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# **Supporting Information**

## **Si-modified Mn-Ce oxide catalyst for selective catalytic reduction of**

## **NO***<sup>x</sup>* **with NH<sup>3</sup> at low temperature**

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#### **1.1 Catalytic activity test**

The NH<sub>3</sub>-SCR performance of the catalysts was evaluated in a fixed-bed quartz reactor. The catalyst samples (40-60 mesh) were put into a quartz tube with an inner diameter of 6 mm, which was placed in a tube furnace, and the temperature was controlled at 50 to 300 °C. The simulated flue gas was composed of 500 ppm NO, 500 ppm NH<sub>3</sub>, 50 ppm SO<sub>2</sub> (when used), 5%  $O_2$  and N<sub>2</sub> balance. The total flow rate was 500 mL·min<sup>-1</sup>, and the corresponding gas hourly space velocity (GHSV) was  $5\times10^4$  h<sup>-1</sup>. The effluent gases, including NH<sub>3</sub>, NO, N<sub>2</sub>O and NO<sub>2</sub>, were analyzed by a Nicolet IS50 FTIR gas analyzer. Activity data were collected when the catalytic reaction actually reached steady-state conditions at each temperature.

#### **1.2 Catalyst Characterization**

The specific surface area and pore characteristics of the samples were measured by  $N_2$ adsorption/desorption analysis on a physisorption analyzer (MicrotracBEL). The samples need to be degassed at 300 °C for 1 h before  $N_2$  physisorption at 77 K.

X-ray diffraction (XRD) patterns of the samples were recorded on a diffractometer (Bruker D8 Advance, Germany) with CuKα radiation (= 0.154056 nm) in a 2θ of 10°–80° at  $0.02$  °s<sup>-1</sup>.

The temperature programmed desorption of  $NH<sub>3</sub>$  (NH<sub>3</sub>-TPD) was carried out on an FTIR spectrometer (Nicolet IS50). The catalyst sample (50 mg) was first pretreated in air at 300 °C for 0.5 h, and then cooled down to 50 °C under N<sub>2</sub> conditions. Afterwards, the catalyst sample was exposed to 500 ppm  $NH<sub>3</sub>/N<sub>2</sub>$  until saturation, followed by N<sub>2</sub> purging for 0.5 h. Finally, the catalyst sample was heated from 50 °C to 650 °C in a N<sub>2</sub> flow (100 mL·min<sup>-</sup> <sup>1</sup>) at a constant heating rate (10 °C·min<sup>-1</sup>). The concentration of NH<sub>3</sub> was detected using Nicolet IS50 FTIR spectroscopy.

The  $H<sub>2</sub>$  temperature programmed reduction ( $H<sub>2</sub>-TPR$ ) experiments were performed on an Autochem 2920 (Micromeritics) analyzer. The samples (50 mg) were pretreated at 300  $°C$  in a quartz reactor in a flow of Ar (50 mL $\cdot$ min<sup>-1</sup>) for 1 h and cooled down to room temperature. Then, from room temperature to 800 °C,  $H_2$ -TPR was performed in a 10 vol.% H<sub>2</sub>/Ar gas flow of 50 mL·min<sup>-1</sup> at a heating rate of 10 °C·min<sup>-1</sup>.

The surface element compositions and chemical states of each catalyst sample were evaluated by an X-ray photoelectron spectroscopy (XPS) analyzer (Axis Ultra, Kratos Analytical Inc.) using Al Kα X-ray radiation (1486.6 eV). All of the binding energies were calibrated using the C 1s peak (binding energy = 284.8 eV) as a standard.

The adsorption behavior of the reactants and their surface reactions were studied by *in situ* diffuse reflectance infrared Fourier transform spectroscopy (*in situ* DRIFTS), which was carried out on a Brooker VERTEX 80/80V Fourier transform infrared spectrometer (Brück, Germany) equipped with liquid nitrogen-cooled MCT detection. The powder sample was pretreated in 20 %  $O_2/N_2$  at 450 °C for 0.5 h prior to adsorption experiments. The following conditions were controlled as follows: 500 ppm NH $_3$ , or 500 ppm NO + 5%  $O_2$ , N<sub>2</sub> balance, and the total flow rate was kept at 300 mL·min<sup>-1</sup>. For the experiments on NH<sub>3</sub> or NO<sub>x</sub> adsorption, the sample was saturated with NH<sub>3</sub>/N<sub>2</sub> or NO<sub>x</sub>/N<sub>2</sub> for 40 min, and then purged with  $N_2$  for 30 min. All spectra were recorded by accumulating 100 scans with a resolution of 4 cm $^{-1}$ .

#### **1.3 Kinetics experiment**

In order to obtain a further understanding of the effect of Si doping and sulfation aftertreatment on the NH<sub>3</sub>-SCR reaction, the kinetics experiments were studied on  $Mn_4Ce_6$ ,  $Mn_4Ce_5Si_1$  and  $Mn_4Ce_5Si_1-1S\%$  catalysts. The samples with particles of 40-60 mesh and a total gas flow rate of 500 mL $\cdot$ min $^{-1}$  were selected to rule out internal and external transfer diffusion. The NO*<sup>x</sup>* conversion was controlled below 20%. The NO*<sup>x</sup>* reduction rates (mol·g·s<sup>-1</sup>) and activation energy ( $E_a$ ) were calculated based on the following equations:

$$
-r = \frac{F}{w} \ln(1-x)
$$

$$
k = \frac{r}{[NO]_0} = Ae^{-Ea/RT}
$$

where F is the NO<sub>x</sub> flow rate,  $[NO_x]_0$  is the NO<sub>x</sub> concentration at the inlet, W is the mass of catalyst,  $E_a$  is the apparent activation energy, T is the Kelvin temperature, R is the gas constant (8.314 J/(mol·K)), and A represents the pre-factor.





**Fig. S1** NO<sub>x</sub> conversion and N<sub>2</sub> selectivity versus temperature over different catalysts: different Ce/Si molar ratios (a), different Mn/Ce molar ratios (b), and  $N_2$  selectivity (c). A series of Si-modified Mn-Ce oxide catalysts were prepared to study the effect of the Si element on the NH<sub>3</sub>-SCR activity of Mn-Ce oxide catalysts, as shown in Fig. S1. When the content of Mn was constant, the increase of Si/Ce ratio resulted in a decrease in NO*<sup>x</sup>* conversion at low temperature. However, the catalyst activity (>200 °C) was in the order following:  $Mn_4Ce_1Si_5 > Mn_4Ce_2Si_4 > Mn_4Ce_3Si_3 > Mn_4Ce_4Si_2 > Mn_4Ce_5Si_1$ . The  $Mn_3Ce_bSi_c$ with different Mn/Ce ratios was also investigated, and the  $Mn_4Ce_5Si_1$  catalyst showed the widest temperature window and highest NO*<sup>x</sup>* conversion (> 90%) at 100-260 °C.



**Fig. S2** (a)  $NH<sub>3</sub>$  conversion and (b) NO conversion in separate  $NH<sub>3</sub>$  and NO oxidation reactions over  $Mn_4Ce_6$ ,  $Mn_4Ce_5Si_1$  and  $Mn_4Ce_5Si_1$ -1%S.

As shown in Fig. S2, the  $Mn_4Ce_6$  catalyst showed the best  $NH_3$  oxidation activity and NO oxidation activity. The introduction of Si resulted in the decrease of activation of NH<sub>3</sub> and NO, which is the reason of the enhanced  $N_2$  selectivity and decreased catalytic activity at low temperature.



Fig. S3 NO<sub>x</sub> conversion of catalysts with different  $H_2SO_4$  loadings at 260 and 110 °C.  $Mn_4Ce_5Si_1$  was sulfation after-treated with varying concentrations of sulfuric acid solution, and the NO*<sup>x</sup>* conversions at 110 °C and 260 °C of catalysts are shown in Fig. S3. With the increase in sulfuric acid concentration, the NO<sub>x</sub> conversion at 110 °C decreased and the NO<sub>x</sub> conversion at 260 °C increased over Mn<sub>4</sub>Ce<sub>5</sub>Si<sub>1</sub>-x%S catalysts. When the loading amount of sulfuric acid was 1%, the  $Mn_4Ce_5Si_1-1%S$  catalyst showed a high  $NO<sub>x</sub>$ conversion above 90% in the range of 110-260 °C.



Fig. S4 Effect of H<sub>2</sub>O on the performance of catalyst.

As shown in Fig. S4, when 5% H2O was added to the reaction gas, the NO*<sup>x</sup>* conversion of all the catalysts decreased below 170°C due to the competitive adsorption of  $H_2O$ , while that increased above 170°C, which may be attributed to the inhibition of the unselective oxidation of NH<sub>3</sub> at high temperature. The N<sub>2</sub> selectivity of all the catalysts was enhanced significantly at the present of  $H_2O$  (Fig. S4b). In comparison, the  $H_2O$ tolerance of Mn-Ce oxide catalysts wasimproved after Si modification and sulfation aftertreatment.



**Fig. S5** NO<sub>x</sub> reduction rates as a function of reaction temperature over  $Mn_4Ce_6$ ,

 $Mn_4Ce_5Si_1$  and  $Mn_4Ce_5Si_1-1%S$  catalysts.

To further understand the effect of Si and sulfation after-treatment on the reaction kinetics of NO<sub>x</sub> reduction over Mn-Ce oxide catalysts, Arrhenius plots of the NH<sub>3</sub>-SCR reaction are shown in Fig. S4. It can be seen that  $Mn_4Ce_6$ ,  $Mn_4Ce_5Si_1$  and  $Mn_4Ce_5Si_1$ -1%S have similar Ea (~37 kJ/mol), indicating of identical catalytic centers and rate-limiting steps.



Fig. S6 SEM images of (a and b)  $Mn_4Ce_6$ , (c and d)  $Mn_4Ce_5Si_1$ , and (e and f)  $Mn_4Ce_5Si_1$ -

1%S catalysts.



**Fig. S7** H<sub>2</sub> consumption of  $Mn_4Ce_6$ ,  $Mn_4Ce_5Si_1$ , and  $Mn_4Ce_5Si_1-1%S$  catalysts.



**Fig. S8** FT-IR spectra of  $Mn_4Ce_6$ ,  $Mn_4Ce_5Si_1$ , and  $Mn_4Ce_5Si_1$ -1%S catalysts.

A distinct band attributed to the Si-OH bond (ca. 910 cm<sup>-1</sup>) was detected on  $Mn_4Ce_5Si_1$ and  $Mn_4Ce_5Si_1-1%S$ , suggesting the abundant surface hydroxyl groups formed on the catalyst surface after the introduction of Si and sulfation after-treatment.<sup>1</sup>



Fig. S9 NO-TPD profiles of Mn<sub>4</sub>Ce<sub>6</sub>, Mn<sub>4</sub>Ce<sub>5</sub>Si<sub>1</sub> and Mn<sub>4</sub>Ce<sub>5</sub>Si<sub>1</sub>-1%S.

The NO-TPD profiles (Fig. S9) showed two distinct desorption peaks at 136-149 °C and 375-389 °C, which were attributed to physical-absorbed NO*<sup>x</sup>* or the decomposition of monodentate nitrate species and the decomposition of bidentate nitrates or bridged nitrate species, respectively.<sup>1</sup>

### **References**

1. W. Tan, A. Liu, S. Xie, Y. Yan, T. Shaw, Y. Pu, K. Guo, L. Li, S. Yu, F. Gao, F. Liu and L. Dong, *Environ. Sci. Technol.*, 2021, **55**, 4017-4026.