## **Supplementary Information**

## **Cutting depth of different processes**

In the process of consolidated abrasive lapping, the material removal mechanism is determined by the maximum cutting depth of a single abrasive grain, which is determined by the undeformed chip thickness  $h_m$ . The equation is as follows,<sup>1</sup>

$$
h_{\text{max}} = \left[\frac{P_0}{2\left(1 + \sqrt{\frac{\pi \sigma_s}{2E^*}}\right)}\right]_D^{\frac{1}{3}} D_{\text{L}}
$$
\n(1)

where  $P_0$  is lapping pressure, *H* is hardness of the sample,  $E^*$  is equivalent elastic modulus of lapping pad,  $\lambda$  is lapping pad bump ratio factor,  $D_L$  is abrasive diameter,  $\eta$  is particle volume concentration and  $\sigma_s$  is yield strength.

Based on experimental parameters and existing literature, 2 the performance parameters of the lapping pad can be determined, as illustrated in Table 1.

|   |                 | Equivalent elastic |                        |
|---|-----------------|--------------------|------------------------|
| Abrasive<br>diameter $D_L$<br>$(\mu m)$ | Particle volume | modulus of lapping | Lapping pad bump       |
|   | concentration η | $pad E^*$          | ratio factor $\lambda$ |
|   |                 | (GPa)              |                        |
| 4.42                                    | 0.12            | 0.87466            | 0.44                   |

Tab. 1 Performance parameters of grinding pad

Based on equation (1), the maximum cutting depth of a single abrasive grain is determined to be 206 nm.

In the process of CMP, The load  $F_p$  on a single abrasive grain and the indentation depth  $\delta_w$  should satisfy the following equation, 3

$$
\delta_{\rm w} = \frac{F_{\rm p}}{\pi R_{\rm p} H}
$$
 (2)

where  $F_p$  is load of single abrasive and  $R_p$  is abrasive radius.  $F_p$  can be calculated using the Hertz contact theory. Assuming that during the polishing process, the abrasive grain size is consistent, the representation ofthe number of effective abrasive grains per unit area during the polishing processis denoted as *η*p,

$$
\eta_{\rm p} = \frac{3C_{\rm a}\rho_{\rm s}}{2\pi R_{\rm p}^2 \rho_{\rm p}}
$$
\n(3)

Where  $C_a$  is mass fraction of the abrasive,  $\rho_s$  is density of polishing slurry and  $\rho_p$  is density of abrasive.

Based on experimental parameters and abrasive information in the manuscript, polishing slurry parameter information could be determined. There are as follows,

| Name      | Abrasive<br>radius $R_p$<br>(nm) | Mass fraction of the<br>abrasive $C_a$<br>$(wt. \% )$ | Density of<br>polishing slurry<br>$\rho_{\rm s}$<br>$(g/cm^3)$ | Density of<br>abrasive $\rho_p$<br>$(g/cm^3)$ |
|-----------|----------------------------------|---|--|---|
| Parameter | 74.3                             | l .O  |  | 7.1   |

Tab. 2 Polishing slurry parameter information

 On the basis of information in Tab. 2 regarding polishing slurry parameters and equation (3), the effective abrasive particle count  $\eta_p$  within a unit area can be calculated,

$$
\eta_{\rm p} = 1.34 \times 10^5 (1/\text{mm}^2) \tag{4}
$$

When the polishing pressure is set at 0.20 MPa, the corresponding calculations of  $\delta_w$  from equations (3) and (4) is 6.5 nm.

## **References**

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