

Supplementary Material

Adsorptive removal of ciprofloxacin by chitosan modified Fe pretreatment biochar composite from aqueous solution

7 Author

- 8 1. Ruiyao Huang, First author, School of Chemistry and Materials Science,
9 Heilongjiang University, Harbin 150080, China, huanghry1102@163.com
- 10 2. Qi Zhu*, Corresponding author, School of Chemistry and Materials Science,
11 Heilongjiang University, Harbin 150080, China, hdzhuqi@126.com
- 12 3. Weixin Wang, School of Chemistry and Materials Science, Heilongjiang
13 University, Harbin 150080, China, wangweixin1010@163.com
- 14 4. Yuhan Hu, School of Chemistry and Materials Science, Heilongjiang University,
15 Harbin 150080, China, huyuhan0001@126.com

17 1.1 Characterization methods

18 XPS (Escalab 250Xi) was used to analyze the surface composition of the
19 produced samples, and the results were fitted using "XPS peak" software. The
20 Brunauer–Emmett–Teller (BET) surface areas of the samples were determined using
21 N₂ adsorption on a Micromeritics ASAP2420 instrument, and the plot of the pore-
22 diameter distribution was determined by using the Barrett–Joyner–Halenda (BJH)
23 method from the desorption branch of the isotherm. The micromorphological
24 characteristics of samples were characterized using a Hitachi S-4800 scanning
25 electron microscope (SEM) at an accelerating voltage of 5.0 kV. The X-ray

26 diffraction (XRD) patterns of samples were obtained using a Rigaku D/max-IIIB X-
27 ray diffractometer with Cu K α radiation ($\lambda = 1.5406 \text{ \AA}$) generated at 40 kV and 20
28 mA. Functional groups in the compounds were analyzed by Fourier Transform
29 Infrared Spectroscopy (FTIR, Nicolet IS10). The Nano Series (Malvern, UK) Zeta
30 Sizer Nano-ZS system was used to detect zeta potentials at a temperature of 25°C.

31 1.2 The information of models

32 The adsorption capacities of CS-FBC at time t (q_t) and at adsorption equilibrium
33 (q_e) were calculated according to the following equations:

$$q_t = \frac{(C_0 - C_t)V}{m} \quad (1)$$

$$q_e = \frac{(C_0 - C_e)V}{m} \quad (2)$$

34 where C_0 and C_e represent the initial and equilibrium time concentrations of CIP
35 (mg/L), respectively. C_t represents the concentration at time t (mg/L), V is the volume
36 of the solutions (L), and m is the mass of the adsorbent (g).

37 1.3 Adsorption kinetics

38 To further understand the adsorption capacity and the underlying adsorption
39 mechanism, adsorption kinetic models are usually selected. The primary focus of
40 adsorption kinetics investigation is the rate of time-dependent adsorption of adsorbent
41 onto adsorbate. The most common adsorption kinetic models include: pseudo-first-
42 order kinetic model, pseudo-second-order kinetic model, intraparticle diffusion model
43 (Weber and Morris), and Elovich kinetic model. The adsorption process of CIP by
44 CS-FBC is studied by two kinetic models, the formula is as follows:

$$\ln(q_e - q_t) = \ln q_e - k_1 t \quad (3)$$

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e} \quad (4)$$

45 where q_e is the amount of CIP (mg/g) at equilibrium time and q_t is the amount of CIP

46 (mg/g) at a certain time t (min), k_1 is the pseudo-first-order rate constant (min^{-1}) and
47 k_2 is the pseudo-second-order rate constant ($\text{g}/(\text{mg}\times\text{min})$).

48 **1.4 Adsorption isotherm**

49 The adsorption of CIP by CS-FBC at various temperatures was investigated, and
50 the Langmuir and Freundlich isotherm models were usually used to analyze the
51 adsorption process. The Langmuir adsorption model, which assumes that the
52 adsorption sites are entirely independent and homogenous, is a monolayer adsorption
53 model. The nonlinear and linear expressions of the Langmuir isothermal adsorption
54 model are as follows:

$$q_e = \frac{q_{max}K_L C_e}{1 + K_L C_e} \quad (5)$$

$$\frac{C_e}{q_e} = \frac{C_e}{q_{max}} + \frac{1}{K_L q_{max}} \quad (6)$$

55 Unlike the Langmuir model, the Freundlich adsorption isotherm model is an
56 empirical equation with no prior assumptions. These are its linear and nonlinear
57 expressions, respectively, are as follows:

$$q_e = K_F C_e^{\frac{1}{n}} \quad (7)$$

$$\ln q_e = \ln K_F + \frac{1}{n} \ln C_e \quad (8)$$

58 where q_{max} (mg/g) is the theoretical maximum adsorption capacity, b (L/mg) is
59 the Langmuir constant related to the adsorption energy, and K_F (mg/g)(L/mg) $^{1/n}$ and n
60 are the Freundlich constants.

61 **1.5 Adsorption thermodynamic**

62 Temperature is another important factor affecting the efficiency of adsorbents.
63 The adsorption of CS-FBC on CIP in solution was studied at 15°C, 25 °C and 35 °C.
64 By computing the standard enthalpy change (ΔH°), the standard entropy change (ΔS°),

65 and the standard free energy variation (ΔG°) to represent the adsorption
66 thermodynamics, the feasibility of the adsorption process was examined. The
67 expressions of the equations are as follows:

$$\ln K_C = -\frac{\Delta H^\circ}{RT} + \frac{\Delta S^\circ}{R} \quad (9)$$

$$\Delta G^\circ = -RT \ln K_C \quad (10)$$

68 where R is the molar constant of the gas with a value of 8.3145 (J/(mol×k)), T is the
69 absolute temperature (k), and K_C is the standard thermodynamic equilibrium constant
70 (L/mg).

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