# **Supporting Information**

# **Combing Experimental Methods and Molecular Simulations to Study Self-Healing Behaviors of Polyurethane Elastomers Containing Multiple Hydrogen Bond Networks and Flexible Blocks**

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### **Lattice model**

In the lattice space, one lattice site has 26 the nearest-neighbor sites (that is, 6 lattice sides, 8 body diagonals and 12 face diagonals), as shown in Fig. S1.



Fig. S1. The lattice space model used in the current simulation.

#### **Chain movement mode**

- (1) We first numbered vacancy sites in the whole system and recorded their positions.
- (2) Then, we selected one vacancy site, and randomly chose one lattice site in its nearest

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neighboring regions. If this lattice site was occupied by one polymer bead, we tried to swap the vacancy site with the polymer bead. (3) If no chain break occurred during the exchange (the length of the newly formed bonds on the both sides of this bead after the exchange is no more than  $\sqrt{3}$ ), this jumping would be accepted, as shown in Fig. S2(a) of the Supporting Information. (4) If the jumping caused the newly formed bonds on the both sides to break (the length of the newly formed bonds on the both sides of this bead after the exchange is more than  $\sqrt{3}$ ), the jumping would be rejected, as shown in Fig. S2(b) of the Supporting Information. (5) If only one newly formed bond would be broken due to the jumping (the length of this newly formed bond on one side of this bead after the jumping is more than  $\sqrt{3}$ ), we would try to find the nearest "kink" along the chain to this side, and then sliding diffusion of beads from the selected bead to that next to the "kind' was carried out, as shown in Fig. S2(c) of the Supporting Information. During simulations, the information about the above motion process of each bead could be recorded, and then the event of bead moving along the sliding path could be checked. We observed that both the jumping and the sliding occur during simulation.



Fig. S2. Schematic diagram of the micro-relaxation model. (a) Jumping mode of one bead that can be accepted. (b) Jumping mode of one bead that cannot be accepted (the forbidden symbol suggests

that the jumping is rejected in this condition); (c) Sliding mode of local chain segments in lattice space. The arrows indicate the directions of bead jumping or sliding.

#### **Setting of simulation parameters**

In the current simulation,  $B_1$  was the mixing-interaction energy for one nearestneighbor pair of interaction sites of the first kind, and  $B_2$  was the mixing-interaction energy for one nearest-neighbor pair of interaction sites of the second kind. The value of  $B_1/E_c$  was set to -0.1, reflecting weak attractive interaction existing between the interaction sites of the first kind. In order to explore the effect of the interaction strength of between the interaction sites of the second kind, the values of  $B_2/E_2$  were set as 0, -0.1,  $-0.2$ ,  $-0.3$ ,  $-0.4$ ,  $-0.5$ ,  $-0.6$ ,  $-0.8$  and  $-1.0$ , respectively (the higher absolute value of  $B_2/E_c$  reflects the higher interaction strength). If we assume  $B_1/E_c = s$ , we can obtain  $B_1$  $= sE_c$ . According to the corresponding literature,<sup>1</sup>  $E_c$  of *trans*- and *cis*-conformers of carbamic acid is around 10 kJ/mol. Then,  $B_1 = 0.1 \times 10$  kJ/mol = 1 kJ/mol. Then, further considering the effect of coordination number  $(q = 26)$  in the lattice space, the total strength of one interaction site of the first kind interacting with other interaction sites of the first kind should be  $B_1\times(q-2) = 24$  kJ/mol. In experiments, it was measured that the hydrogen bonding energy of carbamate groups is 22.42 kJ/mol,<sup>2</sup> the value of which is close to the above value in the simulation (24 kJ/mol).

 $E_f$ <sup>1</sup> and  $E_f$ <sup>2</sup> were introduced in the current simulations to control chain diffusion ability in the two systems, corresponding to the frictional barrier for sliding diffusion of the beads imposed by other neighboring beads. If the value of is set to 0, this means that the local slip process of segments is not restricted. If the value of  $E_f/E_c$  or  $E_f/E_c$  is set larger, the slippage process of the segments in the corresponding system becomes more difficult. In the system with  $E_f/E_c$  or  $E_f/E_c = 0.5$ , almost all chain segments are unable to slip. Thus, for the system 1, the segments in which exhibit relatively strong

diffusion ability, the value of  $E_f/E_c$  is set to 0.02, while the value of  $E_f/E_c$  is set to 0.2 for the system 2, reflecting that the corresponding segments have low diffusion ability. Then, in order to study the effect of segment diffusion ability on self-healing, the values of  $E_f/E_c$  were set as 0, 0.01, 0.02, 0.1, 0.2 and 0.5, respectively (the higher values of  $E_f/E_c$  reflect the weaker segment diffusion ability). But it is difficult to correlate  $E_f$ and  $E_p$  directly with the relevant physical quantities in experiments.

We defined the diffusion ability as the average number of beads involved in the sliding diffusion process in a single MC cycle over the 100 MC cycles in the systems with the same bead density but without the crack. If more beads participate in the sliding diffusion in a single MC cycle, this means the system will have stronger diffusion ability. Then, the effect of the sliding friction parameters  $E_f$  and  $E_f$  can be revealed by calculating the dependence of the diffusion ability on the values of the sliding friction parameters. Fig. S3 in the Supporting Information displayed the diffusion ability as a function of  $E_f$ <sup>1</sup> in the system 1 and as a function of  $E_f$ <sup>2</sup> in the system 2 at  $T^* = 0.5$ , respectively. It can be seen that the diffusion ability in both of the two systems decreases with the increase of the values of  $E_f$  or  $E_f$ , demonstrating that the diffusion ability of polymer chains can be controlled by setting different values of the sliding friction parameters  $E_f$  and  $E_f$ .



Fig. S3. The diffusion ability as a function of  $E_f$  in the corresponding system 1 and as a function of  $E_f$ <sup>2</sup> in the system 2 at  $T^* = 0.5$ , respectively.

#### **The procedure of dynamic MC simulations**

The MC acceptance ratio in our simulation is calculated as follows:

$$
p = \min\{1, \exp(-\Delta E/kT)\}, \Delta E = E_2 - E_1
$$

where Δ*E* represents the total energy difference of molecular configuration before and after the movement of chain segment,  $E_1$  represents the total energy of the molecular configuration before the movement of chain segment,  $E_2$  represents the total energy of the new molecular configuration after the movement of chain segment, *k* represents the Boltzmann constant, exp(-Δ*E/kT*) represents the Boltzmann factor, *T* represents the temperature. If  $\Delta E \leq 0$ , the segment motion is accepted, and the new state participates in the statistics. If  $\Delta E > 0$ , a random number between [0, 1] is generated, and if the random number is less than the Boltzmann factor, the motion is accepted. The increase

of temperature can lead to the decrease of the values of  $kT$ , then resulting in increase of the acceptability, that is, the bead mobility.

 $\Delta E$ 

**Simulation results**



Fig. S4. The PBM values as a function of simulation temperature.

## **References**

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