

Supplementary Information for

Tunable, multifunctional opto-electrical response in multilayer FePS₃/single-layer MoS₂ van der Waals p-n heterojunctions

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S1. Thickness characterization of FePS₃ flakes

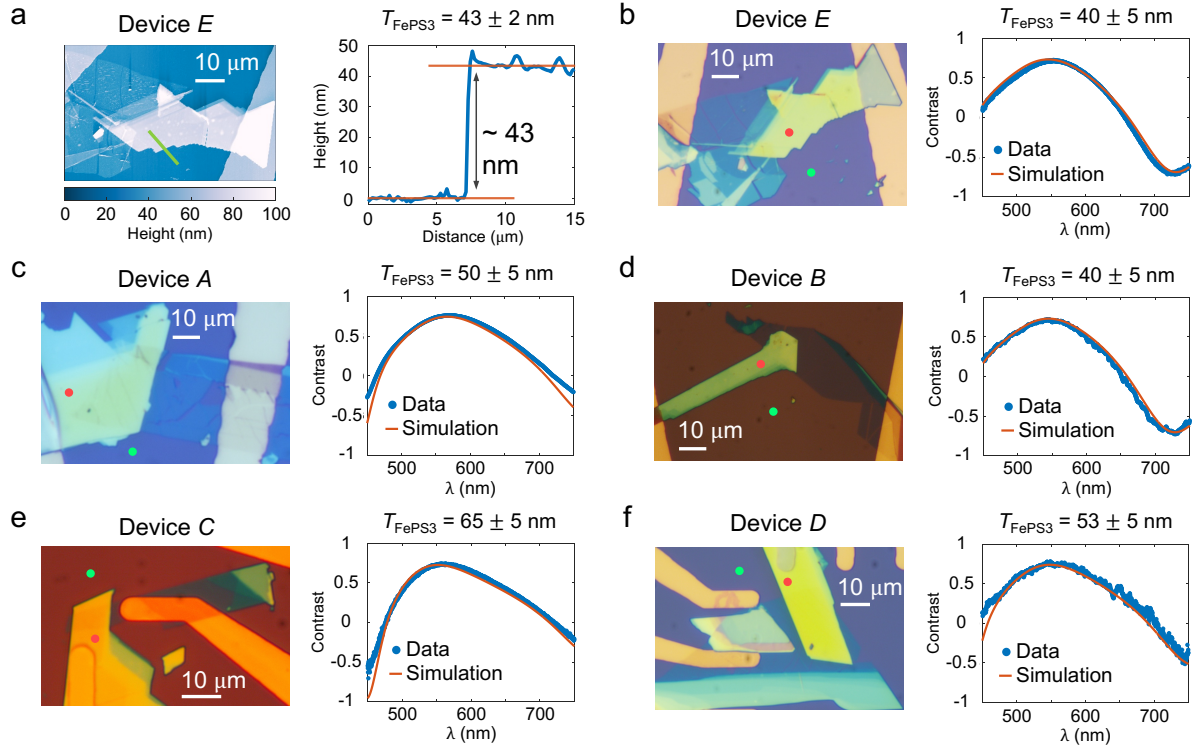


Figure S1. Thickness analysis of the FePS₃ flakes in the different heterostructure devices characterized in this work. (a) Left: AFM topographic image of the device shown in (b). Right: Height profile corresponding to the green line marked in the AFM image. (b) Left: Optical microscopy image of a FePS₃/1L-MoS₂ junction (device *E*). Right: Optical contrast obtained from micro-reflectance spectroscopy measurements performed on the FePS₃ flake on SiO₂/Si (red spot) and the bare SiO₂/Si substrate (green spot). Experimental data is represented by blue dots. The red continuous line represents a simulation of the optical contrast for the multilayer system assuming a SiO₂ thickness of 280 nm and a thickness of 40 nm for the FePS₃ flake. Panels (c)-(f) display images of different devices used in this work accompanied by the corresponding experimental optical contrast (blue dots) obtained from the micro-reflectance spectra measured at the spots at FePS₃ and substrate marked in the images. The thickness of FePS₃ is obtained from the simulation of the optical contrast for the corresponding multilayer system.

The thickness of FePS₃ flakes forming the heterostructure devices was determined by micro-reflectance spectroscopy measurements following the methods described in ref. [s1]. Micro-reflectance spectra were collected from a spot diameter of approx. 3 μm, both at locations on the FePS₃ flake and at the bare SiO₂/Si substrate (indicated in Fig. S1). The reflectance for the FePS₃/SiO₂/Si (R_{FePS_3}) and for the SiO₂/Si substrate (R_{SiO_2}) can be estimated from a simple model for light propagation in an optical multilayer system (see for instance refs. [s1] and [s2]). The optical contrast can be calculated as $C = (R_{\text{FePS}_3} - R_{\text{SiO}_2}) / (R_{\text{FePS}_3} + R_{\text{SiO}_2})$ and strongly depends on the thickness and refractive index values of the different layers constituting the system. Refractive index values for Si and SiO₂ are taken from Palik *et al.* [s3]. The thickness of the SiO₂ layer is approx. 280 nm. In previous works [s1], we extracted an estimation for the refractive index of FePS₃ ($n \sim 2.70$, $k \sim 0.15$, being n and k the real and imaginary parts of the refractive index, respectively) from the analysis of transmittance and optical contrast of samples for which the thickness was precisely identified by AFM measurements. Using these values, we can extract the thickness of the FePS₃ flakes by

comparing the experimental data to the results of the contrast simulations. Figure S1 shows the micro-reflectance characterization of FePS₃ in different devices used in this work. In Figure S1a-b, we show a comparison of AFM topography and micro-reflectance characterization for the same FePS₃ flake, showing a good agreement within error range.

S2. Carrier density and charge transfer in FePS₃/1L-MoS₂ heterostructures

Charge transfer estimate from a mass action law model

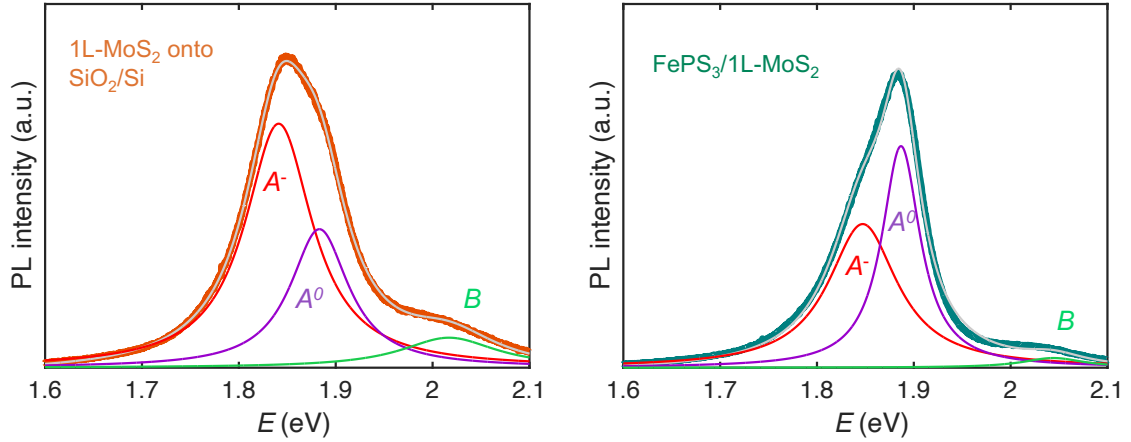


Figure S2. Left: Photoluminescence spectrum taken on device *A* on 1L-MoS₂ on SiO₂ (at the position marked by the red dot in Fig. 1b in the main text). Right: Photoluminescence spectrum taken on device *A* on 1L-MoS₂ below FePS₃ flake, at the corresponding green dot in Fig 1b. PL data is fit to the sum of three lorentzian peaks, which are shown in each panel.

The PL signal of the single-layer MoS₂ can be decomposed into three excitonic Lorentzian peaks both for the isolated MoS₂ on SiO₂ and for the heterojunction formed by FePS₃/1L-MoS₂. Following previous works [s4], these three peaks can be identified as: X^- peak (trion or negatively charged exciton), the X^0 peak (neutral exciton) and the B peak (neutral exciton). Excitons A and B come from the spin-orbit splitting at the valence band of single-layer MoS₂.

The Lorentzian fits in the figure above show that the main contribution to the PL emission in the 1L-MoS₂ onto SiO₂/Si (left) comes from the negatively charged exciton (X^-), showing the n-type of doping, typical of MoS₂. For the case of the heterojunction, we can observe a change in the spectral weight of the negatively charged exciton (X^-) and the neutral exciton (X^0) compared to the isolated MoS₂. This observation suggests a charge transfer of electrons from the monolayer to the FePS₃ flake when both materials are in contact, as described in Refs. [s5, s6]. In a trial to quantify this, we consider the equilibrium between the relative populations of charged and neutral excitonic species, as well as free electrons:



The equilibrium situation is described by a mass action law, where the population of the 3 species is governed by this rate equation:

$$\frac{N_{X^-}}{N_{X^0}} = K_T \cdot n_{el} \quad (S2)$$

where N_{X^-} and N_{X^0} are the number of trions and neutral excitons, K_T is the rate constant for trions and n_{el} is the free electron density.

The ratio of the areas under the PL curve for these two contributions, A^- for charged excitons and A^0 for neutral excitons (see Figure S2), is expected to be proportional to the ratio of the respective populations:

$$\frac{A^-}{A^0} \propto \frac{N_{X^-}}{N_{X^0}} \quad (\text{S3})$$

Taking this into consideration for the 1L-MoS₂ onto SiO₂/Si and for the heterojunction, a first estimation of the relative change of electron concentration in the monolayer MoS₂, $(n_{\text{el}}^{\text{con}} - n_{\text{el}}^{\text{het}})/n_{\text{el}}^{\text{con}}$, due to charge transfer when it is placed in contact with FePS₃, results in a 43% for the case of device A. Moreover, our previous experimental results on similar heterostructures - except that the single-layer MoS₂ was placed on top of FePS₃ - demonstrate a strong tunability of this charge transfer as a function of the FePS₃ thickness (see Ref. s6, Figure 2d). In our current work, where the monolayer MoS₂ is underneath a 40-to-60-nm thick FePS₃, we observe a similar effect on the PL emission (a reduction in the n-doping of the 1L-MoS₂ upon contact with FePS₃), even though if the monolayer material is in contact with the SiO₂ dielectric and part of the light is absorbed by FePS₃, preventing an exact comparison between the two sample geometries.

Mobilities and carrier densities for 1L-MoS₂ and 30-nm thick FePS₃

An estimate for mobilities and carrier densities of FePS₃ and 1L-MoS₂ has been obtained from two-terminal electrical measurements as a function of the applied gate voltage in field-effect transistor devices. The mobilities are calculated as $\mu = \frac{L}{WC} \frac{\partial G}{\partial V_g}$, being L and W the channel's length and width, respectively, C is the oxide capacitance per unit area $C = \epsilon_0 \epsilon_r / d$, where ϵ_0 and ϵ_r are the vacuum and relative permittivities, and d the capacitor thickness. G is the conductance and V_g is the applied gate voltage.

The mobility of FePS₃ has been calculated from the conductance values as a function of applied gate voltage for a 30-nm thick flake, using data from Ramos et al. (ref. s1). Around zero-gate, we obtain $\mu_{\text{FePS}_3} = 9 \cdot 10^{-3} \text{ cm}^2 \text{V}^{-1} \text{s}^{-1}$. Similarly, the mobility of 1L-MoS₂ has been obtained from the conductance as a function of gate voltage from data presented in Figure S3, being $\mu_{\text{MoS}_2} = 3.5 \cdot 10^{-2} \text{ cm}^2 \text{V}^{-1} \text{s}^{-1}$, which is similar to other values reported in the bibliography (see for instance Radisavljevic et al. *Nat. Nanotech.*, 6, 2011, ref. s7).

Carrier densities can be subsequently extracted through the relations between conductivity (σ), conductance (G) and mobility (μ): $\sigma = G \frac{L}{Wt}$ and $\sigma = n\mu e$. Thus, the carrier density is given by: $n = G \frac{L}{Wt\mu e}$, where L , W , t and e are the length and width of the channel, the material's thickness and the electron charge, respectively.

Based on the previous expression, we obtain a carrier density of $n_{\text{FePS}_3} = 5.4 \cdot 10^{17} \text{ cm}^{-3}$ for FePS₃, and $n_{\text{MoS}_2} = 4.4 \cdot 10^{19} \text{ cm}^{-3}$ for MoS₂. Taking into account the one-layer thickness of the MoS₂ ($t_{\text{MoS}_2} = 0.78 \text{ nm}$), we obtain $n_{2\text{D}}(\text{MoS}_2) = n_{3\text{D}} \cdot t = 3 \cdot 10^{12} \text{ cm}^{-2}$ for a single-layer MoS₂. This result is in good agreement with the density of carriers reported for single-layer MoS₂ in other works (see Radisavljevic et al. *Nat. Mater.*, 12, 2013, ref. s8).

From these calculations we find that the carrier density of FePS₃ is almost two orders of magnitude lower than that of 1L-MoS₂. This is consistent with our previous observations in ref. s6, where the charge transferred between the two materials upon contact is limited by the available carriers at the FePS₃ flake (lower carrier density material), growing with increasing FePS₃ thickness.

Table S1. Calculated mobilities and carrier densities for 30-nm thick FePS₃ and single-layer MoS₂.

	FePS₃	1L-MoS₂
Mobility	$9 \cdot 10^{-3} \text{ cm}^2\text{V}^{-1}\text{s}^{-1}$	$3.5 \cdot 10^{-2} \text{ cm}^2\text{V}^{-1}\text{s}^{-1}$
Carrier density	$5.4 \cdot 10^{17} \text{ cm}^{-3}$	$n_{3D} = 4.4 \cdot 10^{19} \text{ cm}^{-3}$ $n_{2D} = 3 \cdot 10^{12} \text{ cm}^{-2}$

Carrier density estimation for MoS₂ in the heterostructure

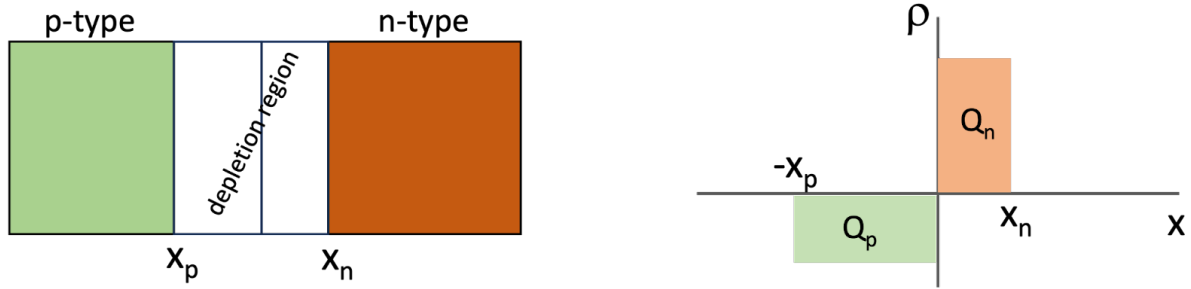
If we recall the mass action law employed to estimate the amount of charge transferred in our devices, taking into account that the ratio of the trion spectral weights between the heterostructure and the control samples must be equal to the ratio of the carrier densities between the heterostructure and the control samples, then we can estimate the carrier density of the heterostructure (device *A*) as:

$$(A/A^0)^{\text{het}}/(A/A^0)^{\text{con}} = n_{\text{el}}^{\text{het}}/n_{\text{el}}^{\text{con}} = 0.57. \quad (\text{S4})$$

Thus, $n_{\text{el}}^{\text{het}} = 0.57n_{\text{el}}^{\text{con}}$. If we assume the previously calculated carrier density for MoS₂ ($n_{3D} = 4.4 \cdot 10^{19} \text{ cm}^{-3}$), then the carrier density for the heterostructure is $2.5 \cdot 10^{19} \text{ cm}^{-3}$. The reduced carrier density in the heterostructure, compared to the single-layer MoS₂ directly placed onto SiO₂, points to a reduced n-doping of MoS₂ when interfaced with FePS₃.

Depletion region picture

To estimate the length of the depletion region in the heterostructure, we assume the system to be an abrupt p-n junction at equilibrium, to which no bias voltage is applied, and that both MoS₂ (n-side) and FePS₃ (p-side) host shallow dopants and therefore the density of acceptors and donors can be approximated by the density of free carriers, that is, $N_A \sim n_h$ in FePS₃ and $N_D \sim n_e$ in MoS₂.



Sketch. Left: Sketch for an abrupt pn-junction where the x_p and x_n depletion regions are marked. Within those limits, charge is proportional to the density of acceptors and donors respectively at the p and n sides. Right: Charge density as a function of position across the junction. The blue and red areas represent the total charge at the p and n region respectively.

After bringing the two materials into contact, once equilibrium is reached, charge neutrality implies that the total charge on the p-side of the depletion region $Q_p = qx_p N_A \sim qx_p n_h$ must be equal to the charge on the n-side $Q_n = qx_n N_D \sim qx_n n_e$. From this equality $Q_p = Q_n$, a the depletion region length on both sides of the junction (x_{MoS_2} and x_{FePS_3} respectively) can be expressed as a function of the carrier densities of each side far from the junction: $x_{\text{MoS}_2}/x_{\text{FePS}_3} \sim n_{\text{FePS}_3}/n_{\text{MoS}_2} \sim 100$, according to the values for carrier densities calculated in this section.

We interpret this result as follows. To fully deplete a single layer of MoS_2 , for which x_n is limited by its thickness (~ 0.7 nm), a depletion region of length ~ 70 nm would be generated on the FePS_3 side. If we bring FePS_3 flakes thinner than 70 nm into contact with 1L- MoS_2 , full depletion cannot be achieved and the resulting density of carriers in MoS_2 will depend on the thickness of FePS_3 . Assuming that FePS_3 flakes are fully depleted, charge neutrality implies that $t_{\text{FePS}_3} \cdot n_{\text{FePS}_3} = t_{\text{1L-MoS}_2} \cdot n_{\text{MoS}_2}$. As long as t_{FePS_3} is below 70 nm, $n_{\text{MoS}_2} = t_{\text{FePS}_3} \cdot n_{\text{FePS}_3} / t_{\text{1L-MoS}_2}$. For example, in a junction with a FePS_3 flake of 35 nm, the carrier density of MoS_2 would be expected to be reduced to a half. This is in a good qualitative agreement to our estimation of charge transfer from mass action law predicts a change from $4.4 \cdot 10^{19}$ to $2.5 \cdot 10^{19}$ $1/\text{cm}^3$ in the carrier density of single-layer MoS_2 after charge transfer in contact with a 40-nm thick FePS_3 flake.

S3. 1L-MoS₂ FET I - V characteristics as a function of back-gate voltage

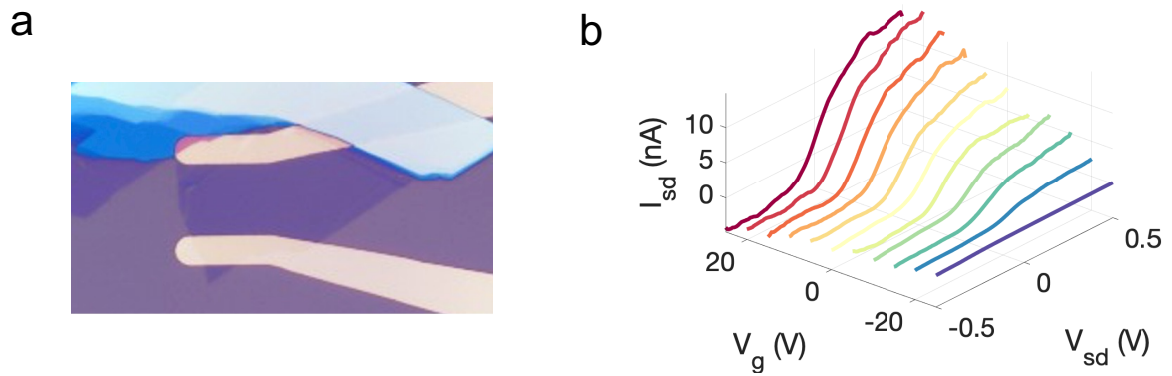


Figure S3. (a) Optical image of a single-layer MoS₂ field effect transistor (FET) device. The distance between the gold leads is 20 μm . (b) Source-drain current-voltage characteristics for a 1L-MoS₂ FET device as a function of back-gate voltage (V_g).

S4. Rectification ratio determination for a FePS₃/1L-MoS₂ diode (device *A*) and comparison with other van der Waals heterojunctions

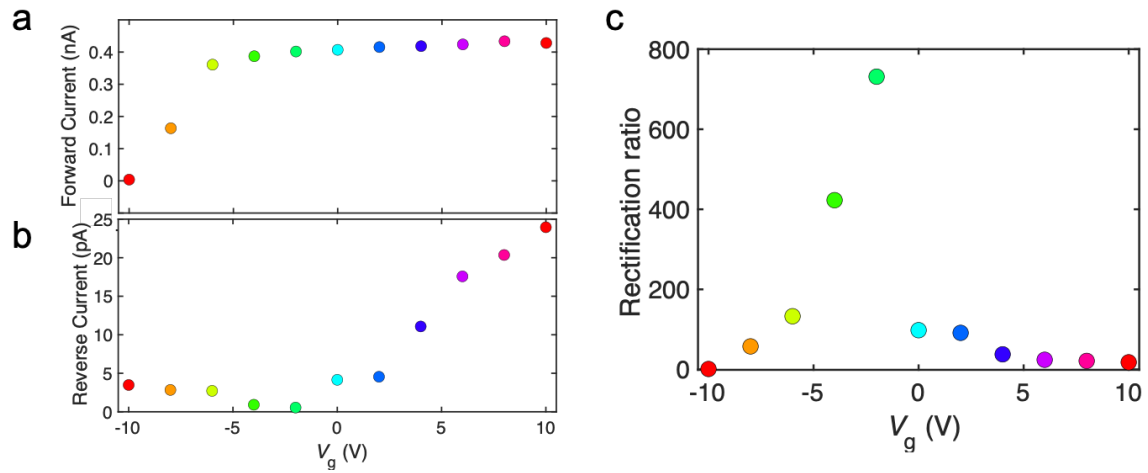


Figure S4. (a) Forward current at $V_{sd} = 0.5$ V as a function of gate voltage (V_g). (b) Reverse current at $V_{sd} = -0.5$ V as a function of gate voltage (V_g). (c) Rectification ratio as a function of the applied gate voltage V_g for device *A*, obtained from the $I_{sd} - V_{sd}$ curve shown in Fig. 1g at $V_{sd} = 0.5$ V.

The rectification ratio is obtained as the quotient between the currents measured for a certain value of V_{sd} with opposite polarities. A maximum rectification ratio of $RR \sim 750$ is obtained for device *A* at $V_g = -2$ V and for $|V_{sd}| = 0.5$ V.

Below, a comparative table including rectification ratios in van der Waals heterojunctions containing MoS₂ is included.

Table S2. Rectification ratios of different van der Waals heterojunctions containing MoS₂. *1L* indicates single layer.

Layer structure	Rectification ratio	V_{sd} (V)	V_g (V)	Reference
Black P/1L-MoS ₂	10^5	2	-30	[s9]
Black P/MoS ₂	182	1	10	[s10]
Franckeite/MoS ₂	400	0.75	40	[s11]
p-MoS ₂ /n-MoS ₂	250	1	0	[s12]
ReSe ₂ /MoS ₂	500	5	0	[s13]
FePS₃/1L-MoS₂	750	0.5	-2	This work

S5. Ideality factor for FePS₃/1L-MoS₂ photodiodes

In the Shockley model, the ideality factor, n_{id} , is an experimental parameter that shows the deviation of the measured I_{sd} - V_{sd} curve from an ideal diode, due to second-order effects occurring in the system [s10, s11]. The diode equation in this model has the following expression:

$$I_{sd} = I_0 \left(\exp\left(\frac{eV_{sd}}{n_{id}k_B T}\right) - 1 \right) - I_{ph} \quad (S5)$$

where I_0 is the saturation current, e is the electron charge, k_B is the Boltzmann constant and I_{ph} is the photocurrent.

In particular, the ideality factor is equal to 1 (ideal diode) if the current is limited by the recombination of minority carriers in the depletion zone (Langevin recombination), and $n_{id} = 2$ if the recombination involving trapped levels in the spatial region of charge is dominant (Shockley-Read-Hall recombination) [s14,s15].

An expression for the ideality factor of a photodiode can be derived from the diode equation (eq. S5) for $I_{sd} = 0$:

$$V_{oc} = n_{id} \left(\frac{k_B T}{q} \right) \ln \left(\frac{I_{ph}}{I_0} + 1 \right) \quad (S6)$$

If the photocurrent scales linearly with the incident effective power P_{eff} , and $I_{ph}/I_0 \gg 1$:

$$V_{oc} = n_{id} \left(\frac{k_B T}{q} \right) \ln(P_{eff}) + K(T) \quad (S7)$$

$$n_{id} = \left(\frac{q}{k_B T} \right) \frac{dV_{oc}}{d(\ln(P_{eff}))} \quad (S8)$$

Fitting the experimental values of V_{oc} as a function of P_{eff} to eq. S7 (Fig. S3b and Fig. 2d in the main text) yields a value of $n_{id} = 1.98$, which indicates that the FePS₃/1L-MoS₂ diode photo-response is dominated by SRH recombination assisted by trapped states.

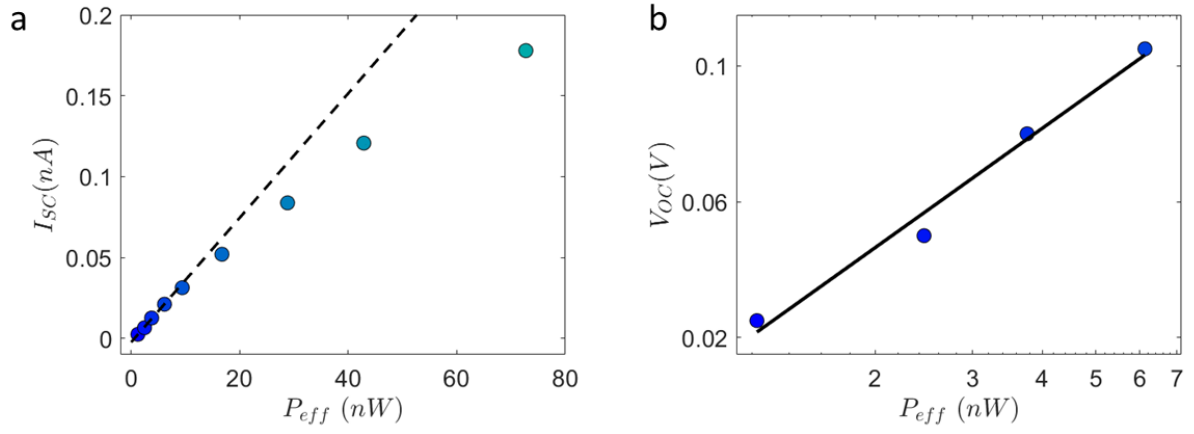


Figure S5. (a) Linear fit to I_{sc} data for the power range where I_{sc} grows linearly with P_{eff} ($I_{sc} \propto P_{eff}$) (device A). (b) Linear fit to V_{oc} data the effective power values that satisfy $I_{sc} \propto P_{eff}$. The slope of the fitting curve is $dV_{oc}/d(\ln(P_{eff})) = 0.051$.

S6. Power conversion efficiency for FePS₃/1L-MoS₂ (device *A*).

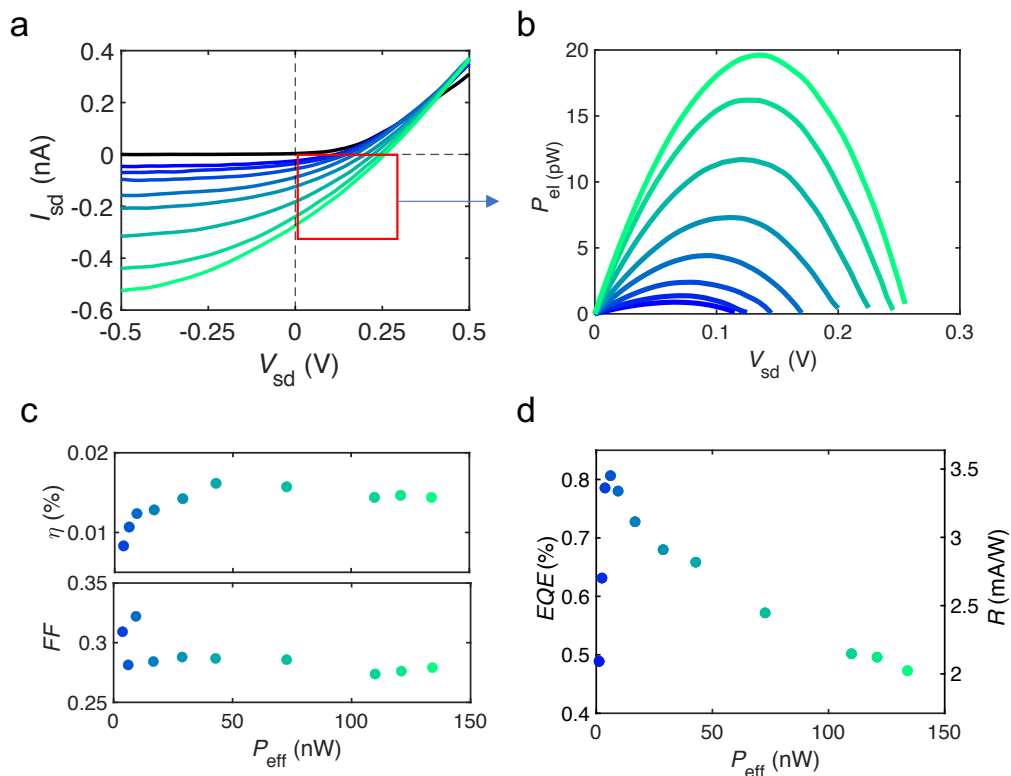


Figure S6. (a) I_{sd} - V_{sd} characteristics of device *A* (same plot as Fig. 2a in the main text). The red square highlights the quadrant in which the device is evaluated for power conversion. (b) Electrical power produced by the photovoltaic cell (device *A*) as a function of the source-drain voltage at several incident, effective, optical powers. The range of effective powers used goes from 1.2 nW (blue) up to 130 nW (green). (c) Power conversion efficiency (top) and fill factor (bottom) as a function of effective power. (d) Corresponding external quantum efficiency and responsivity at $V_{sd} = 0$ upon illumination with 530 nm light.

The fourth quadrant of the $I_{sd} - V_{sd}$ curve in Fig. S6a (Fig. 2a of the main text), which is delimited by $I_{sd} = I_{sc}$ and $V_{sd} = V_{oc}$, defines the region in which the device can be tested as a photovoltaic solar cell. The electrical power delivered by the cell is defined as the product between the applied voltage and the output current: $P_{el} = I_{sd} \cdot V_{sd}$. A maximum value of $P_{el,m} = 19.6$ pW is obtained at $V_m = 0.14$ V upon illumination at $P_{eff} = 130$ nW. The power conversion efficiency of the cell, η , is defined as the ratio between the maximum electrical power delivered by the cell and the effective illumination power, $\eta = P_{el,m} / P_{eff}$. The fill factor FF is defined as the ration between the electrical power delivered by the cell and the ideal maximum given by $P_{el,ideal} = I_{sc} \cdot V_{oc}$.

Table S3. Power conversion efficiency and fill factor for different van der Waals heterostructure devices.

Layer structure		Device performance		Reference
		η (%)	FF	
Containing single-layer TMDs	Black P (11 nm) /1L-MoS ₂	0.57	~ 0.5	[s9]
	WSe ₂ /1L-MoS ₂	0.2	~ 0.5	[s15]
	WSe ₂ /1L-MoS ₂	0.4	-	[s16]
	FePS₃/1L-MoS₂	0.015	0.3	This work
Containing multi-layer TMDs	p-MoS ₂ /n-MoS ₂	-	0.46	[s12]
	ReSe ₂ /MoS ₂	0.072	0.34	[s13]

S7. EQE and responsivity comparison between van der Waals heterostructures

Table S4. External quantum efficiency EQE at $V_{sd} = 0$ V for different van der Waals heterostructure devices.

Layer structure	EQE (%)	λ (nm)	Reference
Containing single-layer TMDs	BP/1L-MoS ₂	0.3	633 [s9]
	WSe ₂ /1L-MoS ₂	1.5	Halogen lamp (~590 nm) [s15]
	1L-WSe ₂ /1L-MoS ₂	2.4	532 [s16]
	1L-WSe ₂ /1L-MoS ₂	2	495 [s16]
	WSe ₂ /1L-MoS ₂	12	514 [s17]
	FePS ₃ /1L-MoS ₂	1.2	532 This work
	FePS₃/1L-MoS₂	2	385 This work
Containing multi-layer TMDs	p-MoS ₂ /n-MoS ₂	4.7	660 [s12]
	FePS ₃ /MoSe ₂	12	522 [s18]

Table S5. Responsivity for different van der Waals heterostructure devices.

Layer structure	Responsivity (mA/W)	λ (nm)	V_{sd} (V)	Reference
Containing single-layer TMDs	BP /1L-MoS ₂	418	633	-2 [s9]
	WSe ₂ /1L-MoS ₂	11	~590 nm (halogen)	-1 [s15]
	1L-WSe ₂ /1L-MoS ₂	2-10	532	0 [s16]
	1L-WSe ₂ /1L-MoS ₂	8	495	0 [s16]
	1L-WSe ₂ /1L-MoSe ₂	~5	514	-1 V [s21]
	FePS ₃ /1L-MoS ₂	~20	532	-1 This work
	FePS₃/1L-MoS₂	40	385	-1 This work
Containing multi-layer TMDs	Black P/MoS ₂	$8.5 \cdot 10^3$	500	0.7 [s10]
	p-MoS ₂ /n-MoS ₂	14	660	0 [s12]
	ReSe ₂ /MoS ₂	$6.75 \cdot 10^3$	633	1 [s13]
	FePS ₃ /MoSe ₂	52	522	0 [s18]
	FePSe ₃ /MoS ₂	$3.3 \cdot 10^4$	265	4 [s19]
	FePS ₃ /ReS ₂	$\sim 1 \cdot 10^5$	305	-1 [s20]

S8. Optoelectronic characterization for device *B*

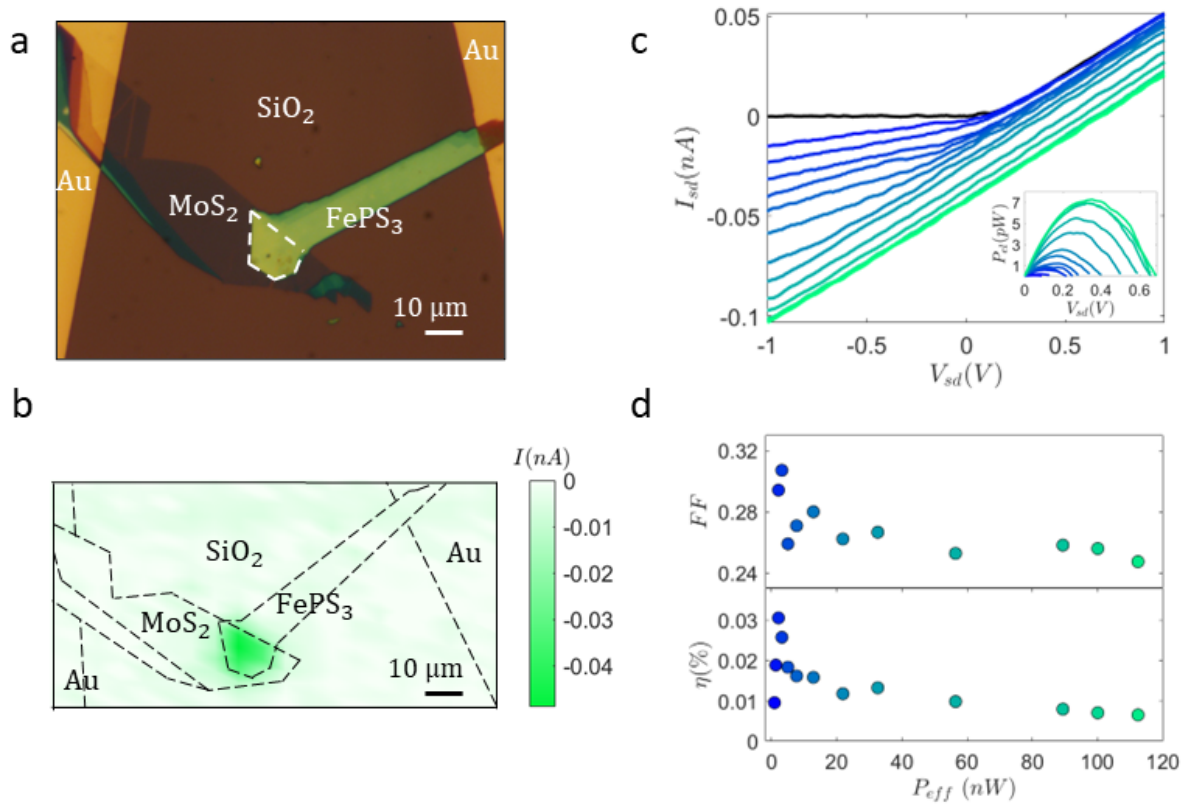


Figure S7. (a) Optical microscopy image of a device *B*. (b) Scanning photocurrent map of device *B*, at $V_{sd} = V_g = 0$ V, obtained with an illumination spot of ~ 1 μm diameter and $P_{opt} = 80$ nW. (c) $I_{sd} - V_{sd}$ characteristics at $V_g = 0$ V, upon dark and illumination conditions ($\lambda = 532$ nm) with optical power up to 120 nW. Inset: Electrical power harvested by the FePS₃/1L-MoS₂ p-n junction as a function of the illumination power. (d) Fill factor and power conversion efficiency extracted from panel (c).

S9. Bias voltage dependence of photoluminescence for device *D*

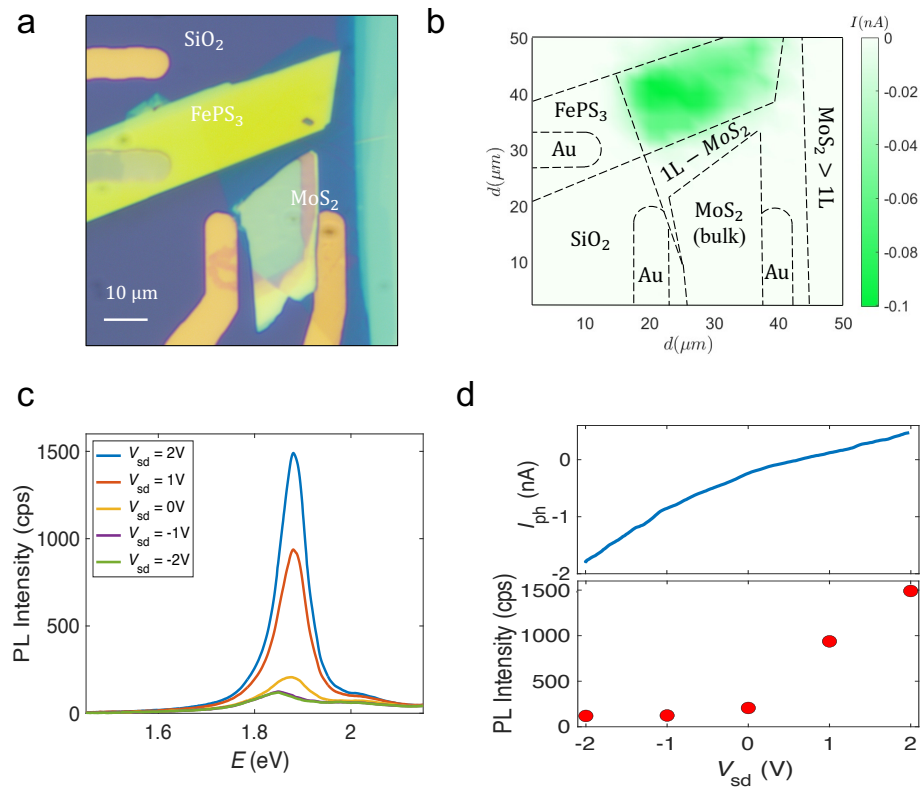


Figure S8. (a). Optical microscopy image of device *D*. (b) Scanning photocurrent map for the same device at zero applied bias voltage. (c) Photoluminescence emission from device *D* as a function of the applied bias voltage for a $P_{\text{eff}} = 180\ \mu\text{W}$ and $\lambda = 532\ \text{nm}$. (d) Photocurrent $I_{\text{ph}} = I_{\text{light}} - I_{\text{dark}}$ (top) and PL maximum intensity (bottom) as a function of the applied bias voltage.

S10. Photocurrent maps under applied bias

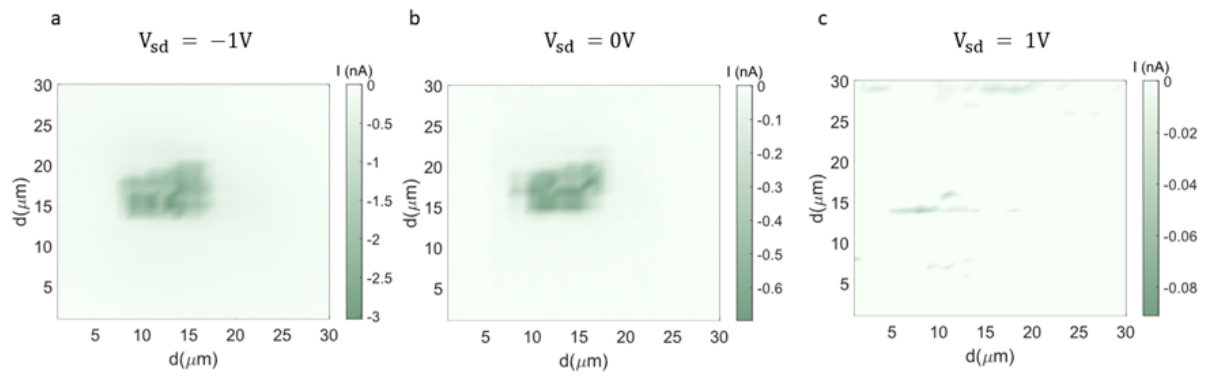


Figure S9. Photocurrent maps for device *C* at different bias voltage V_{sd} . Maps are recorded using a 532 nm laser for excitation with a spot size of $\sim 1 \mu\text{m}$ diameter and an effective power of $P_{\text{opt}} = 72 \text{ nW}$.

S11. Gate dependence of dark and bright I_{sd} - V_{sd} characteristics for device B

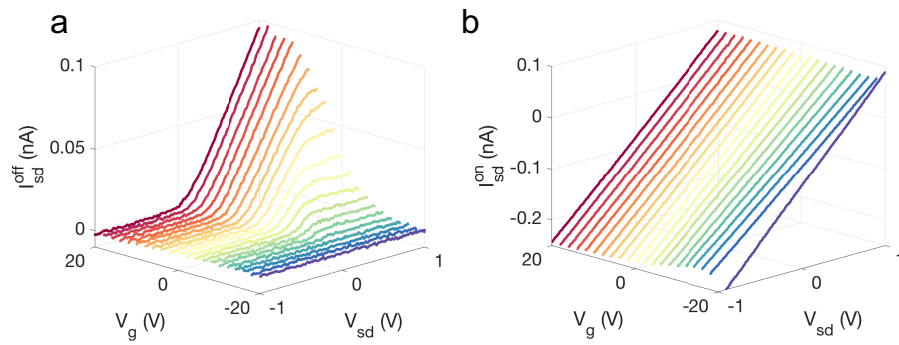


Figure S10. I_{sd} as a function of V_{sd} and V_g in (a) dark and (b) upon illumination with $\lambda = 530$ nm and $P_{eff} = 95$ nW.

S12. Raman spectroscopy for device *A*

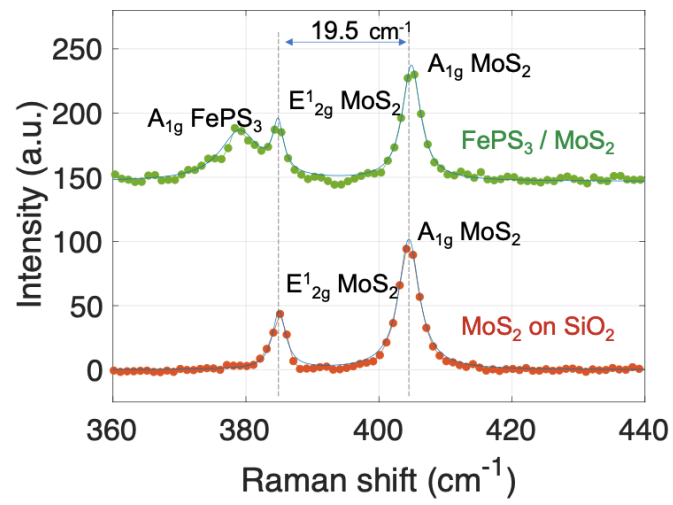


Figure S11. Raman spectra for device *A* at a spot on the 1L- MoS_2 on SiO_2/Si (red curve) and at a spot at the junction with FePS_3 (green curve). Spectra were taken using a 532 nm excitation line with 100 μW power.

S13. Spectral weights for trions and neutral excitons in FePS₃/1L-MoS₂ devices as a function of applied bias

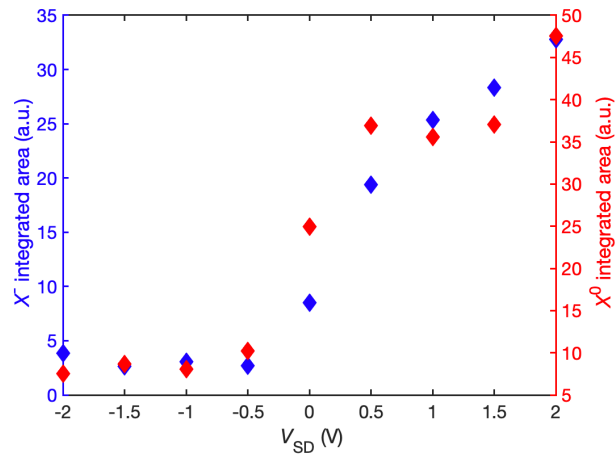


Figure S12. Trion (blue) and neutral exciton (red) spectral weights obtained from a three-Lorentzian fit to the PL spectra shown in Figure 3a of the main manuscript, as a function of the applied bias voltage.

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