

Supporting Information: Energetic optimization of thermochemical air separation for the production of sustainable nitrogen

1 Thermodynamic properties

Thermodynamic properties of the materials investigated are summarized in table 1. The values of $\text{Ca}_{1-x}\text{Sr}_x\text{MnO}_{3-\delta}$ are extracted from¹ with a linear approximation. The original data was collected via the van't Hoff approach of thermogravimetric measurements.

Table 1 Thermodynamic properties of the materials investigated.

Material	$\Delta h_{\delta}^{\circ}$ [kJmol ⁻¹]	$\Delta s_{\delta}^{\circ}$ [Jmol ⁻¹ K ⁻¹]	a [-]	extracted from
SrFeO _{3-δ}	74	47	1.07	2
Sr _{0.8} Ca _{0.2} FeO _{3-δ}	57.5	-	-	3
CaMnO _{3-δ}	180	108	1	1
Ca _{0.9} Sr _{0.1} MnO _{3-δ}	168	100	1	1
Ca _{0.8} Sr _{0.2} MnO _{3-δ}	157	92	1	1
Ca _{0.7} Sr _{0.3} MnO _{3-δ}	146	84	1	1
Ca _{0.6} Sr _{0.4} MnO _{3-δ}	135	76	1	1

2 Calculation of pressure drop Δp

The pressure drop Δp during oxidation and reduction at 1 bar is calculated based on the Ergun equation⁴. The necessary input values are listed in the following:

length of the packed bed ΔL : 500 mm

fluid velocity in the empty pipe v : 0.422 $\frac{\text{m}}{\text{s}}$

porosity of the filling ψ : 0.4

Sauter particle diameter d : 1.5 mm

The temperature and pressure dependent dynamic viscosity and fluid density are summarized in table 2 and 3. These values are calculated based on the material properties of air extracted from⁵.

Table 2 Dynamic viscosity η in $\frac{\text{kg}}{\text{ms}}$ calculated for the applied temperatures and pressures during oxidation and reduction.

		Temperature [K]					
		623	873	973	1023	1173	1223
pressure [bar]	1	316.5	398.0	427.9	442.4	484.6	498.4
	2	316.8		427.7	442.1		
	3	316.8		427.7	442.1		
	4	316.8		427.7	442.1		
	5	317.1		427.6	441.9		

Table 3 Fluid density of air in $\frac{\text{kg}}{\text{m}^3}$ calculated for the applied temperatures and pressures during oxidation and reduction.

		Temperature [K]					
		623	873	973	1023	1173	1223
pressure [bar]	1	0.56	0.398	0.358	0.341	0.3	0.288
	2	1.092		0.728	0.702		
	3	1.626		1.097	1.060		
	4	2.161		1.465	1.418		
	5	2.691		1.873	1.782		

The resulting pressure drop Δp is listed in the following table.

Table 4 Pressure drop Δp in bar. Calculated for the applied temperatures and pressures during oxidation and reduction.

		Temperature [K]					
		623	873	973	1023	1173	1223
pressure [bar]	1	0.0143	0.0248	0.0295	0.0319	0.0395	0.0423
	2	0.0073		0.0145	0.0155		
	3	0.0049		0.0096	0.0103		
	4	0.0037		0.0072	0.0077		
	5	0.0030		0.0057	0.0060		

3 Material composition of SrFeO_{3- δ} granules

The material composition of the SrFeO_{3- δ} granules was studied with powder X-ray diffraction (XRD) using a *D8-Advance (A25)* instrument from *Bruker* with a cobalt

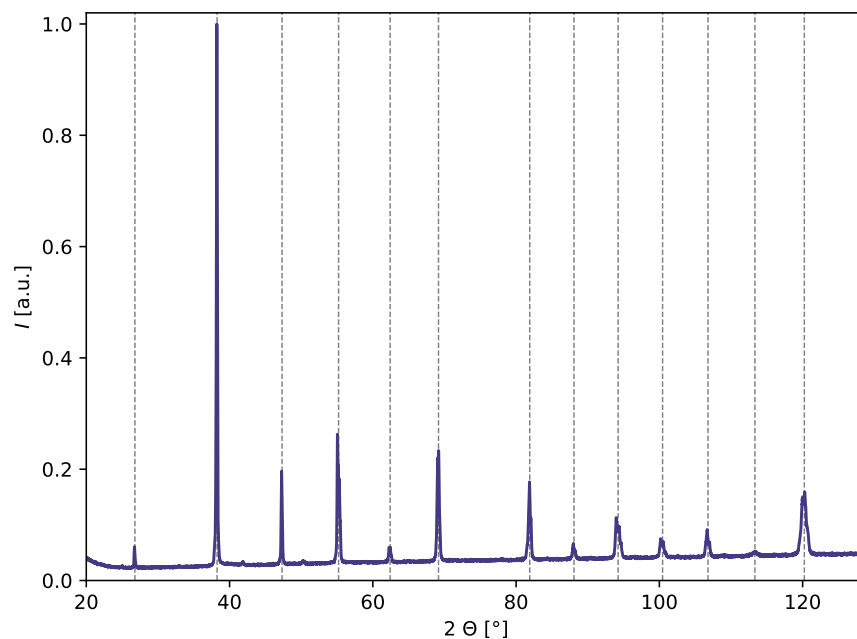


Figure 1 XRD-pattern of the $\text{SrFeO}_{3-\delta}$ granules. This pattern was measured with a cobalt anode. The vertical lines indicate the main peaks of the structure with which this pattern was identified. They refer to PDF 01-081-9514 of the database *PDF 2 - Release 2019 RDB* of the *International Center for Diffraction Data (ICCD)*.

anode and a *Lynxe-EyeXET-Detector* (fig.1).

The figure 1 shows that the granules prepared are $\text{SrFeO}_{3-\delta}$ granules without major side phases. The vertical lines indicate the peak positions of the PDF 01-081-9514 of the database *PDF 2 - Release 2019 RDB* of the *International Center for Diffraction Data (ICCD)*.

4 Additional graphs for parametric study

The figures 2 and 3 display both graphs of fig. 6d in the main manuscript separately.

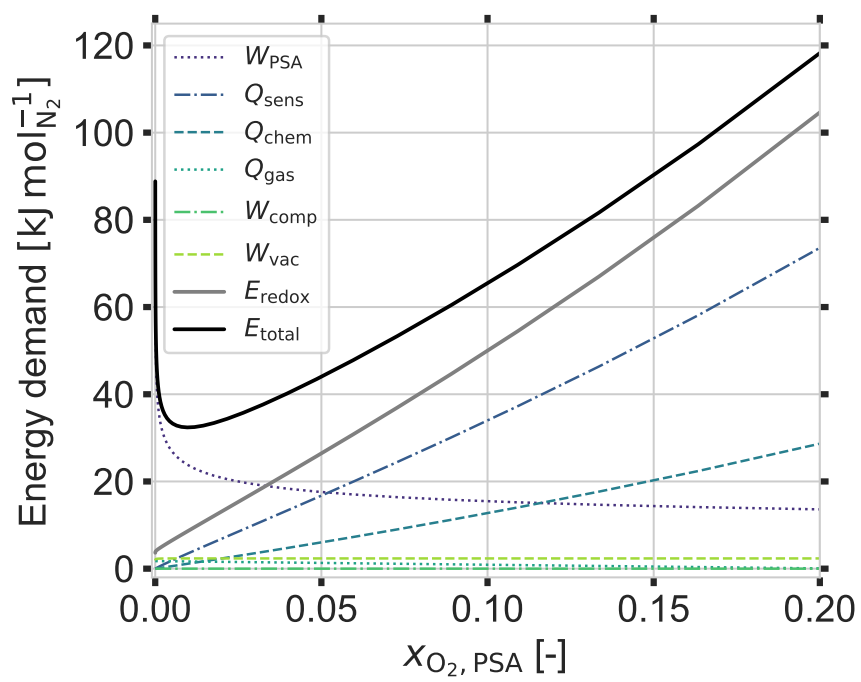


Figure 2 Variation of the PSA output oxygen x_{O_2} mole fraction and thus of the oxygen partial pressure during oxidation for $Sr_{0.8}Ca_{0.2}FeO_{3-\delta}$.

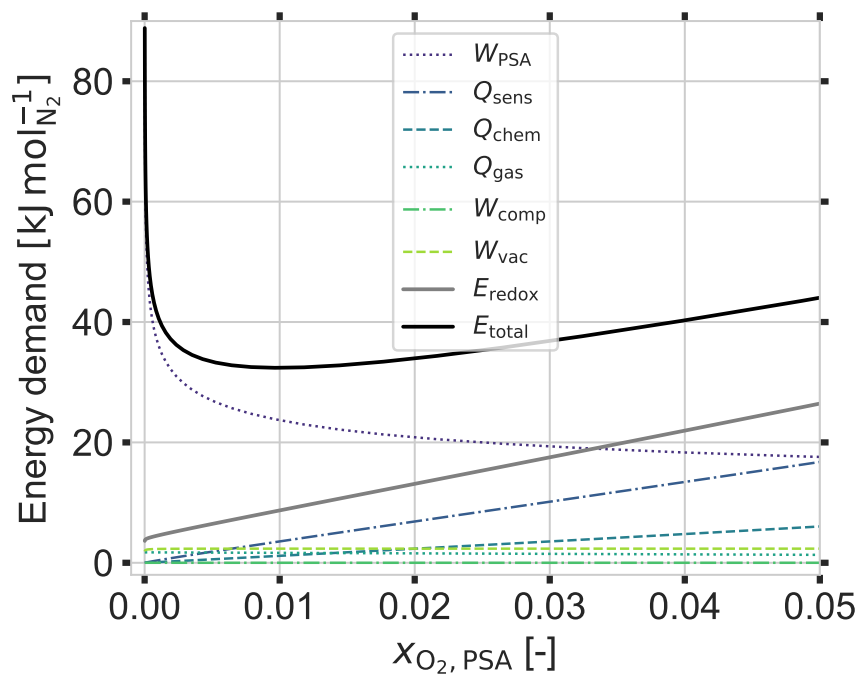


Figure 3 Extract from fig. 2.

References

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