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Supplementary Information (SI)

Efficient noble metal promoted bimetallic Cobalt Catalysts in the selective Synthesis of Acetaldehydedimethylacetale K. A. Sheikh^{[a],[b]}, T. A. Zevaco^[a], J. Jelic^[a], F. Studt^[a], M. Bender^[b] ^[a]Karlsruher Institut für Technologie (KIT), ^[b]BASF SE

Standard procedure for catalyst screening:

1 g of catalyst was weighed into the autoclave under inert gas flow. The autoclave was closed and filled with argon to 2 bar and released, this process was repeated three times. After that the HiBatch receipt was started. Generally, the receipt starts after the user admits to have performed all precautions before starting the experiment. Like opening the pressure equalisation valve for the methanol container, opening manual gas inlet valves for CO, H₂ and Ar, and opening the gas cylinders. After that the counters for the amount dosed of CO and H₂ are resetted for all three reactors. Followed by the adjustment of the multivalve into the Position 1 (for reactor 1). The Multiportvalve controls the flow of the solvent to each of the reactor. After adjusting it, the liquid dosing starts (User has to give amount of methanol needed). Simultaneously the gas dosing starts, where the user has to give the maximum pressure value, stirrer speed (and ramp) and the needed mixture of H₂ and CO. After that the Mass-Flow Controllers (MFC) for H₂ and CO are started. All setpoints for the MFCs are reached with a ramp. This prevents overshooting of the MFC. Still we dose the mixture into the fume hood until the MFCs are in a steady state. After that the user has to give the permission and the valves towards the fume hood close and the valve towards the reactor open and the gas dosing starts. The gas dosing can be controlled with the total amount of CO/H₂ dosed (in ml) or with the total pressure needed (in bar). All runs in this study where performed with the total pressure variant. After the end of liquid dosing the receipt automatically switches to the next reactor. After the end of gas dosing the system automatically stops the dosing, switches of the MFCs, closes the valves and starts the heating procedure (Reactor inlet temperature regulation and Jacket temperature regulation is possible).

PASCAR plant:

The plant is controlled with 21 pneumatic valves. This allows a separate dosing of CO and H₂ into each reactor. Additionally one Argon MFC is used for the purging of the reactors with intert gas. It can also be used as a pressure control. As the use of reactant gas reduces the reaction pressure, fresh synthesis gas (CO/H₂) or inert gas can be dosed into the system to keep the pressure of all reactors constant all throughout the experiments. Most experiments are run for 24 h or 45 h. A mechanical stirrer can stir the mixture up to 1200 RPM. Inlet pressures of the gases and the reactor pressures are monitored. The inlet temperature and the mantle temperature is recorded separately. Both temperatures can be regulated. Furthermore hexane, dimethoxymethane, methanol and other solvents can easily exchanged and dosed with two available HPLC. Therefore also mixtures of these solvents can be dosed. The catalyst have to be introduced before closing the reactors. Liquid catalysts or catalyst solutions can also be dosed with the HPLC pump. Beside liquids, gaseous compounds can be dosed in total amounts. Therefore, one gaseous compound can be dosed and the mixture heated to the desired temperature, after reaching the temperature the second (reactive) gaseous compound is dosed into the reactor, which marks the starting point of the reaction. For slower reactions starting points can be marked by the time the reaction temperature is reached.



Figure S1: Picture of the PASCAR plant showing all three reactors.



Figure S2: Close up picture of one reactor of the PASCAR plant and the sample loop.

ICP-OES Results of the recycling runs

Table S1: Results of the ICP measurements of the methanolic solutions after the reaction. The values in the brackets show the cobalt concentration on the second run.

| Sample | Ru_ICP µg/ml | Co_ICP μg/ml | Pd_ICP µg/ml | Pt_ICP μg/ml | Au_ICP μg/ml |
|--|-----------------|-----------------|-----------------|-----------------|-----------------|
| Co on Al ₂ O ₃ | - | 119.4 | - | - | - |
| RuCo on Al ₂ O ₃ | 8 | 137.5 | - | - | - |
| PdCo on Al ₂ O ₃ | - | 99.7 | 0 | - | - |
| PtCo on Al ₂ O ₃ | - | 326 | - | 0 | - |
| AuCo on Al ₂ O ₃ | - | 155.2 (193.8) | - | - | 0 (0) |
| RuCo on CeO ₂ | 6 | 48.6 | - | - | - |
| PdCo aon CeO ₂ | - | 61.2 | 0 | - | - |
| PtCo on CeO ₂ | - | 47.1 | - | 0 | - |
| AuCo on CeO ₂ | - | 54.2 | - | - | 0 |

Table S2: Results of the time resolved measurements of the cobalt leaching into the methanolic solution in the run with PtCo on Al_2O_3 .

| Time [h] | Co_ICP [µg/ml] |
|----------|-------------------|
| 3 | 177 |
| 24 | 257 |
| 45 | 391 |

GC Method:

| == | | |
|--------------------|-----------|--|
| Agile | ent 8890 | |
| | | |
| == | | |
| | | |
| GC | | |
| GC Summary | | |
| Run Time | 7.6 min | |
| Post Run Time | 0 min | |
| | | |
| Oven | | |
| Equilibration Time | 0 min | |
| Max Temperature | 240 °C | |
| (Initial) | 40 °C | |
| Hold Time | 2 min | |
| Post Run | 110 °C | |
| #1 Rate | 25 °C/min | |
| #1 Value | 180 °C | |
| #1 Hold Time | 0 min | |
| ALS | | |

| Front Injector | |
|-----------------------------|---|
| Syringe Size | 10 μL |
| Injection Volume | 1 μL |
| Solvent A Washes (PreInj) | 5 |
| Solvent A Washes (PostInj) | 5 |
| Solvent A Volume | 8 μL |
| Sample Washes | 1 |
| Sample Wash Volume | 8 μL |
| Sample Pumps | 3 |
| Solvent Wash Draw Speed | 150 µL/min |
| Solvent Wash Dispense Speed | 6000 μL/min |
| Sample Wash Draw Speed | 150 µĹ/min |
| Sample Wash Dispense Speed | 6000 µL/min |
| Injection Dispense Speed | 6000 µL/min |
| Viscosity Delay | 0 sec |
| L1 Airgap | 0.2 μL |
| | |
| | |
| Front SS Inlet He | |
| Mode | Split |
| Heater | On 180 °C |
| Pressure | On 0 |
| Total Flow | On 133.4 mL/min |
| Septum Purge Flow | On 3 mL/min |
| Pre-Run Flow Test | Off |
| Gas Saver | On 20 After 2 min mL/min |
| Split Ratio | 50 :1 |
| Split Flow | 127.84 mL/min |
| Liner | Agilent 5190-3165: 870 µL (Split. taper. wool. low pressure |
| drop) | |
| | |

PolyArc

| Temperature | | |
|-------------|--------|--|
| Setpoint | On | |
| (Initial) | 450 °C | |

Column #1

Column Information Agilent 123-7033UI DB-WAX Ultra I Temperature Range 20 °C—240 °C (240 °C) Dimensions $30 \text{ m x} 320 \text{ } \mu\text{m} \text{ x} 0.5 \text{ } \mu\text{m}$ Front SS Inlet He In Aux EPC 1 Out (Initial) $40 \ ^{\circ}\mathrm{C}$ Pressure 0 Flow 2.5568 mL/min Average Velocity 33.826 cm/sec Holdup Time 1.4781 min Control Mode Constant Flow (Initial) 2.5568 mL/min 1 mL/min Post Run

Column #2

| Agilent FS. Deactivate |
|------------------------|
| 20 °C—240 °C (240 °C) |
| 2.5 m x 250 μm x 0 μm |
| Front Detector FID |
| 40 °C |
| 0 |
| 4 mL/min |
| 122.56 cm/sec |
| 0.033996 min |
| Constant Flow |
| On |
| 4 mL/min |
| 9.5407 mL/min |
| |

Front Detector FID

| Makeup | Не |
|-----------------------------|------------------------------------|
| Heater | On 250 °C |
| H2 Flow | On 1.5 mL/min |
| Air Flow | On 350 mL/min |
| Makeup Flow | On 25 mL/min |
| Carrier Gas Flow Correction | Constant Makeup and Fuel FlowFlame |
| Initial Baseline Minimum | 2 pA |
| Initial Baseline Maximum | 20 pA |
| Initial Baseline Noise | 0.3 pA |
| Final Baseline Minimum | 2 pA |
| Final Baseline Maximum | 40 pA |
| Final Baseline Noise | 0.6 pA |
| Total Peak Area | 100 pA*sec |
| Maximum Peak Height | 3 pA |
| Time Window Start | 0 min |
| Time Window End | 0.533333333 min |

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Column(s)

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Column Description : DB-WAX Ultra IInventory#: autoID-2Model#: 123-7033UIManufacturer: AgilentDiameter: 320.0 μmLength: 30.0 mFilm thickness: 0.50 μmVoid time: 1.478 minMaximum Temperature:240.0 °C

Comment :

Column Description : FS. Deactivate Inventory# : autoID-3 Model# : Manufacturer : Agilent : 250.0 µm Diameter : 2.5 m Length Film thickness : $0.00 \,\mu\text{m}$: 0.034 min Void time Maximum Temperature: 240.0 °C Comment :



Figure S3: Exemplary chromatogram of a cobalt catalysed homologation reaction at 90 °C. RT 1.819 min = Dimethylether. RT 2.190 min = Acetaldehyde. RT 2.799 min = Acetaldehyde dimethylacetale. RT 3.026 min = Methylacetate.



Figure S4: Picture of the gas chromatograph (right) and the PolyArc Reactor (left).

XRD-Diffractograms



Figure S5: XRD-diffractograms of all tested heterogeneous catalysts on γ -Al₂O₃ in calcined and reduced state.



Figure S6: XRD-diffractograms of all tested heterogeneous catalysts on CeO_2 in calcined and reduced state.

Density functional theory

As a first step we compared DFT calculated and experimental enthalpies for the gas phase reactions and find good agreement:

CO + 2 CH₃OH — > CH₃COOCH₃ (Methylacetate) + H₂O — > Δ Hexp= -142.6 kJ/mol DFT = -140.736 kJ/mol

 $CO + CH_3OH + H_2 \longrightarrow CH_3CHO \text{ (acetaldehyde)} + H_2O \longrightarrow \Delta Hexp= -96.5 \text{ kJ/mol}$ DFT = -99.456 kJ/mol

As a second step. we calculated reaction enthalpy for the hydrogenation reaction of dicobalt octacarbonyl to two cobalt tetracarbonyl hydrides $HCo(CO)_4$ for different GGA+U values (0. 4. 5. 6) and find the *respective values of* 36.2. 26.1. 24.4 and 22.6 kJ/mol. Calculated reaction enthalpy for U= 4 compares well with the experimental values provided in NIST Chemistry WebBook (13.4 - 27.6 kJ/mol) as well as the value obtained in the work in [Angew. Chem. 2014. 126. 8816 –8820].

In the calculation of the Gibbs free energy reaction diagrams. H_2 . CO. CH_4 as well as all cobalt carbonyl species were treated as gas phase species while CH_3OH . H_2O . AA and MeOAc as liquid phase by using S values for the liquid phase and by correcting enthalpy value for the liquid-gas difference obtained from the NIST Chemistry WebBook. Total energies. zero point energy correction energies. cpdT and S values are provided in the Table S1 in the SI.

All of the Figures discussed in the DFT part of the main text can be found here. The Figure 4 of the main text was separated into three different Figures for better understanding. these separated Figures are shown in the supporting information Figures S10-S12.



Figure S7: Reaction energy diagram for the CH₃OH activation and CH₃Co(CO)₃ formation on $HCo(CO)_4$ at T= 423.15 K



Figure S8: Reaction energy diagram for the CH₃OH protonation and CH₃Co(CO)₃ formation on HCo(CO)₄ at T= 423.15 K. Blue arrow shows the reduction of the barrier by increasing the number of methanol molecules.



Figure S9: Reaction energy diagram for the disproportionation start reaction in $2xCo(CO)_4[Co(CH_3OH)_6]$.



Figure S10: Reaction energy diagram for AA formation on $HCo(CO)_4$ at T= 423.15 K. p(CO)=20 bar. $p(H_2) = 60$ bar.



Figure S11: Reaction energy diagram for MeOAc formation on $HCo(CO)_4$ at T= 423.15 K. p(CO)=20 bar. $p(H_2) = 60$ bar.



Figure S12: Reaction energy diagram for CH_4 formation on $HCo(CO)_4$ at T= 423.15 K. p(CO)=20 bar. $p(H_2) = 60$ bar.

Table S3: DFT calculated total energies (eV). zero point energy (eV). cpdT (eV) and S (eV/T) values.

| | Е | ZPE | cpdT | S |
|-----------------------|--------------|-------|-------|------------|
| CO(g) | -12.07474556 | 0.137 | 0.108 | 0.002117 |
| $H_2O(1)$ | -12.80978117 | 0.582 | 0.122 | 0.00072865 |
| | -0.2846 | | | |
| $H_2(g)$ | -7.16240358 | 0.279 | 0.125 | 0.001454 |
| CH ₃ OH(l) | -27.74244005 | 1.380 | 0.172 | 0.001325 |
| | -0.2648 | | | |

| AcH(1) | -35.40713962 | 1.483 | 0.172 | 0.00122188 |
|--|--------------|-------|-------|------------|
| MeOAc(1) | -56.28467272 | 2.382 | 0.277 | 0.00270208 |
| CH ₄ (g) | -23.275 | 1.205 | 0.183 | 0.0023567 |
| | | | | |
| HCo(CO) ₄ | -54.86862657 | 1.054 | 0.513 | 0.0051078 |
| HCo(CO) ₄ +CH ₃ OH | -82.73115255 | 2.450 | 0.755 | 0.0068202 |
| TS | -81.206 | 2.36 | 0.812 | 0.0071504 |
| Co(CO) ₄ -CH ₃ +H ₂ O | -83.0172 | 2.474 | 0.785 | 0.0067006 |
| Co(CO) ₄ -CH ₃ | -70.07488619 | 1.860 | 0.602 | 0.0055474 |
| TS | -69.6516 | 1.848 | | |
| Co(CO) ₃ -CH ₃ CO | -69.99392876 | 1.884 | 0.584 | 0.0054584 |
| H ₂ -Co(CO) ₃ - | -77.06857435 | 2.320 | 0.645 | 0.0057215 |
| CH ₃ CO | | | | |
| 2H-Co(CO) ₃ - | -76.6947 | 2.302 | 0.636 | 0.0057297 |
| CH ₃ CO | | | | |
| TS | -76.62 | 2.302 | 0.682 | 0.0059472 |
| HCo(CO) ₃ - | -77.13440433 | 2.323 | 0.660 | 0.0060621 |
| CH ₃ CHO | | | | |
| HCo(CO) ₃ | -41.28142491 | 0.712 | 0.469 | 0.0048734 |
| HCo(CO) ₃ -CH ₃ OH | -69.66847049 | 2.269 | 0.610 | 0.0056881 |
| TS | -67.93955367 | 2.24 | 0.596 | 0.0054381 |
| OH-HCo(CO) ₃ - | -68.586112 | 2.200 | 0.618 | 0.0055514 |
| CH ₃ | | | | |
| TS | -68.27952103 | 2.162 | 0.638 | 0.0057518 |
| $Co(CO)_3$ - CH_3 + H_2O | -70.0013 | 2.274 | 0.646 | 0.0058027 |
| Co(CO) ₃ -CH ₃ | -56.96434718 | 1.620 | 0.496 | 0.0049584 |
| $Co(CO)_3-CH_3+H_2$ | -64.23331176 | 2.049 | 0.557 | 0.0051874 |
| Co(CO) ₃ -CH ₃ +2H | -63.77965687 | 2.054 | 0.535 | 0.0051063 |
| TS | -63.66973241 | 1.97 | 0.567 | 0.0054314 |
| HCo(CO) ₃ -CH ₄ | -64.91091259 | 2.042 | 0.621 | 0.0060442 |
| | | | | |
| Co(CO) ₄ -CH ₃ CO | -82.86346751 | 2.098 | 0.711 | 0.0062634 |
| Co(CO) ₄ - | -110.8507837 | 3.50 | 0.932 | 0.007608 |
| CH ₃ CO+CH ₃ OH | | | | |
| TS | -109.98302 | 3.45 | 0.748 | 0.0069630 |
| HCo(CO) ₄ -MeOAc | -111.3323544 | 3.472 | 0.899 | 0.0074895 |