Supporting Information

Boosting ammonia synthesis activity of ceria-supported Ru catalyst achieved through trace Pr addition

Chunyan Li^{a,b}, Zecheng Zhang^b, Lingyun Zhou^a, Biyun Fang^b, Jun Ni^b, Jianxin Lin^b,

Bingyu Lin^{*}^b, and Lilong Jiang^{*}^b

^a Key Laboratory of Low-Dimensional Materials and Big Data, School of Chemical Engineering,

Guizhou Minzu University, Guiyang 550025, China

^b National Engineering Research Center of Chemical Fertilizer Catalyst, College of Chemical

Engineering, Fuzhou University, Fuzhou 350002, Fujian, China

E-mail: bylin@fzu.edu.cn (Bingyu Lin); jll@fzu.edu.cn (Lilong Jiang); Fax: +86 0591-83738808; Tel: +86 0591-

83731234

1. Preparation of Samples

The CeO₂ and Pr-doped CeO₂ with 0.1% content were prepared using the hydrothermal method. Typically, 8 mmol of Ce(NO₃)₃•6H₂O in 20 mL distilled water was added into 1 mol NaOH aqueous solution (140 mL), and stirred at 50 °C for 0.5 h. The mixture solution was held at 100 °C for 24 h in an autoclave. The separated resultant product was washed with distilled water and ethanol to control the pH to neutral, dried at 60 °C overnight, and finally calcined at 550 °C for 4 h. The Pr-doped CeO₂ simple with the Pr/Ce mole ratio of 0.1% was prepared in a similar procedure.

The Ru catalysts were obtained using ruthenium nitrosyl nitrate solution (1.5% w/v) as Ru precursor by impregnation method, and the loading of Ru was fixed at 3wt%. The as-prepared simples were then reduced in $25\%N_2$ -75%H₂ at 400 °C for 6 h and labeled as Ru/CeO₂ and Ru/PrCe.

2. Catalysts evaluation and Characterization

2.1 Catalysts evaluation

Ammonia synthesis was carried out in a continuous flow fixed-bed stainless steel reactor (inner diameter = 12 mm). Prior to reaction, the catalyst (0.2 g, 32–60 mesh) was diluted with quartz sand of similar size and reduced in a stoichiometric H_2 – N_2 gas mixture at 500 °C for 6 h. There were no external and internal diffusion limitations under the conditions adopted in this work.^{1, 2} Catalyst evaluation was conducted after the reaction was maintained for more than 3 h under a selected condition. The produced ammonia was trapped by sulfuric acid solution and then analyzed by ion chromatography (Thermo Scientific, ICS-600); subsequently, the reaction rates and TOF values were calculated according to the following equations:

reaction rate =
$$\frac{\text{mol of NH}_{4}^{+}}{\text{mass of catalyst (g) × time (h)}}$$

TOF = $\frac{\text{mol of NH}_{4}^{+}}{\text{mol of metallic Ru atom × time (s)}}$

2.2 Catalysts Characterization

Transmission electron microscopy (TEM) and high-angle annular dark-field scanning transmission electron microscopy (HAADF-STEM) images were obtained by a FEI Tecnai G2 F30 microscope. The Brunauer–Emmett–Teller (BET) surface area, pore volume, and pore size distribution of the samples were measured with an ASAP 2020M instrument using adsorption of N₂ at 77 K. Prior to adsorption analysis, the catalysts were degassed in a flowing N₂ at 300 °C for 3 h. The phase purity and crystal structure of the catalysts were examined by X-ray diffraction (XRD, PANalytical X'Pert3 Powder diffractometer), using Cu K α radiation (λ =0.154 32 nm). Raman spectra of samples were acquired on an InVia Reflex Raman microscope equipped with a 532 nm laser.

Diffuse reflectance infrared Fourier transform spectroscopy (DRIFTS) was measured on a Nicolet 6700 spectrometer operated at a resolution of 4 cm⁻¹ with 32 scans. For CO adsorption measurements, For CO adsorption measurements of fresh catalysts, the samples were reduced in hydrogen at 500 °C for 6 h, then purged with He and cooled down to 50 °C. After the collection of background spectrum, the

sample was exposed to 5% CO/He (50 mL/min) for 10 min. To acquire the information related to deuterium species, the sample was reduced at 500 $^{\circ}$ C in H₂ and then cooled down to 50 $^{\circ}$ C in a flow of He.

Hydrogen temperature-programmed reduction (H₂-TPR) of as-prepared catalysts was carried out on a Micromeritics AutoChem II 2920. The catalyst (100 mg, sieve fraction 0.30–0.56 mm) was pretreated in Ar at 150 °C for 60 min and then cooled to -20 °C. Afterward, the samples were heated in a flow of 10% H₂/Ar mixture (30 mL min⁻¹) to 600 °C at a rate of 10 °C min⁻¹. Temperature-programmed desorption (TPD) experiment was also performed using the same AutoChem II 2920 equipment. A sample (100 mg) was reduced in H₂ at 500 °C for 6 h, and then purged with Ar and cooled to 400 °C. Afterwards, the gas flow was switched to H₂ for sample exposure at 400 °C for 1 h. After cooling to 50 °C, the sample was purged with Ar for 1 h, and then heated to 600 °C at a rate of 10, 20 and 30 °C/min.

X-ray photoelectron spectroscopy (XPS) measurement was recorded on an ESCALAB 250Xi photoelectron spectrometer (Thermo Fisher Scientific). Charging effects were corrected by adjusting the main C 1s peak to a position of 284.6 eV. For the fresh catalysts, the sample was first reduced at 500 °C for 6 h in a flow of 5% H₂/Ar mixture (30 mL/min) in the pretreatment chamber. After cooling down to room temperature, the catalyst was transferred into the analysis chamber for XPS acquisition without exposure to air.

3 Computational details

3.1 Computational methods

Density functional theory (DFT) executed in the Vienna ab initio simulation package (VASP6.3.3) were used for all the calculations³⁻⁶. Exchange and correlation were treated within the Perdew-Burke-Ernzerhof (PBE) generalized gradient approximation (GGA)⁷. The valence electrons were described by a plane wave basis set with the kinetic cutoff energy of 400 eV, and the core electrons were replaced by the projector augmented wave (PAW) pseudopotentials^{8, 9}. DFT + U corrections were applied to describe

the 4f orbitals of Ce and Pr with the value of U - J = 4.5 eV and 6.0 eV, respectively, which were proposed by previous works^{10, 11}. The Hellman-Feynman forces on each ion were lower than 0.03 eV/Å for all the structures.

The adsorption energy (ΔE_{ads}) was given by Eq(1), in which E_{total} was the total energy of the whole system upon adsorption, E_{mol} was the energy of the gas-phase molecule, and E_{slab} was the energy of the clean slab.

The energy for the formation of oxygen vacancy (ΔE_{Ovac}) was calculated by Eq(2).

$$\Delta E_{\text{Ovac}} = (E_{\text{slab-Ovac}} + E_{\text{O}}) - E_{\text{slab}}$$
 Eq(2)

Where E_{O} and E_{slab-O} represented the energies of O atom and slab without the O atom.

3.2 Theoretical models

The CeO₂(111) surface was modelled by a (3×3) supercell with symmetric nine-layer, which was separated by a 15 Å vacuum layer, and a $3\times3\times1$ Monkhorst-Pack procedure¹². This model is equal to three stoichiometric layers of CeO₂. The Pr modified model was constructed by replacing a Ce in the top layer of CeO₂(111), denoted as PrCeO₂(111) (see Fig. Sx). Four-layer Ru(0001) was constructed with (3 × 3) supercell. Due to the complexity of the catalysts synthesized in the experiment, a relatively simplified model was used to decouple the role of Pr. In order to obtain data faster, we used a single Ru adsorbed on the surface before and after Pr modification to form a Ru catalyst loaded on CeO₂. We put Ru on a oxygen vacancy to get the Ru model, similar with previous work¹³.

4. Mass and Heat Transfer Calculations for Ammonia Synthesis over Ru/CePr

Mass and Heat Transfer Calculations for Ammonia Synthesis on Ru/CePr

Mears Criterion for External Diffusion (Fogler, p841; Mears, 1971)

If
$$\frac{-r_A' \rho_b Rn}{k_c C_{Ab}} < 0.15$$
, then external mass transfer effects can be neglected.

 $-r_A'$ = reaction rate of nitrogen, kmol/kg-cat·s

n = reaction order with respect to N₂ (e.g. K. Aika et al, Appl. Catal., 28(1986) 57-68).

R = catalyst particle radius, m

 ρ_b = bulk density of catalyst bed, kg/m³

 C_{Ab} = bulk gas concentration of nitrogen, kmol/m³

 k_c = mass transfer coefficient, m/s

$$\frac{-r_{A}^{'}\rho_{b}Rn}{k_{c}C_{Ab}} = [3.3 \text{ x } 10^{-6} \text{ kmol-N}_{2}/\text{kg-cat} \cdot \text{s}] [910 \text{ kg/m}^{3}][3 \text{ x } 10^{-4} \text{ m}][1]/([1.7 \text{ m/s}]*[0.045$$

kmol/m³])= 1.2x10⁻⁵ <0.15 {Mears for External Diffusion}

Weisz-Prater Criterion for Internal Diffusion (Fogler, p839)

If
$$C_{WP} = \frac{-r'_A \rho_c R^2}{D_e C_{Ab}} < 1$$
, then internal mass transfer effects can be neglected

 $-r_A'$ = reaction rate of nitrogen, kmol/(kg-cat·s)

- ρ_c = solid catalyst density (kg m⁻³)
- R = catalyst particle radius, m
- ρ_b = bulk density of catalyst bed, kg/m³

 C_{Ab} = bulk gas concentration of nitrogen, kmol/m³

- $k_c = mass transfer coefficient, m/s$
- D_e = effective gas-phase diffusivity, m²/s

$$C_{WP} = \frac{-r'_{A} \rho_{c} R^{2}}{D_{e} C_{Ab}} = [3.3 \text{ x } 10^{-6} \text{ kmol-N}_{2}/\text{kg-cat} \cdot \text{s}] \times [4 \times 10^{3} \text{ kg-cat/m}^{3}] \times [3 \text{ x } 10^{-4} \text{ m}]^{2} / ([3.34 \text{ m}]^{2} + (3.34 \text{ m})^{2})]$$

 $x \ 10^{-6} \ m^2/s] \times [0.045 \ kmol/m^3]) = \ \textbf{7.9x10^{-3} < 1} \quad \{ \textbf{Weisz-Prater Criterion for Internal} \\ \label{eq:weiss}$

Diffusion}

Mears Criterion for External (Interphase) Heat Transfer (Fogler, p842)

$$\left|\frac{-\Delta H_r(-r_A')\rho_b RE}{h_t T_b^2 R_g}\right| < 0.15$$

 $[136.9 \text{ kJ/mol} \times 3.3 \text{ x } 10^{-6} \text{ kmol} \cdot \text{N}_2/(\text{kg-cat} \cdot \text{s}) \times 910 \text{ kg-cat/m}^3 \times 3 \text{ x } 10^{-4} \text{ m} \times 150 \text{ kJ/mol}] / [185.3 \text{ kJ/m}^2.\text{K.s} \times 673^2 \text{ K}^2 \times 8.314 \times 10^{-3} \text{ kJ/mol}.\text{K}] = 2.7 \text{x} 10^{-5} < 0.15$ {Mears Criterion for External

(Interphase) Heat Transfer}

Mears Criterion for Combined Interphase and Intraparticle Heat and Mass Transport (Mears,

$$\frac{-r'_{A}R^{2}}{C_{Ab}D_{e}} < \frac{1+0.33\gamma\chi}{|n-\gamma_{b}\beta_{b}|(1+0.33n\omega)}$$

$$\gamma = \frac{E}{R_{g}T_{s}}; \gamma_{b} = \frac{E}{R_{g}T_{b}}; \beta_{b} = \frac{(-\Delta H_{r})D_{e}C_{Ab}}{\lambda T_{b}}; \chi = \frac{(-\Delta H_{r})-r'_{A}R}{h_{t}T_{b}}; \omega = \frac{-r'_{A}R}{k_{c}C_{Ab}}$$

 γ = Arrhenius number; β_b = heat generation function;

 λ = catalyst thermal conductivity, W/m.K;

 χ = Damköhler number for interphase heat transport

 ω = Damköhler number for interphase mass transport

$$\frac{-r'_{A} \rho_{b} R^{2}}{C_{Ab} D_{e}} = [3.3 \text{ x } 10^{-6} \text{ kmol-N}_{2}/\text{kg-cat} \cdot \text{s} \times 910 \text{ kg-cat/m}^{3} \times (3 \text{ x } 10^{-4})^{2} \text{ m}^{2}]/([3.34 \text{ x } 10^{-6} \text{ m}^{2}/\text{s}])$$

 \times [0.045 kmol/m³])= 1.8x10⁻³

$$\frac{1+0.33\gamma\chi}{\left|n-\gamma_{b}\beta_{b}\right|\left(1+0.33n\omega\right)}=2.25$$

Left member < Right member {Mears Criterion for Interphase and Intraparticle Heat and Mass

Transport }

	Rate	TOF ^a	Reaction	SV	Re
Samples	$(\mu mol g^{-1} h^{-1})$	(Ru atom ^{-1} s ^{-1})	conditions	$(mL g^{-1} h^{-1})$	f.
Ru(3%)/CePr	23 500	22.6×10 ⁻³	1MPa, 400 °C	36 000	This
Ru(3%)/CeO ₂	16 500	15.9×10 ⁻³	1MPa, 400 °C	36 000	
Ru(3%)/CePr-CO	13 000	12.5×10 ⁻³	1MPa, 400 °C	36 000	
Ru(3%)/Pr ₂ O ₃	16 800	16.2×10 ⁻³	1MPa, 400 °C	36 000	
$Ru(3\%)/PrO_x$ -CeO ₂	19 200	18.5×10 ⁻³	1MPa, 400 °C	36 000	
Ru(3%)/CePr(0.5 mol%Pr)	18 635	18.0×10 ⁻³	1MPa, 400 °C	36 000	work
Ru(3%)/Ti-Ce-S	14 580	14.1×10 ⁻³	1MPa, 400 °C	36 000	14
Ru(3%)/Ti _{0.18} -Ce	18 912	18.7×10 ⁻³	1MPa, 400 °C	36 000	15
	23 028	22.7×10^{-3}	1MPa, 400 °C	72 000	
Ba-Ru(5%)/Al ₂ O ₃	2 796	1.7×10 ⁻³	1MPa, 400 °C	36 000	16
	2 083	1.3×10 ⁻³	1MPa, 400 °C	18 000	
Ru(0.25%)/CeO2	1 950	21.9×10 ⁻³	1 MPa, 400 °C	36 000	17
	2 647	29.8×10 ⁻³	1 MPa, 400 °C	72 000	
Ru(3%)/CeO ₂	22 075	21.3×10 ⁻³	1 MPa, 400 °C	36 000	
SC-Ru(1%)/CeO ₂	6 909	19.6×10 ⁻³	1MPa, 400 °C	36 000	18
Ru(1%)/CeO ₂ -N ₂ H ₄	5 521	15.6×10 ⁻³	1MPa, 400 °C	36 000	19
Ru(1%)/CeO ₂ -BH	5 454	15.4×10 ⁻³	1 MPa, 400 °C	36 000	20
Ru(3%)/Ti _{0.18} -Ce	18 912	18.7×10 ⁻³	1MPa,400°C	36 000	
Ru(10%)/Ba-Ca(NH ₂) ₂	50 000	14.0×10 ⁻³	0.9MPa,400°C	36 000	21
Ru(6%)-Cs/MgO	23 000	6.5×10 ⁻³	0.9MPa,360°C	36 000	
Ru(10%)/Ba-Ca(NH ₂) ₂	60 400	16.9×10 ⁻³	1 MPa, 400 °C	36 000	
Ru(9.1%)-Ba/AC	8 285	2.6×10 ⁻³	1 MPa, 400 °C	18 000	22
Ru(6%)-Cs/MgO	12 117	5.7×10 ⁻³	1 MPa, 400 °C	18 000	
Ru(4%)/C ₁₂ A ₇ :e ⁻	6 089	4.3×10 ⁻³	1 MPa, 400 °C	18 000	
Ru(7.8%)/Y ₅ Si ₃	4 100	1.5×10 ⁻³	1 MPa, 400 °C	18 000	23
Ru(4%)/r-CeO2	3 830	2.7×10 ⁻³	1 MPa, 400 °C	18 000	24

Table S1 Catalytic performance of Ru-based catalysts on various supports.

Ru(4%)/c-CeO ₂	1 289	0.9×10 ⁻³	1 MPa, 400 °C	18 000	
Ru(4%)/p-CeO ₂	529	0.4×10^{-3}	0.9MPa,400°C	18 000	
Ru(5%)/CeO ₂	7 200	4.0×10 ⁻³	0.9MPa,400°C	18 000	25
Ru(5%)/MgO	1 800	1.0×10^{-3}	0.1MPa,400°C	18 000	
Ru(1.8%)/LaScSi	28 00	×10 ⁻³	1 MPa, 400 °C	18 000	
Ba-Ru(5%)/Al ₂ O ₃ -980	7 217	4.5×10 ⁻³	5 MPa, 400 °C	60 000	26
Cs-Ru(1%)/MgO	2 700	1.0×10^{-3}	5 MPa, 400 °C	66 000	27
Ru(1%)/BaTiO ₃	4 100	1.5×10^{-3}	1 MPa, 400 °C	66 000	
Ru(5%)/La _{0.5} Ce _{0.5} O _{1.75}	65 000	36.5×10 ⁻³	1 MPa, 400 °C	72 000	28
$Ru(5\%)/La_{0.5}Pr_{0.5}O_{1.75}$	60 200	33.8×10 ⁻³	1 MPa, 400 °C	72 000	29

^a based on total number of Ru atoms

Table 52 The compositions of Ru catalysis obtained from Ref analysis.				
		Ru (wt.%)		
Sample	Pr (wt.%)	Theoretical value (wt. %)	Actual value (wt. %)	
Ru/CeO ₂		2.90	2.40	
Ru/CePr	0.08		2.35	

Table S2 The compositions of Ru catalysts obtained from ICP analysis.

C 1	Surface area	Pore volume	Average pore size
Samples	$(m^2 g^{-1})$	(cm^3g^{-1})	(nm)
CeO ₂	71	0.3	17
CePr	79	0.4	19
Ru/CeO ₂	63	0.3	20
Ru/CePr	63	0.4	24

Table S3 Textural properties of Ru catalysts with different reduction conditions.

	Ru/CeO ₂		Ru/CePr		
Region	Binding	Binding FWHM	Binding energy	FWHM	
	energy	1 00 1100	Dinang energy	1 ((111))	
C 1s	284.60	1.14	284.60	1.14	
	285.25	1.72	285.42	1.65	
	289.04	3.07	289.09	3.15	
Ru 3d 5/2	279.62	0.91	279.54	0.91	
	280.25	1.44	280.31	1.44	
	282.69	1.94	282.74	1.94	
O 1s	529.15	1.12	529.15	1.04	
	531.03	1.50	531.22	1.52	
Ce 3d _{5/2}	880.60	2.44	880.62	2.44	
	884.57	3.50	884.78	3.50	
	882.27	1.62	882.27	1.62	
	888.81	3.50	888.76	3.50	
	898.10	2.08	898.08	2.08	

Table S4 Binding energies and FWHM of the C 1s, O 1s, Ce 3d_{5/2} and Ru 3d_{5/2} regions for Ru catalysts determined by XPS



Fig. S1 XRD patterns of Ru/CePr catalyst.



Fig. S2 HRTEM images of Ru/CePr catalyst (a) before reaction and (b) after reaction.



Fig. S3 SEM images of (a) Ru/CeO $_2$ and (b) Ru/CePr.



Fig. S4 TEM images of (a, c) $\mbox{Ru/CeO}_2$ and (b, d) $\mbox{Ru/CePr}.$



Fig. S5 HAADF-STEM elemental mapping of (a) Ru/CeO_2 and (b) Ru/CePr.



Fig. S6 XRD patterns of supports and Ru catalysts.



Fig. S7 Raman spectra of (a) supports and (b) Ru catalysts.



Fig. S8 H₂-TPR profiles of the samples with oxidization in oxygen at 150 $^\circ\text{C}.$



Fig. S9. Top view (a) and side view (b) of the $CeO_2(111)$ surface with or without Pr modification.



Fig. S10. Top view of the slab with one oxygen vacancy and its formation energy. (a) $CeO_2(111)$, (b) $PrCeO_2(111)$.



Fig. S11. Top view and side view of the Ru/CeO_2 (111) surface without or with Pr modification. (a) Ru/CeO_2 (111), (b) $Ru/PrCeO_2$ (111).



Fig. S12. The optimized structures of H_2 on CeO_2 (111) with oxygen vacancy (a) and (b) Ru(0001).



Fig. S13 The CO-IR spectra of Ru/CePr-CO catalyst.

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