

## SUPPLEMENTARY INFORMATION FOR

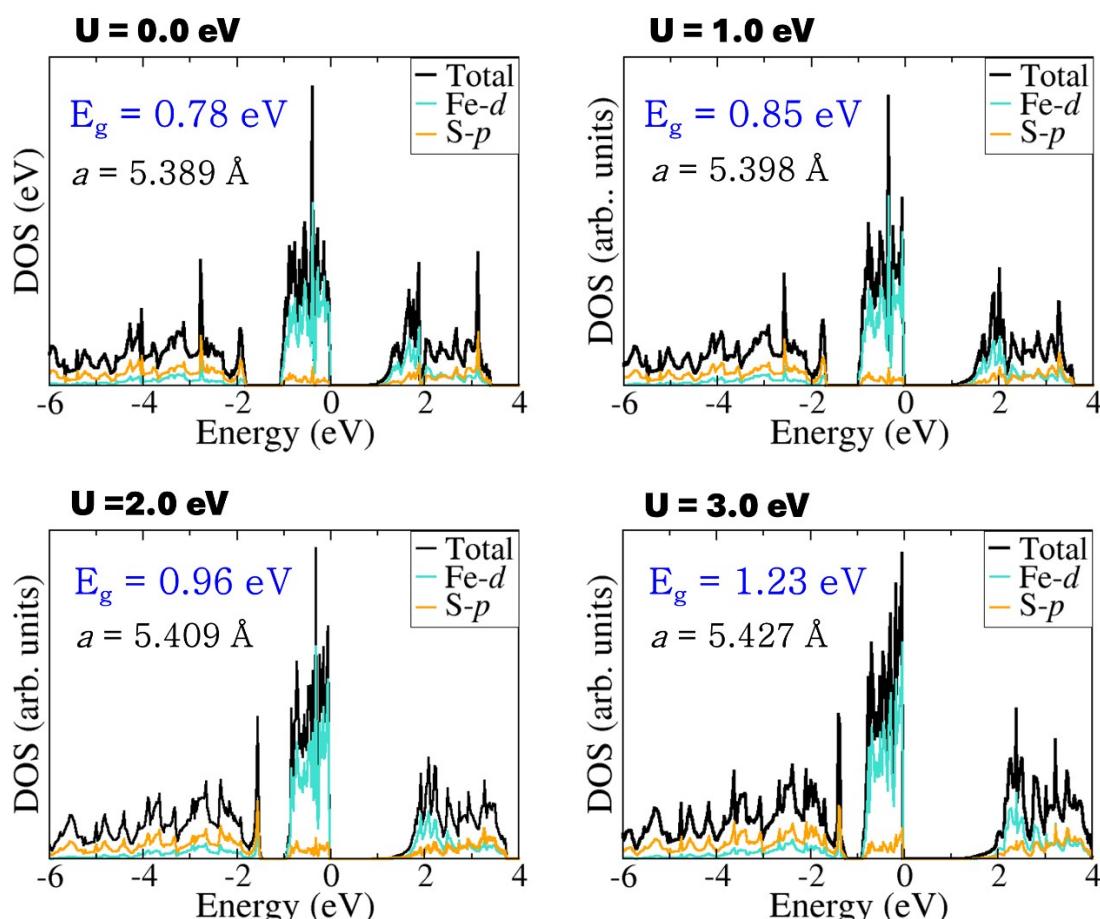
### Unraveling the Origin of High Photocatalytic Properties of Earth-abundant $\text{TiO}_2/\text{FeS}_2$ Heterojunction: Insights from First-Principles Density Functional Theory

Oluwayomi F. Awe,<sup>1</sup> Henry I. Eya<sup>1</sup>, Ricardo Amaral<sup>1</sup>, Nikhil Komalla<sup>1</sup>, Pascal Nbelayim<sup>2</sup>, Nelson Y. Dzade<sup>1,\*</sup>

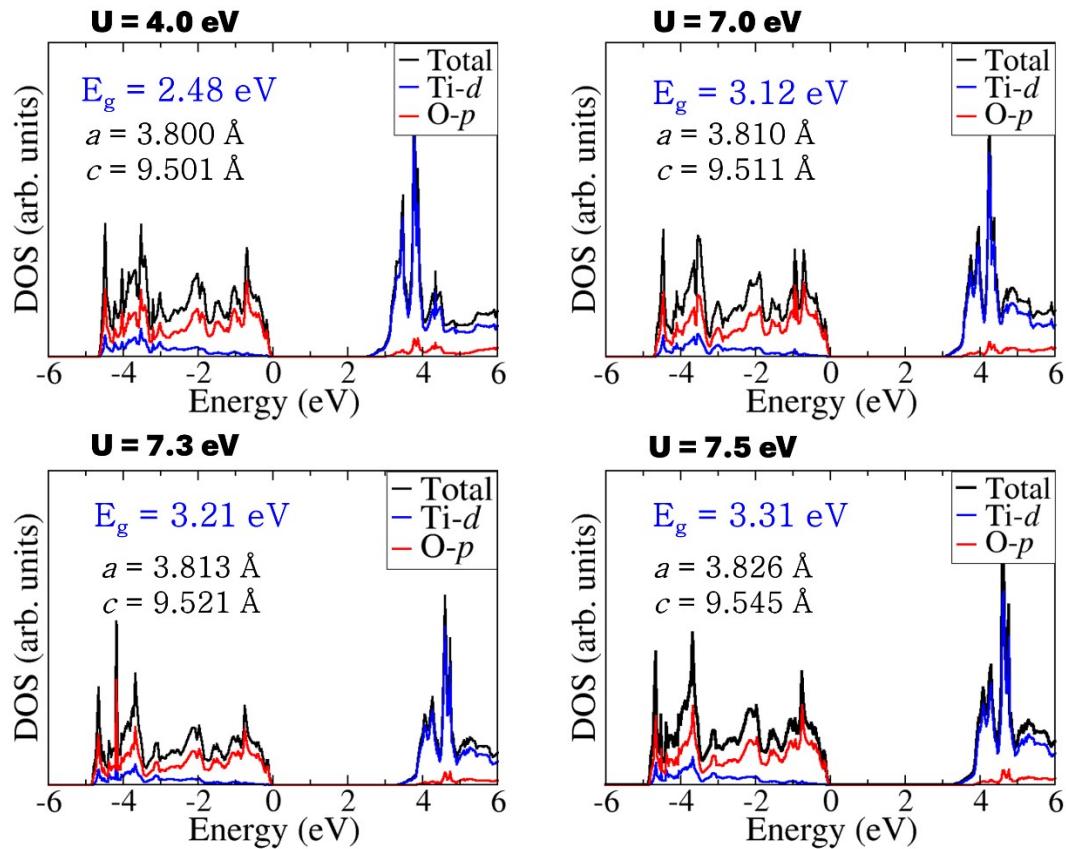
<sup>1</sup> Department of Energy and Mineral Engineering, Pennsylvania State University, University Park, PA 16802, United States.

<sup>2</sup> Department of Materials Science and Engineering, School of Engineering Sciences, College of Basic and Applied Sciences, University of Ghana, Accra, Ghana

**Figure S1:** The projected density of states (PDOS) of bulk  $\text{FeS}_2$  calculated at different effective U-values. The bandgap ( $E_g$ ) predicted at each U value is displayed on each figure in blue.



**Figure S2:** The projected density of states (PDOS) of bulk anatase  $\text{TiO}_2$  calculated at different effective U-values. The bandgap ( $E_g$ ) predicted at each U value is displayed on each figure in blue.



**Table S1:** Bader charge analysis results FeS<sub>2</sub>(100)-TiO<sub>2</sub>(001) heterojunction. The sum of the charges of FeS<sub>2</sub> ions (Fe and S) is 0.8734 e<sup>-</sup>, whereas that of TiO<sub>2</sub> ions (Ti and O) is -0.8733 e<sup>-</sup>. This indicates that a total charge of 0.87 e<sup>-</sup> is transferred from the FeS<sub>2</sub>(100) layers to the top of the TiO<sub>2</sub>(001) layer.

| Element | Bader charge (e <sup>-</sup> ) |
|---------|--------------------------------|
| Fe      | 0.9479                         |
| Fe      | 1.0418                         |
| Fe      | 0.9039                         |
| Fe      | 0.9069                         |
| Fe      | 0.9002                         |
| Fe      | 0.9012                         |
| Fe      | 0.9317                         |
| Fe      | 0.9093                         |
| Fe      | 0.8955                         |
| Fe      | 0.9312                         |
| Fe      | 0.8982                         |
| Fe      | 0.9041                         |
| Fe      | 0.9116                         |
| Fe      | 0.9075                         |
| Fe      | 0.9298                         |
| Fe      | 0.9021                         |
| Fe      | 0.9749                         |
| Fe      | 0.9191                         |
| Fe      | 0.9052                         |
| Fe      | 0.9                            |
| Fe      | 0.9038                         |
| Fe      | 0.8994                         |
| Fe      | 0.8986                         |
| Fe      | 0.9341                         |
| Fe      | 0.6347                         |
| Fe      | 0.9468                         |
| Fe      | 0.9015                         |
| Fe      | 0.908                          |
| Fe      | 0.906                          |
| Fe      | 0.9117                         |
| Fe      | 0.9025                         |
| Fe      | 0.9284                         |
| S       | -0.5219                        |
| S       | -0.4944                        |
| S       | -0.4639                        |
| S       | -0.4935                        |
| S       | -0.454                         |
| S       | -0.4512                        |
| S       | -0.485                         |

|   |         |
|---|---------|
| S | -0.4234 |
| S | -0.4401 |
| S | -0.462  |
| S | -0.4298 |
| S | -0.3987 |
| S | -0.4894 |
| S | -0.5196 |
| S | -0.4272 |
| S | -0.4618 |
| S | -0.4671 |
| S | 1.0116  |
| S | -0.5367 |
| S | -0.481  |
| S | -0.4313 |
| S | -0.4292 |
| S | -0.4975 |
| S | -0.4837 |
| S | -0.4525 |
| S | -0.44   |
| S | -0.4125 |
| S | -0.4287 |
| S | -0.5085 |
| S | -0.496  |
| S | -0.436  |
| S | -0.4322 |
| S | -0.5089 |
| S | -0.5864 |
| S | -0.5294 |
| S | -0.4897 |
| S | -0.3685 |
| S | -0.3881 |
| S | -0.4686 |
| S | -0.4687 |
| S | -0.4899 |
| S | -0.4572 |
| S | -0.4434 |
| S | -0.4193 |
| S | -0.4956 |
| S | -0.5059 |
| S | -0.4268 |
| S | -0.4259 |
| S | -0.6423 |
| S | -0.3239 |
| S | -0.4919 |
| S | -0.519  |

|    |         |
|----|---------|
| S  | -0.435  |
| S  | -0.4007 |
| S  | -0.4539 |
| S  | -0.4636 |
| S  | -0.4471 |
| S  | -0.471  |
| S  | -0.4124 |
| S  | -0.4258 |
| S  | -0.5297 |
| S  | -0.519  |
| S  | -0.4548 |
| S  | -0.4246 |
| Ti | 2.7581  |
| Ti | 2.7536  |
| Ti | 2.8086  |
| Ti | 2.7026  |
| Ti | 2.7359  |
| Ti | 2.7644  |
| Ti | 2.7585  |
| Ti | 2.7695  |
| Ti | 2.7562  |
| Ti | 2.794   |
| Ti | 2.7755  |
| Ti | 2.7167  |
| Ti | 2.7559  |
| Ti | 2.7608  |
| Ti | 2.7679  |
| Ti | 2.7392  |
| Ti | 2.733   |
| Ti | 2.7654  |
| Ti | 2.7713  |
| Ti | 2.711   |
| Ti | 2.7467  |
| Ti | 2.7556  |
| Ti | 2.7843  |
| Ti | 2.7134  |
| Ti | 2.7609  |
| Ti | 2.7805  |
| Ti | 2.7939  |
| Ti | 2.7407  |
| Ti | 2.772   |
| Ti | 2.7589  |
| Ti | 2.7807  |
| Ti | 2.7335  |
| Ti | 2.7439  |

|    |         |
|----|---------|
| Ti | 2.7615  |
| Ti | 2.7734  |
| Ti | 2.5465  |
| O  | -1.3342 |
| O  | -1.4004 |
| O  | -1.3991 |
| O  | -1.408  |
| O  | -1.3744 |
| O  | -1.4294 |
| O  | -1.435  |
| O  | -1.3552 |
| O  | -1.3206 |
| O  | -1.3984 |
| O  | -1.3925 |
| O  | -1.387  |
| O  | -1.3781 |
| O  | -1.4105 |
| O  | -1.3967 |
| O  | -1.3577 |
| O  | -1.3323 |
| O  | -1.4175 |
| O  | -1.4065 |
| O  | -1.3834 |
| O  | -1.3952 |
| O  | -1.4127 |
| O  | -1.4108 |
| O  | -1.2295 |
| O  | -1.3331 |
| O  | -1.4029 |
| O  | -1.404  |
| O  | -1.3864 |
| O  | -1.3764 |
| O  | -1.4166 |
| O  | -1.3796 |
| O  | -1.2907 |
| O  | -1.3229 |
| O  | -1.4098 |
| O  | -1.3885 |
| O  | -1.3914 |
| O  | -1.3842 |
| O  | -1.4169 |
| O  | -1.3858 |
| O  | -1.2853 |
| O  | -1.3323 |
| O  | -1.4096 |

|   |         |
|---|---------|
| O | -1.3791 |
| O | -1.3979 |
| O | -1.3807 |
| O | -1.4043 |
| O | -1.4129 |
| O | -1.2902 |
| O | -1.3322 |
| O | -1.4102 |
| O | -1.3978 |
| O | -1.3874 |
| O | -1.3945 |
| O | -1.4106 |
| O | -1.399  |
| O | -1.3477 |
| O | -1.3341 |
| O | -1.4108 |
| O | -1.4052 |
| O | -1.3965 |
| O | -1.3821 |
| O | -1.4056 |
| O | -1.3958 |
| O | -1.8931 |
| O | -1.337  |
| O | -1.4079 |
| O | -1.3824 |
| O | -1.4052 |
| O | -1.3858 |
| O | -1.3891 |
| O | -1.4152 |
| O | -1.346  |