

Supporting Information

Thermal and Bisphenol-A Adsorption Properties of Zinc Ferrite/ β -Cyclodextrin Polymer Nanocomposite

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Table

Table S1. Details of chemicals used in the present study (purity ~98-99%)

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Fig. S6 Effect of (a) β -CD-E-T/ZnFe₂O₄ dose and (b) BPA amount in aqueous solution on the adsorption capacity and R% of β -CD-E-T/ZnFe₂O₄

Fig. S7 Plot of $\ln K_e$ against $1/T$ for the removal of BPA using β -CD-E-T/ZnFe₂O₄ adsorbent

Equations

Linear forms of Langmuir equation:

$$\frac{C_e}{q_e} = \frac{1}{q_m} C_e + \frac{1}{K_L q_m} \quad (\text{S1})$$

$$\frac{q_e}{C_e} = K_L q_m - K_L q_e \quad (\text{S2})$$

$$\frac{1}{q_e} = \frac{1}{q_m} + \frac{1}{K_L q_m} \times \frac{1}{C_e} \quad (\text{S3})$$

$$q_e = q_m - \frac{1}{K_L} \times \frac{q_e}{C_e} \quad (\text{S4})$$

The plot of C_e/q_e vs. C_e (Eq. S1), q_e/C_e vs. q_e (Eq. S2), $1/q_e$ vs. $1/C_e$ (Eq. 3), or q_e vs. q_e/C_e can be used to obtain Langmuir isotherms parameters using slope and the interception.

Tables

Table S1. Details of chemicals used in the present study (purity ~98-99%)

| Chemical | Molar mass (g mol⁻¹) | CAS | Supplier |
|-----------------------------------|--|------------|-----------------|
| Zinc (II) nitrate hexahydrate | 297.5 | 10196-18-6 | SRL |
| Iron (III) nitrate nonahydrate | 404.0 | 7782-61-8 | SRL |
| sodium hydroxide | 40.0 | 1310-73-2 | Samir Tech |
| Sodium acetate | 82.0 | 127-09-3 | SRL |
| β -Cyclodextrin | 1135.0 | 7585-39-9 | HiMedia |
| Epichlorohydrin | 92.5 | 106-89-8 | Merck |
| Tetrafluoroterephthalonitrile | 200.1 | 1835-49-0 | Merck |
| Ethylene diamine | 60.1 | 107-15-3 | SRL |
| Tetrahydrofuran | 72.1 | 109-99-9 | Samir Tech |
| Ethylene glycol | 62.1 | 107-21-1 | SRL |
| Bisphenol A | 228.3 | 80-05-7 | SRL |

Table S2. Temperature at different conversion percentage values for the decomposition of β -CD-E-T and β -CD-E-T/ZnFe₂O₄ ($\beta=5, 10, 15,$ and $20 \text{ }^\circ\text{C min}^{-1}$)

| Extent of conversion | β -CD-E-T | | | | β -CD-E-T/ZnFe ₂ O ₄ | | | |
|-------------------------|---|-----------------|-----------------|-----------------|--|-----------------|-----------------|-----------------|
| | Temperature (K) at different heating rates | | | | Temperature (K) at different heating rates | | | |
| α (%) | T_α (5) | T_α (10) | T_α (15) | T_α (20) | T_α (5) | T_α (10) | T_α (15) | T_α (20) |
| 10 | 567 | 580 | 587 | 594 | 561 | 572 | 577 | 580 |
| 12.5 | 573 | 585 | 592 | 599 | 566 | 577 | 582 | 585 |
| 15 | 577 | 589 | 596 | 602 | 570 | 581 | 586 | 590 |

| | | | | | | | | |
|------|-----|-----|-----|-----|-----|-----|-----|-----|
| 17.5 | 581 | 592 | 599 | 606 | 573 | 585 | 589 | 593 |
| 20 | 584 | 595 | 602 | 608 | 576 | 588 | 592 | 597 |
| 22.5 | 586 | 598 | 605 | 611 | 579 | 591 | 595 | 599 |
| 25 | 589 | 600 | 607 | 613 | 581 | 593 | 598 | 602 |
| 27.5 | 591 | 602 | 609 | 615 | 584 | 596 | 600 | 604 |
| 30 | 593 | 604 | 611 | 617 | 586 | 598 | 602 | 607 |
| 32.5 | 594 | 606 | 612 | 618 | 588 | 600 | 604 | 609 |
| 35 | 596 | 608 | 614 | 620 | 590 | 602 | 606 | 611 |
| 37.5 | 597 | 609 | 616 | 622 | 592 | 603 | 608 | 612 |
| 40 | 599 | 611 | 617 | 623 | 593 | 605 | 610 | 614 |
| 42.5 | 600 | 612 | 619 | 625 | 595 | 607 | 612 | 616 |
| 45 | 602 | 614 | 620 | 626 | 597 | 609 | 613 | 618 |
| 47.5 | 603 | 615 | 622 | 627 | 598 | 610 | 615 | 619 |
| 50 | 604 | 617 | 623 | 629 | 600 | 612 | 616 | 621 |
| 52.5 | 605 | 618 | 624 | 630 | 602 | 613 | 618 | 622 |
| 55 | 607 | 620 | 626 | 631 | 603 | 615 | 620 | 624 |
| 57.5 | 608 | 621 | 627 | 632 | 605 | 617 | 621 | 626 |
| 60 | 609 | 622 | 628 | 634 | 607 | 618 | 623 | 627 |
| 62.5 | 611 | 624 | 630 | 635 | 609 | 620 | 625 | 629 |
| 65 | 612 | 625 | 631 | 636 | 610 | 622 | 626 | 630 |
| 67.5 | 614 | 627 | 633 | 638 | 612 | 623 | 628 | 632 |
| 70 | 616 | 629 | 634 | 639 | 614 | 625 | 630 | 634 |
| 72.5 | 618 | 631 | 636 | 641 | 616 | 627 | 632 | 636 |
| 75 | 620 | 632 | 638 | 642 | 619 | 629 | 634 | 638 |
| 77.5 | 622 | 635 | 639 | 644 | 622 | 632 | 636 | 640 |
| 80 | 625 | 637 | 642 | 646 | 625 | 635 | 639 | 642 |
| 82.5 | 628 | 640 | 644 | 648 | 629 | 638 | 642 | 645 |
| 85 | 631 | 643 | 647 | 651 | 633 | 642 | 645 | 648 |
| 87.5 | 636 | 647 | 651 | 654 | 639 | 647 | 649 | 652 |
| 90 | 641 | 653 | 656 | 658 | 647 | 653 | 655 | 657 |

Figures

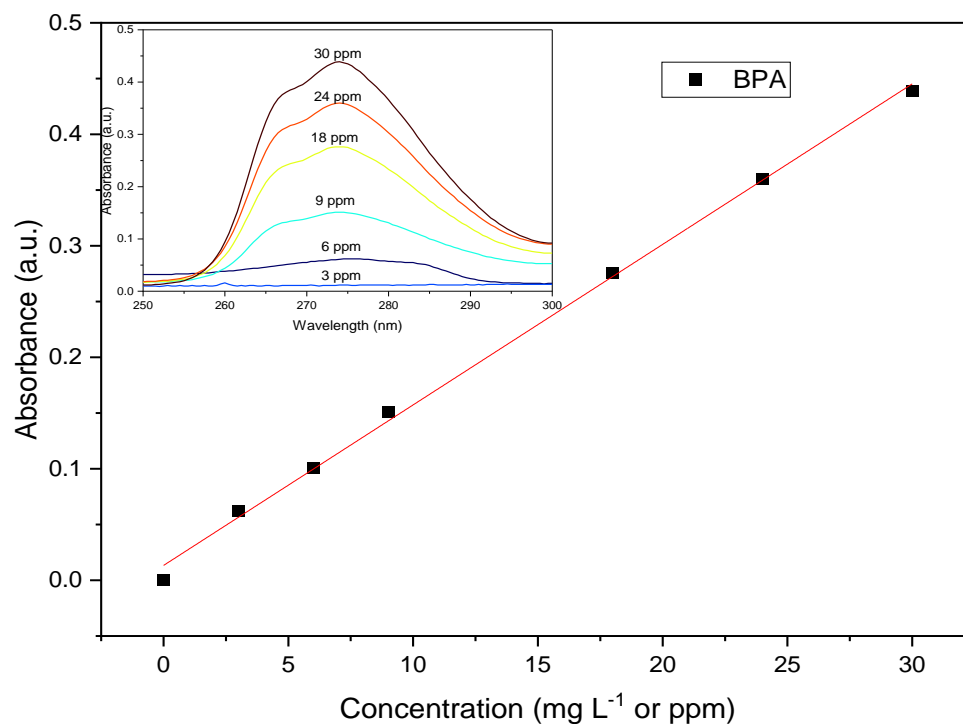


Fig. S1 Calibration curve of BPA

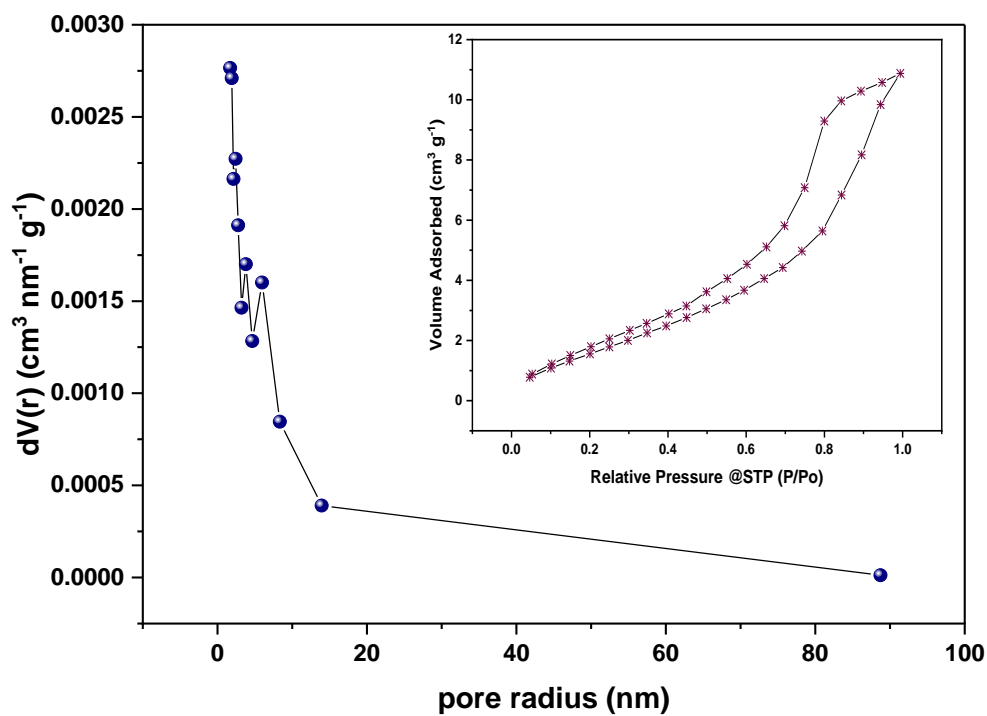


Fig. S2 BJH analysis for the pore size distribution and N₂ adsorption-desorption curve (Inset) of β -CD-E-T/ZnFe₂O₄

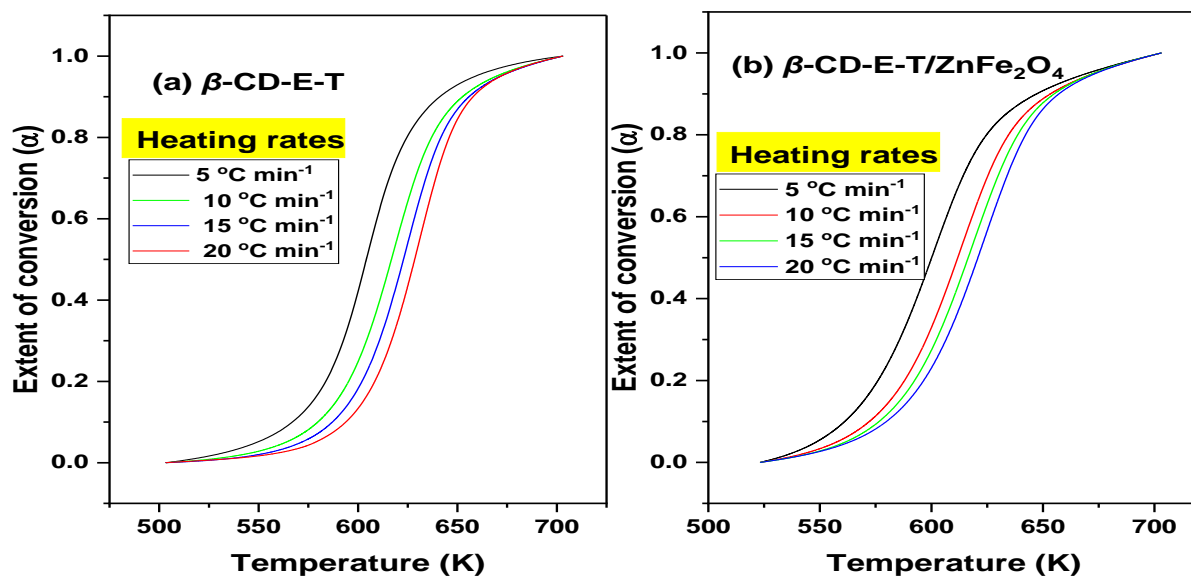


Fig. S3 Conversion plots ($\alpha \rightarrow T$) of (a) β -CD-E-T and β -CD-E-T/ ZnFe_2O_4 at 5, 10, 15, and 20 $^\circ\text{C min}^{-1}$

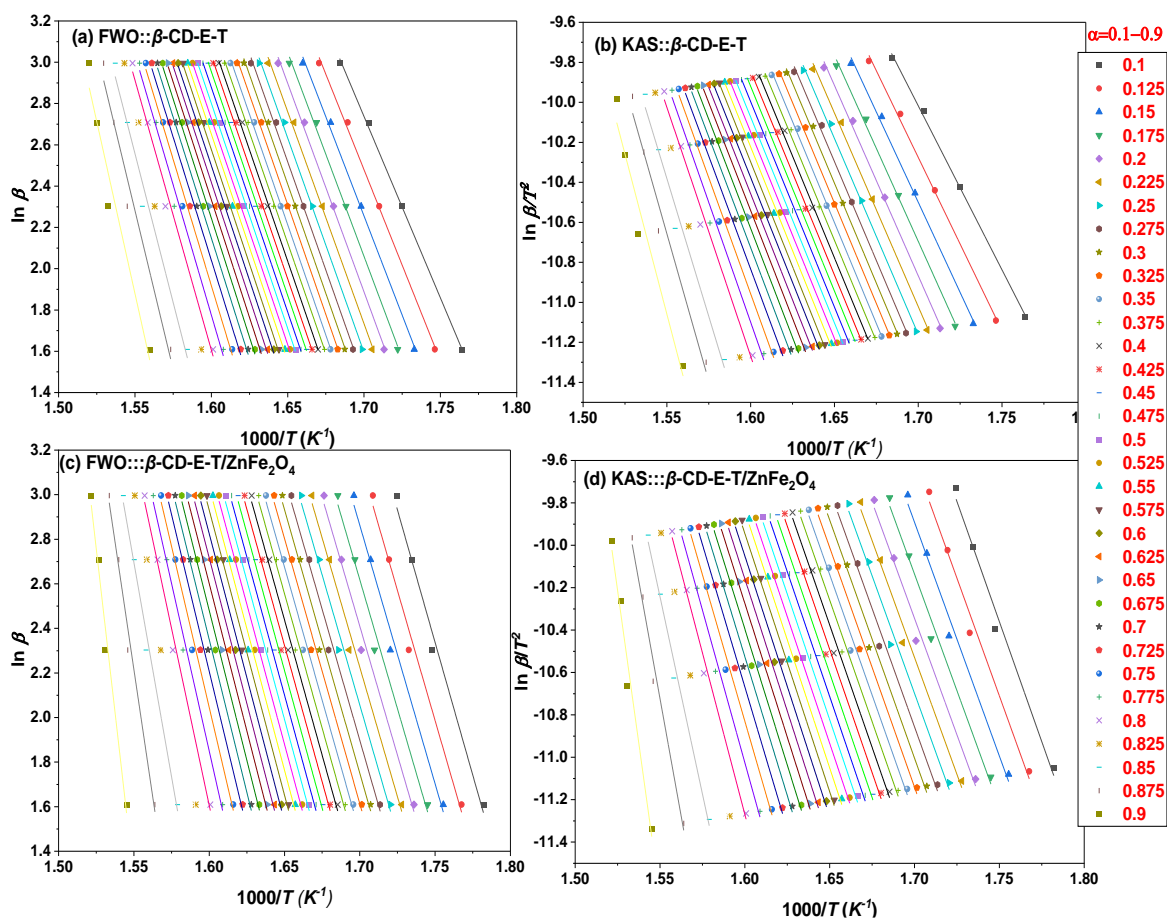


Fig. S4 Kinetics plots of β -CD-E-T (a) FWO, (b) KAS, and β -CD-E-T/ ZnFe_2O_4 (c) FWO, and (d) KAS

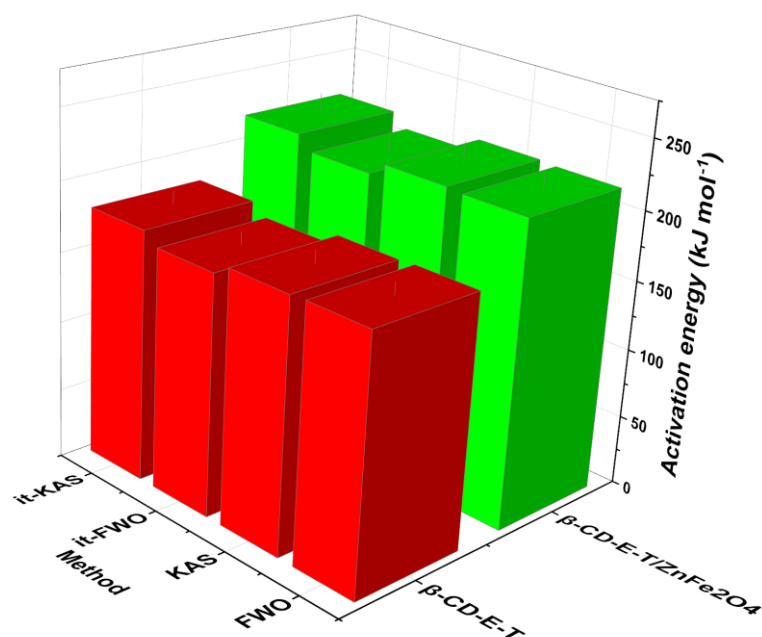


Fig. S5 Average activation energy of β -CD-E-T and β -CD-E-T/ZnFe₂O₄ obtained using FWO, KAS, it-FWO, and it-KAS method.

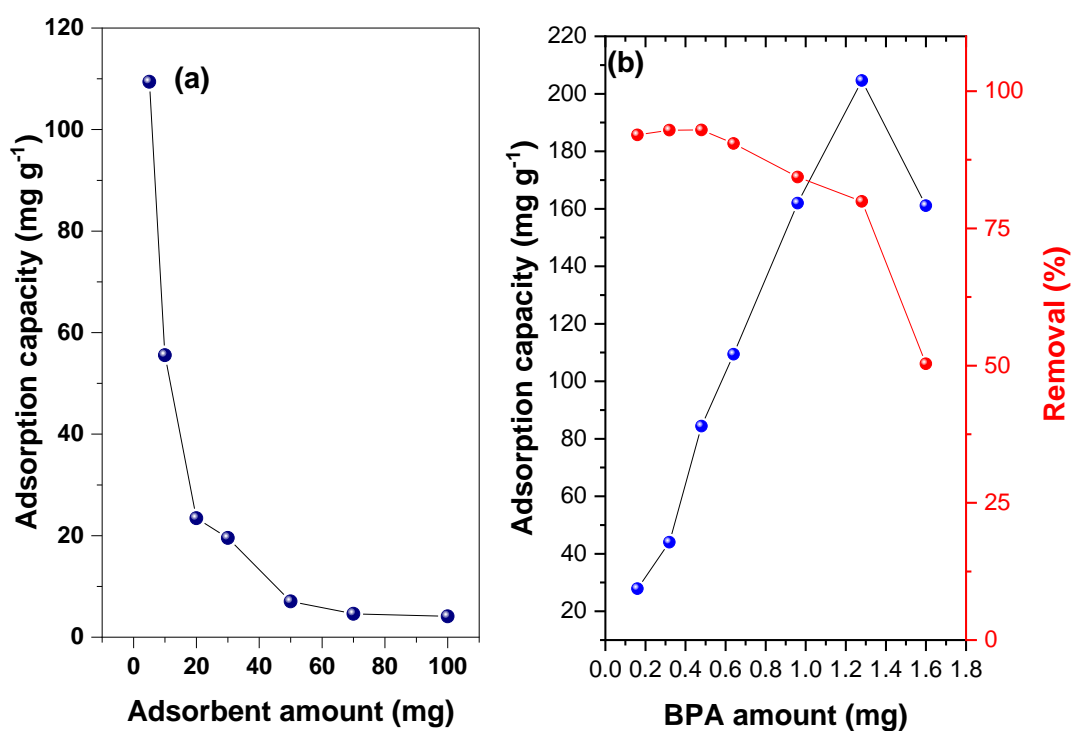


Fig. S6 Effect of (a) β -CD-E-T/ZnFe₂O₄ dose and (b) BPA amount in aqueous solution on the adsorption capacity and R% of β -CD-E-T/ZnFe₂O₄

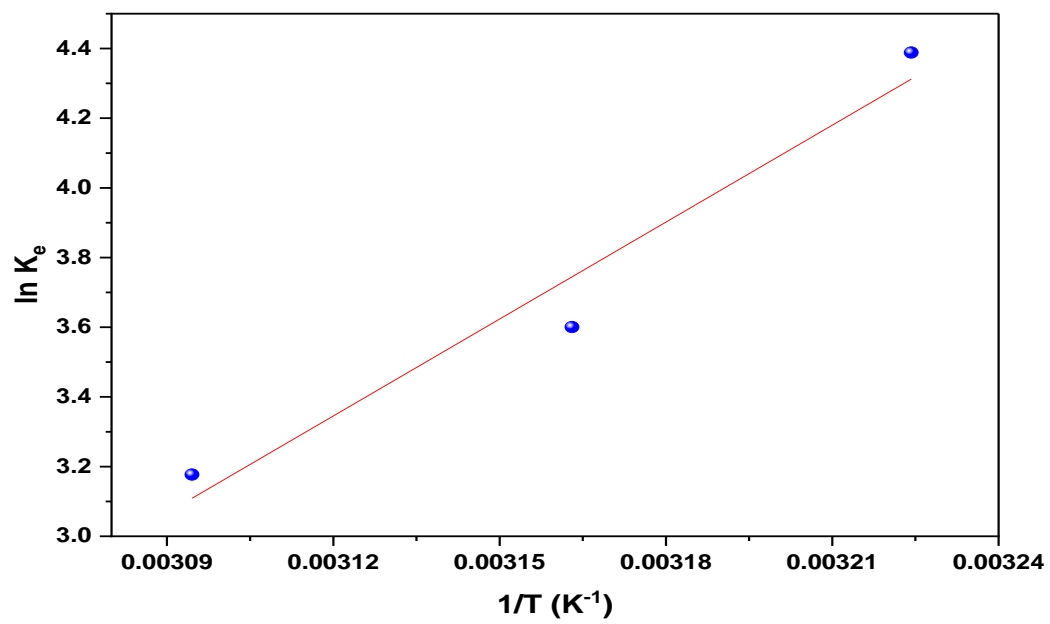


Fig. S7 Plot of $\ln K_e$ against $1/T$ for the removal of BPA using β -CD-E-T/ $ZnFe_2O_4$ adsorbent