## Electronic Supplementary Information (ESI)

## Machine-Learning Assisted Optimisation During Heterogeneous Photocatalytic Degradation Utilising a Static Mixer under Continuous Flow

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1. Additional figures and data


Figure S1 - Replicate experiments processing 0.7-1.0 L of Reactive Orange 16 dye through the continuous photoreactor with catalyst regeneration carried out at the end of each experiment. Conditions: residence time $=3.22 \mathrm{~min}$, temperature $=$ $20^{\circ} \mathrm{C}$ and reactor pressure $=10 \mathrm{bar}$.


Figure S2 - Variation in the catalyst activity decay slope observed at different flow rates of Reactive Orange 16. A reciprocal function fitted over the observed flow rate range is shown. Conditions: temperature $=20^{\circ} \mathrm{C}$ and reactor pressure $=10$ bar.

Table S1 - Summary of experimental data from the experiments carried out during ML training (light blue. \# 1-6) and optimisation (\# 7-17) of the continuous flow photocatalytic degradation of the azo-dye Reactive Orange 16. Dye $C_{1}$ is the initial Reactive Orange dye concentration, $Q_{s}$ indicates the set flow rate, $Q_{M}$ indicates the measured flow rate, $\tau$ indicates the residence time, $T_{S}$ indicates the set temperature, $T_{M}$ indicates the measured temperature, catalyst regen indicates if the catalyst was regenerated prior to the experiment or not, X indicates conversion and dye over catalyst is the amount of dye that had passed over the catalyst prior to the start of the reaction (UV lights on, steady state conditions).

| $\#$ | Dye $C_{1}$ <br> $(\mathrm{mg} / \mathrm{L})$ | $\mathrm{Q}_{\mathrm{s}}$ <br> $(\mathrm{ml} / \mathrm{min})$ | $\mathrm{Q}_{\mathrm{M}}$ <br> $(\mathrm{ml} / \mathrm{min})$ | $\tau$ <br> $(\mathrm{min})$ | $\mathrm{T}_{\mathrm{S}}$ <br> $\left({ }^{\circ} \mathrm{C}\right)$ | $\mathrm{T}_{\mathrm{M}}$ <br> $\left({ }^{\circ} \mathrm{C}\right)$ | Catalyst <br> $($ Regen. $)$ | X <br> $(\%)$ | X <br> $(\% / \mathrm{min})$ | Dye over <br> catalyst $(\mathrm{mg})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 84 | 3.00 | 3.13 | 1.99 | 20 | 19.9 | Yes | 77 | 38.6 | 13.2 |
| 2 | 75 | 0.98 | 1.00 | 6.24 | 24.4 | 23.0 | Yes | 96 | 15.4 | 12.2 |
| 3 | 75 | 10.00 | 7.10 | 0.88 | 20.0 | 20.5 | Yes | 50 | 56.9 | 0.0 |
| 4 | 75 | 3.00 | 3.09 | 2.02 | 20.0 | 19.1 | Yes | 80 | 39.6 | 9.0 |
| 5 | 75 | 1.00 | 1.02 | 6.12 | 20.0 | 19.8 | No | 97 | 15.9 | 23.0 |
| 6 | 75 | 3.00 | 3.13 | 1.99 | 80.0 | 68.9 | No | 93 | 46.6 | 30.8 |
| 7 | 74 | 7.50 | 6.94 | 0.90 | 20.0 | 19.0 | Yes | 57 | 63.4 | 10.4 |
| 8 | 74 | 7.30 | 7.27 | 0.86 | 38.6 | 35.5 | No | 50 | 58.3 | 32.9 |
| 9 | 74 | 8.99 | 8.92 | 0.70 | 20.0 | 19.4 | No | 29 | 41.5 | 71.7 |
| 10 | 85 | 9.01 | 7.92 | 0.79 | 79.9 | 67.5 | Yes | 73 | 92.7 | 12.8 |
| 11 | 85 | 9.96 | 8.60 | 0.73 | 78.1 | 66.3 | No | 63 | 86.8 | 24.4 |
| 12 | 85 | 8.05 | 7.43 | 0.84 | 79.5 | 67.5 | No | 60 | 71.4 | 38.2 |
| 13 | 85 | 9.96 | 9.64 | 0.65 | 57.6 | 49.4 | No | 39 | 60.3 | 62.0 |
| 14 | 81 | 9.99 | 8.99 | 0.69 | 80.0 | 67.4 | No | 62 | 89.3 | 92.6 |
| 15 | 81 | 7.47 | 7.59 | 0.82 | 79.9 | 67.3 | Yes | 84 | 102.2 | 15.7 |
| 16 | 81 | 7.26 | 7.34 | 0.85 | 71.2 | 60.8 | No | 74 | 87.0 | 28.2 |
| 17 | 81 | 9.98 | 10.00 | 0.62 | 58.3 | 50.5 | No | 52 | 83.3 | 39.8 |

