Design and development of a new flowable and photocurable lactide and caprolactonebased polymer for bone repair and augmentation

Hamidi AS^a, Hadis MA^a, Williams RL^b, Grover LM^b, Palin WM^{a*}

^a Dental and Biomaterials Science, School of Dentistry, College of Medical and Dental Science, Institute of Clinical Sciences, University of Birmingham, 5 Mill Pool Way, Edgbaston, Birmingham, B5 7EG, UK.

^b Healthcare Technologies Institute (HTI), School of Chemical Engineering, University of Birmingham, Edgbaston, Birmingham, B15 2TT, UK

Supplementary Data – 1B

1 Absolute irradiances and molar absorptivity

The absolute irradiance of AURA and EPSE Vario, represented by area integral under an irradiance curve, were measured using a miniature UV-Vis spectrometer (USB4000; Ocean Optics, USA), equipped with a 400 µm optical fiber that was coupled to an opal glass cosine corrector (CC3-UV, sensor diameter: 3.9 mm). Prior to any measurements, the spectrophotometer setup was calibrated with a deuterium (UV) and halogen (Visible-NIR) calibration light source (DH-2000-CAL; Ocean Optics, Florida, USA), as per NIST standards. Figure 1b displays emission spectra of AURA and ESPE Vario.

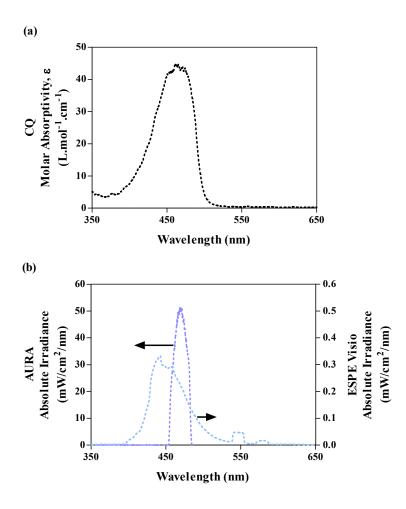


Figure 1: (a) Molar Absorptivity (Right axis) of CQ in pure methanol (1.11 x 10^{-4} mol/mL), measured using a miniature UV-Vis spectrophotometer (USB400). (b) Spectral irradiances of light curing units, used in present study.

2 GPC - M_n and M_w of Monomers

MW averages of monomers were determined using GPC, which involved molecular size separation based on hydrodynamic elution volume. However, since a constant flow rate of 1.0 mL/min was used, separation of molecules was measured in retention time (minutes) instead. Figure 2 and 3 illustrate chromatograms of both monomers. Elution peaks highlighted by green gridlines represent the distribution of monomer chain sizes as a function of retention time and RI. High MW chains (large coiled-up polymers) eluted first and marked the upper limit, while small polymer chains eluted last marking the lower limit.

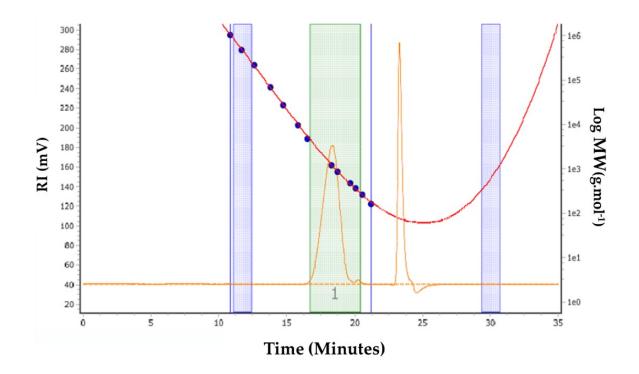


Figure 2: Chromatogram of PLLA-DM (SP-POL-116). Courtesy of SP (Montpelier, France).

Relative number (\bar{M}_n) and weight (\bar{M}_w) , along with polydispersity index (PDI) was generated using the calibration curve. It is worth noting that the narrow peak at about 23 minutes corresponds to an additive, generally introduced to ensure more uniform flow and/or avoid non-size exclusion interactions with the column [99]. Variation in M_n , M_w and PDI among three PLLA-DM batches were \pm 6.85, 6.60 and 3.63 %, respectively. Equally, variation among PCF-DM batches were \pm 11.36, 18.60 and 7.23 %, respectively.

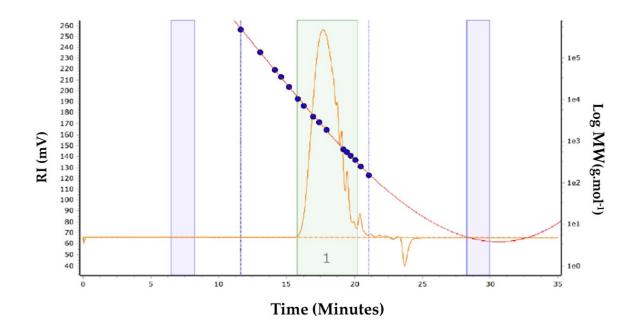


Figure 3: Chromatogram of PCF-DM (SP-POL-132). Courtesy of SP (Montpelier, France).

3 Apparent viscosity and flow behaviour

3.1 Methods

Apparent viscosities of unpolymerised neat monomers and their respective formulations were determined using Discovery Hybrid Rheometer HR1 (TA instruments, Brusselsesteenweg, Belgium). To measure viscosity as a function of strain, a shear rate sweep of 1 to 2000 s⁻¹ was performed using a 20 mm cone-on-plate geometry with a cone angle of 2° and truncation height/gap (between the cone and a plate) of 53 μ m. The geometry setup was calibrated for inertial, frictional, and rotational mapping prior to any measurements. Shear rate change and data acquisition were acquired algorithmically (Log₁₀) by dispensing 0.10 mL of monomer sample between the cone and a plate using a 1 mL syringe. Plate temperature was adjusted accordingly (25 / 37°C), with an initial 60 s 'temperature soaking time'. Viscosity measurements were conducted in triplicates per monomer / formulation and per temperature group. Data were analysed using TRIOS software (v5.0.0).

3.2Results

Figure 4 depicts apparent viscosities of monomer formulations, as a function of shear rate (s⁻¹) at 25°C (Figure 4a) and 37°C (Figure 4b). Two-way ANOVA analysis revealed significant reduction (P < 0.05) in apparent viscosities as a function of shear rate (1/s) and operating (environmental) temperature.

At 25°C, the effect of high-speed shearing was more apparent for formulations containing higher PLLA-DM content (F4 and F5). Fluid shear thinning (Flow Index, n < 1) was significant with greater reduction in apparent viscosities (Post hoc, Bonferroni, P < 0.05), when compared with F1–3 formulations which displayed relatively gradual shear thinning behaviours.

An increase in temperature (to 37°C) led to significant decline (P < 0.05), with as much as 77 and 86 % reduction in apparent viscosities of F4 and F5 formulations when compared at 100 shear rate (s⁻¹) under 25°C operating temperature, respectively. Equally, formulations with lower PLLA-DM content (F1–F3), apparent viscosities were reduced by 60 to 70 %, when compared at 100 shear rate (s⁻¹) under 25°C (P < 0.05). It is worth noting that the influence of shear rate under 37°C was less noticeable with non-significant (P > 0.05) reduction in apparent viscosities at various shear rate steps for each formulation.

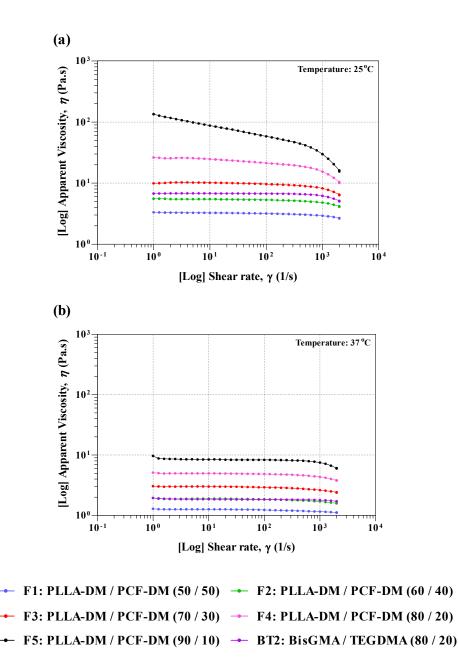


Figure 4: Apparent viscosities of unpolymerised formulations under a shear rate sweep of 1-2000 (s⁻¹) at 25 (a) and 37° C (b) operating temperatures with a temperature soaking time of 60 s.

3.3Discussion

Generally, monomer formulations exhibited shear thinning behaviour which was more apparent for formulations containing higher PLLA-DM content. Propensity towards applied shear stresses might be attributed to higher intermolecular forces and entanglement of chains than PCF-DM. This may explain somewhat the 'sticky wax' nature of neat PLLA-DM as opposed to the 'oily' texture observed for neat PCF-DM. The effect of temperature on apparent viscosities of formulations was more influential than shearing. Increased temperature may have led polymer chains to gain enough energy to overcome intermolecular interactions and disrupt entanglement from the bulk structure [100]. As a result, resistance to flow (viscosity) decreased and polymer networks began to flow more readily.

A significant reduction in the apparent viscosity of F5 at relatively low shear rates under 25°C might be attributed to the '*Weissenburg effect*', caused by normal stress forces generated during shear deformation. A phenomenon commonly occurs in paints and polymer solutions involving an elastic fluid mixed in a highly viscous solvent. PCF-DM chains may have experienced relatively larger elastic deformation and stretching than PLLA-DM under the same shear stresses away from the centre. In cone-on-plate geometry, this can create outward normal forces which in turn affect polymer contact with cone and the plate [100-102].

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