ratios if the sample composition is known (done with both precursors).

Fragments obtained from the reaction of the O_2^+ precursor with n-hexane are presented in figure 3. This figure shows the linearity of product ion intensities as a function of n-hexane mixing ratio.



Figure 3: Intensities of the products issued from O_2^{+} reaction with n-hexane as a function of n-hexane mixing ratio.

$$O_2^+ + C_6 H_{14} \to C_6 H_{14}^+ + O_2 \qquad 11\% \qquad (20\%) \qquad (5)$$

$$\rightarrow C_5 H_{11}^{+} + O_2 + C H_3 \qquad 3\% \qquad (5\%) \qquad (6) \rightarrow C_4 H_9^{+} + O_2 + C_2 H_5 \qquad 37\% \qquad (35\%) \qquad (7)$$

$$\rightarrow C_4 H_8^+ + O_2 + C_2 H_6 \qquad 32\% \qquad (25\%) \qquad (8)$$

$$\rightarrow C_3 H_7^{\ +} + O_2 + C_3 H_7 \qquad 8\% \qquad (5\%) \qquad (9)$$

$$\rightarrow C_3 H_6^{+} + O_2 + C_3 H_8 \qquad 8\% \qquad (10\%) \qquad (10)$$



Figure 4: H_2 mixing ratio at the exit of the DBD for mixing ratios of n-hexane in air (SED: 225 J/L, applied voltage: 23.4 kV, HV-pulse repetition frequency: 500 Hz, gas flow rate: 0.5 L/min).

Ozone generation in a non-thermal plasma [1]–[3] can be simplified by the following reactions:

The initial step in forming O_3 is the electron impact dissociation of molecular O_2 :

$$O_2 + e^- \to O(^{3}P) + O(^{3}P) + e^-$$
 (11)

$$O_2 + e^- \to O(^1D) + O(^3P) + e^-$$
 (12)

$$O(^{1}D) + M \rightarrow O(^{3}P) + M$$
(13)

The addition of a molecule in the air plasma, n-hexane in this case, leads to a decrease in the measured mixing ratio of ozone as illustrated by the results presented in figure 5. This can be explained by the consumption of atomic oxygen in oxidation reactions at the expense of ozone formation.

Since the degradation of most VOCs in air plasma is mainly initiated by atomic oxygen, measuring ozone mixing ratio in the plasma reactor is a good method to assess the capacity of the plasma to oxidize a VOC or a hydrocarbon via the formation of oxygen atom.

5 ppm	0.009	0.007	2.15536	0	0.0976	0.001	0	0.198	0.015	0	0	0.010	0.068	0.002	0.030	0.039	0.004	0	0.026
10 ppm	0.01534	0.023	4.887	0.006	0.220	0.026	0.090	0.381	0.034	0	0.009	0.006	0.130	0	0.060	0.126	0.017	0.010	0.037
17.5 ppm	0.036	0.046	7.273	0.033	0.425	0.048	0.374	0.658	0.048	0.002	0.054	0.032	0.223	0.018	0.103	0.265	0.024	0.001	0.086
$25 \ \mathrm{ppm}$	0.046	0.057	10.022	0.043	0.558	0.087	0.672	0.828	0.068	0.066	0.060	0.062	0.318	0.048	0.151	0.411	0.047	0.032	0.115
37.5 ppm	0.075	0.088	13.847	0.095	0.827	0.159	1,324	1,130	0.091	0.263	0.143	0.093	0.473	0.055	0.224	0.681	0.082	0.138	0.200
$50 \ \mathrm{ppm}$	0.086	0.104	17.431	0.146	1,043	0.218	2,003	$1,\!438$	0.089	0.465	0.185	0.130	0.604	0.131	0.292	0.954	0.109	0.190	0.253
k	3.33	0.89	1.84	2.3	2.4	1.64	3.09	1.2	1.81	3.13	2.2	3.7	1.6	1.91	2.96	2.05	3	4	2.7
Attribution	hydrogen cyanide	nitrogen oxyde	formaldehyde	methanol	ketene	propene	acetaldehyde	nitrogen dioxyde	nitrous acid	propanal	acetic acid	nitromethane	nitric acid	pentene	methyl nitrate	hexene	ethyl nitrate	hexanal	PAN
Ion	$\rm HCN-H^+$	NO^+	$\rm COH_2-H^+$	CH_4O-H^+	$\mathrm{C_2H_2O-H^+}$	$C_3H_6-H^+$	$\mathrm{C_2H_4O-H^+}$	NO_{2}^{+}	$\rm NO_2H-H^+$	$C_3H_6O-H^+$	$\mathrm{C_2H_4O_2-H^+}$	$CH_3NO_2-H^+$	$\rm HNO_{3}-H^{+}$	$\mathrm{C_5H_{10}-H^+}$	$\rm CH_3NO_3-H^+$	$\mathrm{C_6H_{12}-H^+}$	$\mathrm{C_2H_5NO_3-H^+}$	$\mathrm{C_6H_{12}O-H^+}$	$C_2H_3NO_5-H^+$
Exact mass (u)	28.019	29.998	31.018	33.034	43,018	43,055	45.034	45.993	48.008	59.05	61.029	62.024	64.003	71.086	78.019	85.102	92.035	101.097	122.009

Table 1: Mixing ratios of the by-products detected with H_3O^+ precursor as a function of the mixing ratio of n-hexane injected with their rate coefficients k (10⁻⁹ cm³s⁻¹) (SED: 225 J/L, applied voltage: 23.4 kV, HV-pulse repetition frequency: 500 Hz, gas flow rate: 0.5 L/min).



Figure 5: Measurement of ozone mixing ratio at the exit of the DBD for mixing ratios of n-hexane in air up to 200 ppm (SED: 225 J/L, applied voltage: 23.4 kV, HV-pulse repetition frequency: 500 Hz, gas flow rate: 0.5 L/min).

For the heaviest compounds, where several isomers are possible, quantification is carried out using an average value for the rate coefficient. Attributions and rate coefficients obtained from the PTR library (Pagonis, D., Sekimoto, K., & de Gouw, J. (2019)).

References

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