

Supplementary Information for
**A simple, sustainable route to flexible
microporous carbon cloth for energy storage
applications**

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1. Synthesis

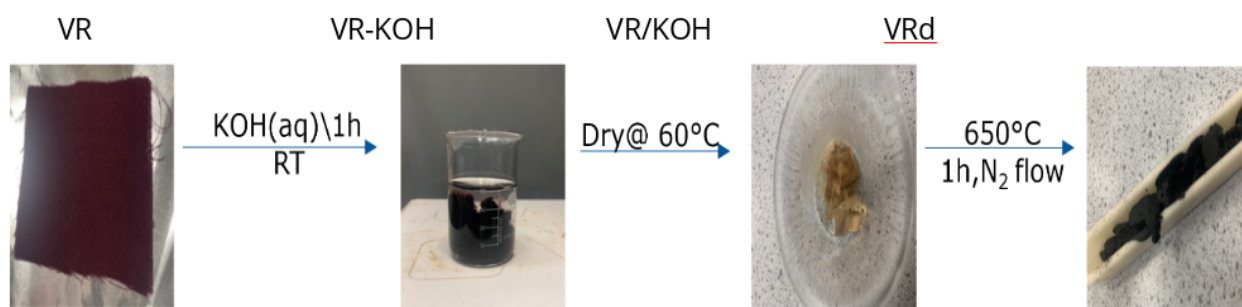


Fig. S1: Steps in the direct activation of viscose rayon (VR) with KOH. This process yields powdered activated carbon.

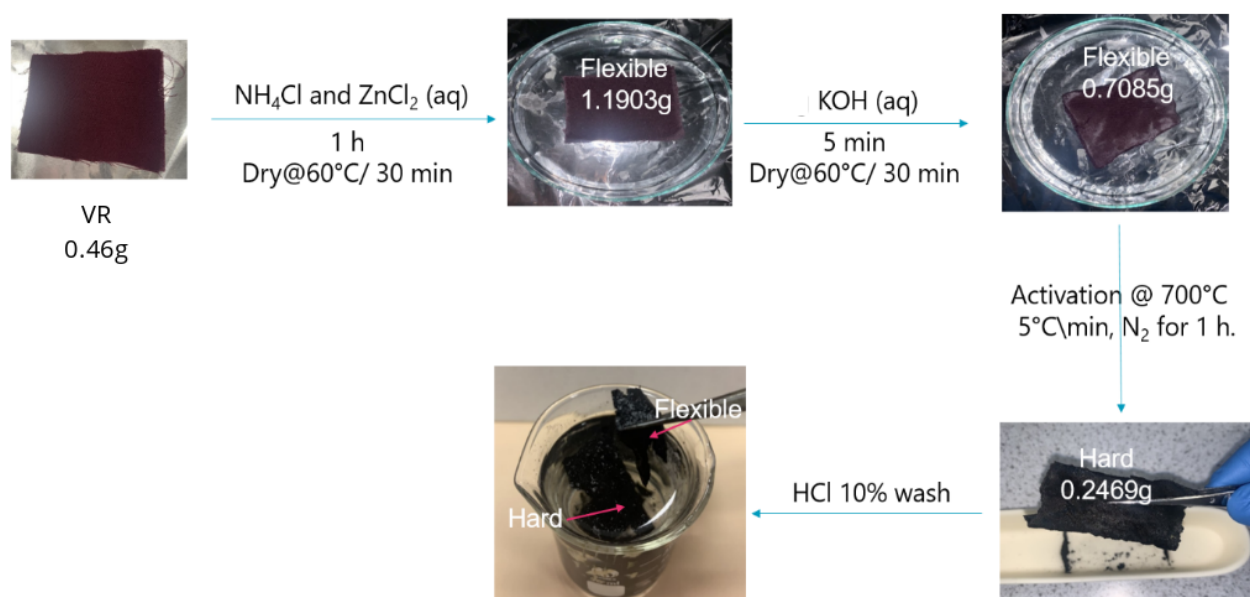


Fig. S2: Steps in the stabilisation of viscose rayon (VR) with NH₄Cl and ZnCl₂ prior to activation with KOH. This process yields both hard (powdered) and flexible activated carbon.

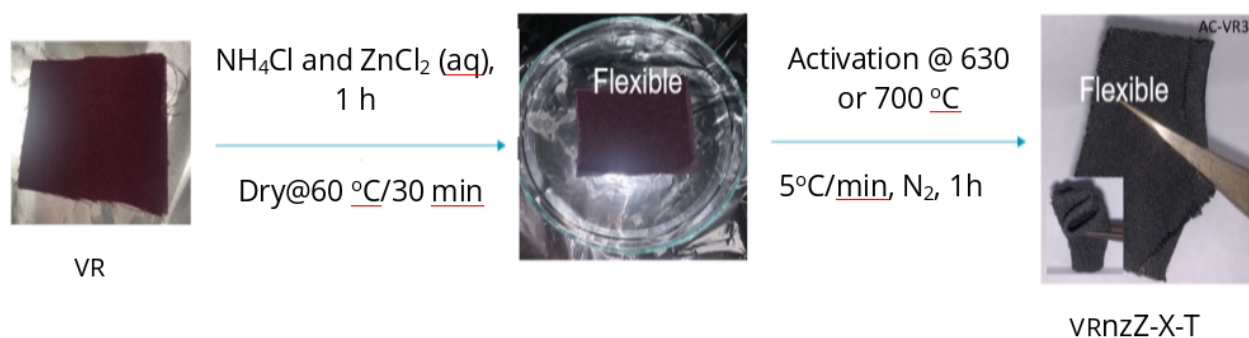


Fig. S3: Steps in the stabilisation of viscose rayon (VR) with NH_4Cl and ZnCl_2 prior to thermal treatment to facilitate activation with the latter (ZnCl_2). This process yields flexible activated carbon cloth - series VRnzZ-X-T.

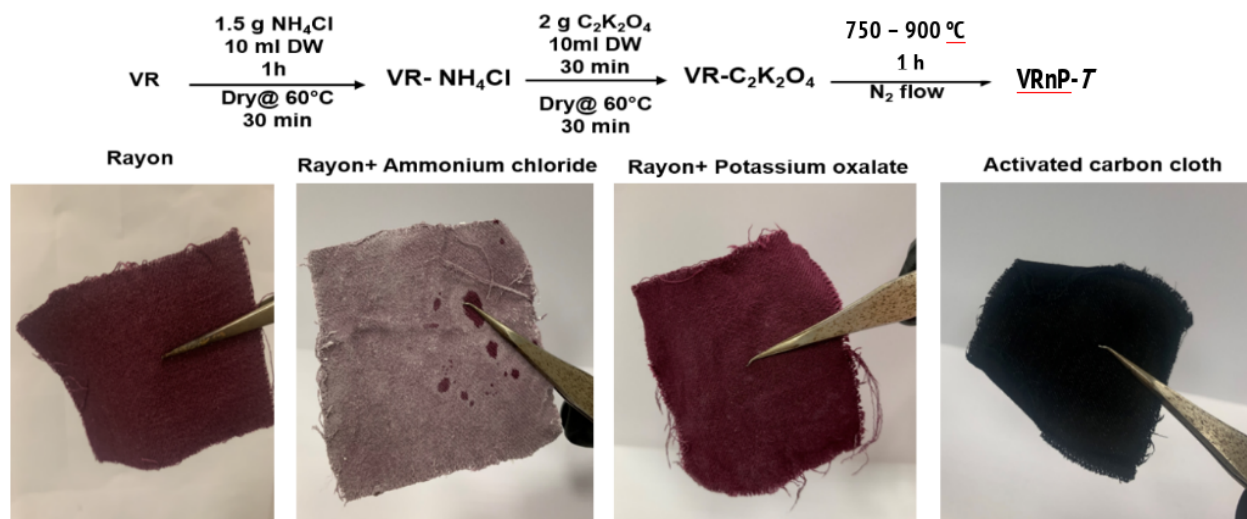


Fig. S4: Steps in the stabilisation of viscose rayon (VR) with NH_4Cl only followed by activation with PO. This process yields flexible activated carbon cloth - series VRnP-T.

2. Powder X-ray Diffraction

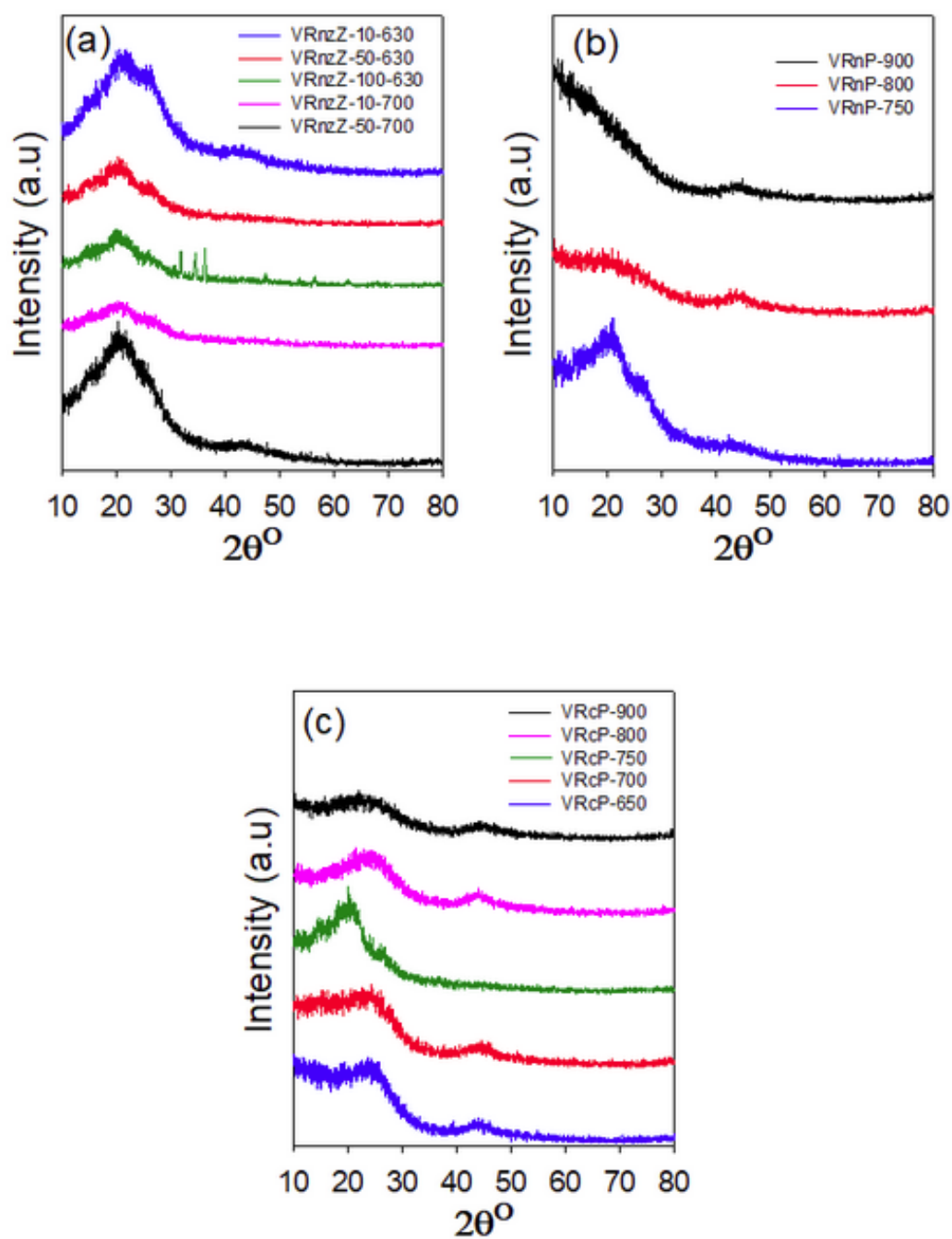


Fig. S5: XRD patterns of flexible VR-derived ACCs; (a) series VRnzZ-X-T, (b) series VRnP-T, and (c) series VRcP-T.

3. Thermogravimetric Analysis

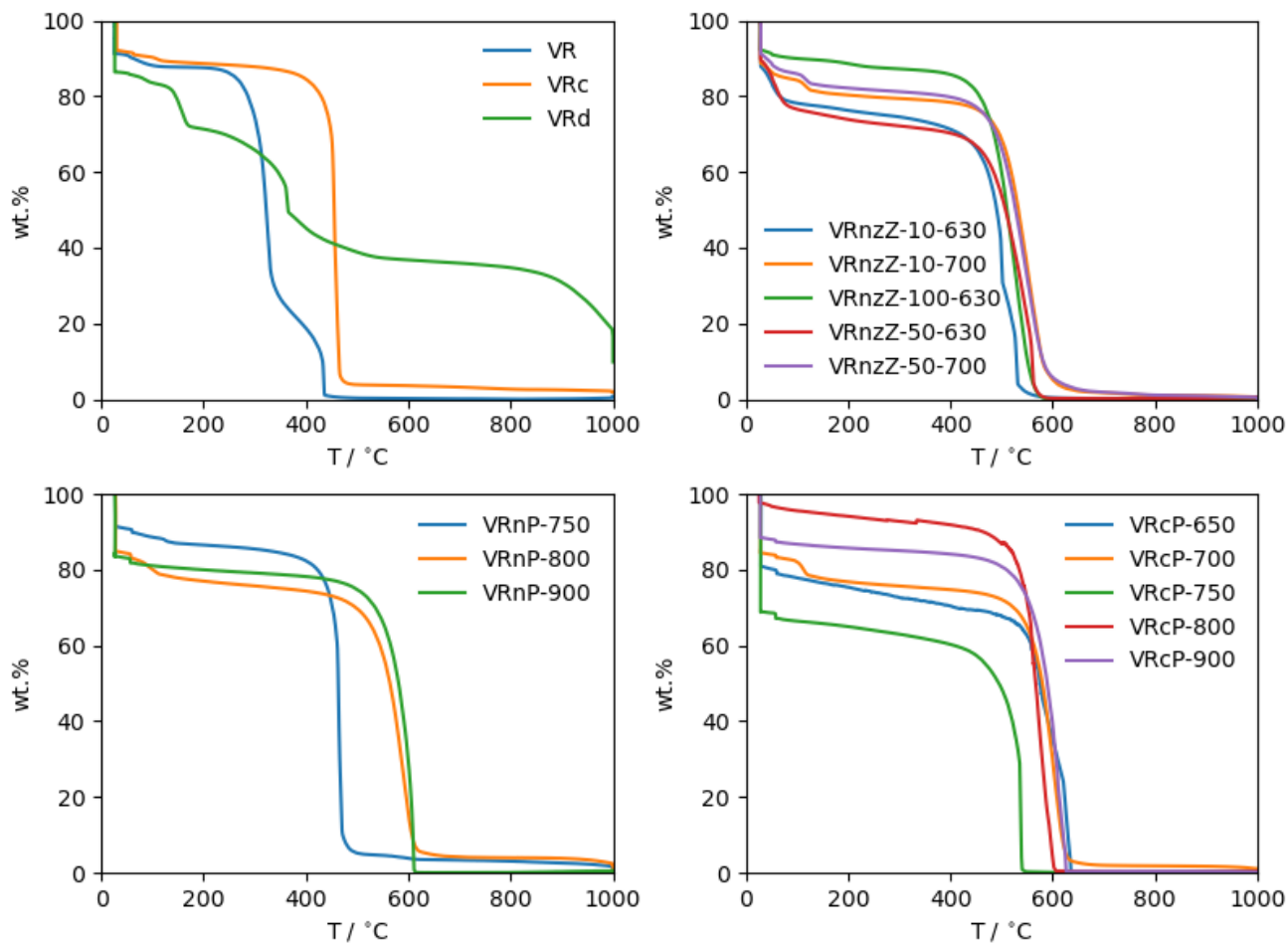


Fig. S6: TGA curves of VR, powdered carbons and flexible ACCs synthesised in this work.

4. Scanning electron Microscopy

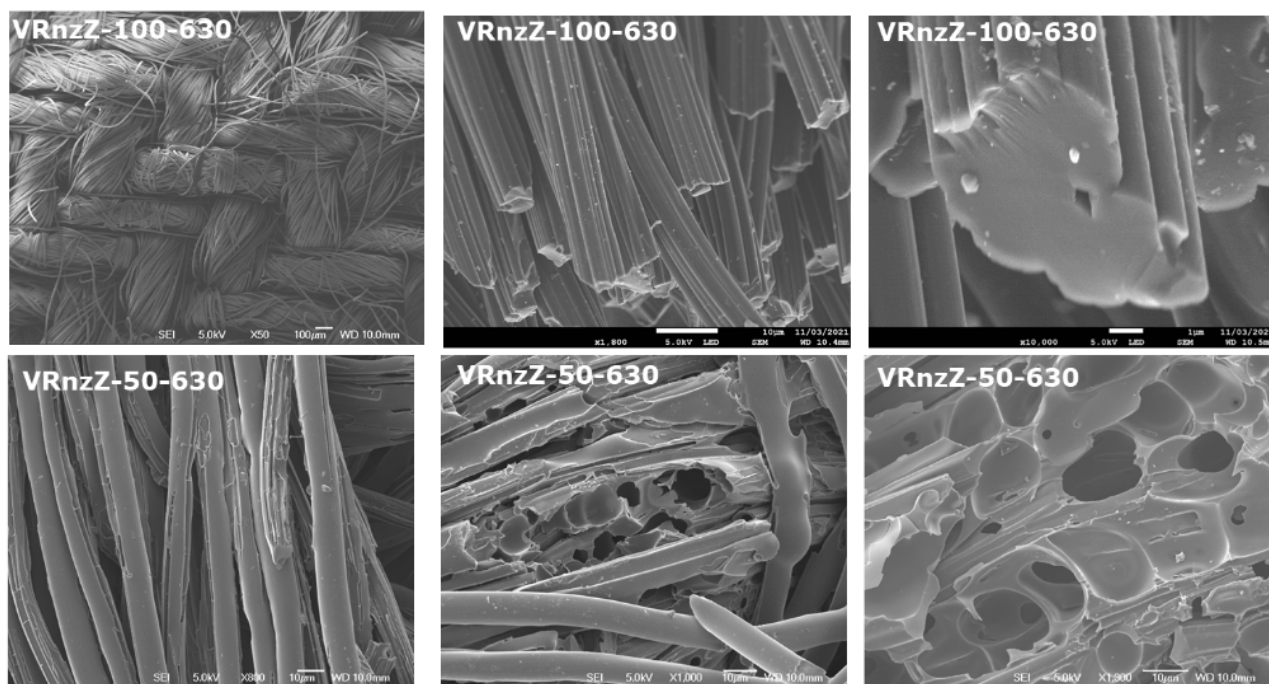


Fig. S7: SEM images of series VRnzZ-X-T flexible VR-derived ACCs activated at 630 °C.

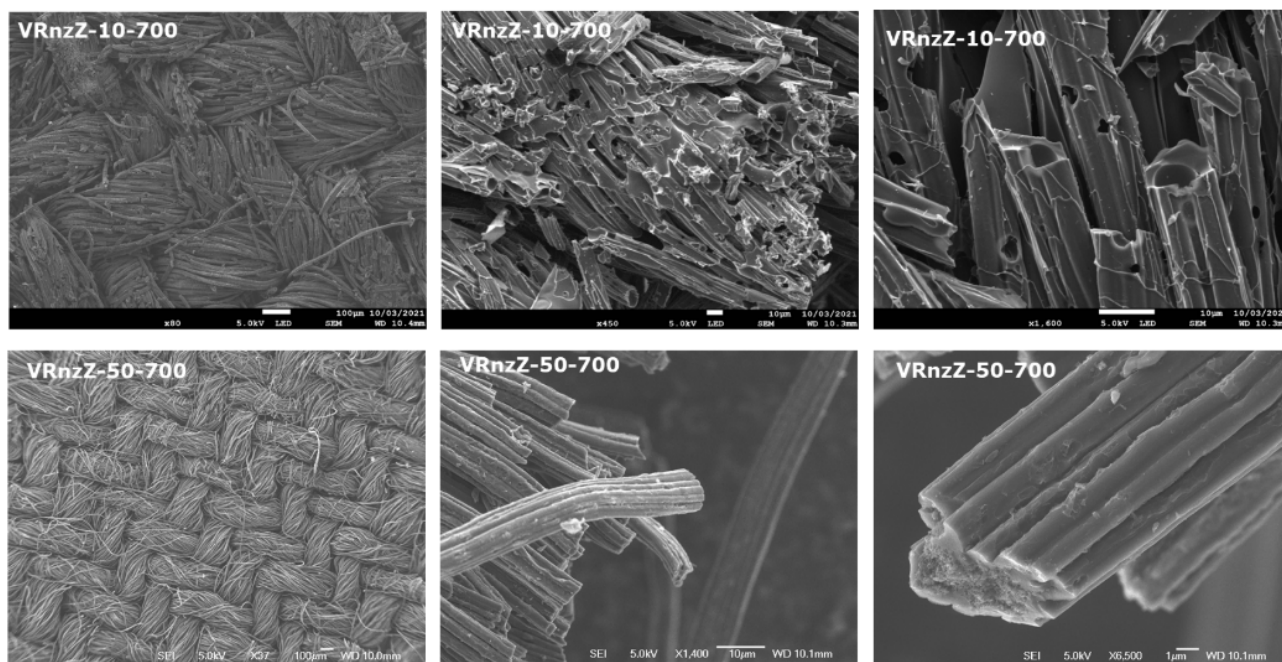


Fig. S8: SEM images of series VRnzZ-X-T flexible VR-derived ACCs activated at 700 °C.

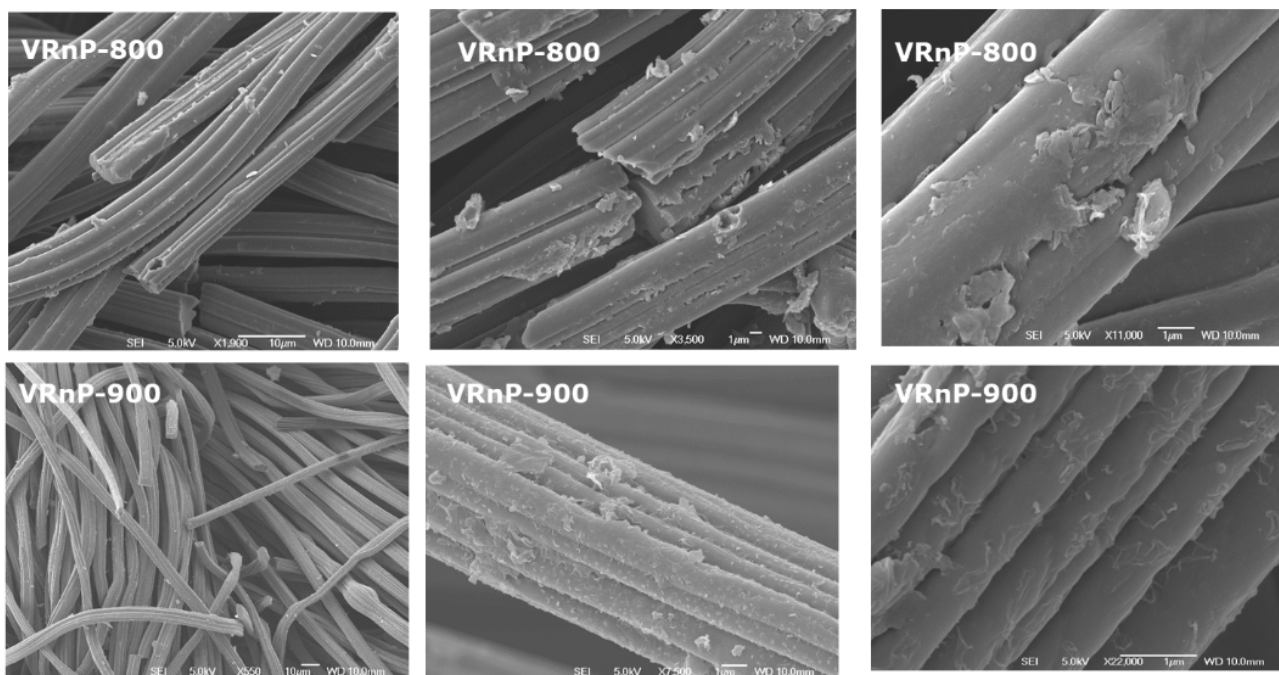


Fig. S9: SEM images of VRnP-*T* flexible VR-derived ACCs.

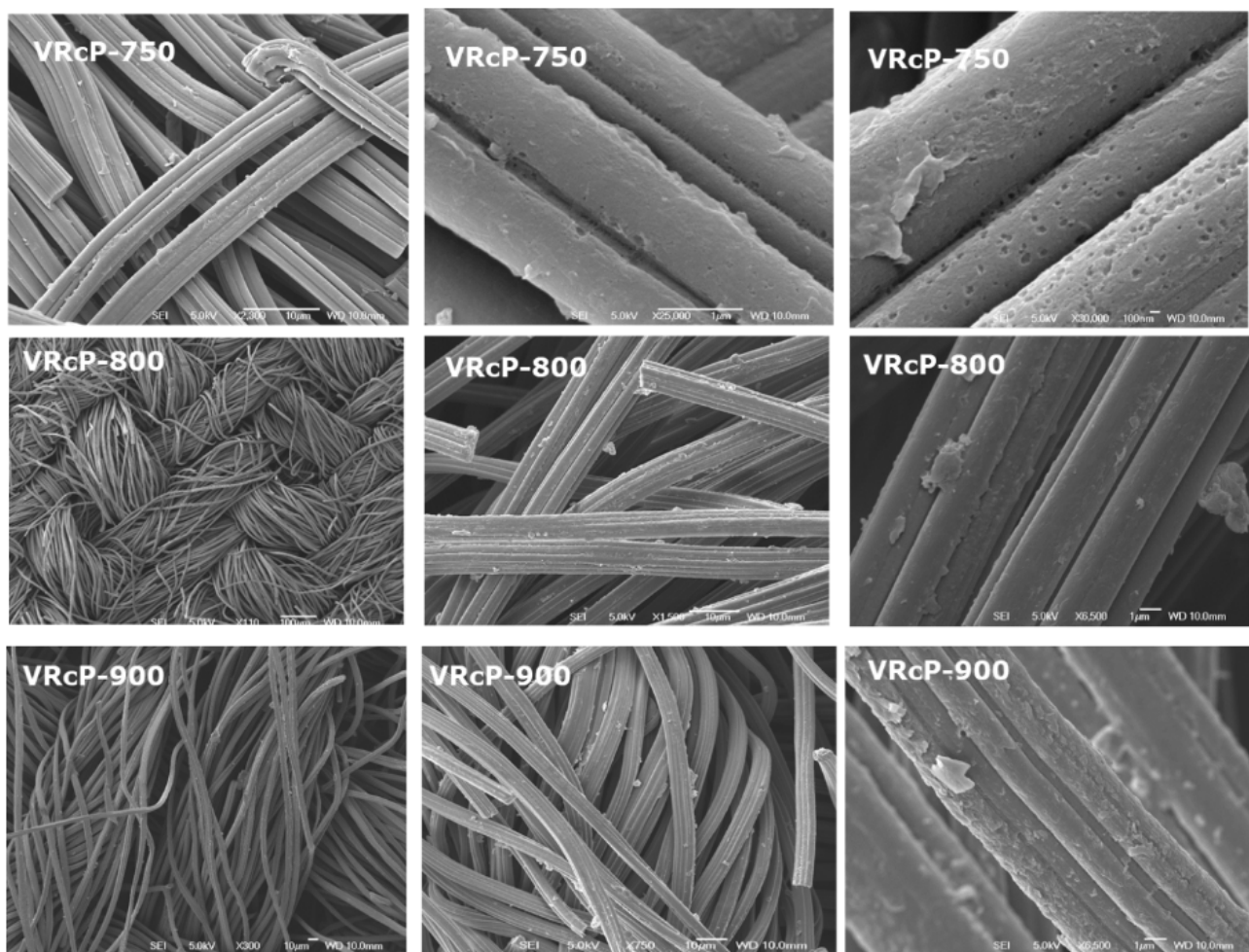


Fig. S10: SEM images of series VRcP-*T* flexible VR-derived ACCs

5. Isotherm measurement conditions

Table S1: Conditions used for measuring N_2 isotherms for porosimetry. Pressure points either controlled by initial and final relative pressure, a relative pressure increment or quantity of gas dosed. Equilibration time (t_E) was higher at low pressures due to equilibration issues in small pores.^{S1}

P/P_0 initial	P/P_0 increment	dose / $\text{cm}^3 \text{g}^{-1} \text{stp}$	t_E / s	P/P_0 final
0.00e+00		10	45	4.00e-04
4.00e-04		25	35	1.00e-01
1.00e-01	0.05		10	1.50e-01
1.50e-01	0.05		10	2.00e-01
2.00e-01	0.05		10	2.50e-01
2.50e-01	0.05		10	3.00e-01
3.00e-01	0.05		10	3.50e-01
3.50e-01	0.05		10	4.00e-01
4.00e-01	0.05		10	4.50e-01
4.50e-01	0.05		10	5.00e-01
5.00e-01	0.05		10	5.50e-01
5.50e-01	0.05		10	6.00e-01
6.00e-01	0.05		10	6.50e-01
6.50e-01	0.05		10	7.00e-01
7.00e-01	0.05		10	7.50e-01
7.50e-01	0.05		10	8.00e-01
8.00e-01	0.05		10	8.50e-01
8.50e-01	0.05		10	9.00e-01
9.00e-01	0.05		10	9.50e-01
9.50e-01			10	9.90e-01
9.90e-01			10	9.95e-01
9.95e-01			10	9.98e-01
9.98e-01			10	9.95e-01
9.95e-01			10	9.90e-01
9.90e-01			10	9.50e-01
9.50e-01			10	9.00e-01
9.00e-01			10	8.50e-01
8.50e-01			10	8.00e-01
8.00e-01			10	7.50e-01
7.50e-01			10	7.00e-01
7.00e-01			10	6.50e-01
6.50e-01			10	6.00e-01
6.00e-01			10	5.50e-01
5.50e-01			10	5.00e-01
5.00e-01			10	4.50e-01
4.50e-01			10	4.00e-01
4.00e-01			10	3.50e-01
3.50e-01			10	3.00e-01
3.00e-01			10	2.50e-01
2.50e-01			10	2.00e-01
2.00e-01			10	1.50e-01
1.50e-01			10	1.00e-01

6. BETSI analysis

BETSI analysis^{S2} was performed with the constraints of having maximum percentage error of 20%, a minimum r^2 of 0.995, and starting with a minimum number of 10 points. In cases where a 10 point range could not be found to satisfy the other requirements, this number was reduced and the calculation repeated until a fit could be achieved - in this study this only applied to VRnzZ-10-700. Results summary is tabulated in table S2.

Table S2: Summary of BETSI results for optimum fitting. An r^2 of >0.9999 was consistently rounded down as opposed to rounding up to 1.0000 as to not give the false impression of a perfect fit.

Sample	$A_{BET}/m^2 g^{-1}$	points	r^2	Slope	intercept	C	$Q_m / cm^3 g^{-1} stp$
VRd	939	11	0.9996	0.004635	2.144×10^{-7}	21620	215.7
VRnzK-700 (hard)	1503	12	0.9999	0.002892	3.789×10^{-6}	764.2	345.3
VRnzK-700 (flexible)	1010	29	0.9999	0.004302	7.652×10^{-6}	563.1	232.1
VRnzZ-10-630	947	11	0.9999	0.004596	2.641×10^{-6}	1741	217.4
VRnzZ-50-630	1222	11	0.9999	0.003561	1.248×10^{-6}	2856	280.7
VRnzZ-100-630	926	21	0.9998	0.004700	6.125×10^{-8}	76740	212.8
VRnzZ-10-700	598	7	0.9999	0.007284	1.573×10^{-7}	46290	137.3
VRnzZ-50-700	965	11	0.9999	0.004509	1.025×10^{-6}	4399	221.7
VRnP-750	1934	11	0.9999	0.002250	1.346×10^{-6}	1673	444.2
VRnP-800	993	11	0.9999	0.004381	1.039×10^{-6}	4220	228.2
VRnP-900	1095	11	0.9999	0.003971	1.546×10^{-6}	2570	251.7
VRc	85	11	0.9996	0.05139	4.637×10^{-5}	1109	19.44
VRcP-650	942	11	0.9996	0.004619	2.584×10^{-7}	17870	216.5
VRcP-700	1013	11	0.9996	0.004298	3.553×10^{-7}	12100	232.6
VRcP-750	2227	11	0.9996	0.001953	1.740×10^{-6}	1123	511
VRcP-800	713	11	0.9999	0.006107	2.005×10^{-6}	3048	163.7
VRcP-900	701	11	0.9999	0.006209	1.478×10^{-6}	4202	701.1

BETSI Analysis for VRc

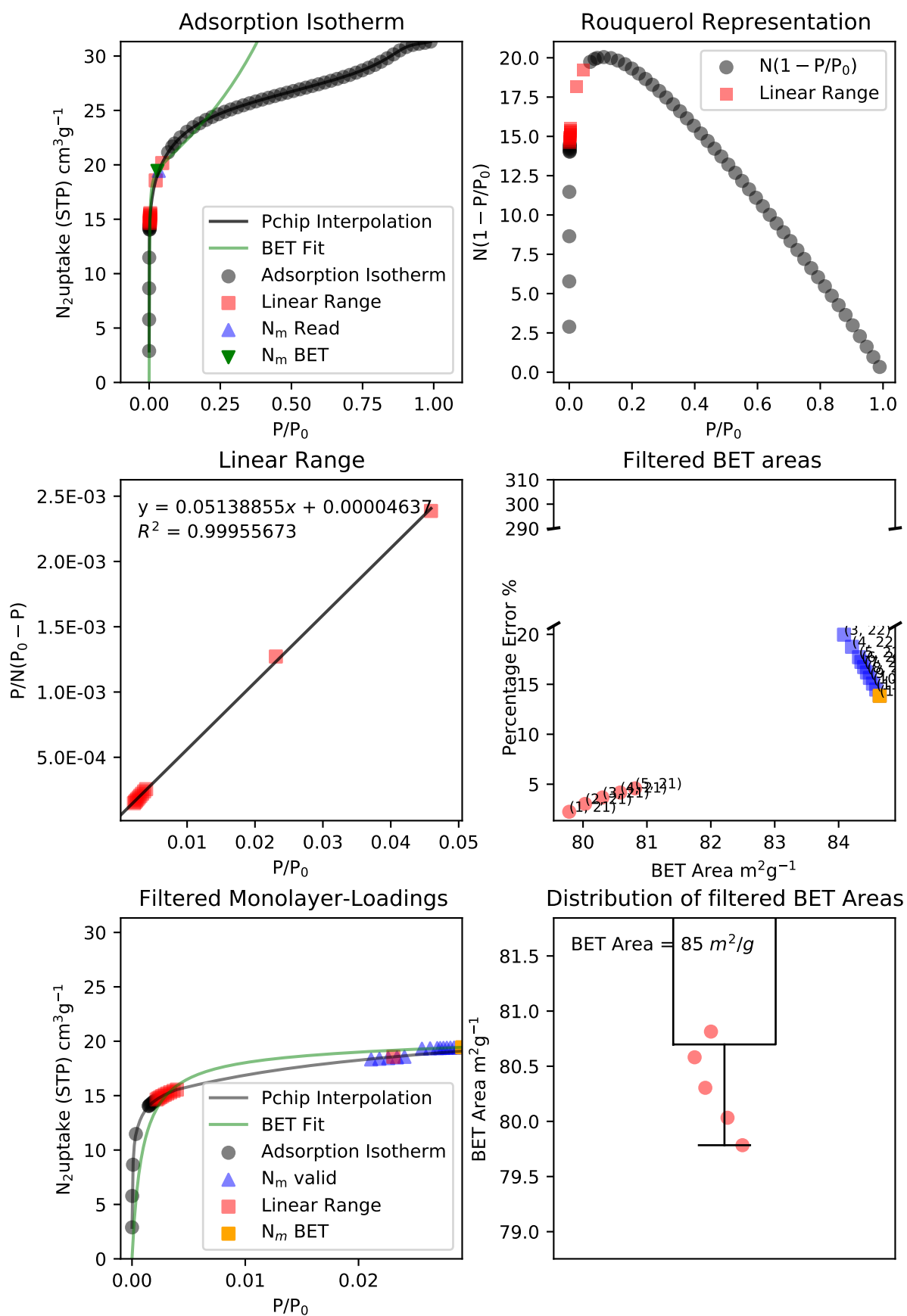


Fig. S11: BETSI analysis for VRc.

BETSI Analysis for VRcP-650

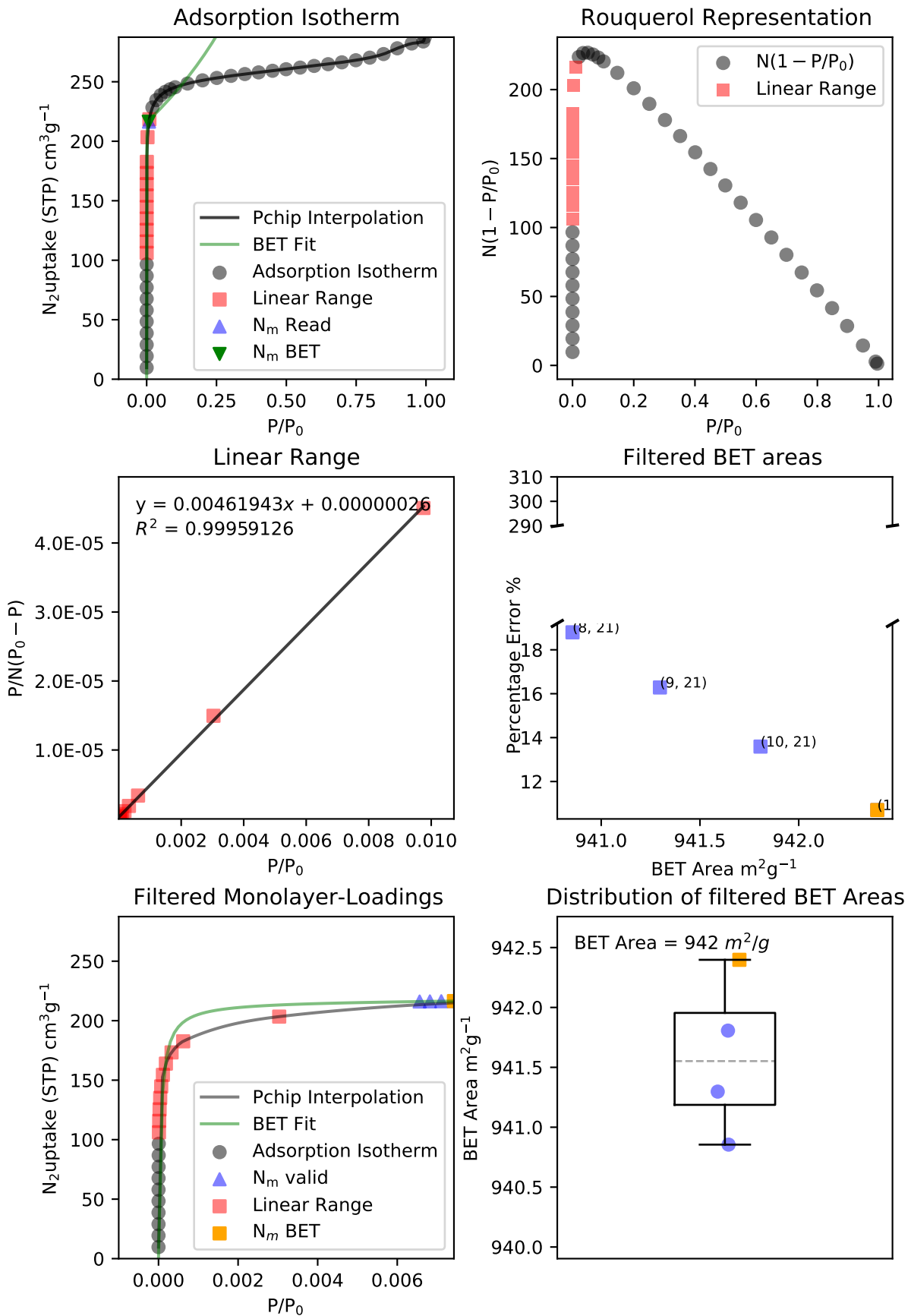


Fig. S12: BETSI analysis for VRcP-650.

BETSI Analysis for VRcP-700

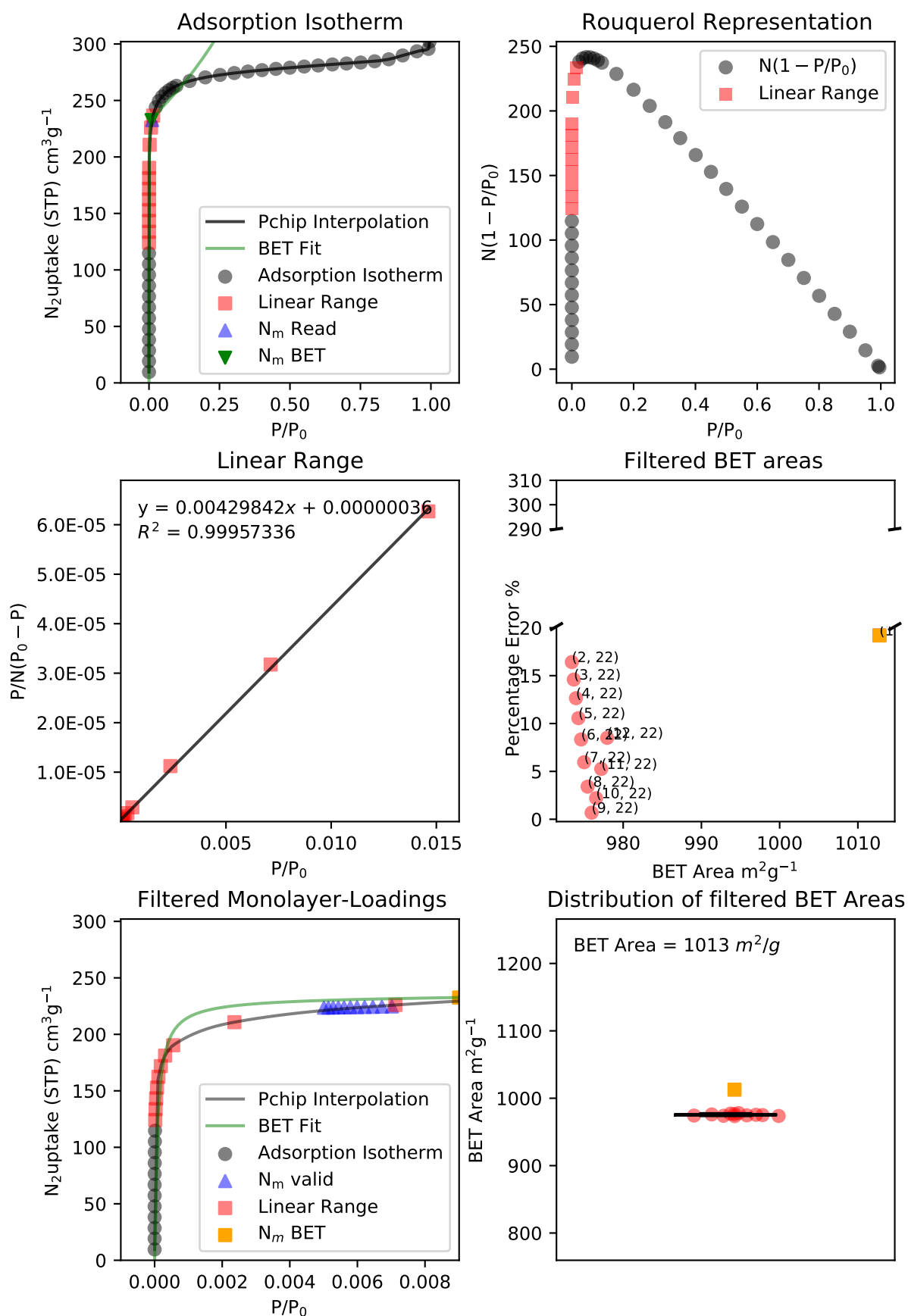


Fig. S13: BETSI analysis for VRcP-700.

BETSI Analysis for VRcP-750

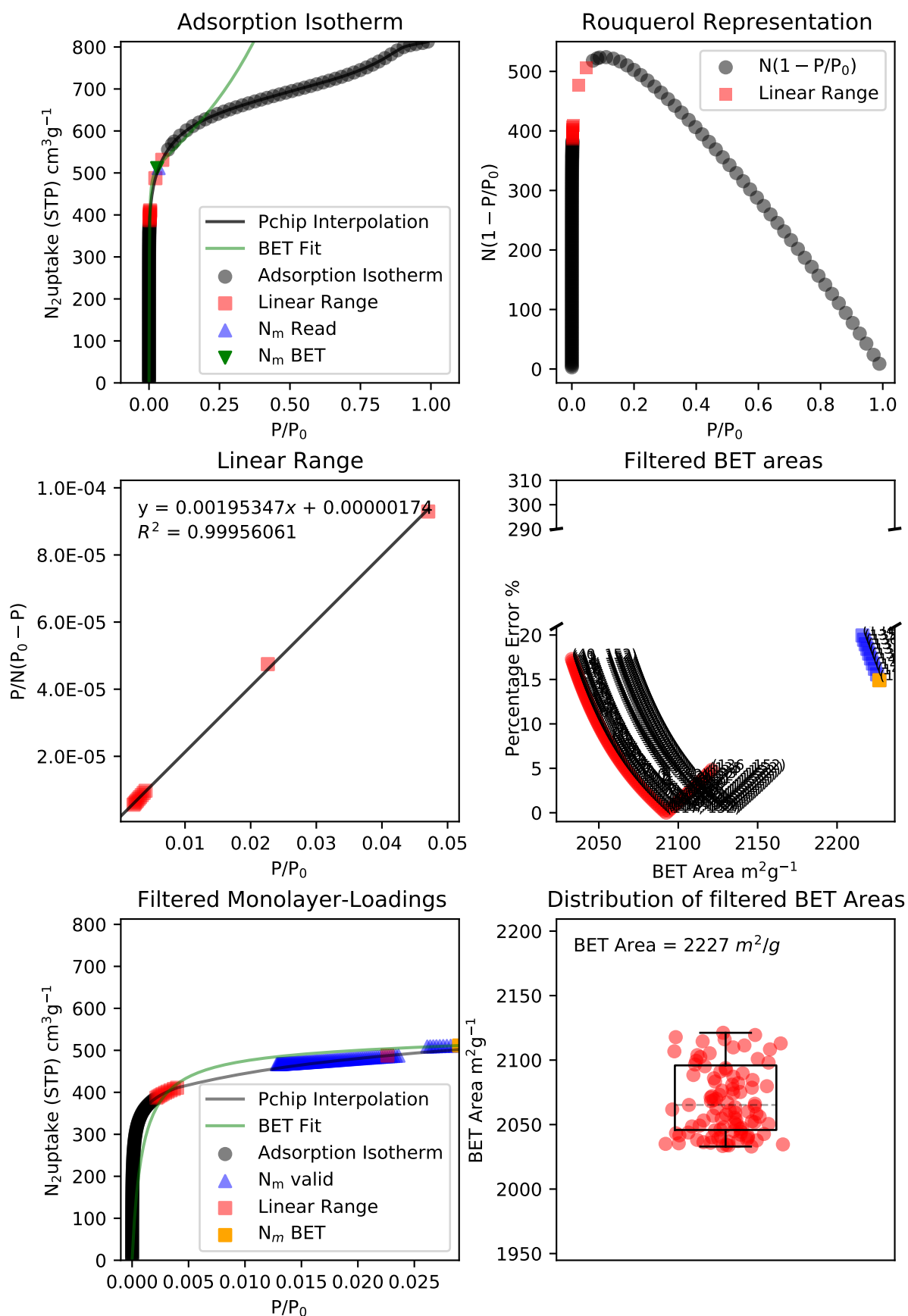


Fig. S14: BETSI analysis for VRcP-750.

BETSI Analysis for VRcP-800

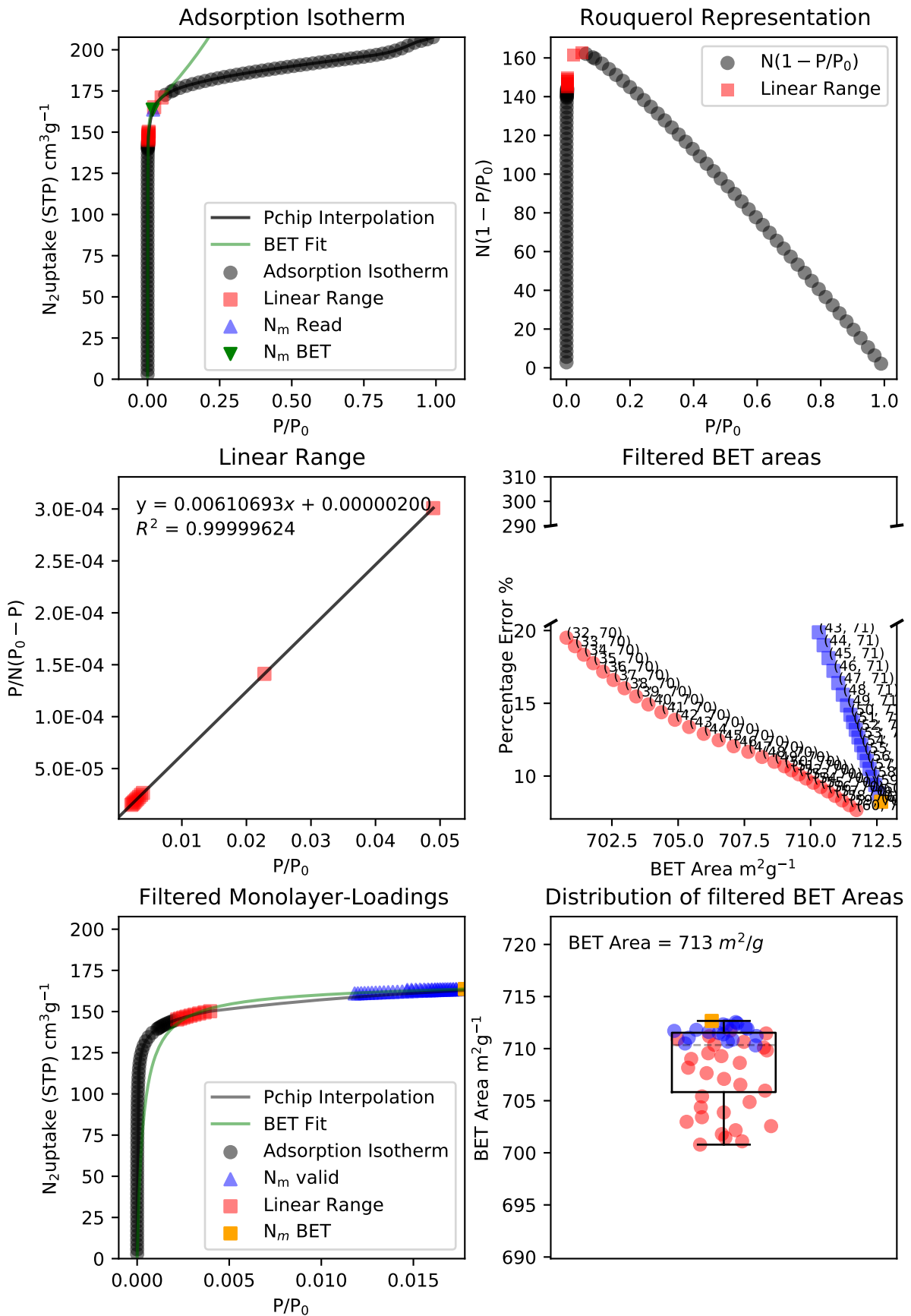


Fig. S15: BETSI analysis for VRcP-800.

BETSI Analysis for VRcP-900

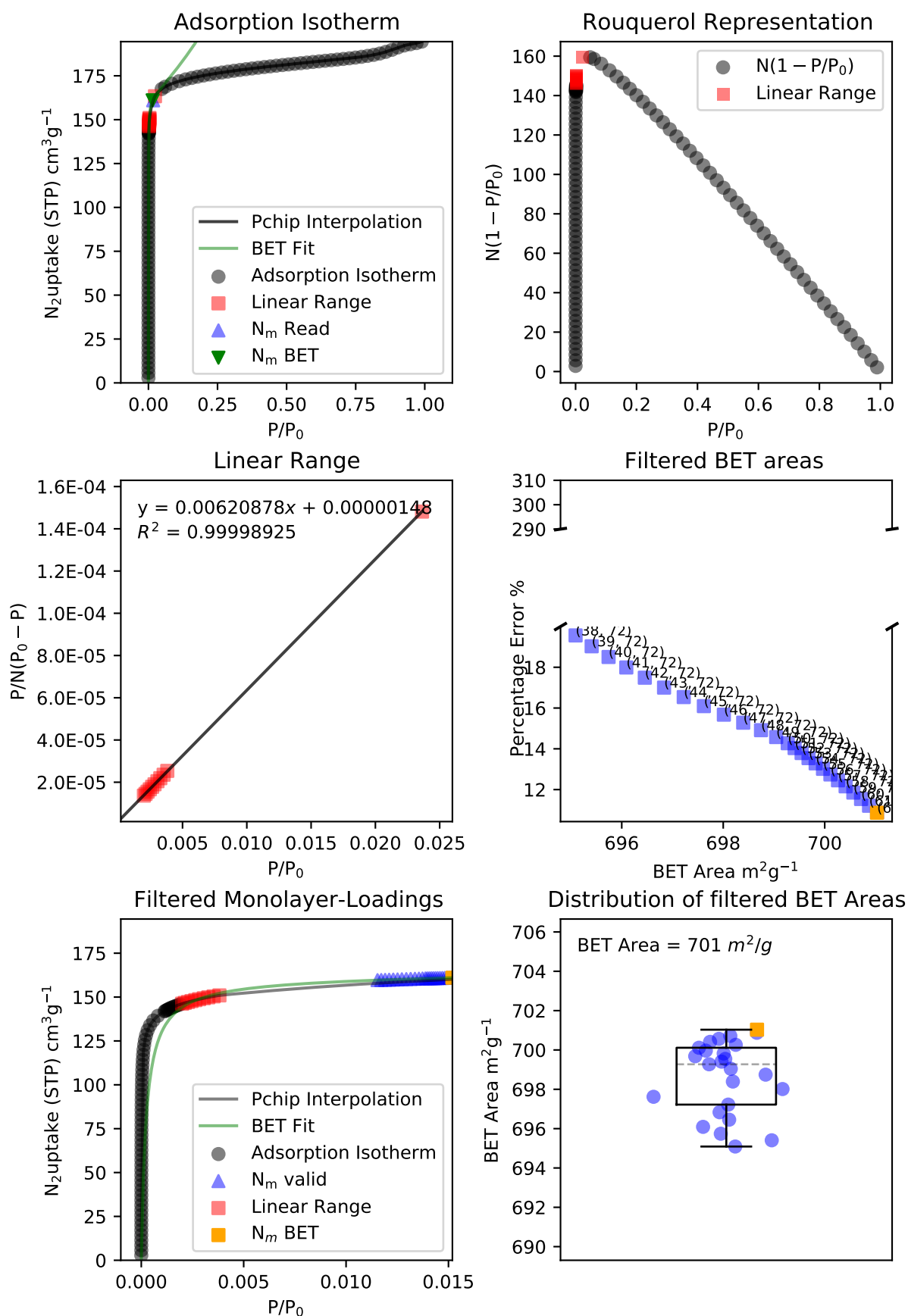


Fig. S16: BETSI analysis for VRcP-900.

BETSI Analysis for VRd

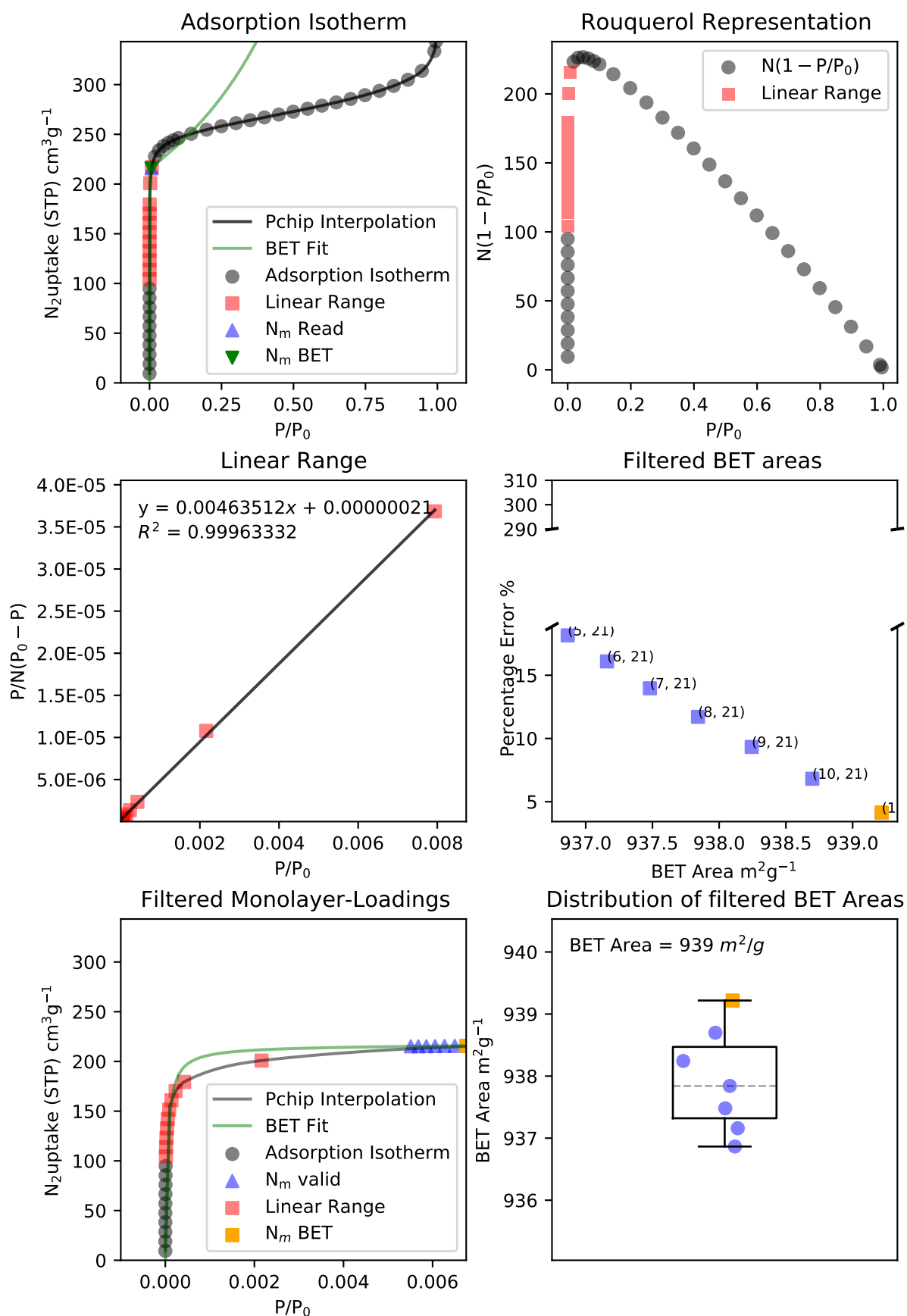


Fig. S17: BETSI analysis for VRd.

BETSI Analysis for VRnP-800

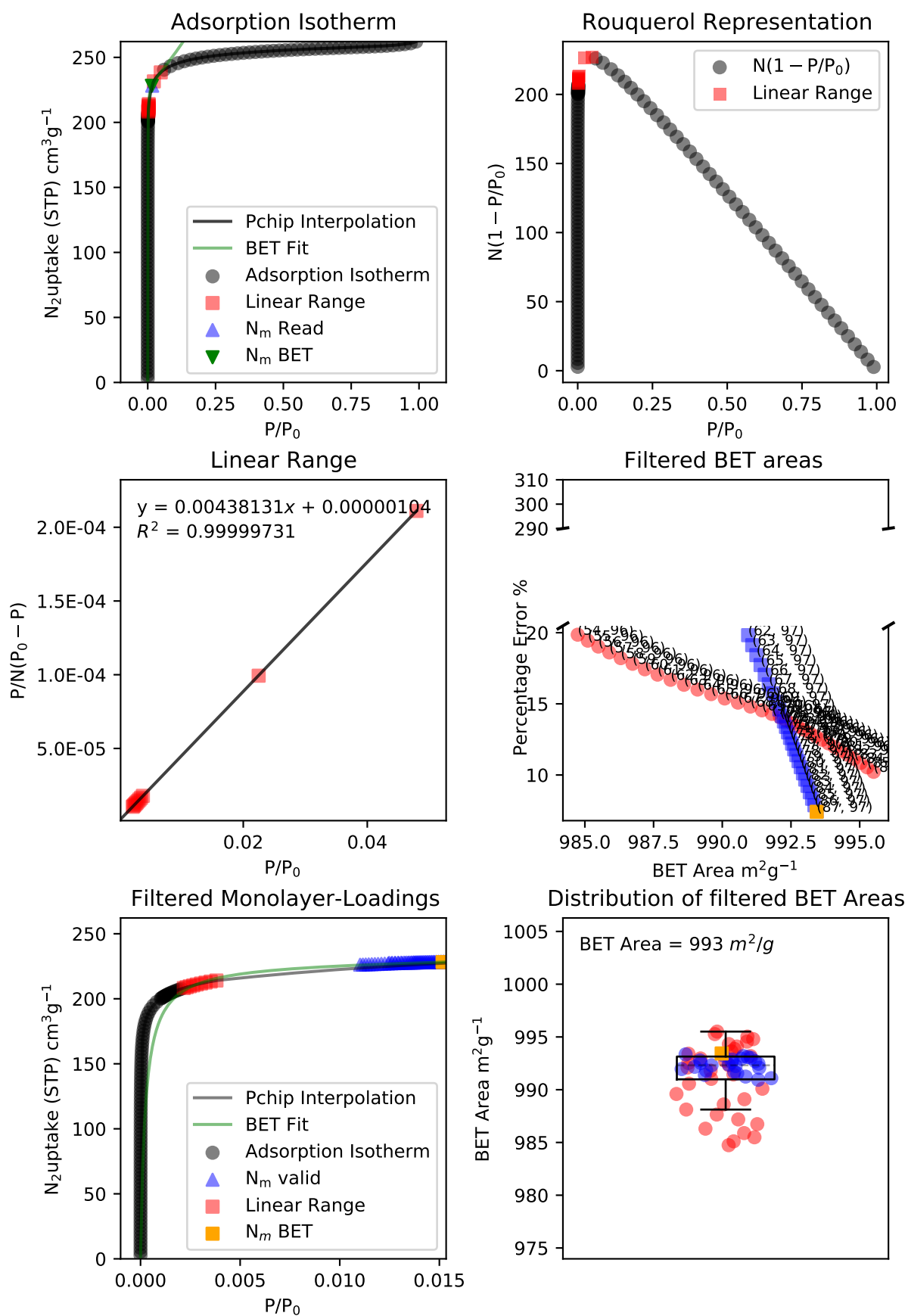


Fig. S19: BETSI analysis for VRnP-800.

BETSI Analysis for VRnP-900

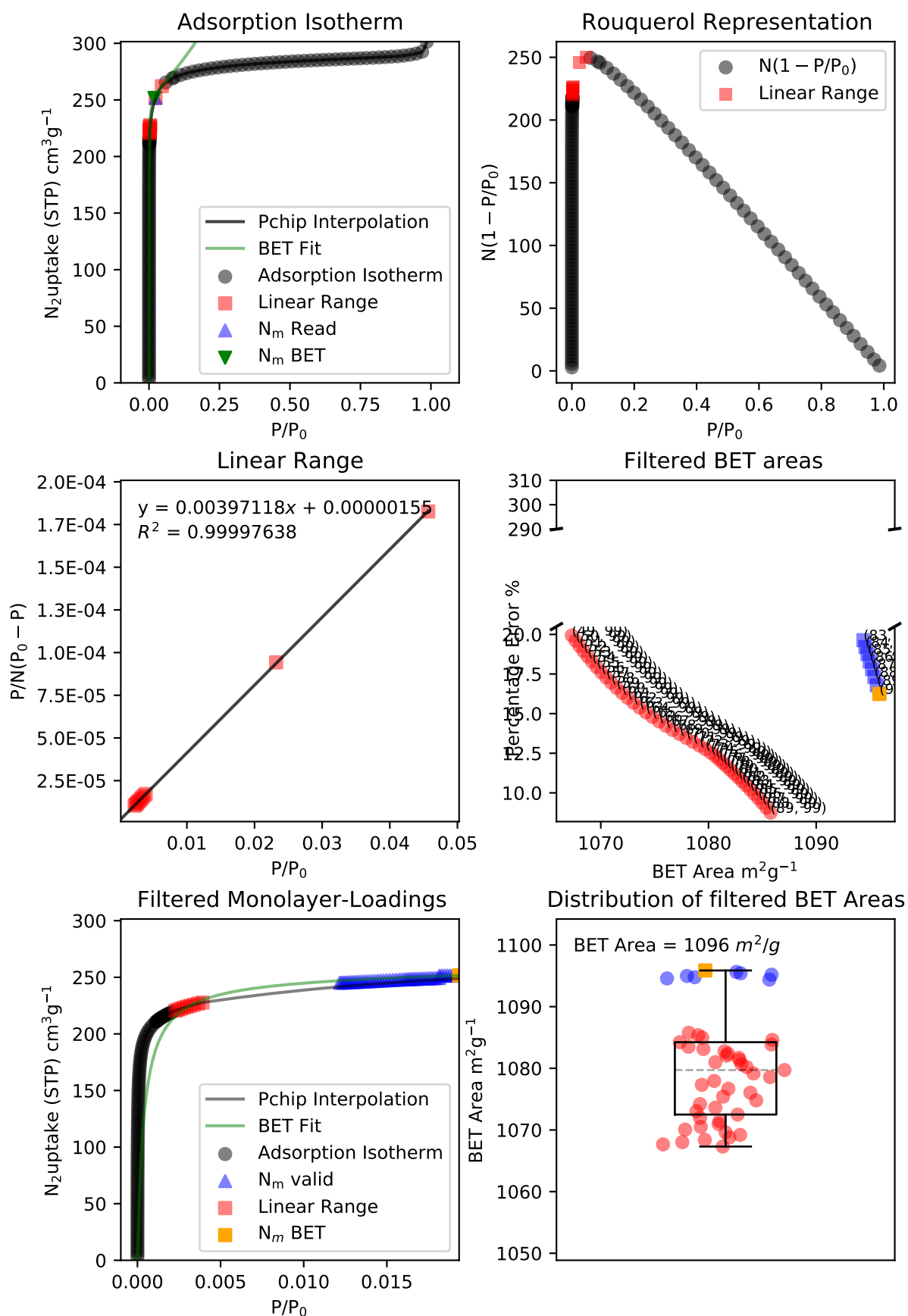


Fig. S20: BETSI analysis for VRnP-900.

BETSI Analysis for VRnzK (Flexible)

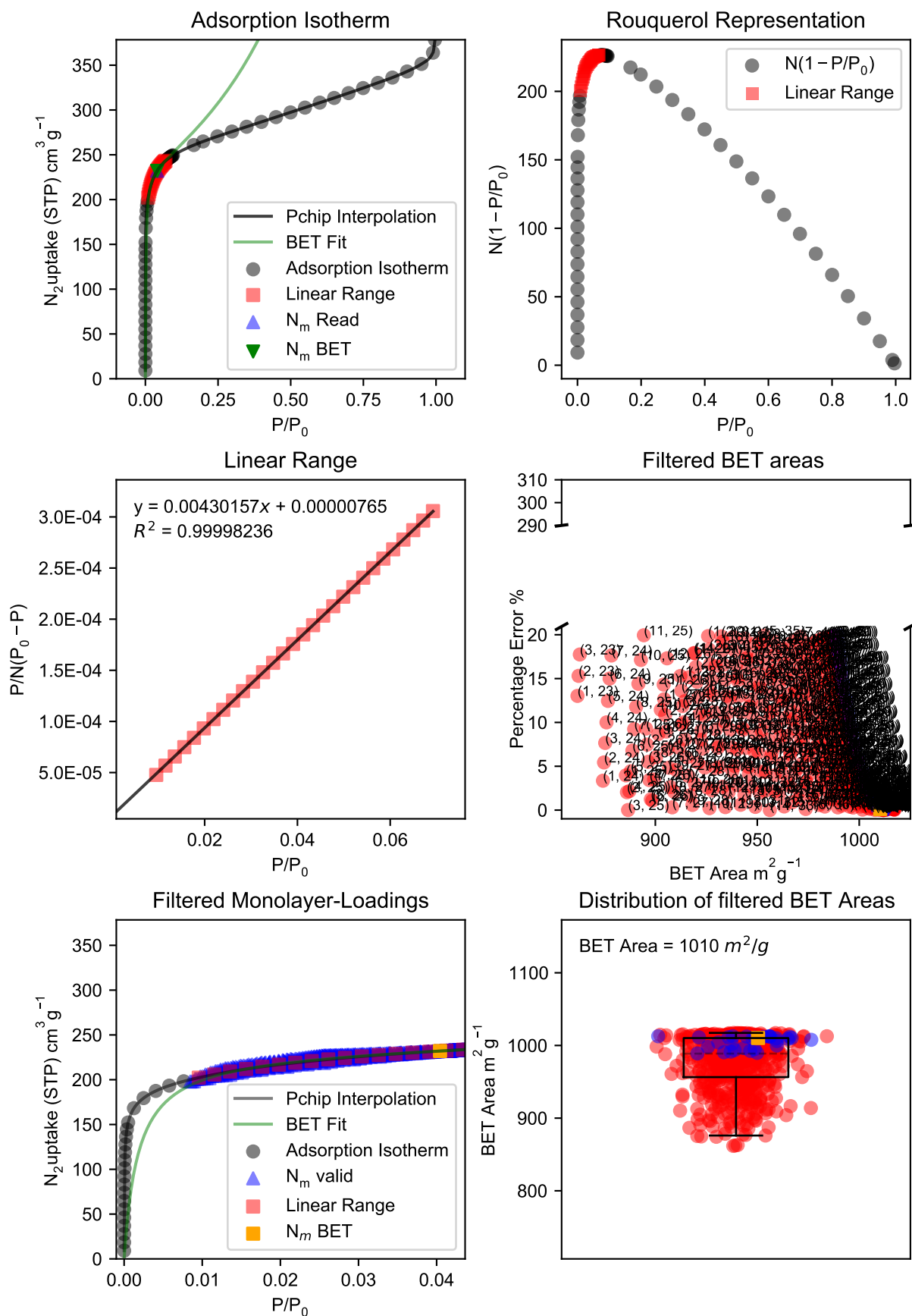


Fig. S21: BETSI analysis for VRnzK (flexible).

BETSI Analysis for VRnzK (Hard)

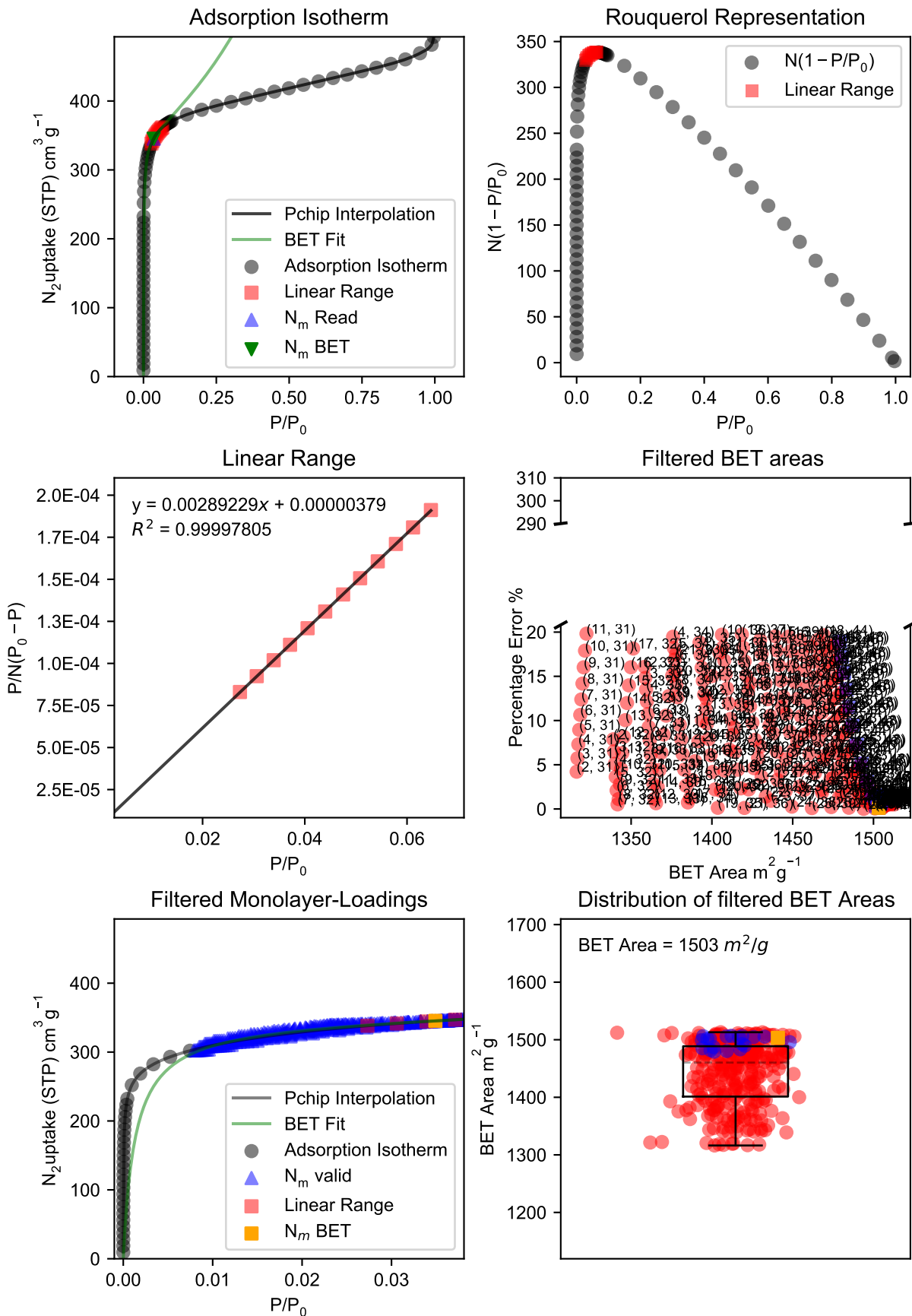


Fig. S22: BETSI analysis for VRnzK (hard).

BETSI Analysis for VRnzZ-10-630

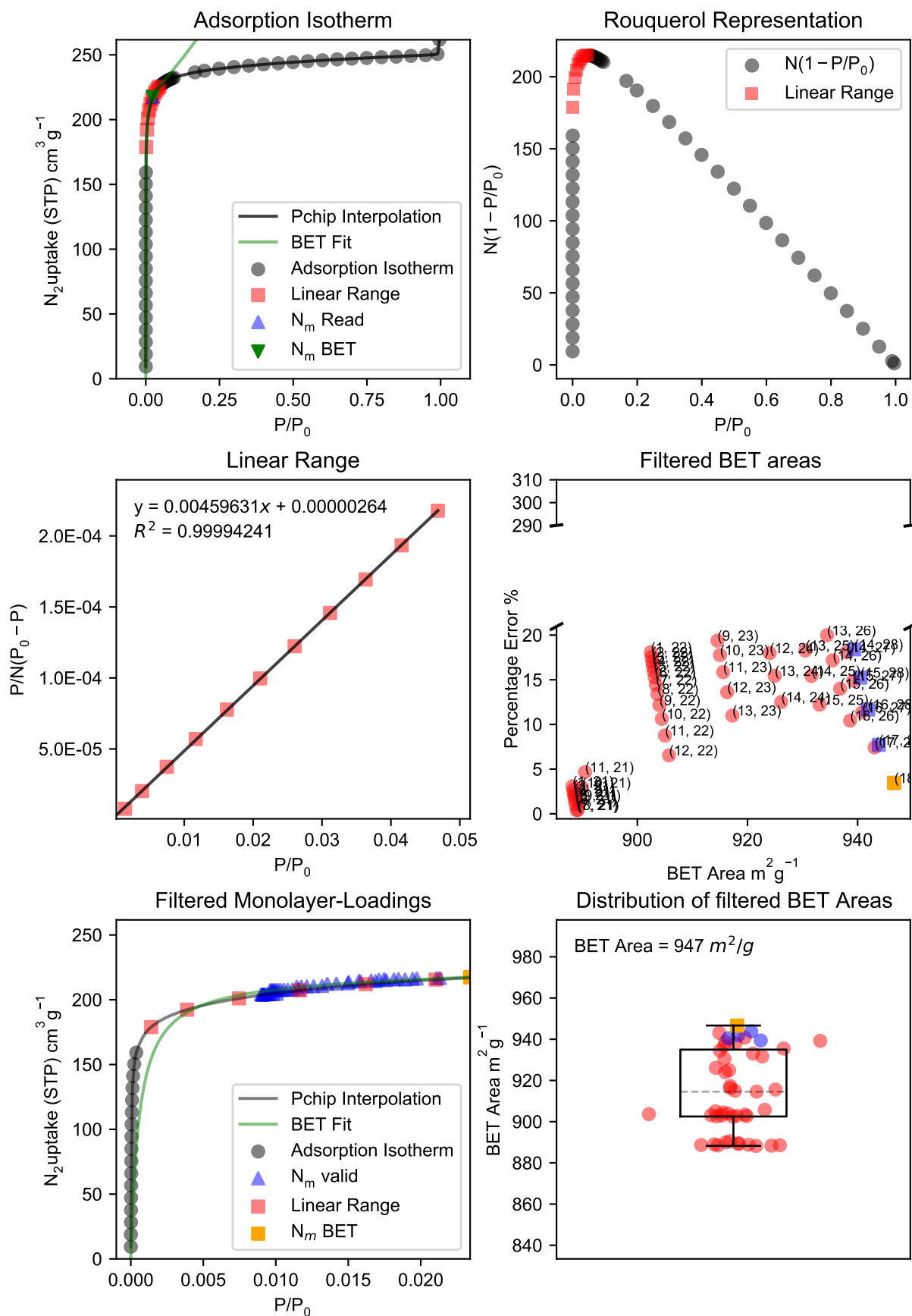


Fig. S23: BETSI analysis for VRnzZ-10-630.

BETSI Analysis for VRnzZ-10-700

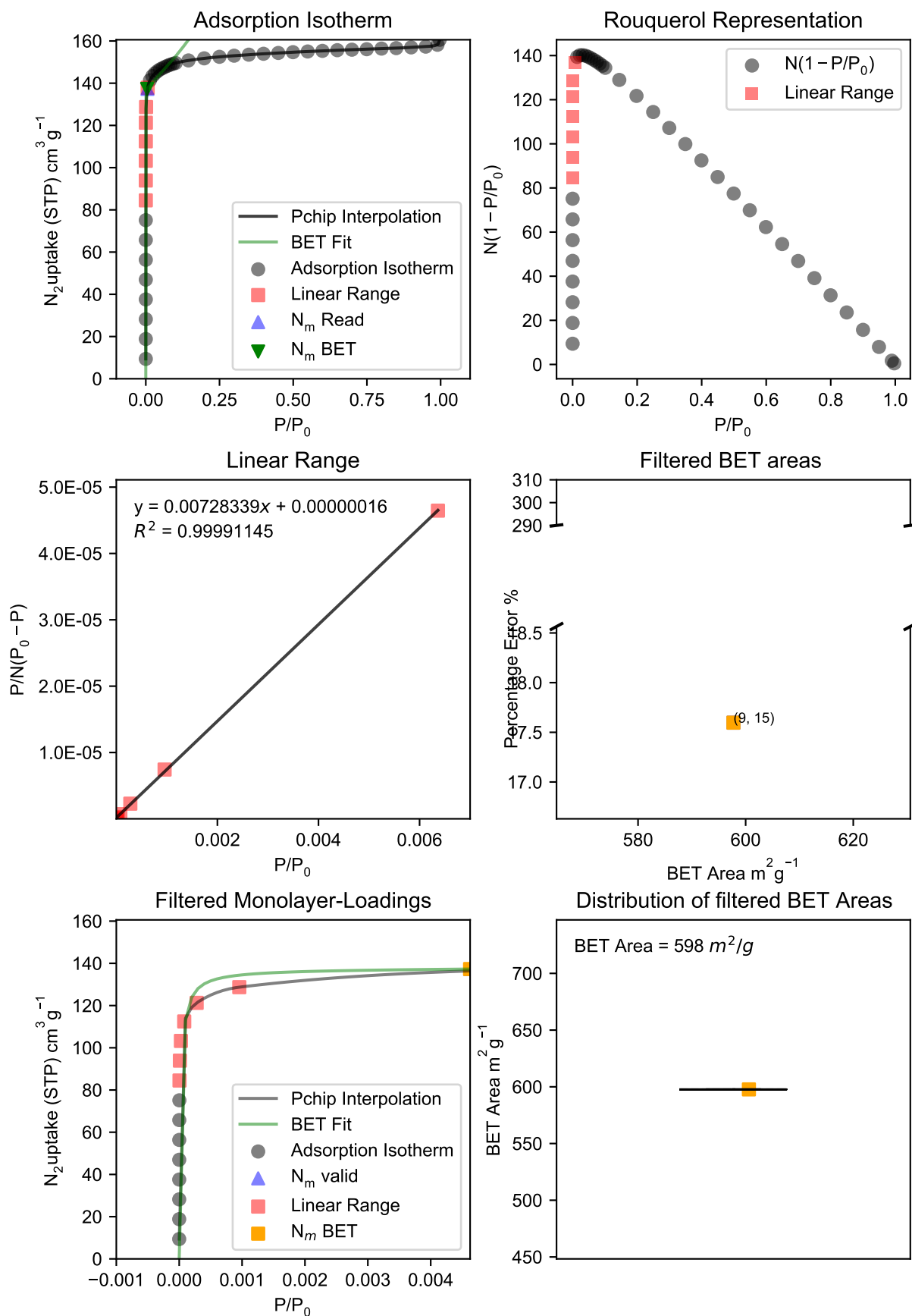


Fig. S24: BETSI analysis for VRnzZ-10-700.

BETSI Analysis for VRnzZ-100-630

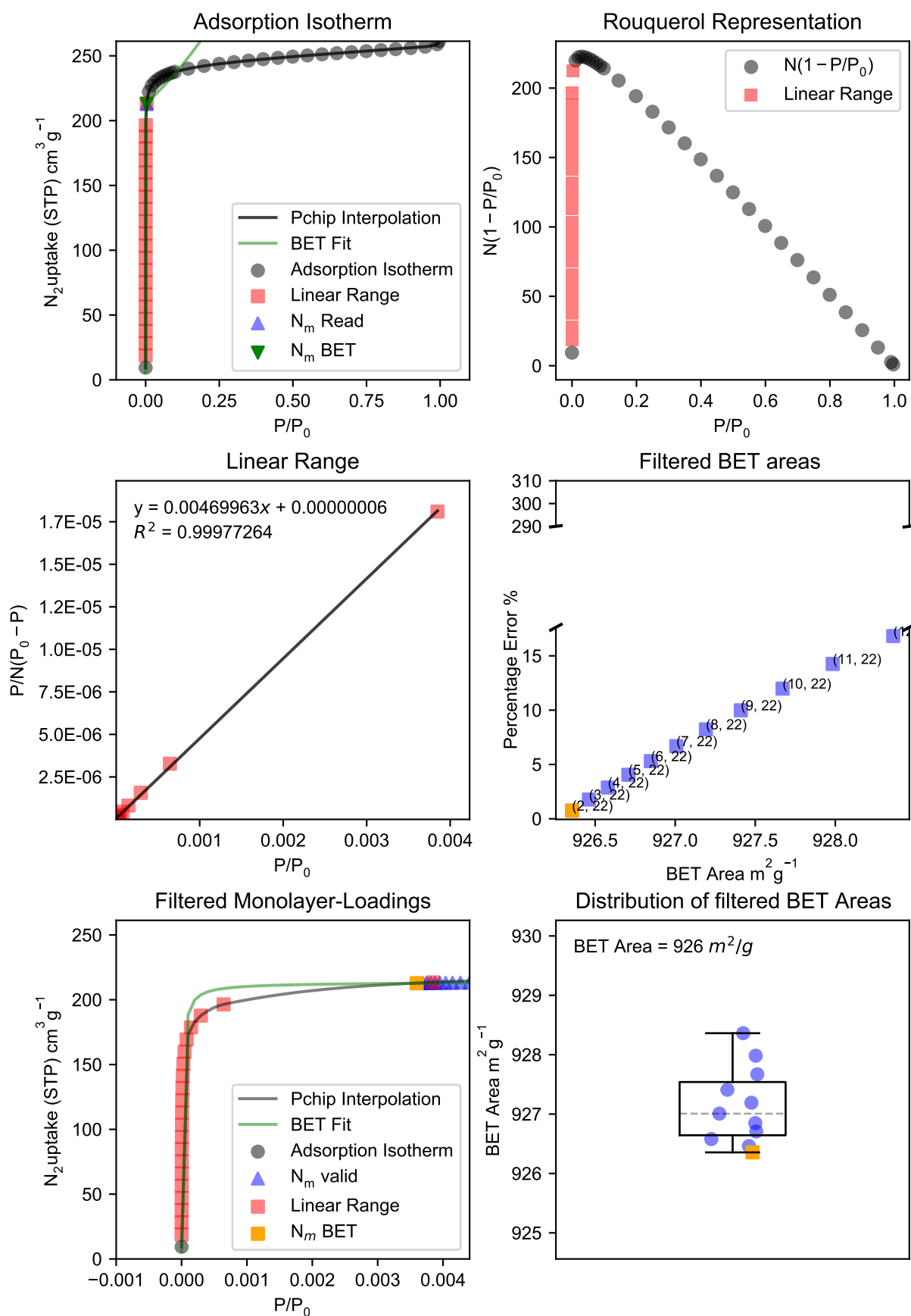


Fig. S25: BETSI analysis for VRnzZ-100-630.

BETSI Analysis for VRnzZ-50-630

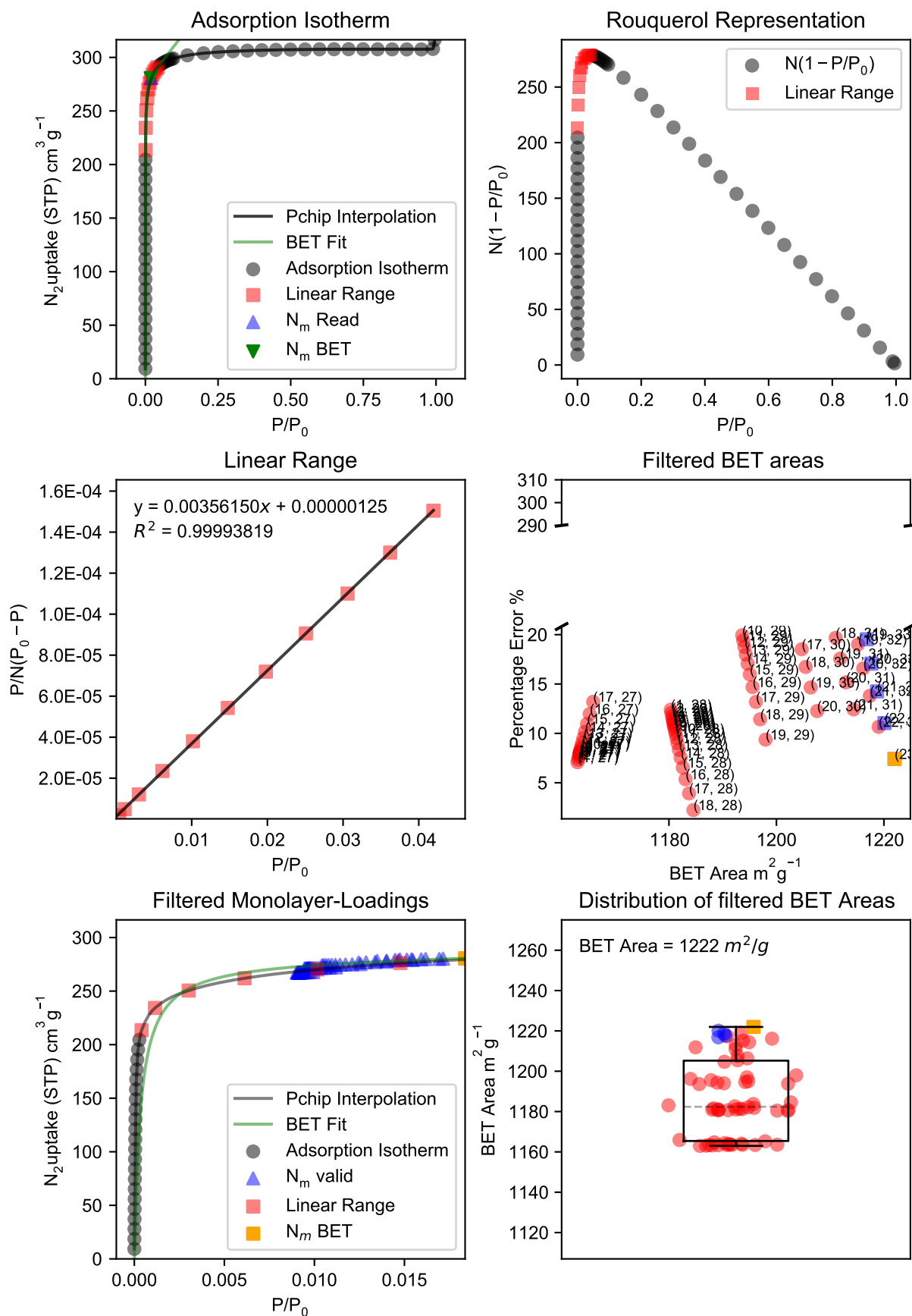


Fig. S26: BETSI analysis for VRnzZ-50-630.

BETSI Analysis for VRnzZ-50-700

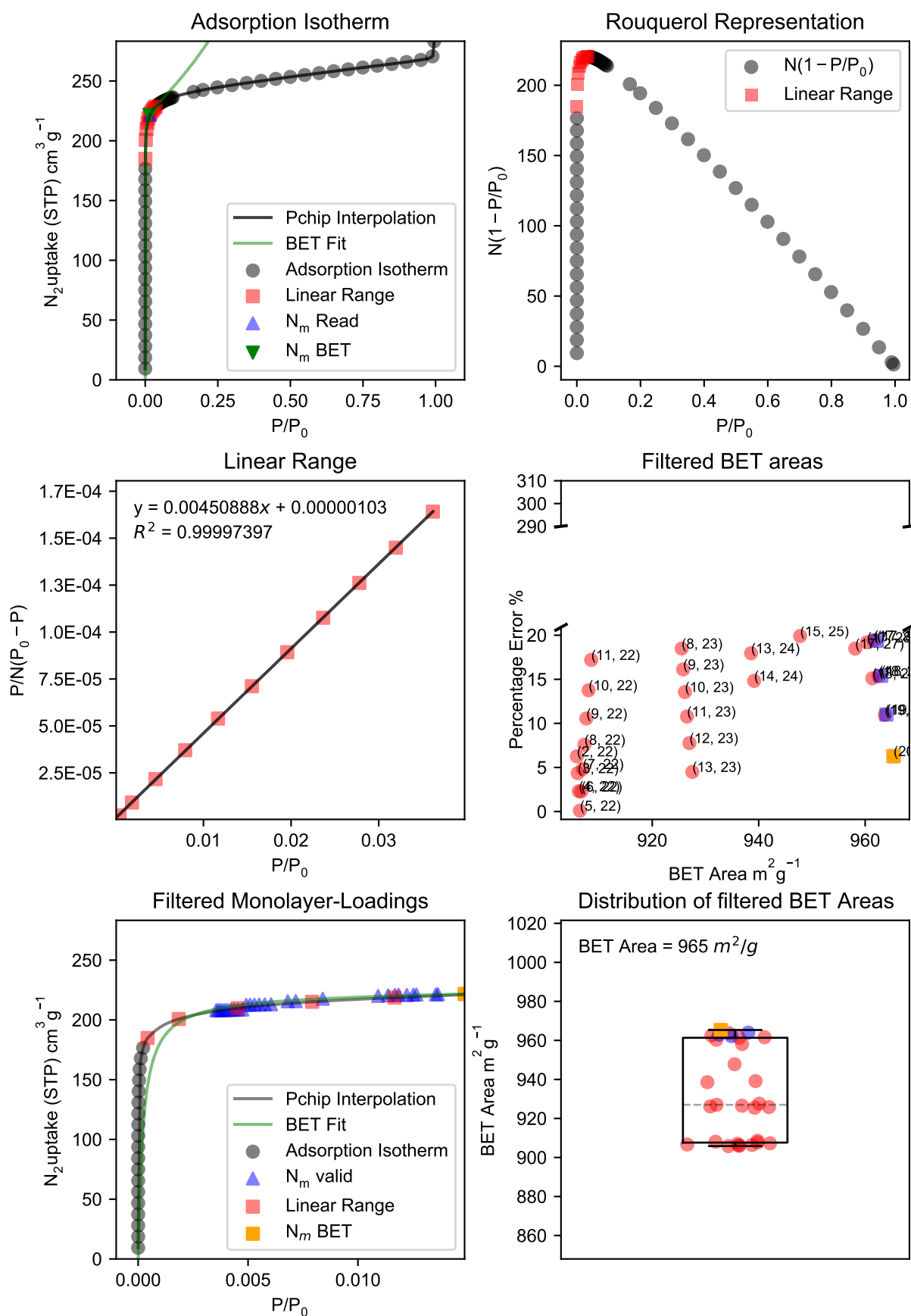


Fig. S27: BETSI analysis for VRnzZ-50-700.

7. PSD determination

PSDs and fits of isotherms to 2D-NLDFT heterogeneous surface kernel^{S3} are included on the following pages.

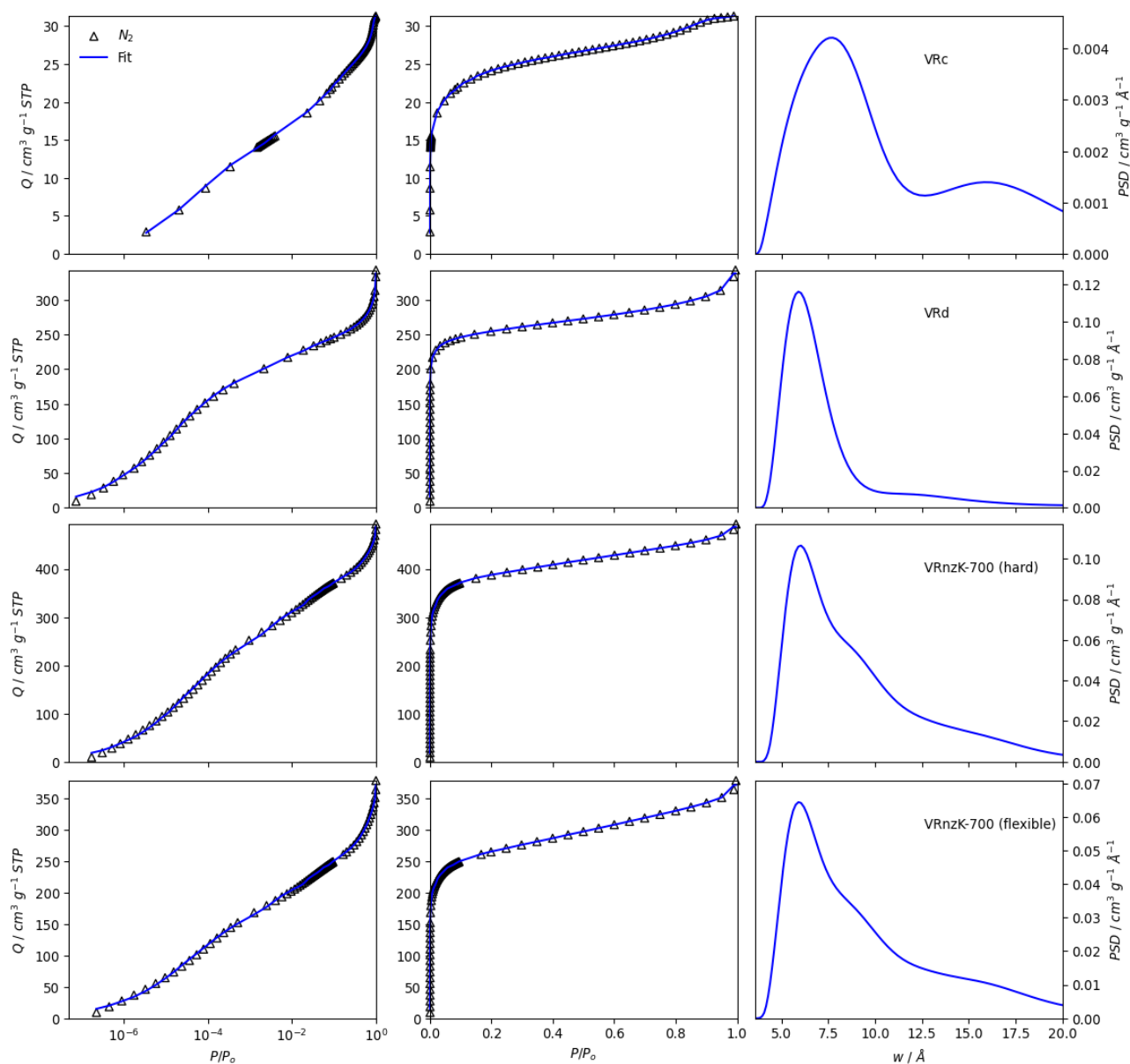


Fig. S28: Fits of N_2 isotherms of samples VRc, VRd, as well as hard and flexible portions of VRnzK-700.

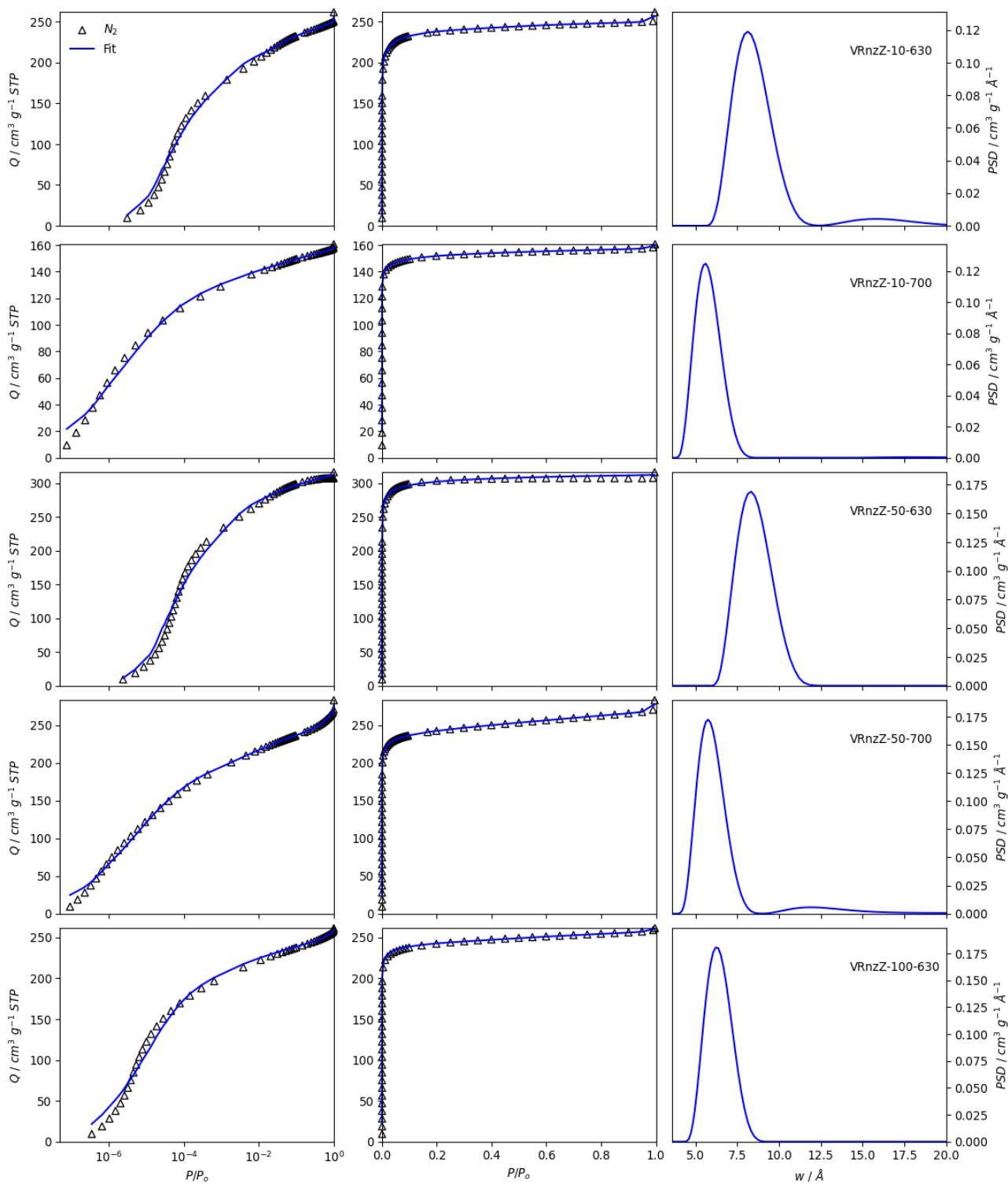


Fig. S29: Fits of N_2 isotherms of samples in set VRnZ-X-T.

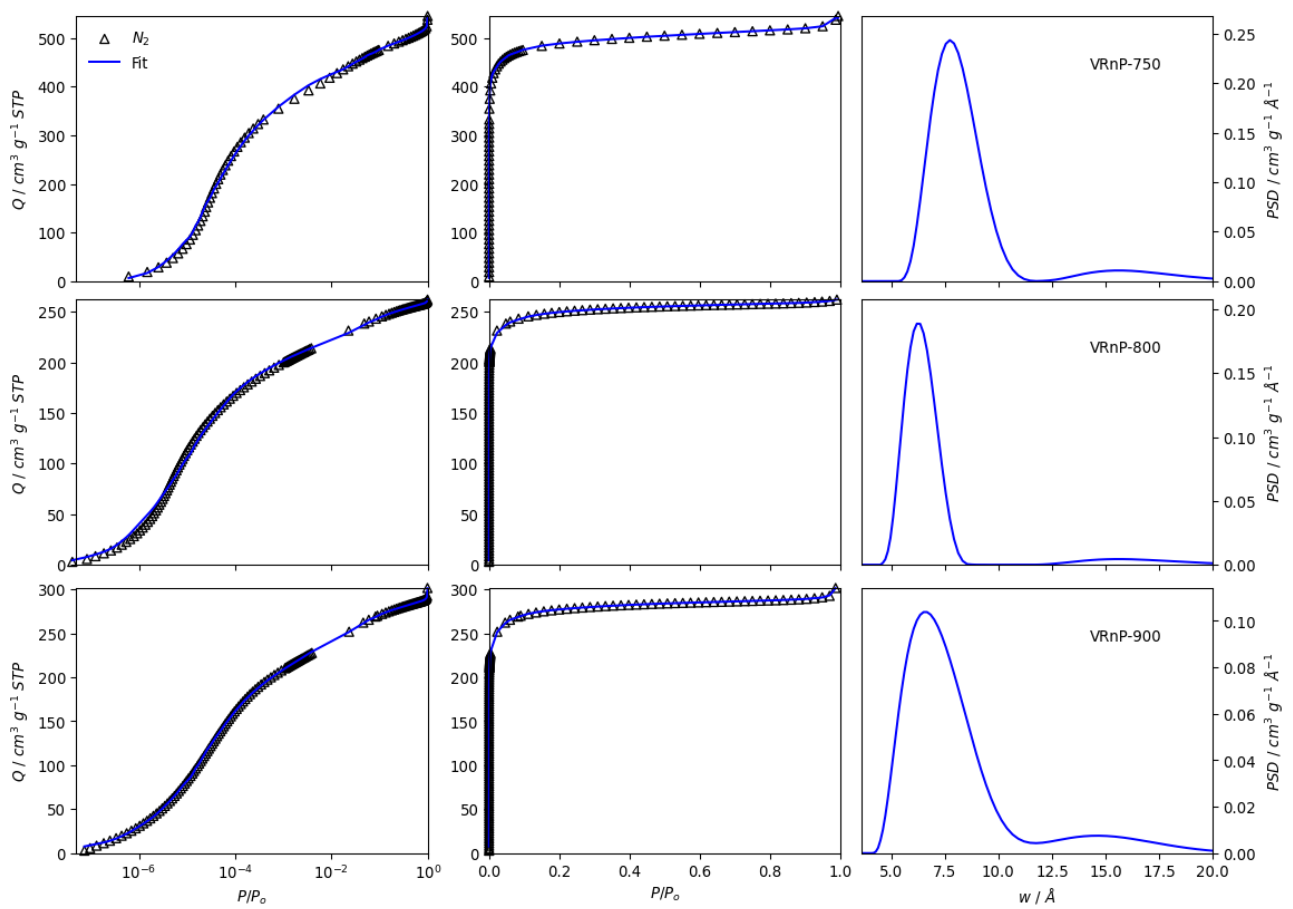


Fig. S30: Fits of N_2 isotherms of samples in set VRnP-T.

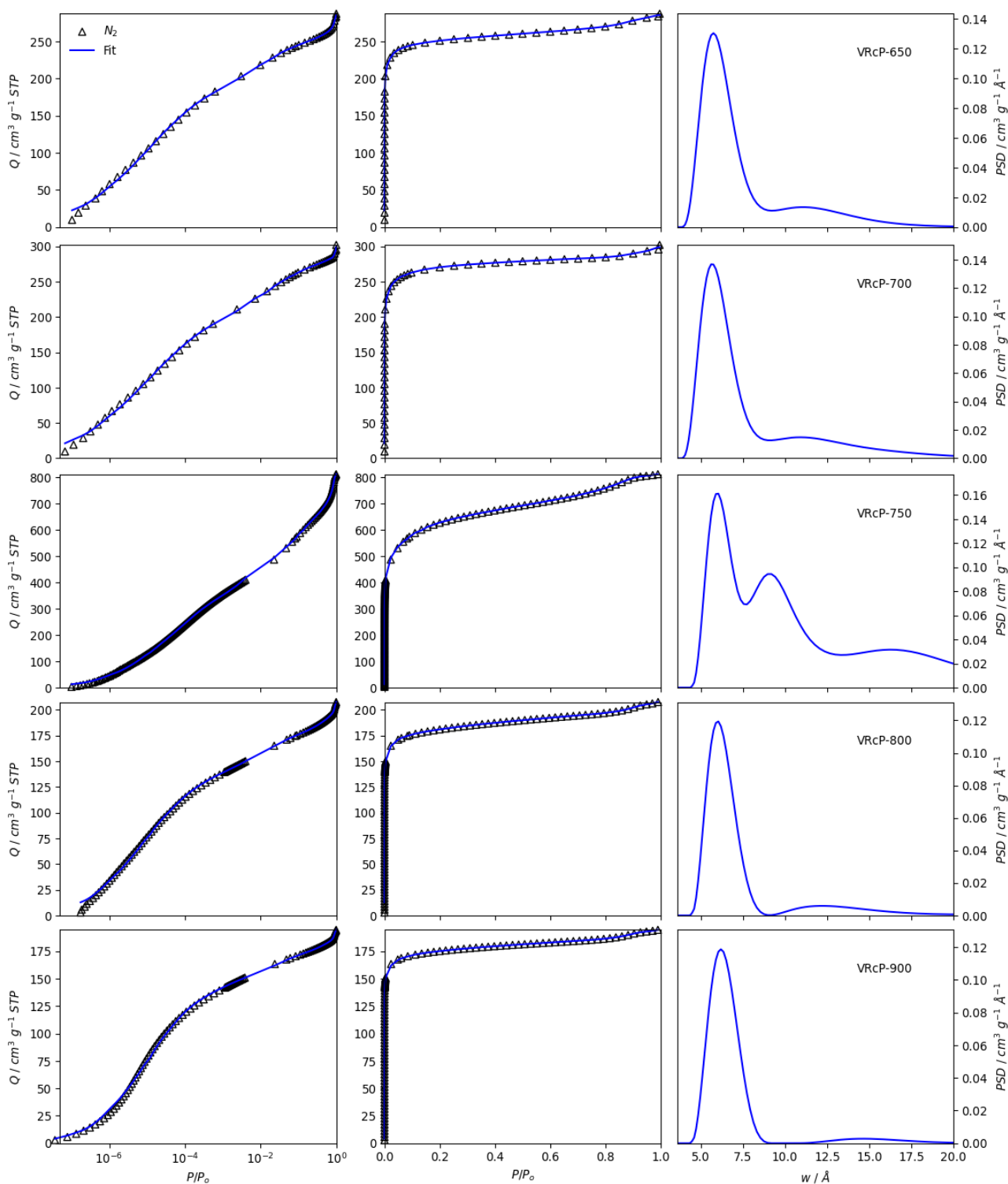


Fig. S31: Fits of N_2 isotherms of samples in set VRcP-T.

8. Gas uptake

This section contains comparison of CO₂ and CH₄ uptakes of the carbons in this work to those in the literature (table S3), as well as all gravimetric uptake isotherms and fits to models (figures S32, S33).

Table S3: Tabulated excess uptake of CO₂ and total uptake of CH₄ at 25 °C and various pressures (bar), of selected samples produced in the work and ACCs in the literature.

Sample	CO ₂ uptake / mmol g ⁻¹			CH ₄ uptake / mmol g ⁻¹			ref
	1.0	20	40	1.0	20	35	
VRcP-750	2.9	14.0	16.3	1.3	8.3	10.4	this work
VRnP-750	4.1	12.3	13.3	1.9	8.3	10.0	this work
VRnzZ-50-630	3.5	8.9	9.5	1.2	5.6	6.8	this work
C60-CC-PNP		14.3			7.5		S4
C30-CC-PNP	4.2	11.9			7.0		S4
ACC	2.0			0.7			S5
FIPC	2.8			1.3			S6
FIAC	1.7						S6
Cloth 1		6.0					S7 (commercial)
Cloth 2		7.0					S7 (commercial)
CC-CH	2.5	3.8		1.0	2.3		S8
C60-CCC-PNP		3.3			1.6		S8
C60-CFT-PNP		3.1			1.8		S8

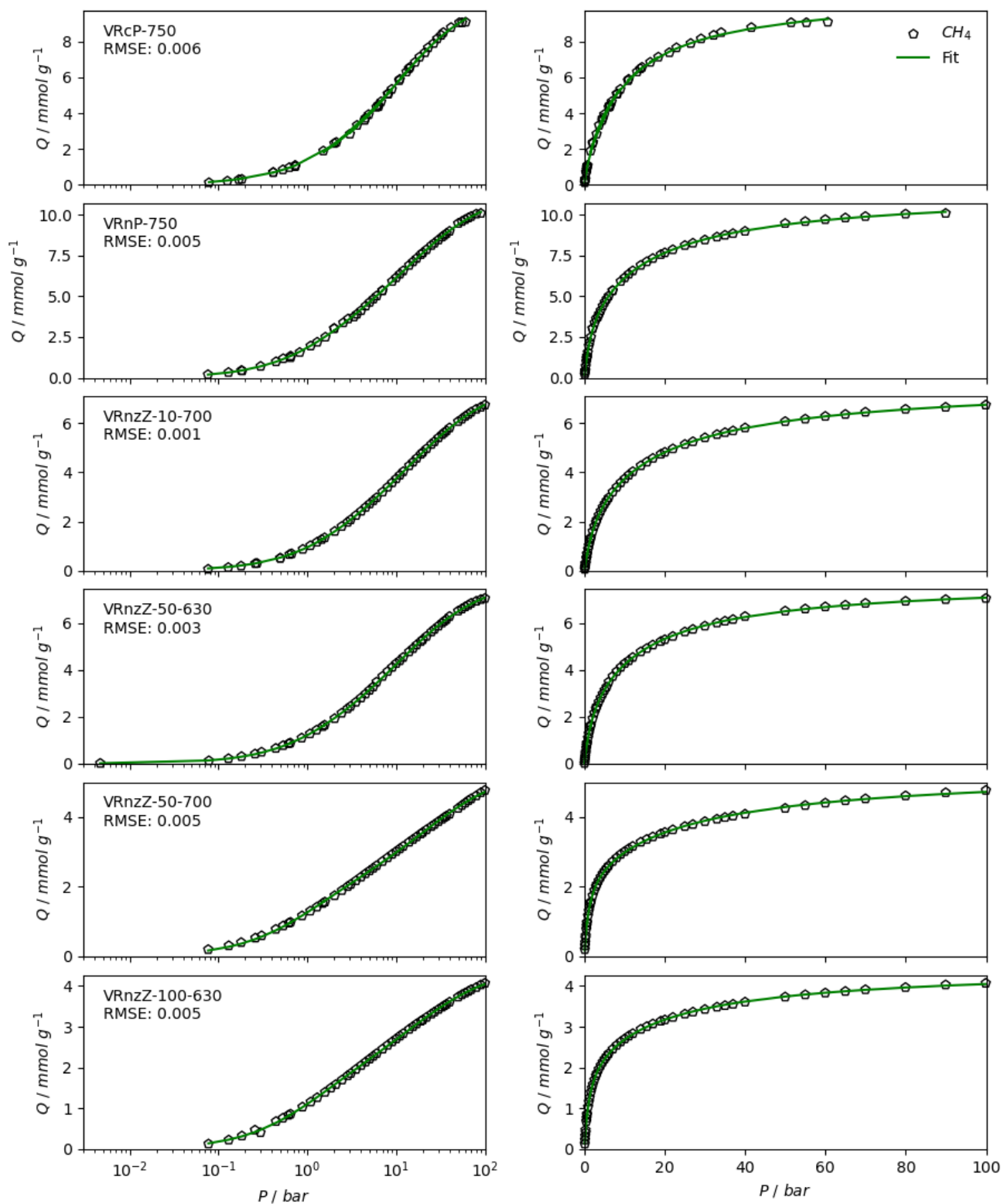


Fig. S32: Excess CH_4 isotherms and fits to double site Langmuir^{S9} model for purposes of extracting loadings at specific pressures. Where samples became saturated at some pressure, data after this is excluded for the purposes of the fit.

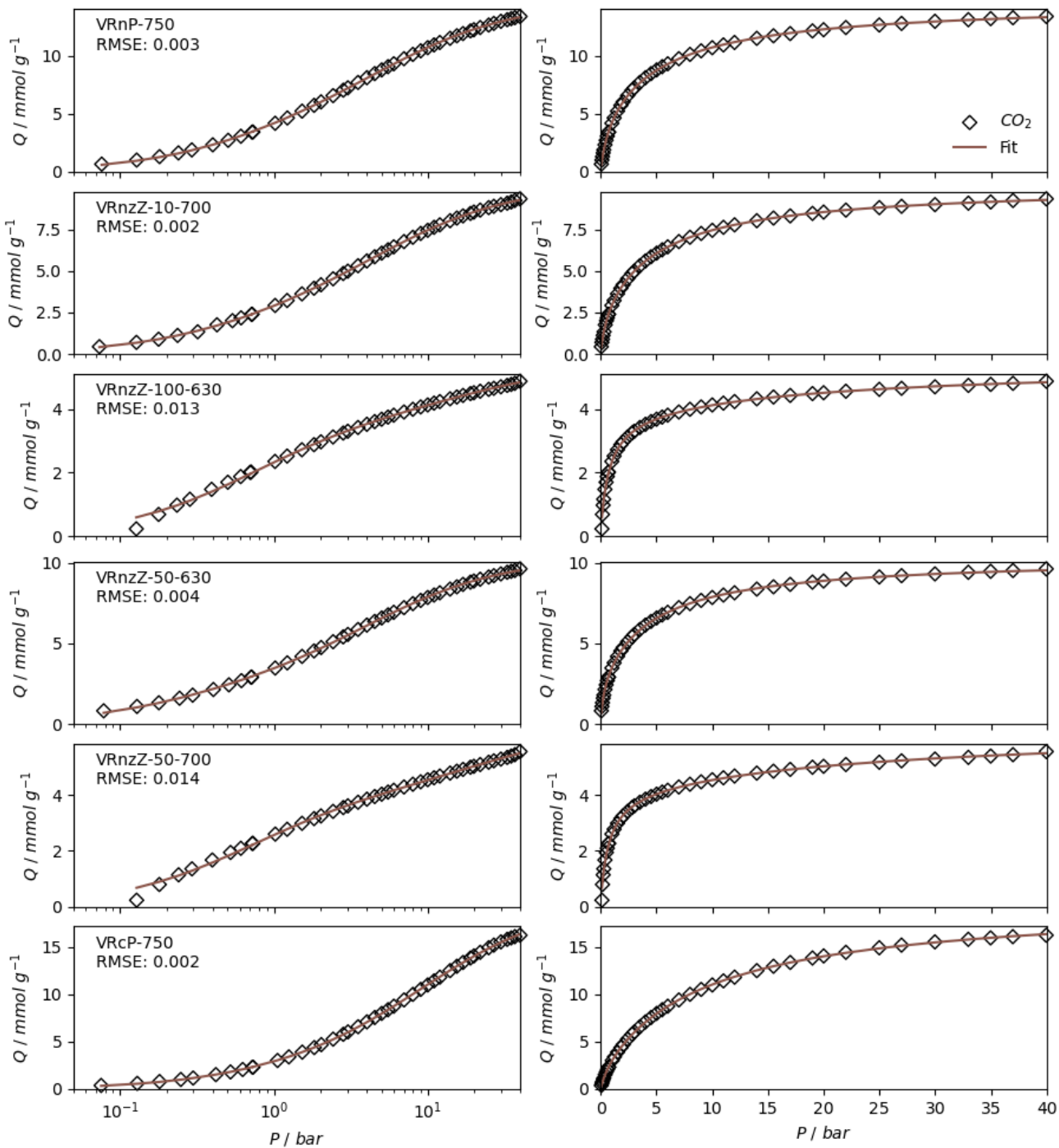


Fig. S33: Excess CO₂ isotherms and fits to double site Langmuir⁵⁹ model for purposes of extracting loadings at specific pressures.

References

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