

## Supplementary Information

### Waveguide-integrated self-powered van der Waals heterostructure photodetector with high performance at telecom wavelength

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#### S1. Tunable optoelectronic characteristics of the MZI-integrated BP/MoS<sub>2</sub> photodetector by simple electrostatic gatings.

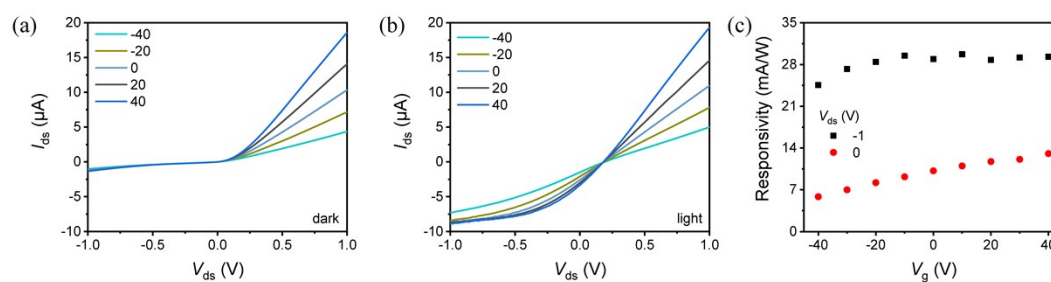


Figure S1. (a) and (b) Gate tunable  $I$ - $V$  characteristics of the photodetector under dark and illuminated condition, respectively. (c) Responsivities of the device as a function of back gate voltages at -1 V and 0 V.

The gate-tunable electrical characteristics were investigated. Figure S1(a) and (b) present the output  $I$ - $V$  characteristics under the dark condition and illuminated condition, respectively, in which the current gradually increased at voltages between -1 and 1 V in accordance with an increase in the gate voltage from -40 to 40 V.

We measure the responsivities of the photodetector under zero-bias and reverse bias of 1 V as a function of the gate voltage, as shown in Fig S1(c). In all cases, the responsivity increases with increasing the gate voltage. The responsivity is improved from 5.84 mA W<sup>-1</sup> to 13.06 mA W<sup>-1</sup> for the zero-bias case and 24.56 mA W<sup>-1</sup> to 29.30 mA W<sup>-1</sup> for the case of  $V_{ds} = -1$  V. These results indicate that the photoresponse of the MZI-integrated BP/MoS<sub>2</sub> transistor can be actively controlled and gradually tuned by the electrical gate, which can be a promising adaptive photodetector/voltaic device.

## S2. Comparison with BP/MoS<sub>2</sub> photodetectors operating in the free space.

Table S1. A summary of BP/MoS<sub>2</sub> heterojunction photodetectors.

Material	Wavelength	Response time	Ref.
BP/MoS <sub>2</sub>	365 nm to 660 nm	>10 s	1
BP/MoS <sub>2</sub>	532 nm 1.55	15 μs	2
BP/MoS <sub>2</sub>	650 nm 1000 nm	13 μs	3
BP/MoS <sub>2</sub>	582 nm	<1 s	4
BP/MoS <sub>2</sub>	650 nm 808 nm	~50 μs ~50 ms	5
BP/MoS <sub>2</sub>	1527.4 nm	2.08 μs/3.54 μs	This work

We compare the performance of our waveguide-integrated BP/MoS<sub>2</sub> photodetector with other reported BP/MoS<sub>2</sub> photodetectors operating in the free space, as shown in Table S1. Compared with the BP/MoS<sub>2</sub> photodetectors operating in the free space, our waveguide-integrated BP/MoS<sub>2</sub> photodetector has a faster response speed. This could be attributed to the enhanced light-matter interaction on the BP/MoS<sub>2</sub> van der Waals junction, which improves the light absorption as well as the photoresponse. Benefiting from the orthogonal directions in the path of photogenerated carriers and light propagation, the trade-off between the responsivity and rise/decay times in photodetectors can be overcome for high response and fast speed device. Moreover, the waveguide-integration architecture has much smaller device footprint, which therefore could reduce the dark current and promise much higher response speed.

## S3. Theory of grating design of waveguide

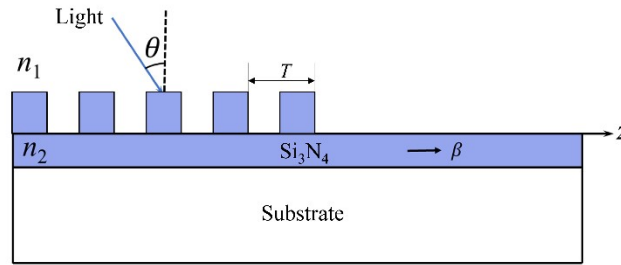


Figure S2. Schematic of light coupling into the grating coupler.

Figure S2 shows, the Bragg condition  $\frac{2\pi}{\lambda}n_1\sin\theta + m\frac{2\pi}{T} = \beta$  should be satisfied when coupling, where  $\lambda$  represents the wavelength coupled into,  $n_1$  is the refractive index of air,  $\theta$  is the incident angle,  $T$  is the grating period,  $m$  is the diffraction order, and  $\beta$  is the propagation constant of traveling wave in the waveguide. When  $\lambda$  ( $m = 0$  and  $\theta, T, \beta$  are constants) is changed, owing to the mismatch of two sides of the Bragg condition, grating couplers could only support relative flat spectral coupling around the central wavelength  $\frac{2\pi n_1 \sin \theta}{\beta}$ , i.e., there is a limited bandwidth.

## References

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