

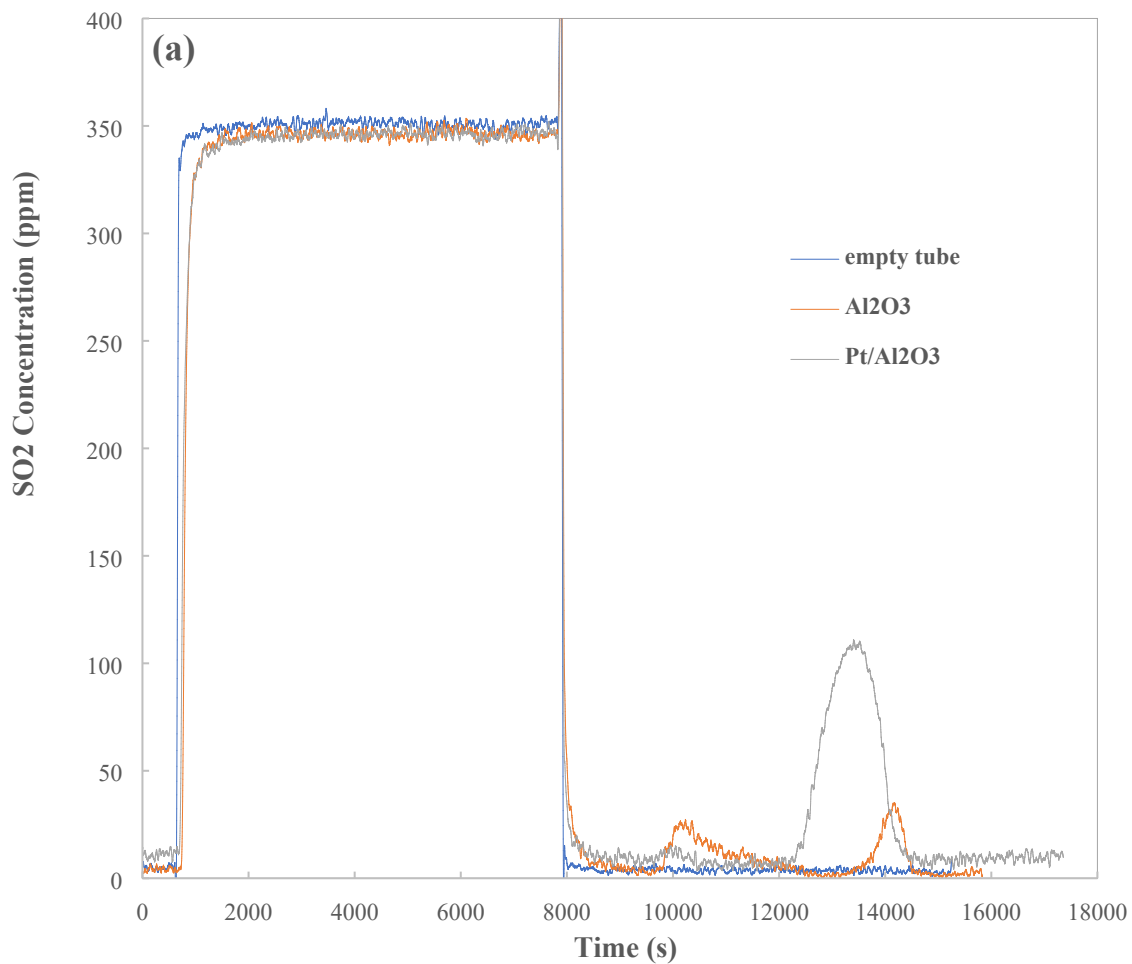
Supporting Information

Sulfur Poisoning and NH₃ Regeneration of Pt/Al₂O₃ Monolith Catalyst

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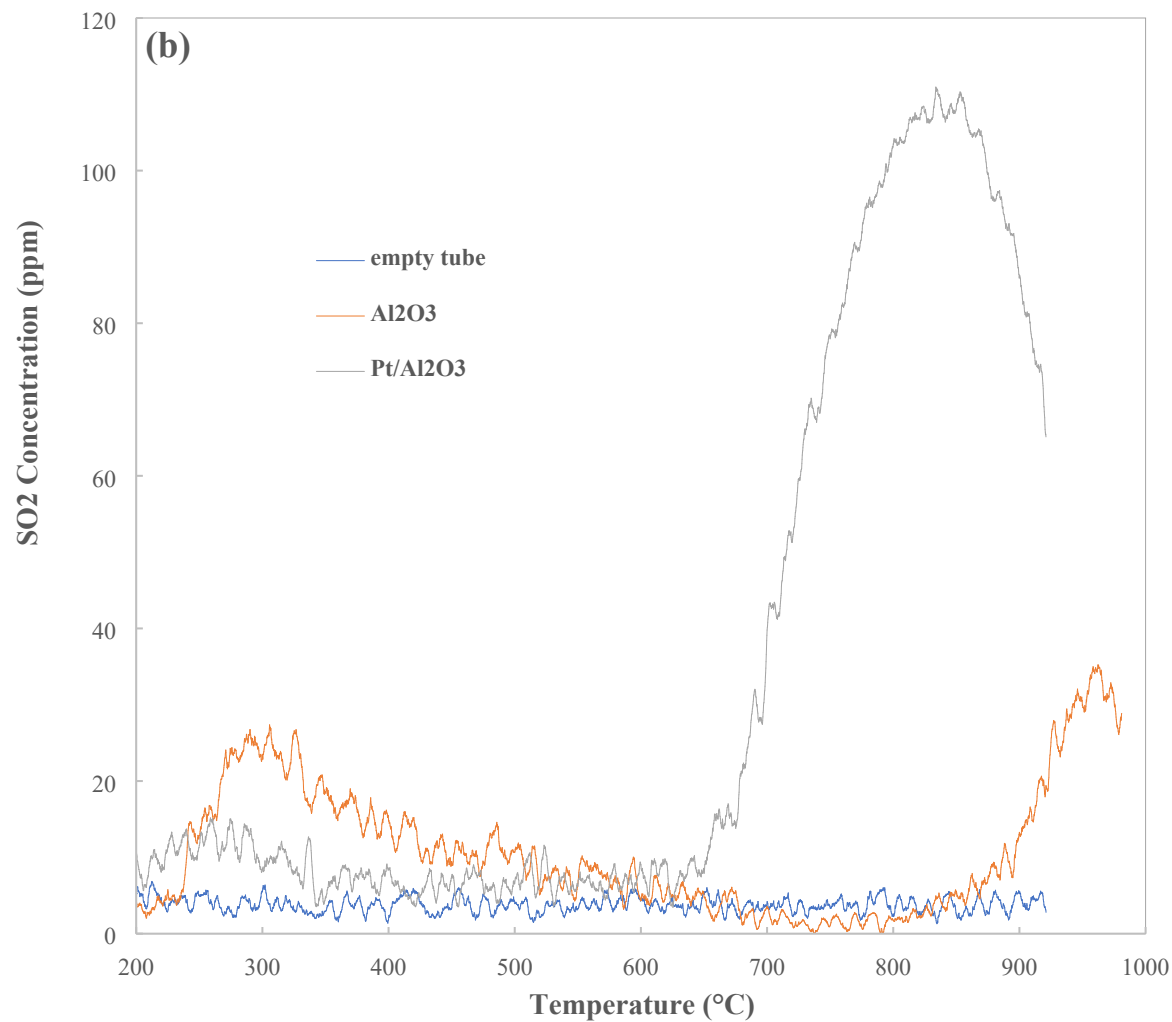
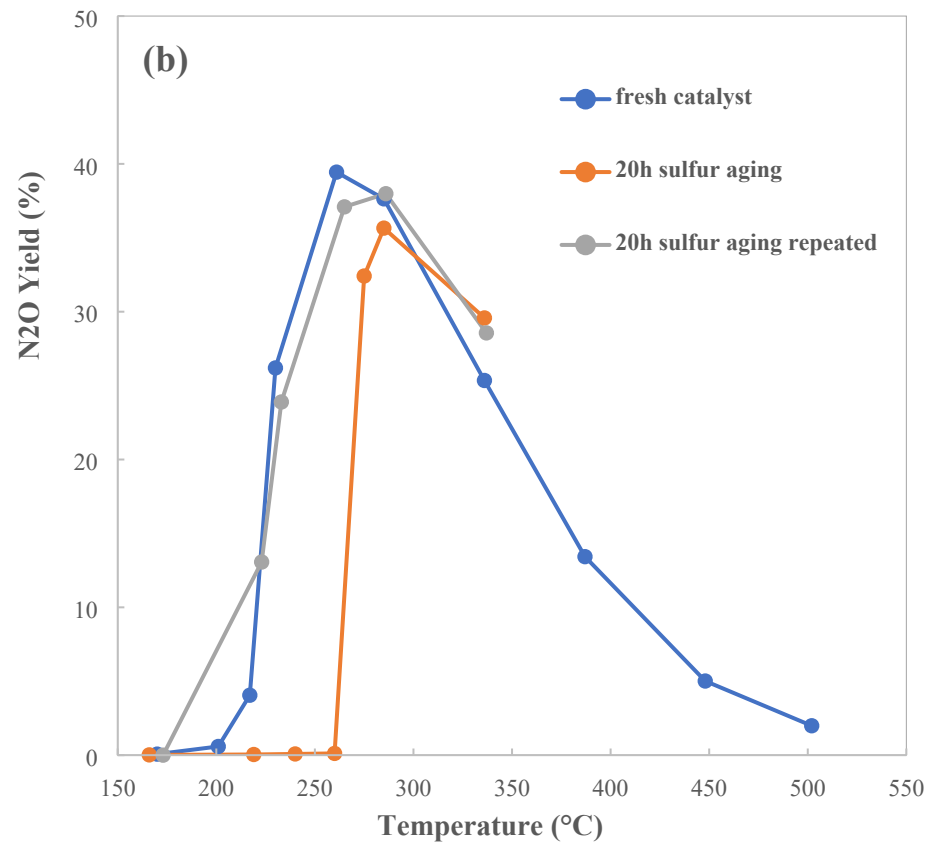
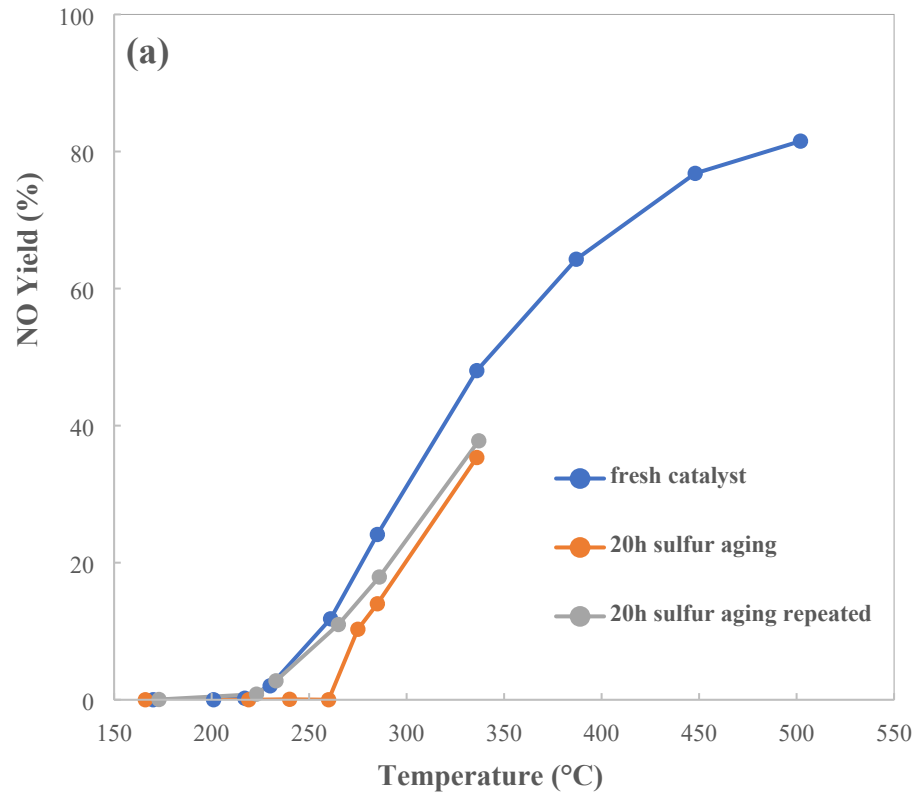


Fig. S1 SO₂ TPD profiles for Al₂O₃ and Pt/Al₂O₃ (a) concentration versus time and (b) concentration versus temperature.

Table S1 Amount of SO₂ adsorbed and desorbed during SO₂ TPD in Ar

Sample	SO ₂ adsorbed (μmol)	SO ₂ desorbed (μmol)
Al ₂ O ₃	4.66	4.29
Pt/Al ₂ O ₃	8.78	8.7



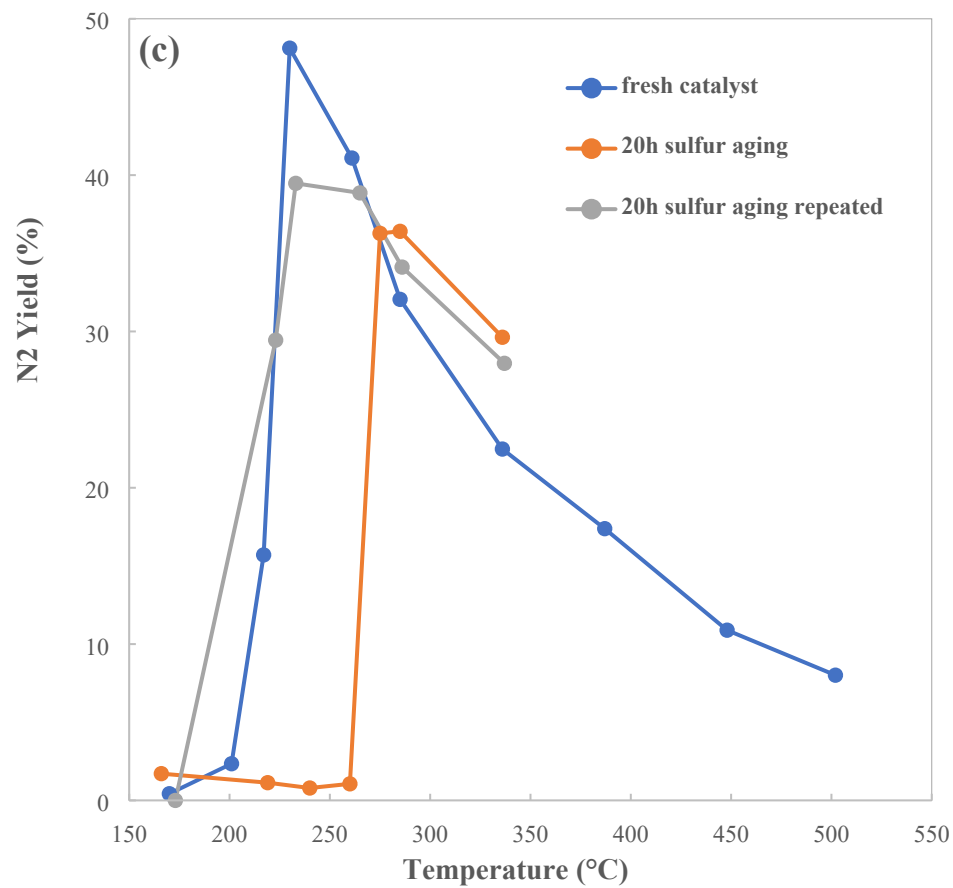
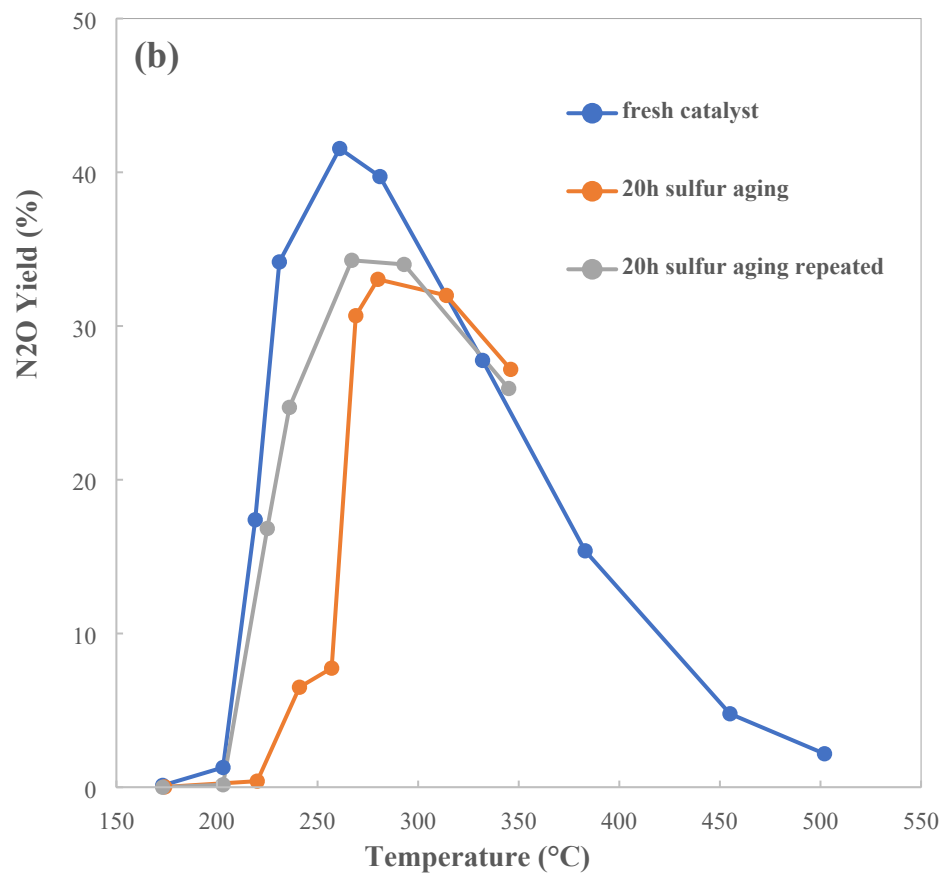
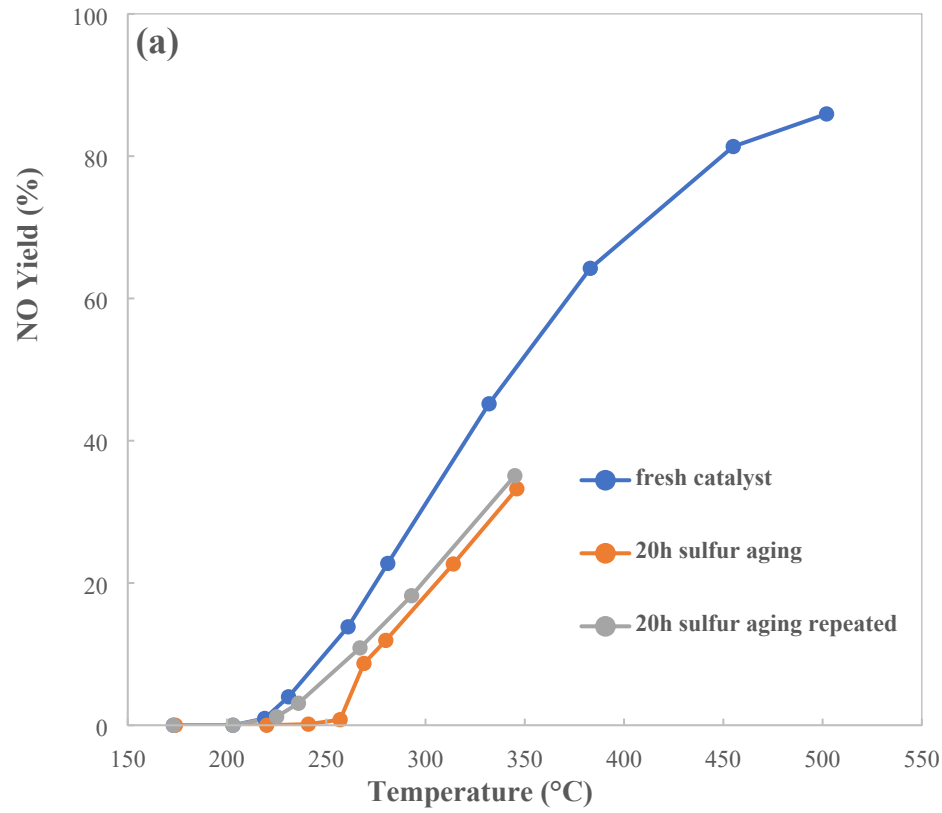


Fig. S2 Steady-state (a) NO yield, (b) N₂O yield, (c) N₂ yield over fresh and poisoned Pt/Al₂O₃ catalyst which is sulfur poisoned in the absence of water.



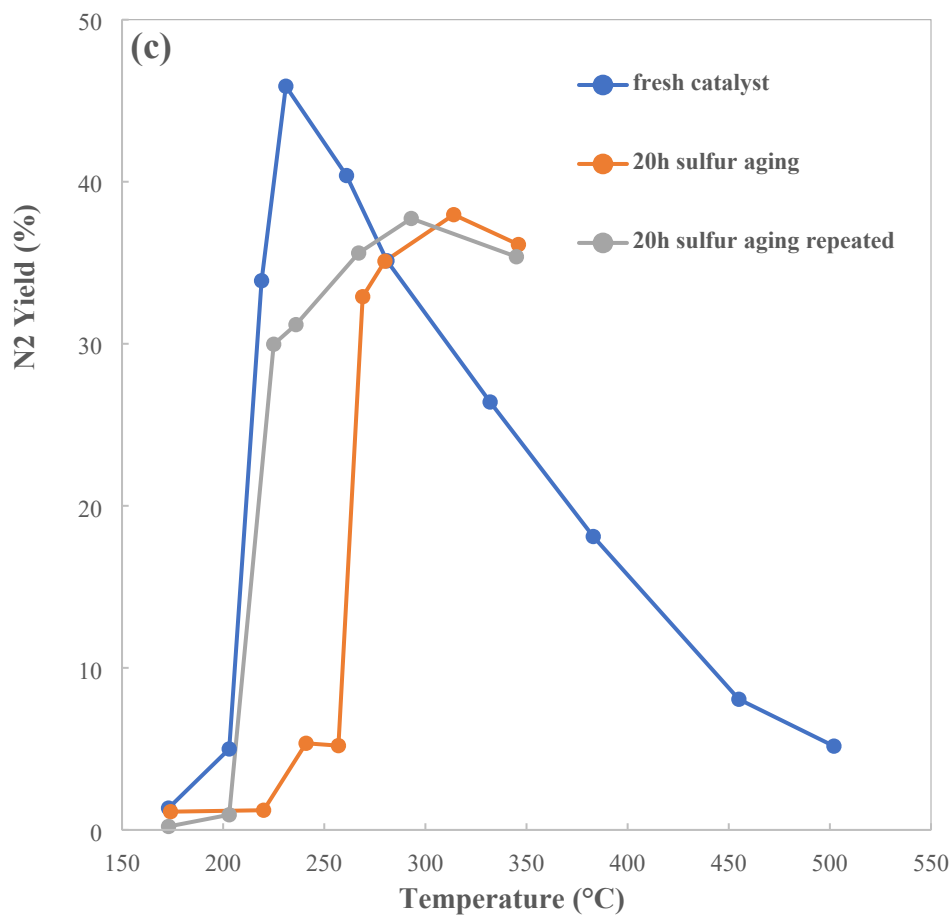


Fig. S3 Steady-state (a) NO yield, (b) N₂O yield, (c) N₂ yield over fresh and poisoned Pt/Al₂O₃ catalyst which is sulfur poisoned in the presence of water.

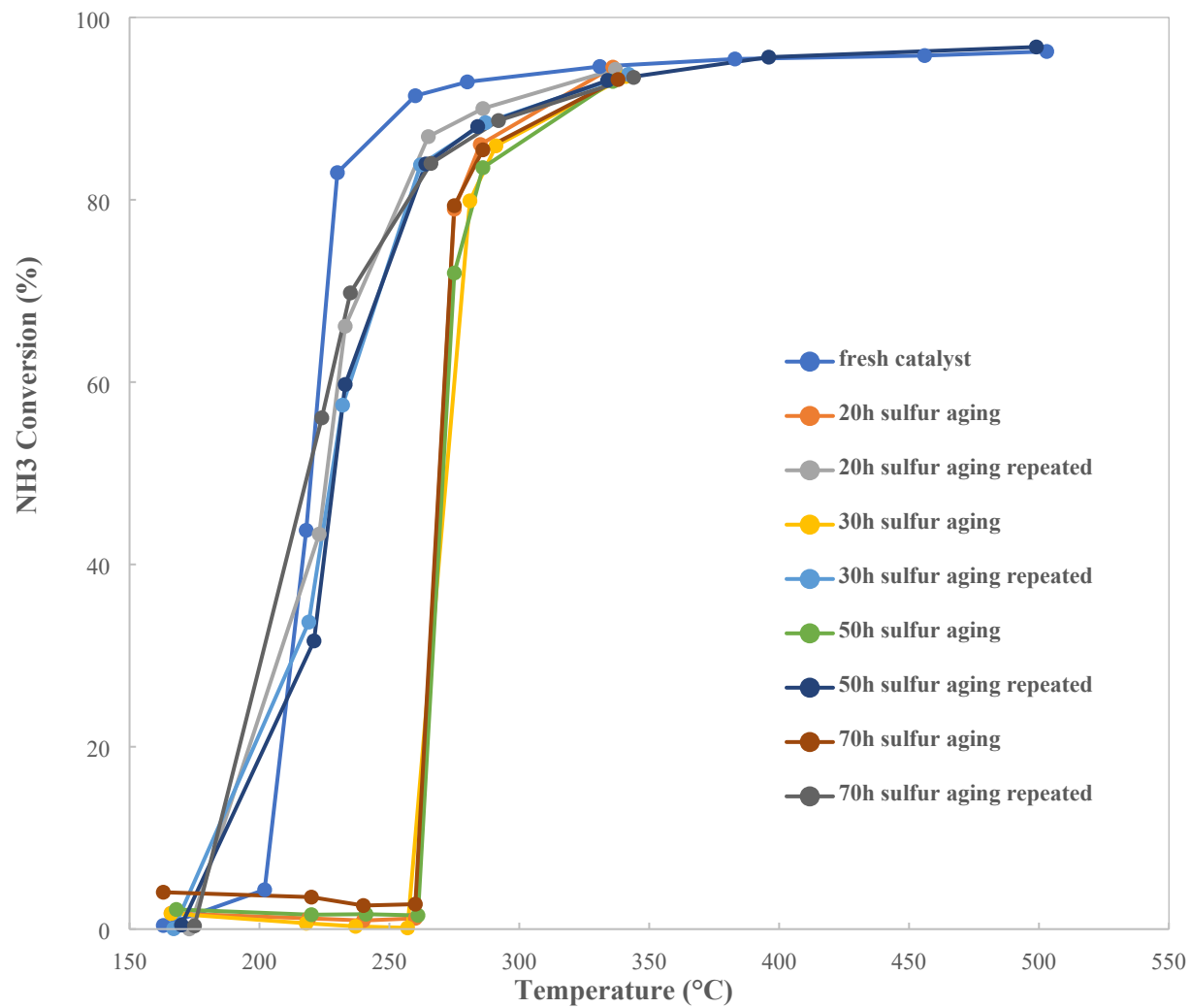


Fig. S4 Steady-state NH₃ oxidation over fresh and various sulfur aged catalyst.

S5. Adiabatic temperature rise for NH₃ oxidation

In this section, the adiabatic temperature rise for NH₃ oxidation taking place during typical light-off experiments is estimated. Considering the following reaction of NH₃ oxidation over Pt:



The adiabatic temperature rise is determined from:

$$\Delta T = \frac{(-\Delta H)C_{0,\text{NH}_3}}{\rho_g C_{pg}} \Delta X$$

where

ΔH = enthalpy of reaction (kJ/mole NH₃)

C_{0,NH_3} = Molar concentration of NH₃ (mole/m³)

ρ_g = Density of reacting gas (kg/m³)

C_{pg} = Specific heat of the reacting gas (kJ/kg/K)

ΔX = NH₃ conversion

We evaluate the case of high NH₃ concentration feed at complete NH₃ conversion.

Case 1: 5000 ppm NH₃, 10 vol. % O₂, balance Argon @ 100% ammonia conversion for washcoated monolith

$$\Delta T = \frac{(-\Delta H)C_{0,\text{NH}_3}}{\rho_g C_{pg}} \Delta X = \frac{(226) * 0.22}{1.7307 * 0.61} * 1 = 48 \text{ K}$$

