

*Electronic Supplementary Information*

**Highly active and stable RuO<sub>2</sub>/MgF<sub>2</sub> catalysts for efficient HCl oxidation in the fluorochemical industry**

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**Fig. S7.** Differential adsorption heat of O<sub>2</sub> on RuO<sub>2</sub>/MgF<sub>2</sub>-SRT as a function of O<sub>2</sub> coverage ( $\theta$ ) at 40.0 °C.

**Fig. S8.** HCl conversion as a function of time on stream over RuO<sub>2</sub>/MgF<sub>2</sub>-SRT catalysts.

Reaction conditions: 350.0 °C and a GHSV of 48,000.0 mL (STP)·(h·g<sub>catal</sub>)<sup>-1</sup>.

**Fig. S9.** XRD pattern of the used RuO<sub>2</sub>/MgF<sub>2</sub>-1 catalyst.

**Fig. S10.** TEM (C) and HRTEM (D) images of the used RuO<sub>2</sub>/MgF<sub>2</sub>-1 catalyst.

**Fig. S11.** Raman spectrum of the used RuO<sub>2</sub>/MgF<sub>2</sub>-1 catalyst.

**Fig. S12.** Ru 3d (A) and Cl 2p (B) XPS spectra of the used RuO<sub>2</sub>/MgF<sub>2</sub>-1 catalyst.

## Models for the kinetic adsorption of Ru ions on MgF<sub>2</sub>-SRT supports

To quantitatively analyze the adsorption kinetics of Ru ions on MgF<sub>2</sub>-SRT supports, the plots of  $q_t$  versus  $t$  were further analyzed by employing the pseudo first-order and pseudo second-order models as shown in Equations (S1) and (S2) [1].

Pseudo first-order model:

$$\ln(q_e - q_t) = \ln q_e - k_1 t \quad (\text{S1})$$

Pseudo second-order model:

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_t} \quad (\text{S2})$$

where  $q_t$  and  $q_e$  in  $\mu\text{mol}\cdot\text{g}^{-1}$  are the adsorption amounts of Ru ions at time  $t$  and equilibrium, respectively,  $t$  represents the contact time (min), and  $k_1$  ( $\text{min}^{-1}$ ) and  $k_2$  ( $\text{g}\cdot\mu\text{mol}^{-1}\cdot\text{min}^{-1}$ ) are denoted as the rate constants for the above two models, respectively.

## Reference

1. S. S. Gupta, K.G. Bhattacharyya, *Adv. Colloid Interface Sci.*, 2011, **162**, 39-58.

## Evaluation on mass transfer limitations

The influence of mass transfer limitations on reaction kinetics was evaluated using the Mears ( $C_M$ ) and Weisz-Prater ( $C_{WP}$ ) criteria, which were calculated using Equations (S3) and (S4), respectively [1,2].

$$C_M = \frac{n \cdot r_{\text{obs}} \cdot \rho_{\text{cat}} \cdot R_{\text{cat}}}{k_c \cdot C_{\text{HCl}}} \quad (\text{S3})$$

$$C_{WP} = \frac{r_{\text{obs}} \cdot \rho_{\text{cat}} \cdot R_{\text{cat}}^2}{D_{\text{eff}} \cdot C_{\text{HCl},s}} \quad (\text{S4})$$

where  $n$  is the reaction order,  $r_{\text{obs}}$  is the observed reaction rate,  $\rho_{\text{cat}}$  is the bulk density of catalyst bed,  $R_{\text{cat}}$  is the particle radius of catalyst,  $k_c$  is the external mass transfer coefficient,  $C_{\text{HCl}}$  is the bulk concentration of HCl,  $D_{\text{eff}}$  is the effective diffusion coefficient and  $C_{\text{HCl},s}$  is the HCl concentration on the surface of a catalyst particle, which is equal to  $C_{\text{HCl}}$  when the external mass transfer limitation is neglected.

$k_c$  was estimated with Equations (S5)-(S7) by means of similarity numbers such as the Sherwood number  $Sh$ , the Reynolds number of the catalyst pellet  $Re_p$ , and the Schmidt number  $Sc$  [1].

$$Sh = \frac{k_c \cdot d_{\text{cat}}}{D_{\text{eff}}} = 2 + 0.6 \cdot Re_p^{1/2} \cdot Sc^{1/3} \quad (\text{S5})$$

$$Re_p = \frac{U \cdot \rho \cdot d_{\text{cat}}}{\mu} \quad (\text{S6})$$

$$Sc = \frac{\mu}{D_{\text{eff}} \cdot \rho} \quad (\text{S7})$$

where  $d_{\text{cat}}$  is the diameter of a catalyst particle,  $U$  is the free-stream velocity,  $\rho$  and  $\mu$  are the density and viscosity of a feed mixture, which can be determined from Aspen Plus software.

$D_{\text{eff}}$  was estimated with Equations (S8)-(S11) using the coefficients for Knudsen

diffusion  $D_A^K$  and bulk diffusion  $D_A^b$  [1].

$$\frac{1}{D_{\text{eff}}} = \frac{1}{D_A^K} + \frac{1}{D_A^b} \quad (\text{S8})$$

$$D_A^K = \frac{2}{3} \cdot r_{\text{po}} \cdot \sqrt{\frac{8 \cdot R \cdot T}{\pi \cdot M_i}} \cdot \frac{\varepsilon}{\tau} \quad (\text{S9})$$

$$r_{\text{po}} = 4 \cdot \frac{\varepsilon}{S_{\text{cat}} \cdot \rho_{\text{cat,g}}} \quad (\text{S10})$$

$$D_A^b = D_A \cdot \frac{\varepsilon}{\tau} \quad (\text{S11})$$

where  $\varepsilon$ ,  $\tau$ ,  $r_{\text{po}}$ ,  $S_{\text{cat}}$ , and  $\rho_{\text{cat,g}}$  are the porosity, tortuosity, average pore radius, surface area, and grain density of catalyst,  $T$  and  $M_i$  are the temperature and relative molecular weight of component  $i$ , and  $D_A$  is the free diffusion coefficient, which can be determined from Aspen Plus software.

The data used in the above-mentioned equations and the calculations of the Mears and Weisz-Prater parameters are given in Tables S3 and S4. Apparently,  $C_M/n$  is less than 0.15 while  $n$  ranges from 1 to 2, implying that there is no external mass-transfer limitation. In addition,  $C_{\text{WP}}$  is much less than 1 at different temperatures, indicating that the internal diffusion limitations can be neglected.

## References:

1. H. S. Fogler, *Diffusion and reaction in elements of chemical reaction engineering*, Pearson Education Inc.: New York, 2016, pp 734-743.
2. T. R. Marrero, E.A. Mason, *J. Phys. Chem. Ref. Data*, 1972, **1**, 1-118.

**Table S1.** Extracted parameter values for the kinetic adsorption of Ru ions on MgF<sub>2</sub>-SRT supports at 30.0 °C

Support	Pseudo first-order parameters			Pseudo second-order parameters		
	$q_e$	$k_1$	$R^2$	$q_e$	$k_2$	$R^2$
	( $\mu\text{mol}\cdot\text{g}^{-1}$ )	( $\text{min}^{-1}$ )		( $\mu\text{mol}\cdot\text{g}^{-1}$ )	( $\text{g}\cdot\mu\text{mol}^{-1}\cdot\text{min}^{-1}$ )	
MgF <sub>2</sub> -1	117	0.51	0.834	120	0.63	0.993
MgF <sub>2</sub> -8	101	0.43	0.786	104	0.52	0.996
MgF <sub>2</sub> -24	75	0.38	0.802	77	0.41	0.995
MgF <sub>2</sub> -36	56	0.32	0.819	58	0.34	0.995

**Table S2.** Measured reaction rates over RuO<sub>2</sub>/MgF<sub>2</sub>-SRT catalysts at different reaction temperatures for  $E_a$  calculations<sup>a</sup>

Catalyst	Temperature (°C)	HCl conversion (%)	Reaction rate ( $\times 10^{-4}$ mol·g <sup>-1</sup> ·s <sup>-1</sup> )
RuO <sub>2</sub> /MgF <sub>2</sub> -1	305	1.58	7.9
	315	1.86	9.3
	325	1.96	9.8
	335	2.28	11.4
	345	2.71	13.6
	355	3.62	18.1
RuO <sub>2</sub> /MgF <sub>2</sub> -8	305	1.27	6.4
	315	1.48	7.4
	325	1.79	9.0
	335	2.10	10.5
	345	2.47	12.4
	355	3.10	15.5
RuO <sub>2</sub> /MgF <sub>2</sub> -24	305	0.94	4.7
	315	1.13	5.7
	325	1.45	7.3
	335	1.69	8.5
	345	1.94	9.7



	355	2.24	11.2
	305	0.84	4.2
	315	1.03	5.2
	325	1.16	5.8
RuO <sub>2</sub> /MgF <sub>2</sub> -36	335	1.29	6.5
	345	1.49	7.5
	355	1.77	8.9

<sup>a</sup> The different, high gas hourly space velocities were set in order to maintain HCl conversions always below 10%, and the reaction rates were measured after 1 h of the oxidation reaction.

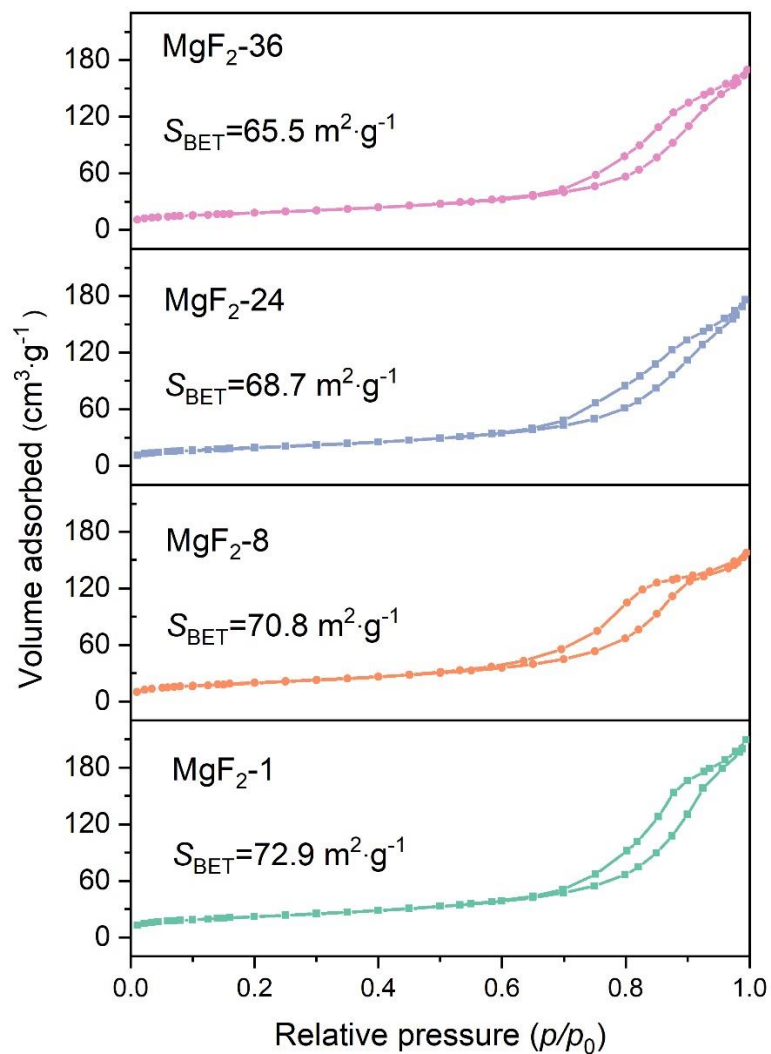
**Table S3.** Data for calculating the Mears and Weisz-Prater criterion parameters

Parameters	Values
$\rho_{\text{cat}}$	806 kg·m <sup>-3</sup>
$R_{\text{cat}}$	0.20 mm
$\rho_{\text{cat,g}}$	3,074 kg·m <sup>-3</sup>
$\varepsilon$	0.65
$\tau^{\text{a}}$	3

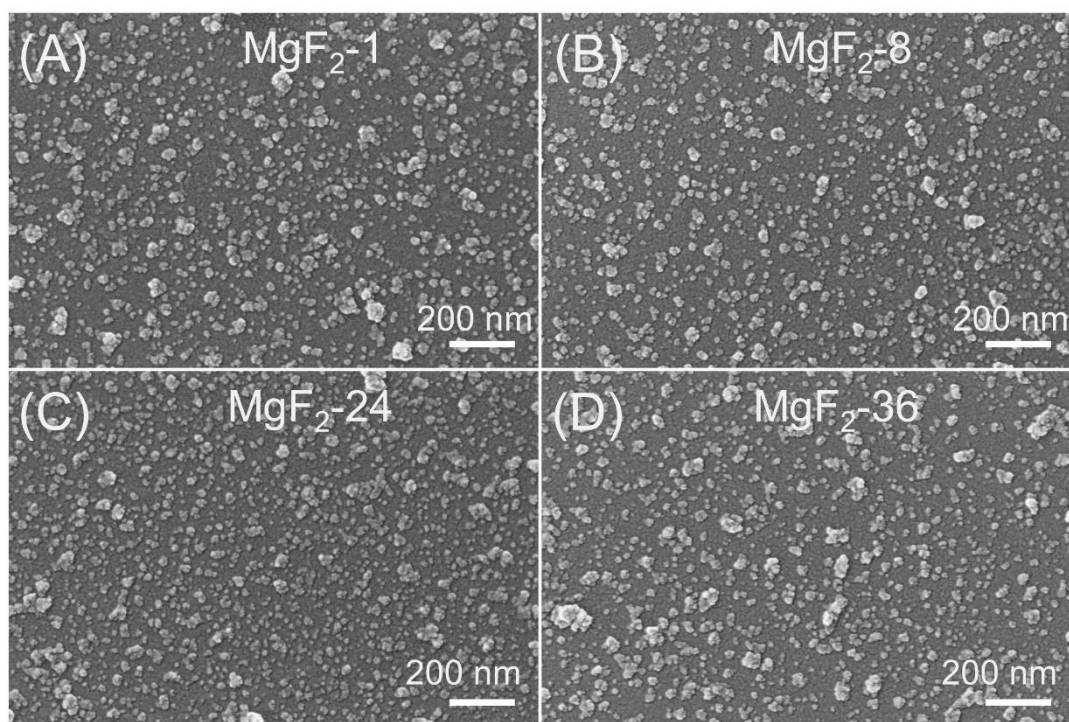
<sup>a</sup> The pore tortuosity was assumed to be 3 for a spherical catalyst particle.

**Table S4.** Evaluation on the Mears ( $C_M$ ) and Weisz-Prater ( $C_{WP}$ ) criterion parameters

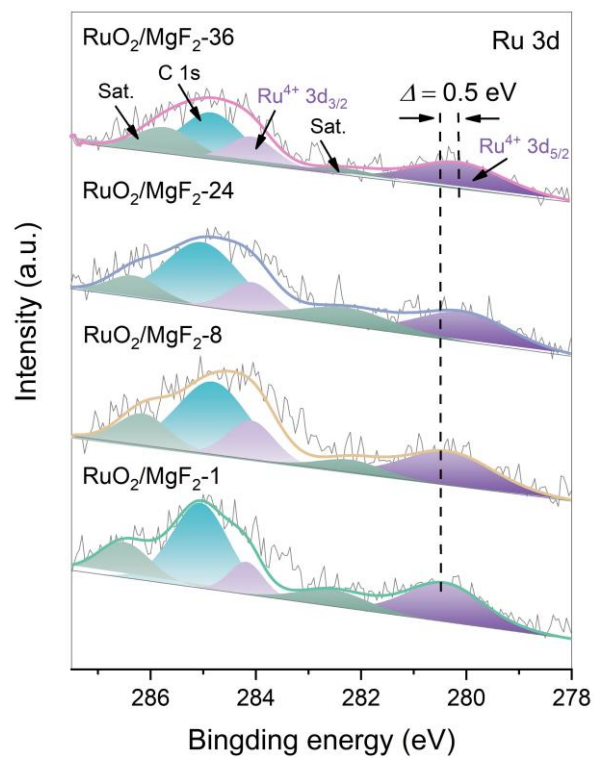
Catalyst	Temperature (°C)	$C_M$	$C_{WP}$
RuO <sub>2</sub> /MgF <sub>2</sub> -1	325	$4.5 \times 10^{-3}$	$1.8 \times 10^{-2}$
	335	$5.5 \times 10^{-3}$	$2.2 \times 10^{-2}$
	345	$6.9 \times 10^{-3}$	$2.7 \times 10^{-2}$
	355	$8.9 \times 10^{-3}$	$3.5 \times 10^{-2}$
RuO <sub>2</sub> /MgF <sub>2</sub> -8	325	$5.6 \times 10^{-3}$	$2.2 \times 10^{-2}$
	335	$6.5 \times 10^{-3}$	$2.6 \times 10^{-2}$
	345	$7.5 \times 10^{-3}$	$3.0 \times 10^{-2}$
	355	$8.8 \times 10^{-3}$	$3.5 \times 10^{-2}$
RuO <sub>2</sub> /MgF <sub>2</sub> -24	325	$7.4 \times 10^{-3}$	$3.1 \times 10^{-2}$
	335	$8.6 \times 10^{-3}$	$3.6 \times 10^{-2}$
	345	$9.9 \times 10^{-3}$	$4.1 \times 10^{-2}$
	355	$1.1 \times 10^{-2}$	$4.7 \times 10^{-2}$
RuO <sub>2</sub> /MgF <sub>2</sub> -36	325	$5.8 \times 10^{-3}$	$2.4 \times 10^{-2}$
	335	$6.7 \times 10^{-3}$	$2.7 \times 10^{-2}$
	345	$8.1 \times 10^{-3}$	$3.3 \times 10^{-2}$
	355	$9.7 \times 10^{-3}$	$3.9 \times 10^{-2}$



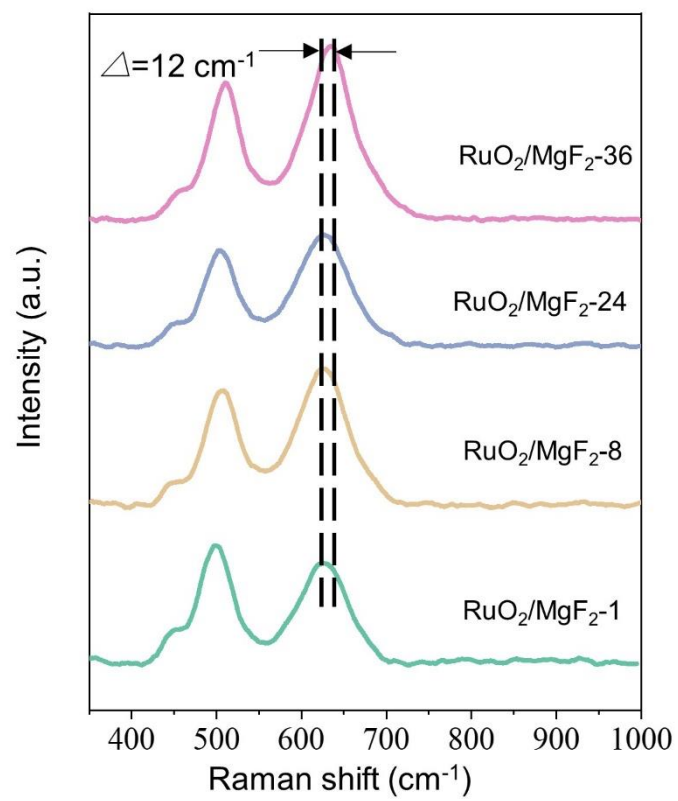
**Fig. S1.** Adsorption-desorption isotherms of N<sub>2</sub> on MgF<sub>2</sub>-SRT supports at -196.0 °C.



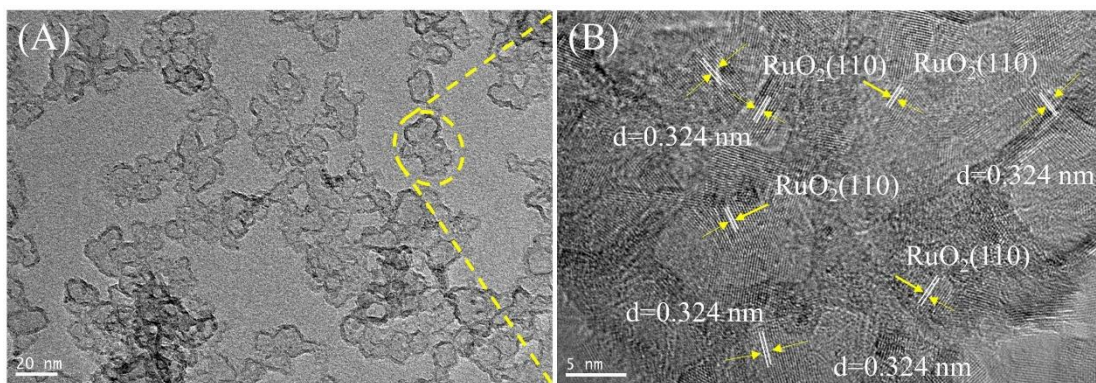
**Fig. S2.** SEM images of MgF<sub>2</sub>-SRT supports.



**Fig. S3.** Ru 3d XPS spectra of RuO<sub>2</sub>/MgF<sub>2</sub>-SRT catalysts.

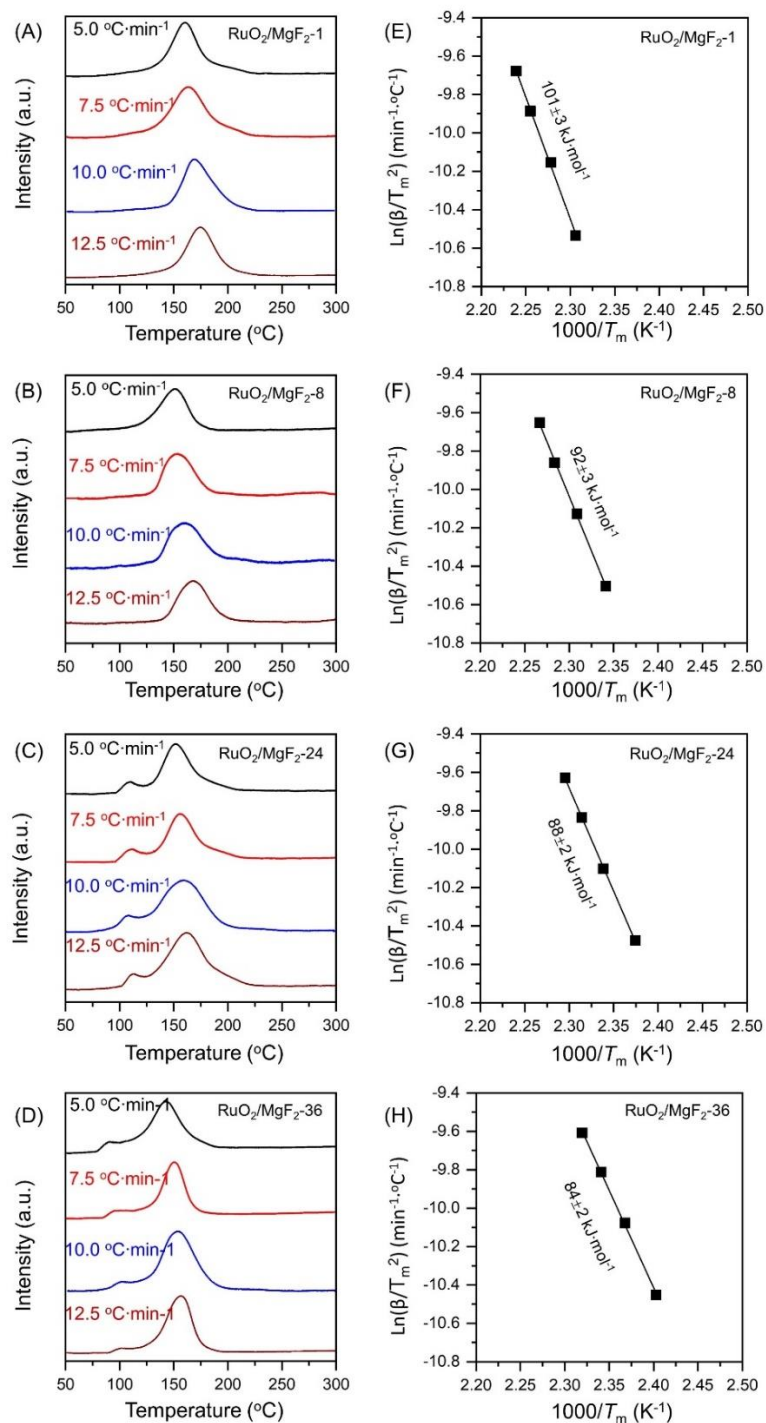


**Fig. S4.** Raman spectra of RuO<sub>2</sub>/MgF<sub>2</sub>-SRT catalysts.

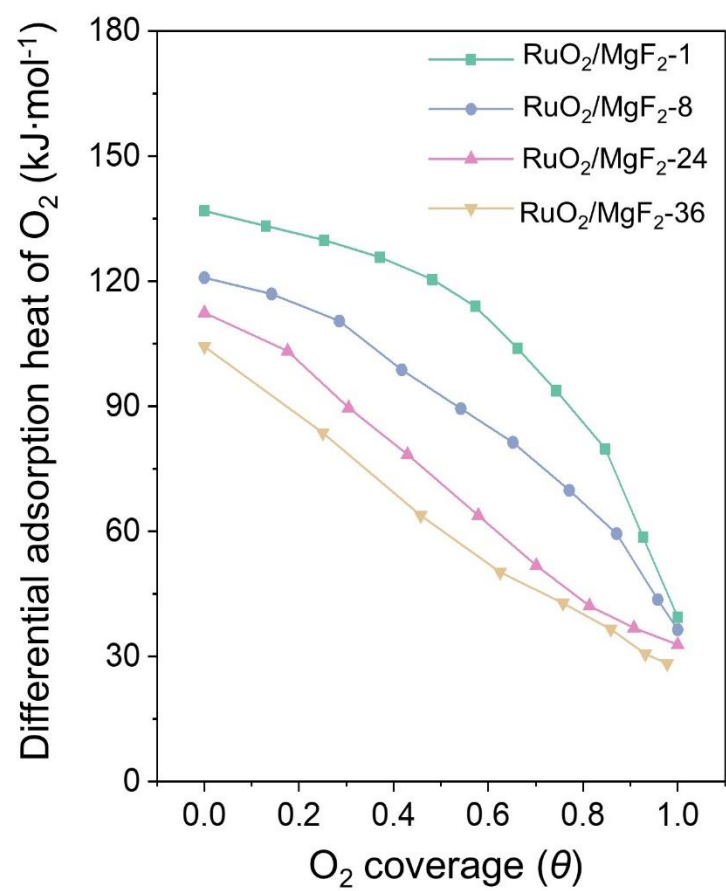


**Fig. S5.** TEM (A) and HRTEM (B) images of RuO<sub>2</sub>/MgF<sub>2</sub>-1 catalyst.

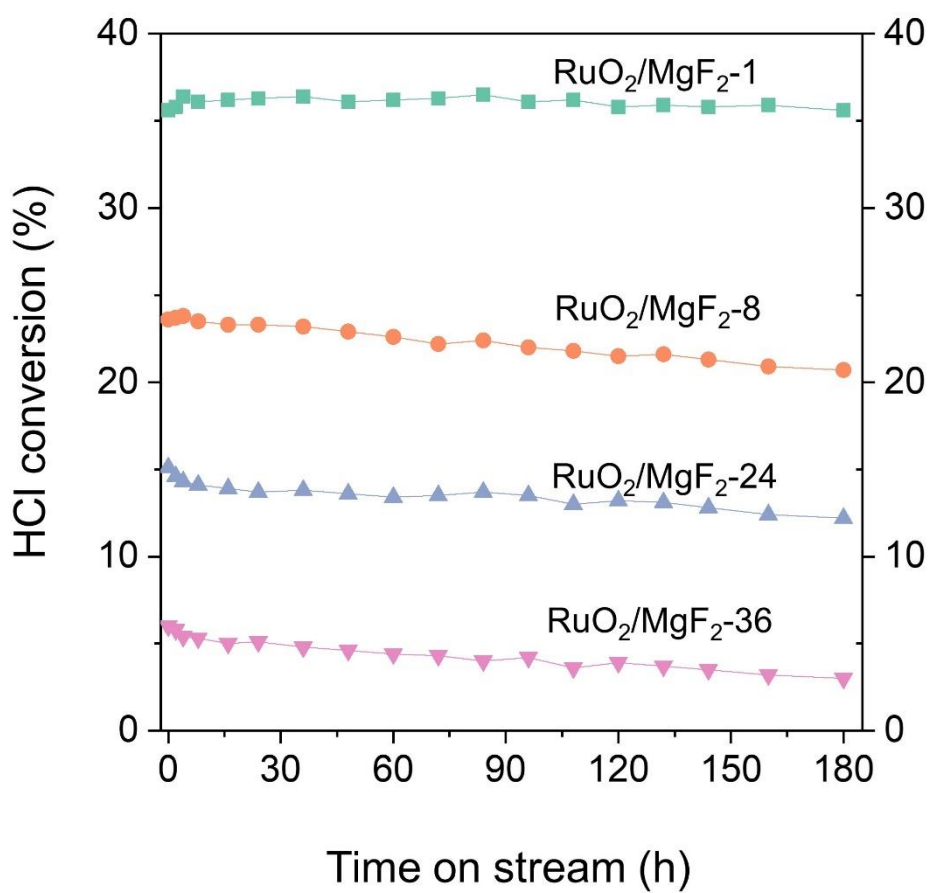




**Fig. S6.** H<sub>2</sub>-TPR curves at different heating rates for RuO<sub>2</sub>/MgF<sub>2</sub>-SRT catalysts and the Kissinger plots for the reduction peaks of RuO<sub>2</sub>/MgF<sub>2</sub>-SRT catalysts. The apparent activation energy of the Ru-O bond dissociation was calculated by the Kissinger equation.

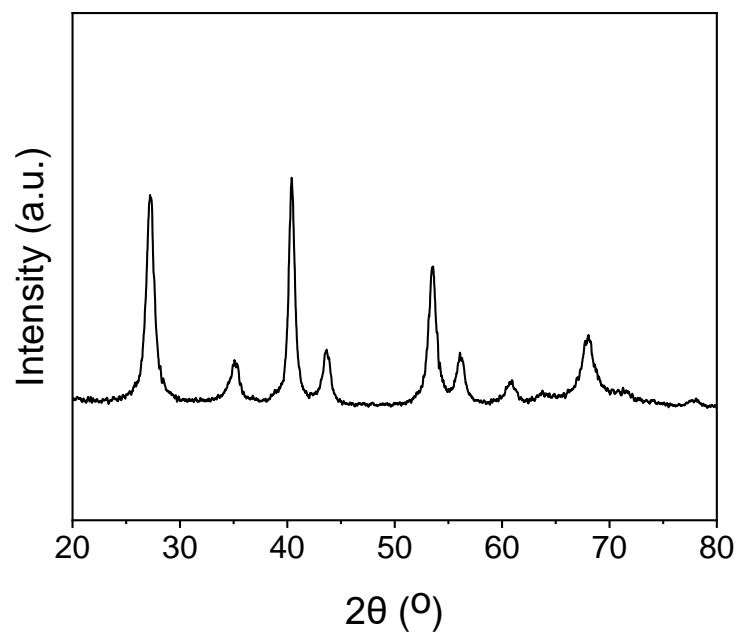


**Fig. S7.** Differential adsorption heat of O<sub>2</sub> on RuO<sub>2</sub>/MgF<sub>2</sub>-SRT as a function of O<sub>2</sub> coverage ( $\theta$ ) at 40.0 °C.

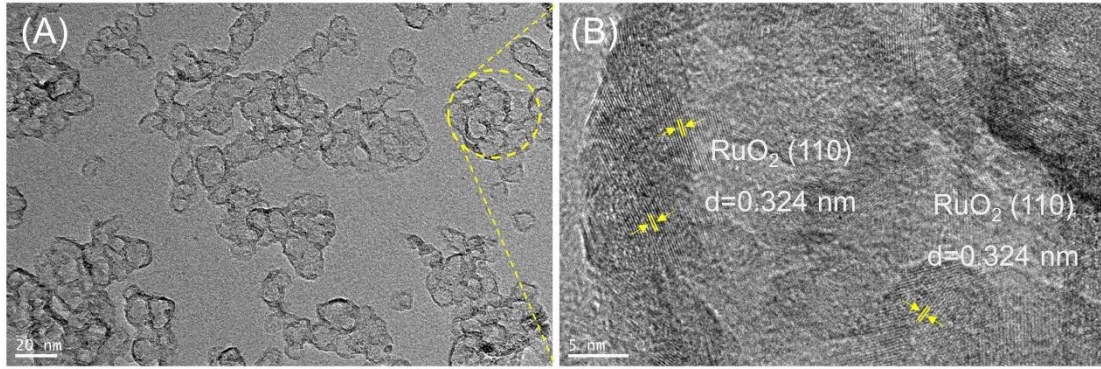


**Fig. S8.** HCl conversion as a function of time on stream over RuO<sub>2</sub>/MgF<sub>2</sub>-SRT catalysts.

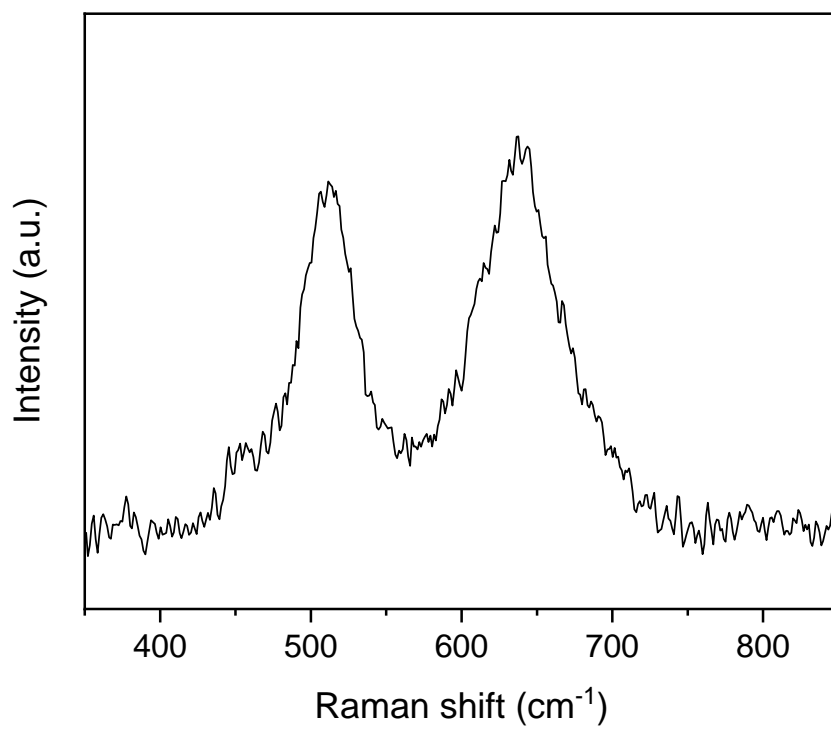
Reaction conditions: 350 °C and a GHSV of 48,000.0 mL (STP)·(h·g<sub>catal</sub>)<sup>-1</sup>.



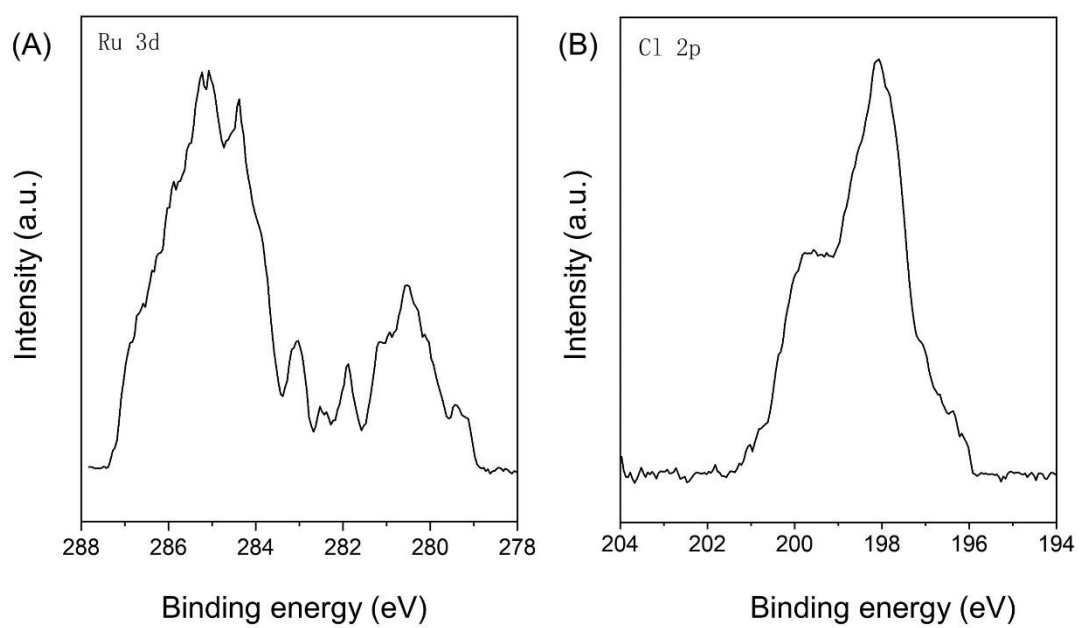
**Fig. S9.** XRD pattern of the used RuO<sub>2</sub>/MgF<sub>2</sub>-1 catalyst.



**Fig. S10.** TEM (A) and HRTEM (B) images of the used RuO<sub>2</sub>/MgF<sub>2</sub>-1 catalyst.



**Fig. S11.** Raman spectrum of the used RuO<sub>2</sub>/MgF<sub>2</sub>-1 catalyst.



**Fig. S12.** Ru 3d (A) and Cl 2p (B) XPS spectra of the used RuO<sub>2</sub>/MgF<sub>2</sub>-1 catalyst.