

# Supplementary Materials for Predicting the Physical Properties of Three-Component Lignocellulose Derived Advanced Biofuel Blends Using a Design of Experiments Approach

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## S1 Predictions of Other Properties

### S1.1 Calculated Property Values

Table S1.1.1. Lower Heating Value (LHV) and Oxygen Content of Different Blend Components.

| Fuel Component              | LHV (MJ/kg) <sup>a</sup> | Oxygen Content (%) |
|-----------------------------|--------------------------|--------------------|
| EN 590 Limits <sup>1</sup>  | None specified           | None specified     |
| BS 2869 Limits <sup>2</sup> | None specified           | None specified     |
| Diesel                      | 42.7                     | 3.0                |
| EL                          | 24.8                     | 33.3               |
| nBL                         | 27.4                     | 27.9               |
| DEE                         | 33.9                     | 21.6               |
| DNBE                        | 38.3                     | 12.3               |
| EtOH                        | 26.8                     | 34.7               |
| nBuOH                       | 33.1                     | 21.6               |

<sup>a</sup>from<sup>3-7</sup>

Table S1.1.2. Predicted Lower Heating Values using Linear-by-Mass Blending Law and Oxygen Content Predicted using a Linear Blending Law.

| Fuel Blend Composition (vol%) | Calculated LHV (MJ/kg) | Oxygen Content (%) |
|-------------------------------|------------------------|--------------------|
| D0Et100 – 80:5:15             | 25.5                   | 33.1               |
| D0Et100 – 50:40:10            | 27.7                   | 28.6               |
| D75Et25 – 50:45:5             | 38.9                   | 9.2                |
| D0Bu100 – 80:5:15             | 28.6                   | 25.9               |
| D0Bu100 – 50:40:10            | 31.8                   | 21.4               |
| D75Bu25 – 50:45:5             | 39.9                   | 7.4                |

## S1.2 Diesel Thermogravimetric Analysis

The diesel was analysed using a Mettler Toledo TGA/DSC 3+, using an alumina crucible with a pierced lid to build up vapour pressure, under a nitrogen atmosphere. The heating rate used was 10 °C/min.

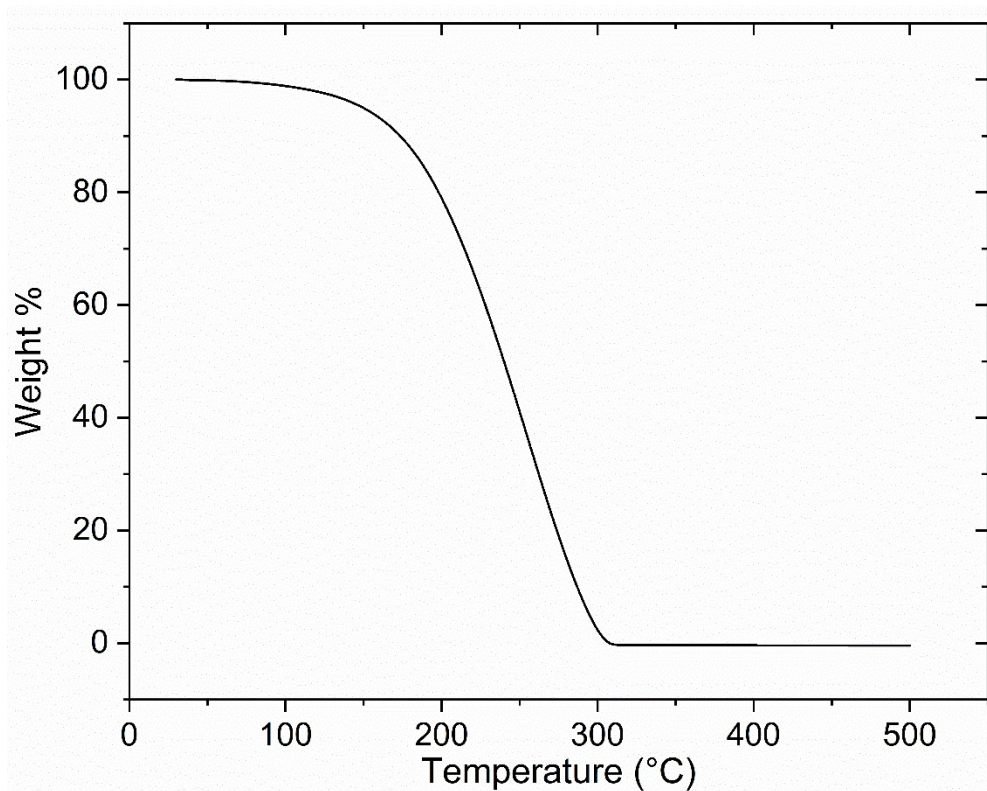


Figure S1. Diesel TGA curve.

Table S1.2.1 Temperatures for given mass fractions remaining from the TGA analysis of the ULSD.

| Mass Remaining (%) | Temperature (°C) |
|--------------------|------------------|
| 99.5               | 78               |
| 95                 | 150              |
| 90                 | 173              |
| 85                 | 188              |
| 80                 | 198              |
| 75                 | 207              |
| 70                 | 215              |
| 65                 | 222              |
| 60                 | 228              |
| 55                 | 234              |
| 50                 | 240              |
| 45                 | 246              |
| 40                 | 251              |
| 35                 | 257              |
| 30                 | 262              |
| 25                 | 268              |
| 20                 | 274              |
| 15                 | 280              |
| 10                 | 287              |
| 5                  | 295              |
| 0.5                | 305              |

The tables below show the different model coefficients determined by MODDE for the linear, quadratic, and cubic models for predicting the density at 15 °C of the different blends tested.

## S2 Density Model Coefficients

### S2.1 Ethyl-Based Blends

Table S2.1.1. Linear Model Coefficients for Density Predictions of Ethyl-Based Blends

|                 | Coefficient | Standard Error | P-Value                | 95% Confidence interval ( $\pm$ ) |
|-----------------|-------------|----------------|------------------------|-----------------------------------|
| <b>Constant</b> | 0.924       | 0.002          | 0.00                   | 0.005                             |
| <b>EtOH</b>     | -0.133      | 0.004          | $1.45 \times 10^{-25}$ | 0.008                             |
| <b>EL</b>       | 0.093       | 0.003          | $1.26 \times 10^{-25}$ | 0.005                             |
| <b>DEE</b>      | -0.189      | 0.004          | $4.93 \times 10^{-30}$ | 0.008                             |

The R<sup>2</sup> value of the model was 0.996.

Table S2.1.2. Quadratic Model Coefficients for Density Predictions of Ethyl-Based Blends

|                         | Coefficient | Standard Error | P-Value                | 95% Confidence interval ( $\pm$ ) |
|-------------------------|-------------|----------------|------------------------|-----------------------------------|
| <b>Constant</b>         | 0.921       | 0.004          | 0.00                   | 0.009                             |
| <b>EtOH</b>             | -0.127      | 0.009          | $1.88 \times 10^{-13}$ | 0.019                             |
| <b>EL</b>               | 0.086       | 0.005          | $8.68 \times 10^{-15}$ | 0.011                             |
| <b>DEE</b>              | -0.172      | 0.010          | $1.09 \times 10^{-15}$ | 0.021                             |
| <b>EtOH<sup>2</sup></b> | 0.052       | 0.035          | $1.44 \times 10^{-1}$  | 0.072                             |
| <b>EL<sup>2</sup></b>   | 0.024       | 0.008          | $4.86 \times 10^{-3}$  | 0.016                             |
| <b>DEE<sup>2</sup></b>  | 0.061       | 0.034          | $7.95 \times 10^{-2}$  | 0.069                             |
| <b>EtOH×EL</b>          | -0.081      | 0.031          | $1.64 \times 10^{-2}$  | 0.065                             |
| <b>EtOH×DEE</b>         | 0.174       | 0.068          | $1.67 \times 10^{-2}$  | 0.139                             |
| <b>EL×DEE</b>           | -0.086      | 0.028          | $4.91 \times 10^{-3}$  | 0.057                             |

The R<sup>2</sup> value of the model was 0.990, which is lower than the R<sup>2</sup> of the linear model. In addition the EtOH<sup>2</sup> term is insignificant as it has a p-value above the 0.05 threshold. Removal of this would remove all the EtOH interaction terms due to the model hierarchy and would result in the linear model being reproduced after all of the resultant insignificant terms were removed.

### S2.2 Butyl-Based Blends Density Models

Table S2.2.1. Linear Model Coefficients for Density Predictions of Butyl-Based Blends

|                 | Coefficient | Standard Error | P-Value                | 95% Confidence interval ( $\pm$ ) |
|-----------------|-------------|----------------|------------------------|-----------------------------------|
| <b>Constant</b> | 0.908       | 0.004          | 0.00                   | 0.008                             |
| <b>nBuOH</b>    | -0.112      | 0.007          | $2.30 \times 10^{-16}$ | 0.013                             |
| <b>nBL</b>      | 0.070       | 0.005          | $3.54 \times 10^{-15}$ | 0.009                             |
| <b>DNBE</b>     | -0.128      | 0.006          | $4.04 \times 10^{-18}$ | 0.013                             |

The R<sup>2</sup> value of the model was 0.977 and all terms are statistically significant.

Table S2.2.2 Quadratic Model Coefficients for Density Predictions of Butyl-Based Blends

|                          | Coefficient | Standard Error | P-Value                | 95% Confidence interval (±) |
|--------------------------|-------------|----------------|------------------------|-----------------------------|
| <b>Constant</b>          | 0.906       | 0.003          | 0.00                   | 0.006                       |
| <b>nBuOH</b>             | -0.098      | 0.006          | 1.35×10 <sup>-14</sup> | 0.013                       |
| <b>nBL</b>               | 0.067       | 0.004          | 4.81×10 <sup>-16</sup> | 0.007                       |
| <b>DNBE</b>              | -0.133      | 0.007          | 6.41×10 <sup>-17</sup> | 0.014                       |
| <b>nBuOH<sup>2</sup></b> | 0.043       | 0.023          | 7.48×10 <sup>-2</sup>  | 0.048                       |
| <b>nBL<sup>2</sup></b>   | 0.013       | 0.005          | 1.58×10 <sup>-2</sup>  | 0.011                       |
| <b>DNBE<sup>2</sup></b>  | 0.053       | 0.023          | 2.74×10 <sup>-2</sup>  | 0.047                       |
| <b>nBuOH×nBL</b>         | -0.043      | 0.021          | 4.76×10 <sup>-2</sup>  | 0.043                       |
| <b>nBuOH×DNBE</b>        | 0.063       | 0.045          | 1.71×10 <sup>-1</sup>  | 0.092                       |
| <b>nBL×DNBE</b>          | -0.049      | 0.019          | 1.44×10 <sup>-2</sup>  | 0.038                       |

The R<sup>2</sup> value of the model was 0.992, although this is higher than the linear model there were insignificant terms. Upon removal of the insignificant terms, starting with the nBuOH×DNBE term this resulted in the other quadratic terms becoming insignificant, resulting in the linear model.

### S2.3 Pentyl Based Blends Density Models

Table S2.3.1 Linear Model Coefficients for Density Predictions of Pentyl-Based Blends

|                 | Coefficient | Standard Error | P-Value                | 95% Confidence interval (±) |
|-----------------|-------------|----------------|------------------------|-----------------------------|
| <b>Constant</b> | 0.906       | 0.001          | 0.00                   | 0.002                       |
| <b>nPeOH</b>    | -0.090      | 0.001          | 5.63×10 <sup>-33</sup> | 0.003                       |
| <b>nPL</b>      | 0.060       | 0.001          | 3.39×10 <sup>-32</sup> | 0.002                       |
| <b>DNPE</b>     | -0.117      | 0.001          | 1.30×10 <sup>-36</sup> | 0.003                       |

The R<sup>2</sup> value of the model was 0.998 and all terms are significant.

Table S2.3.2 Quadratic Model Coefficients for Density Predictions of Pentyl-Based Blends

|                          | Coefficient | Standard Error | P-Value                | 95% Confidence interval (±) |
|--------------------------|-------------|----------------|------------------------|-----------------------------|
| <b>Constant</b>          | 0.905       | 0.001          | 0.00                   | 0.003                       |
| <b>nPeOH</b>             | -0.088      | 0.003          | 1.13×10 <sup>-21</sup> | 0.006                       |
| <b>nPL</b>               | 0.058       | 0.002          | 7.41×10 <sup>-23</sup> | 0.004                       |
| <b>DNPE</b>              | -0.114      | 0.003          | 5.52×10 <sup>-24</sup> | 0.007                       |
| <b>nPeOH<sup>2</sup></b> | 0.030       | 0.012          | 1.56×10 <sup>-2</sup>  | 0.024                       |
| <b>nPL<sup>2</sup></b>   | 0.008       | 0.003          | 4.69×10 <sup>-3</sup>  | 0.005                       |
| <b>DNPE<sup>2</sup></b>  | 0.030       | 0.011          | 1.37×10 <sup>-2</sup>  | 0.024                       |
| <b>nPeOH×nPL</b>         | -0.027      | 0.010          | 1.30×10 <sup>-2</sup>  | 0.021                       |
| <b>nPeOH×DNPE</b>        | 0.033       | 0.021          | 1.36×10 <sup>-1</sup>  | 0.044                       |
| <b>nPL×DNPE</b>          | -0.027      | 0.009          | 6.91×10 <sup>-3</sup>  | 0.019                       |

The R<sup>2</sup> value of the model was 0.997.

The nPeOH×DNPE term was insignificant with a p-value >0.05. Upon removal of this term, it generated other insignificant terms, ultimately resulting in the linear model.

## S3 Flash Point Coefficients

### S3.1 Butyl-Based Blends Flash Model Coefficients

Table S3.1.1. Linear Model Coefficients for Flash Point Predictions of Butyl-Based Blends

|                 | Coefficient | Standard Error | P-Value               | 95% Confidence interval (±) |
|-----------------|-------------|----------------|-----------------------|-----------------------------|
| <b>Constant</b> | 37.342      | 3.556          | $4.19 \times 10^{-9}$ | 7.471                       |
| <b>nBuOH</b>    | -22.885     | 6.386          | $2.12 \times 10^{-3}$ | 13.417                      |
| <b>nBL</b>      | 18.726      | 4.133          | $2.59 \times 10^{-4}$ | 8.683                       |
| <b>DNBE</b>     | -41.805     | 6.265          | $2.93 \times 10^{-6}$ | 13.163                      |

The R<sup>2</sup> value of the model was 0.813, indicating it may not be that accurate at predicting the flash points of the blends.

Table S3.1.2. Quadratic Model Coefficients for Flash Point Predictions of Butyl-Based Blends

|                          | Coefficient | Standard Error | P-Value                | 95% Confidence interval (±) |
|--------------------------|-------------|----------------|------------------------|-----------------------------|
| <b>Constant</b>          | 34.930      | 2.268          | $1.38 \times 10^{-14}$ | 4.66128                     |
| <b>nBuOH</b>             | -7.989      | 4.856          | $1.12 \times 10^{-1}$  | 9.98254                     |
| <b>nBL</b>               | 8.066       | 2.903          | $1.00 \times 10^{-2}$  | 5.96782                     |
| <b>DNBE</b>              | -19.876     | 5.292          | $8.80 \times 10^{-4}$  | 10.8769                     |
| <b>nBuOH<sup>2</sup></b> | 82.012      | 18.411         | $1.42 \times 10^{-4}$  | 37.8448                     |
| <b>nBL<sup>2</sup></b>   | 26.872      | 4.135          | $6.90 \times 10^{-7}$  | 8.50037                     |
| <b>DNBE<sup>2</sup></b>  | 54.242      | 17.801         | $5.25 \times 10^{-3}$  | 36.5907                     |
| <b>nBuOH×nBL</b>         | -100.870    | 16.602         | $2.03 \times 10^{-6}$  | 34.1255                     |
| <b>nBuOH×DNBE</b>        | 184.435     | 35.841         | $2.29 \times 10^{-5}$  | 73.6715                     |
| <b>nBL×DNBE</b>          | -84.792     | 14.750         | $4.72 \times 10^{-6}$  | 30.3179                     |

The R<sup>2</sup> value of the model was R<sup>2</sup> 0.924. The insignificance of the nBuOH term was discussed in section Flash Points section.

### S3.2 Pentyl-Based Blends Flash Point Model Coefficients

Table S3.2.1 Linear Model Coefficients for Flash Point Predictions of Pentyl-Based Blends

|                 | Coefficient | Standard Error | P-Value               | 95% Confidence interval (±) |
|-----------------|-------------|----------------|-----------------------|-----------------------------|
| <b>Constant</b> | 61.775      | 2.614          | 0.00                  | 5.338                       |
| <b>nPeOH</b>    | -41.346     | 4.057          | 0.00                  | 8.285                       |
| <b>nPL</b>      | 16.683      | 2.872          | 0.00                  | 5.865                       |
| <b>DNPE</b>     | -16.286     | 3.989          | $3.00 \times 10^{-4}$ | 8.147                       |

The R<sup>2</sup> value of the model was 0.870, indicating it may not be that accurate at predicting the flash points of the blends.

Table S3.2.2 Quadratic Model Coefficients for Flash Point Predictions of Pentyl-Based Blends

|                          | Coefficient | Standard Error | P-Value                | 95% Confidence interval (±) |
|--------------------------|-------------|----------------|------------------------|-----------------------------|
| <b>Constant</b>          | 58.956      | 1.099          | 5.69×10 <sup>-29</sup> | 2.255                       |
| <b>nPeOH</b>             | -42.840     | 2.332          | 8.67×10 <sup>-17</sup> | 4.785                       |
| <b>nPL</b>               | 14.790      | 1.394          | 3.93×10 <sup>-11</sup> | 2.860                       |
| <b>DNPE</b>              | -8.254      | 2.460          | 2.36×10 <sup>-3</sup>  | 5.047                       |
| <b>nPeOH<sup>2</sup></b> | 103.317     | 8.888          | 5.12×10 <sup>-12</sup> | 18.237                      |
| <b>nPL<sup>2</sup></b>   | 15.329      | 1.920          | 1.40×10 <sup>-8</sup>  | 3.939                       |
| <b>DNPE<sup>2</sup></b>  | 31.103      | 8.663          | 1.29×10 <sup>-3</sup>  | 17.774                      |
| <b>nPeOH×nPL</b>         | -73.858     | 7.694          | 3.38×10 <sup>-10</sup> | 15.786                      |
| <b>nPeOH×DNPE</b>        | 48.514      | 16.176         | 5.76×10 <sup>-3</sup>  | 33.190                      |
| <b>nPL×DNPE</b>          | -32.051     | 6.981          | 9.14×10 <sup>-5</sup>  | 14.325                      |

The R<sup>2</sup> value of the model was 0.982.

## S4 KV40 Model Coefficients

### S4.1 Butyl-Based Blends KV40 Model Coefficients

Table S4.1.1. Linear Model Coefficients for KV40 Predictions of Butyl-Based Blends

|                 | Coefficient | Standard Error | P-Value                | 95% Confidence interval (±) |
|-----------------|-------------|----------------|------------------------|-----------------------------|
| <b>Constant</b> | 1.509       | 0.030          | 5.13×10 <sup>-29</sup> | 0.061                       |
| <b>nBuOH</b>    | -0.172      | 0.048          | 1.17×10 <sup>-3</sup>  | 0.097                       |
| <b>nBL</b>      | 0.378       | 0.033          | 4.19×10 <sup>-12</sup> | 0.067                       |
| <b>DNBE</b>     | -1.133      | 0.047          | 2.32×10 <sup>-20</sup> | 0.096                       |

The R<sup>2</sup> value of the model was 0.973.

Table S4.1.2. Quadratic Model Coefficients for KV40 Predictions of Butyl-Based Blends

|                          | Coefficient | Standard Error | P-Value                | 95% Confidence interval (±) |
|--------------------------|-------------|----------------|------------------------|-----------------------------|
| <b>Constant</b>          | 1.469       | 0.033          | 2.75×10 <sup>-25</sup> | 0.068                       |
| <b>nBuOH</b>             | -0.163      | 0.072          | 3.37×10 <sup>-2</sup>  | 0.149                       |
| <b>nBL</b>               | 0.317       | 0.043          | 8.39×10 <sup>-8</sup>  | 0.088                       |
| <b>DNBE</b>              | -0.932      | 0.077          | 6.62×10 <sup>-12</sup> | 0.159                       |
| <b>nBuOH<sup>2</sup></b> | 1.596       | 0.273          | 4.25×10 <sup>-6</sup>  | 0.562                       |
| <b>nBL<sup>2</sup></b>   | 0.264       | 0.060          | 1.94×10 <sup>-4</sup>  | 0.124                       |
| <b>DNBE<sup>2</sup></b>  | 0.309       | 0.265          | 2.54×10 <sup>-1</sup>  | 0.545                       |
| <b>nBuOH×nBL</b>         | -1.284      | 0.244          | 1.88×10 <sup>-5</sup>  | 0.502                       |
| <b>nBuOH×DNBE</b>        | 1.242       | 0.524          | 2.58×10 <sup>-2</sup>  | 1.079                       |
| <b>nBL×DNBE</b>          | -0.538      | 0.218          | 2.05×10 <sup>-2</sup>  | 0.448                       |

The R<sup>2</sup> value of the model was 0.975. The removal of the insignificant terms reduced the model to an inaccurate model.

## S4.2 Pentyl-Based Blends KV40 Model Coefficients

Table S4.2.1 Linear Model Coefficients for KV40 Predictions of Pentyl-Based Blends

|                 | Coefficient | Standard Error | P-Value                | 95% Confidence interval (±) |
|-----------------|-------------|----------------|------------------------|-----------------------------|
| <b>Constant</b> | 1.866       | 0.031          | 1.15×10 <sup>-32</sup> | 0.064                       |
| <b>nPeOH</b>    | -0.155      | 0.049          | 3.44×10 <sup>-3</sup>  | 0.100                       |
| <b>nPL</b>      | 0.358       | 0.035          | 2.02×10 <sup>-11</sup> | 0.071                       |
| <b>DNPE</b>     | -1.080      | 0.048          | 2.39×10 <sup>-20</sup> | 0.098                       |

The R<sup>2</sup> value of the model was 0.967.

Table S4.2.2. Quadratic Model Coefficients for KV40 Predictions of Pentyl-Based Blends

|                          | Coefficient | Standard Error | P-Value                | 95% Confidence interval (±) |
|--------------------------|-------------|----------------|------------------------|-----------------------------|
| <b>Constant</b>          | 1.831       | 0.008          | 0.00                   | 0.017                       |
| <b>nPeOH</b>             | -0.196      | 0.018          | 1.63×10 <sup>-11</sup> | 0.036                       |
| <b>nPL</b>               | 0.339       | 0.011          | 5.01×10 <sup>-23</sup> | 0.022                       |
| <b>DNPE</b>              | -0.977      | 0.019          | 1.13×10 <sup>-28</sup> | 0.038                       |
| <b>nPeOH<sup>2</sup></b> | 1.363       | 0.068          | 8.03×10 <sup>-18</sup> | 0.139                       |
| <b>nPL<sup>2</sup></b>   | 0.178       | 0.015          | 1.67×10 <sup>-12</sup> | 0.030                       |
| <b>DNPE<sup>2</sup></b>  | 0.288       | 0.066          | 1.59×10 <sup>-4</sup>  | 0.135                       |
| <b>nPeOH×nPL</b>         | -0.926      | 0.058          | 3.38×10 <sup>-15</sup> | 0.120                       |
| <b>nPeOH×DNPE</b>        | 0.473       | 0.123          | 6.53×10 <sup>-4</sup>  | 0.252                       |
| <b>nPL×DNPE</b>          | -0.304      | 0.053          | 4.29×10 <sup>-6</sup>  | 0.109                       |

The R<sup>2</sup> value of the model was 0.998. All terms were statistically significant.

## S5 Experimental Data

All the errors reported for the measured density, flash points, and KV40 are the standard deviations of three repeated measurements. The errors reported for the predicted values are the model's 95% confidence intervals.

### S5.1 Ethyl-Based Three-Component Blends

Table S5.1.1. Measured and Predicted Density of the Ethyl-Based Blends.

| Data Use                                  | EL (vol%) | DEE (vol%) | EtOH (vol%)   | Measured Density (g/cm <sup>3</sup> ) | Predicted Density (g/cm <sup>3</sup> ) |
|---|-----------|------------|---------------|---------------------------------------|--|
| MODDE<br>Generated<br>blends              | 0.5       | 0.05       | 0.45          | 0.899 ± 0.002                         | 0.901 ± 0.002                          |
|   | 0.7       | 0.05       | 0.25          | 0.945 ± 0.001                         | 0.946 ± 0.001                          |
|   | 0.75      | 0.1        | 0.15          | 0.954 ± 0.001                         | 0.955 ± 0.001                          |
|   | 0.55      | 0.1        | 0.35          | 0.910 ± 0.002                         | 0.909 ± 0.002                          |
|   | 0.6       | 0.2        | 0.2           | 0.915 ± 0.001                         | 0.915 ± 0.001                          |
|   | 0.6       | 0.2        | 0.2           | 0.918 ± 0.001                         | 0.915 ± 0.001                          |
|   | 0.5       | 0.25       | 0.25          | 0.891 ± 0.001                         | 0.890 ± 0.001                          |
|   | 0.6       | 0.2        | 0.2           | 0.916 ± 0.001                         | 0.915 ± 0.001                          |
|   | 0.55      | 0.3        | 0.15          | 0.899 ± 0.002                         | 0.898 ± 0.001                          |
|   | 0.5       | 0.45       | 0.05          | 0.879 ± 0.003                         | 0.878 ± 0.002                          |
|   | 0.9       | 0.05       | 0.05          | 0.989 ± 0.001                         | 0.991 ± 0.002                          |
|   | 0.7       | 0.25       | 0.05          | 0.936 ± 0.001                         | 0.935 ± 0.001                          |
|   | 0.5       | 0.05       | 0.45          | 0.901 ± 0.001                         | 0.901 ± 0.002                          |
|   | 0.5       | 0.45       | 0.05          | 0.876 ± 0.001                         | 0.878 ± 0.002                          |
|   | 0.9       | 0.05       | 0.05          | 0.987 ± 0.001                         | 0.991 ± 0.002                          |
|   | 0.633     | 0.317      | 0.05          | 0.916 ± 0.001                         | 0.916 ± 0.001                          |
|   | 0.767     | 0.183      | 0.05          | 0.949 ± 0.001                         | 0.954 ± 0.001                          |
|   | 0.5       | 0.317      | 0.183         | 0.887 ± 0.002                         | 0.886 ± 0.001                          |
|   | 0.767     | 0.05       | 0.183         | 0.959 ± 0.001                         | 0.961 ± 0.001                          |
|   | 0.633     | 0.183      | 0.183         | 0.919 ± 0.001                         | 0.924 ± 0.001                          |
| 0.633                                     | 0.183     | 0.183      | 0.925 ± 0.001 | 0.924 ± 0.001                         |  |
| Blends added for<br>increased<br>coverage | 0.8       | 0.15       | 0.05          | 0.963 ± 0.001                         | 0.963 ± 0.001                          |
|   | 0.5       | 0.4        | 0.1           | 0.880 ± 0.001                         | 0.881 ± 0.002                          |
|   | 0.5       | 0.1        | 0.4           | 0.897 ± 0.002                         | 0.898 ± 0.002                          |
|   | 0.75      | 0.2        | 0.05          | 0.948 ± 0.001                         | 0.949 ± 0.001                          |
|   | 0.55      | 0.35       | 0.1           | 0.895 ± 0.002                         | 0.895 ± 0.001                          |
|   | 0.6       | 0.15       | 0.25          | 0.918 ± 0.001                         | 0.918 ± 0.001                          |
|   | 0.8       | 0.15       | 0.05          | 0.966 ± 0.001                         | 0.963 ± 0.001                          |
|   | 0.8       | 0.1        | 0.1           | 0.970 ± 0.001                         | 0.966 ± 0.001                          |
|   | 0.8       | 0.05       | 0.15          | 0.973 ± 0.001                         | 0.969 ± 0.001                          |
|   | 0.85      | 0.1        | 0.05          | 0.981 ± 0.001                         | 0.977 ± 0.001                          |
|   | 0.85      | 0.05       | 0.1           | 0.983 ± 0.001                         | 0.980 ± 0.002                          |
| Model<br>Validation                       | 0.55      | 0.2        | 0.25          | 0.908 ± 0.001                         | 0.904 ± 0.001                          |
|   | 0.6       | 0.25       | 0.15          | 0.918 ± 0.001                         | 0.912 ± 0.001                          |
|   | 0.65      | 0.25       | 0.1           | 0.930 ± 0.001                         | 0.924 ± 0.001                          |
|   | 0.65      | 0.1        | 0.25          | 0.937 ± 0.001                         | 0.932 ± 0.001                          |
|   | 0.7       | 0.2        | 0.1           | 0.943 ± 0.002                         | 0.938 ± 0.001                          |
|   | 0.7       | 0.15       | 0.15          | 0.945 ± 0.001                         | 0.941 ± 0.001                          |



## S5.2 Butyl-Based Three-Component Blends

Table S5.2.2. Measured and Predicted Properties of the Butyl-Based Blends.

|  | nBL<br>(vol%) | DNBE<br>(vol%) | nBuOH<br>(vol%) | Measured Density<br>(g/cm <sup>3</sup> ) | Predicted Density<br>(g/cm <sup>3</sup> ) | Measured Flash<br>Point (°C) | Predicted Flash<br>Point (°C) | Measured KV40<br>(mm <sup>2</sup> /s) | Predicted KV40<br>(mm <sup>2</sup> /s) |
|--|---------------|----------------|-----------------|--|---|------------------------------|-------------------------------|---------------------------------------|--|
| MODDE<br>Generated<br>blends                 | 0.7           | 0.05           | 0.25            | 0.926 ± 0.001                            | 0.922 ± 0.002                             | 41.3 ± 0.6                   | 37.78 ± 2.34                  | 1.636 ± 0.001                         | 1.605 ± 0.034                          |
|  | 0.5           | 0.25           | 0.25            | 0.882 ± 0.001                            | 0.882 ± 0.002                             | 30.5 ± 1.3                   | 35.39 ± 2.33                  | 1.395 ± 0.001                         | 1.389 ± 0.034                          |
|  | 0.5           | 0.45           | 0.05            | 0.875 ± 0.001                            | 0.879 ± 0.004                             | 26.3 ± 1.5                   | 30.16 ± 2.59                  | 1.186 ± 0.001                         | 1.207 ± 0.038                          |
|  | 0.6           | 0.2            | 0.2             | 0.902 ± 0.001                            | 0.901 ± 0.002                             | 33.0 ± 1.0                   | 34.32 ± 1.31                  | 1.467 ± 0.001                         | 1.442 ± 0.019                          |
|  | 0.55          | 0.3            | 0.15            | 0.890 ± 0.001                            | 0.890 ± 0.002                             | 31.0 ± 1.4                   | 32.93 ± 1.36                  | 1.326 ± 0.001                         | 1.344 ± 0.020                          |
|  | 0.75          | 0.1            | 0.15            | 0.928 ± 0.001                            | 0.930 ± 0.002                             | 42.7 ± 0.6                   | 40.32 ± 1.35                  | 1.608 ± 0.001                         | 1.610 ± 0.020                          |
|  | 0.7           | 0.25           | 0.05            | 0.918 ± 0.001                            | 0.919 ± 0.002                             | 37.3 ± 1.0                   | 35.87 ± 1.98                  | 1.455 ± 0.001                         | 1.479 ± 0.029                          |
|  | 0.9           | 0.05           | 0.05            | 0.956 ± 0.001                            | 0.958 ± 0.003                             | 57.0 ± 0.0                   | 54.93 ± 2.37                  | 1.804 ± 0.001                         | 1.839 ± 0.035                          |
|  | 0.55          | 0.1            | 0.35            | 0.895 ± 0.001                            | 0.894 ± 0.003                             | 33.7 ± 0.6                   | 35.74 ± 1.45                  | 1.553 ± 0.001                         | 1.538 ± 0.021                          |
|  | 0.5           | 0.05           | 0.45            | 0.889 ± 0.001                            | 0.885 ± 0.004                             | 38.3 ± 0.6                   | 37.43 ± 2.62                  | 1.611 ± 0.001                         | 1.623 ± 0.038                          |
|  | 0.6           | 0.2            | 0.2             | 0.897 ± 0.001                            | 0.901 ± 0.002                             | 36.0 ± 0.0                   | 34.32 ± 1.31                  | 1.439 ± 0.001                         | 1.442 ± 0.019                          |
|  | 0.6           | 0.2            | 0.2             | 0.902 ± 0.001                            | 0.901 ± 0.002                             | 35.5 ± 0.6                   | 34.32 ± 1.31                  | 1.472 ± 0.001                         | 1.442 ± 0.019                          |
|  | 0.5           | 0.45           | 0.05            | 0.874 ± 0.001                            | 0.879 ± 0.004                             | 32.0 ± 0.0                   | 30.16 ± 2.59                  | 1.214 ± 0.001                         | 1.207 ± 0.038                          |
|  | 0.9           | 0.05           | 0.05            | 0.957 ± 0.001                            | 0.958 ± 0.003                             | 53.7 ± 0.6                   | 54.93 ± 2.37                  | 1.846 ± 0.001                         | 1.839 ± 0.035                          |
|  | 0.5           | 0.05           | 0.45            | 0.891 ± 0.001                            | 0.885 ± 0.004                             | 37.0 ± 0.0                   | 37.43 ± 2.62                  | 1.585 ± 0.001                         | 1.623 ± 0.038                          |
|  | 0.633         | 0.317          | 0.05            | 0.901 ± 0.001                            | 0.905 ± 0.002                             | 34.7 ± 0.6                   | 32.47 ± 1.94                  | 1.406 ± 0.001                         | 1.378 ± 0.028                          |
|  | 0.767         | 0.183          | 0.05            | 0.928 ± 0.001                            | 0.932 ± 0.002                             | 41.0 ± 0.0                   | 40.77 ± 1.75                  | 1.624 ± 0.001                         | 1.589 ± 0.025                          |
|  | 0.5           | 0.317          | 0.183           | 0.879 ± 0.001                            | 0.881 ± 0.002                             | 33.0 ± 0.0                   | 33.99 ± 2.09                  | 1.287 ± 0.001                         | 1.322 ± 0.030                          |
| 0.767  | 0.05          | 0.183          | 0.936 ± 0.001   | 0.934 ± 0.002                            | 43.7 ± 0.6                                | 41.65 ± 2.03                 | 1.693 ± 0.001                 | 1.656 ± 0.029                         |  |
| 0.633  | 0.183         | 0.183          | 0.907 ± 0.001   | 0.908 ± 0.002                            | 35.0 ± 0.0                                | 34.85 ± 1.28                 | 1.471 ± 0.001                 | 1.469 ± 0.019                         |  |
| 0.633  | 0.183         | 0.183          | 0.908 ± 0.001   | 0.908 ± 0.002                            | 34.8 ± 0.8                                | 34.85 ± 1.28                 | 1.555 ± 0.001                 | 1.469 ± 0.019                         |  |
| Blends<br>added for<br>increased<br>coverage | 0.8           | 0.1            | 0.1             | 0.939 ± 0.001                            | 0.939 ± 0.002                             | 44.0 ± 1.4                   | 44.09 ± 1.16                  | 1.671 ± 0.001                         | 1.668 ± 0.017                          |
|  | 0.8           | 0.05           | 0.15            | 0.941 ± 0.001                            | 0.940 ± 0.002                             | 45.0 ± 0.0                   | 44.25 ± 1.80                  | 1.697 ± 0.001                         | 1.691 ± 0.026                          |
|  | 0.85          | 0.1            | 0.05            | 0.951 ± 0.001                            | 0.948 ± 0.003                             | 46.0 ± 1.0                   | 48.91 ± 1.66                  | 1.711 ± 0.001                         | 1.741 ± 0.024                          |
|  | 0.85          | 0.05           | 0.1             | 0.952 ± 0.001                            | 0.949 ± 0.003                             | 48.5 ± 0.7                   | 49.07 ± 1.69                  | 1.750 ± 0.001                         | 1.757 ± 0.025                          |
|  | 0.8           | 0.15           | 0.05            | 0.938 ± 0.001                            | 0.938 ± 0.002                             | 42.5 ± 0.8                   | 43.73 ± 1.61                  | 1.641 ± 0.001                         | 1.648 ± 0.023                          |
|  | 0.5           | 0.4            | 0.1             | 0.878 ± 0.001                            | 0.880 ± 0.003                             | 31.7 ± 0.6                   | 31.77 ± 1.85                  | 1.220 ± 0.001                         | 1.248 ± 0.027                          |
|  | 0.5           | 0.1            | 0.4             | 0.891 ± 0.001                            | 0.885 ± 0.003                             | 37.0 ± 0.0                   | 37.22 ± 1.98                  | 1.520 ± 0.001                         | 1.560 ± 0.029                          |
| 0.75   | 0.2           | 0.05           | 0.927 ± 0.001   | 0.928 ± 0.002                            | 38.7 ± 0.6                                | 39.38 ± 1.83                 | 1.558 ± 0.001                 | 1.560 ± 0.027                         |  |

|                  |      |      |      |               |               |            |              |               |               |
|------------------|------|------|------|---------------|---------------|------------|--------------|---------------|---------------|
|                  | 0.55 | 0.35 | 0.1  | 0.889 ± 0.001 | 0.890 ± 0.003 | 33.0 ± 0.0 | 31.73 ± 1.32 | 1.286 ± 0.001 | 1.304 ± 0.019 |
|                  | 0.6  | 0.15 | 0.25 | 0.905 ± 0.001 | 0.902 ± 0.002 | 36.0 ± 0.0 | 34.91 ± 1.32 | 1.490 ± 0.001 | 1.486 ± 0.019 |
| Model Validation | 0.55 | 0.2  | 0.25 | 0.895 ± 0.001 | 0.892 ± 0.002 | 34.0 ± 0.0 | 34.73 ± 1.58 | 1.416 ± 0.001 | 1.435 ± 0.023 |
|                  | 0.6  | 0.25 | 0.15 | 0.902 ± 0.001 | 0.900 ± 0.002 | 34.0 ± 0.0 | 33.53 ± 1.25 | 1.422 ± 0.001 | 1.402 ± 0.018 |
|                  | 0.65 | 0.25 | 0.1  | 0.911 ± 0.001 | 0.909 ± 0.002 | 35.7 ± 0.6 | 34.17 ± 1.43 | 1.422 ± 0.001 | 1.433 ± 0.021 |
|                  | 0.65 | 0.1  | 0.25 | 0.915 ± 0.001 | 0.912 ± 0.002 | 38.7 ± 0.6 | 35.93 ± 1.64 | 1.554 ± 0.001 | 1.543 ± 0.024 |
|                  | 0.7  | 0.2  | 0.1  | 0.920 ± 0.001 | 0.919 ± 0.002 | 36.3 ± 0.6 | 36.64 ± 1.41 | 1.498 ± 0.001 | 1.505 ± 0.020 |
|                  | 0.7  | 0.15 | 0.15 | 0.923 ± 0.001 | 0.920 ± 0.002 | 36.7 ± 0.6 | 37.22 ± 1.27 | 1.543 ± 0.001 | 1.535 ± 0.018 |

### S5.3 Pentyl-Based Three-Component Blends

Table S5.3.1. Measured and Predicted Properties of the Pentyl-Based Blends.

|                        | nPL (vol%) | DNPE (vol%) | nPeOH (vol%)  | Measured Density (g/cm <sup>3</sup> ) | Predicted Density (g/cm <sup>3</sup> ) | Measured Flash Point (°C) | Predicted Flash Point (°C) | Measured KV40 (mm <sup>2</sup> /s) | Predicted KV40 (mm <sup>2</sup> /s) |
|------------------------|------------|-------------|---------------|---------------------------------------|--|---------------------------|----------------------------|------------------------------------|-------------------------------------|
| MODDE Generated blends | 0.7        | 0.05        | 0.25          | 0.920 ± 0.001                         | 0.919 ± 0.001                          | 59.7 ± 0.6                | 58.79 ± 1.03               | 1.977 ± 0.001                      | 1.977 ± 0.008                       |
|                        | 0.5        | 0.25        | 0.25          | 0.884 ± 0.001                         | 0.884 ± 0.001                          | 55.7 ± 0.6                | 55.61 ± 1.10               | 1.732 ± 0.001                      | 1.731 ± 0.008                       |
|                        | 0.5        | 0.45        | 0.05          | 0.879 ± 0.001                         | 0.879 ± 0.001                          | 63.7 ± 0.6                | 62.92 ± 1.21               | 1.577 ± 0.001                      | 1.577 ± 0.009                       |
|                        | 0.6        | 0.2         | 0.2           | 0.900 ± 0.001                         | 0.900 ± 0.001                          | 58.0 ± 0.0                | 57.74 ± 0.63               | 1.815 ± 0.001                      | 1.801 ± 0.005                       |
|                        | 0.55       | 0.3         | 0.15          | 0.890 ± 0.001                         | 0.890 ± 0.001                          | 58.7 ± 0.6                | 58.75 ± 0.65               | 1.712 ± 0.001                      | 1.700 ± 0.005                       |
|                        | 0.75       | 0.1         | 0.15          | 0.924 ± 0.001                         | 0.925 ± 0.001                          | 63.0 ± 0.0                | 64.07 ± 0.62               | 1.981 ± 0.001                      | 1.972 ± 0.005                       |
|                        | 0.7        | 0.25        | 0.05          | 0.914 ± 0.001                         | 0.914 ± 0.001                          | 66.3 ± 0.6                | 67.23 ± 0.89               | 1.844 ± 0.001                      | 1.843 ± 0.007                       |
|                        | 0.9        | 0.05        | 0.05          | 0.950 ± 0.001                         | 0.949 ± 0.001                          | 76.7 ± 0.6                | 77.82 ± 1.12               | 2.180 ± 0.001                      | 2.172 ± 0.009                       |
|                        | 0.55       | 0.1         | 0.35          | 0.895 ± 0.001                         | 0.896 ± 0.001                          | 55.3 ± 0.6                | 54.59 ± 0.66               | 1.902 ± 0.001                      | 1.897 ± 0.005                       |
|                        | 0.5        | 0.05        | 0.45          | 0.890 ± 0.001                         | 0.889 ± 0.001                          | 54.3 ± 0.6                | 55.16 ± 1.22               | 1.975 ± 0.001                      | 1.980 ± 0.009                       |
|                        | 0.6        | 0.2         | 0.2           | 0.900 ± 0.001                         | 0.900 ± 0.001                          | 58.7 ± 0.6                | 57.74 ± 0.63               | 1.799 ± 0.001                      | 1.801 ± 0.005                       |
|                        | 0.6        | 0.2         | 0.2           | 0.896 ± 0.001                         | 0.900 ± 0.001                          | 58.7 ± 0.6                | 57.74 ± 0.63               | 1.777 ± 0.001                      | 1.801 ± 0.005                       |
|                        | 0.5        | 0.45        | 0.05          | 0.878 ± 0.001                         | 0.879 ± 0.001                          | 63.0 ± 0.0                | 62.92 ± 1.21               | 1.578 ± 0.001                      | 1.577 ± 0.009                       |
|                        | 0.9        | 0.05        | 0.05          | 0.949 ± 0.001                         | 0.949 ± 0.001                          | 80.7 ± 0.6                | 77.82 ± 1.12               | 2.171 ± 0.001                      | 2.172 ± 0.009                       |
|                        | 0.5        | 0.05        | 0.45          | 0.889 ± 0.001                         | 0.889 ± 0.001                          | 54.7 ± 0.6                | 55.16 ± 1.22               | 1.982 ± 0.001                      | 1.980 ± 0.009                       |
|                        | 0.633      | 0.317       | 0.05          | 0.902 ± 0.001                         | 0.902 ± 0.001                          | 66.0 ± 0.0                | 65.09 ± 0.86               | 1.752 ± 0.001                      | 1.747 ± 0.007                       |
|                        | 0.767      | 0.183       | 0.05          | 0.926 ± 0.001                         | 0.926 ± 0.001                          | 71.0 ± 0.0                | 70.08 ± 0.81               | 1.946 ± 0.001                      | 1.946 ± 0.006                       |
| 0.5                    | 0.317      | 0.183       | 0.883 ± 0.001 | 0.882 ± 0.001                         | 56.7 ± 0.6                             | 57.29 ± 0.99              | 1.665 ± 0.001              | 1.669 ± 0.008                      |                                     |
| 0.767                  | 0.05       | 0.183       | 0.930 ± 0.001 | 0.929 ± 0.001                         | 62.0 ± 0.0                             | 63.45 ± 0.91              | 2.017 ± 0.001              | 2.020 ± 0.007                      |                                     |

|                                     |       |       |       |               |               |            |              |               |               |
|-------------------------------------|-------|-------|-------|---------------|---------------|------------|--------------|---------------|---------------|
|                                     | 0.633 | 0.183 | 0.183 | 0.907 ± 0.001 | 0.906 ± 0.001 | 58.7 ± 0.6 | 58.96 ± 0.61 | 1.833 ± 0.001 | 1.831 ± 0.005 |
|                                     | 0.633 | 0.183 | 0.183 | 0.906 ± 0.001 | 0.906 ± 0.001 | 58.7 ± 0.6 | 58.96 ± 0.61 | 1.835 ± 0.001 | 1.831 ± 0.005 |
| Blends added for increased coverage | 0.8   | 0.15  | 0.05  | 0.932 ± 0.001 | 0.932 ± 0.001 | 71.3 ± 0.6 | 71.74 ± 0.75 | 2.003 ± 0.001 | 2.000 ± 0.006 |
|                                     | 0.5   | 0.4   | 0.1   | 0.880 ± 0.001 | 0.880 ± 0.001 | 59.3 ± 0.6 | 60.45 ± 0.88 | 1.602 ± 0.001 | 1.606 ± 0.007 |
|                                     | 0.5   | 0.1   | 0.4   | 0.889 ± 0.001 | 0.888 ± 0.001 | 55.0 ± 0.0 | 54.63 ± 0.94 | 1.907 ± 0.001 | 1.909 ± 0.007 |
|                                     | 0.75  | 0.2   | 0.05  | 0.923 ± 0.001 | 0.923 ± 0.001 | 69.0 ± 0.0 | 69.29 ± 0.84 | 1.911 ± 0.001 | 1.920 ± 0.006 |
|                                     | 0.55  | 0.35  | 0.1   | 0.889 ± 0.001 | 0.889 ± 0.001 | 60.3 ± 0.6 | 60.86 ± 0.61 | 1.666 ± 0.001 | 1.666 ± 0.005 |
|                                     | 0.6   | 0.15  | 0.25  | 0.903 ± 0.001 | 0.902 ± 0.001 | 57.0 ± 0.0 | 56.41 ± 0.62 | 1.850 ± 0.001 | 1.846 ± 0.005 |
|                                     | 0.6   | 0.35  | 0.05  | 0.896 ± 0.001 | 0.896 ± 0.001 | 64.7 ± 0.6 | 64.29 ± 0.83 | 1.696 ± 0.001 | 1.702 ± 0.006 |
|                                     | 0.6   | 0.05  | 0.35  | 0.905 ± 0.001 | 0.904 ± 0.001 | 55.7 ± 0.6 | 55.05 ± 0.93 | 1.954 ± 0.001 | 1.954 ± 0.007 |
|                                     | 0.8   | 0.1   | 0.1   | 0.933 ± 0.001 | 0.933 ± 0.001 | 67.0 ± 0.0 | 68.85 ± 0.55 | 2.009 ± 0.001 | 2.022 ± 0.004 |
|                                     | 0.8   | 0.05  | 0.15  | 0.935 ± 0.001 | 0.934 ± 0.001 | 66.7 ± 0.6 | 66.38 ± 0.83 | 2.055 ± 0.001 | 2.050 ± 0.006 |
| Model Validation                    | 0.85  | 0.1   | 0.05  | 0.941 ± 0.001 | 0.940 ± 0.001 | 75.0 ± 0.0 | 74.58 ± 0.79 | 2.083 ± 0.001 | 2.084 ± 0.006 |
|                                     | 0.85  | 0.05  | 0.1   | 0.941 ± 0.001 | 0.942 ± 0.001 | 71.0 ± 0.0 | 71.62 ± 0.80 | 2.098 ± 0.001 | 2.105 ± 0.006 |
|                                     | 0.55  | 0.2   | 0.25  | 0.893 ± 0.001 | 0.893 ± 0.001 | 55.0 ± 0.0 | 55.81 ± 0.75 | 1.914 ± 0.001 | 1.787 ± 0.006 |
|                                     | 0.6   | 0.25  | 0.15  | 0.897 ± 0.001 | 0.899 ± 0.001 | 58.7 ± 0.6 | 59.49 ± 0.59 | 1.754 ± 0.001 | 1.762 ± 0.005 |
|                                     | 0.65  | 0.25  | 0.1   | 0.906 ± 0.001 | 0.906 ± 0.001 | 62.0 ± 0.0 | 62.88 ± 0.65 | 1.798 ± 0.001 | 1.797 ± 0.005 |
|                                     | 0.65  | 0.1   | 0.25  | 0.911 ± 0.001 | 0.910 ± 0.001 | 58.0 ± 0.0 | 57.41 ± 0.73 | 1.917 ± 0.001 | 1.910 ± 0.006 |
|                                     | 0.7   | 0.2   | 0.1   | 0.915 ± 0.001 | 0.915 ± 0.001 | 63.0 ± 0.0 | 64.48 ± 0.65 | 1.874 ± 0.001 | 1.868 ± 0.005 |
|                                     | 0.7   | 0.15  | 0.15  | 0.917 ± 0.001 | 0.917 ± 0.001 | 61.0 ± 0.0 | 62.15 ± 0.59 | 1.914 ± 0.001 | 1.898 ± 0.004 |

## S5.4 Butyl-Based Blends with ULSD

Table S.5.4.1. Measured Properties of the Butyl-Based Blends with ULSD.

| ULSD (vol%) | Biofuel Fraction (vol%) | nBL (vol%) | DNBE (vol%) | nBuOH (vol%) | Measured Density (g/cm <sup>3</sup> ) | Measured Flash Point (°C) | KV40 (mm <sup>2</sup> /s) |
|-------------|-------------------------|------------|-------------|--------------|---------------------------------------|---------------------------|---------------------------|
| 100         | 0                       | 0          | 0           | 0            | 0.840 ± 0.001                         | 65.0 ± 0.0                |                           |
| 95          | 5                       | 50         | 45          | 5            | 0.842 ± 0.001                         | 58.0 ± 0.8                | 2.653 ± 0.002             |
| 90          | 10                      |            |             |              | 0.844 ± 0.001                         | 54.3 ± 0.6                | 2.485 ± 0.001             |
| 75          | 25                      |            |             |              | 0.848 ± 0.001                         | 45.0 ± 1.0                | 2.109 ± 0.001             |
| 50          | 50                      |            |             |              | 0.857 ± 0.001                         | 41.7 ± 0.6                | 1.691 ± 0.001             |
| 30          | 70                      |            |             |              | 0.866 ± 0.001                         | 37.0 ± 0.0                | 1.443 ± 0.001             |
| 20          | 80                      |            |             |              | 0.871 ± 0.001                         | 36.7 ± 0.6                | 1.347 ± 0.001             |
| 0           | 100                     |            |             |              | 0.875 ± 0.001                         | 32.0 ± 0.0                | 1.186 ± 0.001             |

|    |     |                   |                |                   |                   |                |                   |
|----|-----|-------------------|----------------|-------------------|-------------------|----------------|-------------------|
| 95 | 5   | 50                | 5              | 45                | $0.843 \pm 0.001$ | $46.7 \pm 0.6$ | $2.666 \pm 0.001$ |
| 90 | 10  |                   |                |                   | $0.845 \pm 0.001$ | $42.0 \pm 0.0$ | $2.536 \pm 0.002$ |
| 75 | 25  |                   |                |                   | $0.852 \pm 0.001$ | $40.3 \pm 0.6$ | $2.269 \pm 0.001$ |
| 50 | 50  |                   |                |                   | $0.866 \pm 0.001$ | $39.7 \pm 0.6$ | $1.989 \pm 0.001$ |
| 30 | 70  |                   |                |                   | $0.877 \pm 0.001$ | $38.7 \pm 0.6$ | $1.807 \pm 0.001$ |
| 20 | 80  |                   |                |                   | $0.882 \pm 0.001$ | $38.7 \pm 0.6$ | $1.732 \pm 0.001$ |
| 0  | 100 |                   |                |                   | $0.889 \pm 0.001$ | $37.7 \pm 0.4$ | $1.611 \pm 0.001$ |
| 95 | 5   |                   |                |                   | 60                | 35             | 5                 |
| 90 | 10  | $0.845 \pm 0.001$ | $53.3 \pm 0.6$ | $2.405 \pm 0.001$ |                   |                |                   |
| 75 | 25  | $0.853 \pm 0.001$ | $50.0 \pm 0.8$ | $2.097 \pm 0.001$ |                   |                |                   |
| 50 | 50  | $0.868 \pm 0.001$ | $43.3 \pm 0.6$ | $1.761 \pm 0.001$ |                   |                |                   |
| 30 | 70  | $0.881 \pm 0.001$ | $41.5 \pm 0.6$ | $1.566 \pm 0.001$ |                   |                |                   |
| 20 | 80  | $0.886 \pm 0.001$ | $38.7 \pm 0.6$ | $1.475 \pm 0.001$ |                   |                |                   |
| 0  | 100 | $0.898 \pm 0.001$ | $31.3 \pm 1.8$ | $1.329 \pm 0.001$ |                   |                |                   |
| 95 | 5   | 60                | 5              | 35                |                   |                |                   |
| 90 | 10  |                   |                |                   | $0.846 \pm 0.001$ | $43.7 \pm 0.6$ | $2.454 \pm 0.001$ |
| 75 | 25  |                   |                |                   | $0.856 \pm 0.001$ | $41.5 \pm 0.6$ | $2.217 \pm 0.001$ |
| 50 | 50  |                   |                |                   | $0.877 \pm 0.001$ | $41.0 \pm 0.0$ | $1.963 \pm 0.001$ |
| 30 | 70  |                   |                |                   | $0.889 \pm 0.001$ | $40.3 \pm 0.6$ | $1.807 \pm 0.001$ |
| 20 | 80  |                   |                |                   | $0.897 \pm 0.001$ | $40.0 \pm 0.0$ | $1.733 \pm 0.001$ |
| 0  | 100 |                   |                |                   | $0.911 \pm 0.001$ | $35.3 \pm 2.1$ | $1.611 \pm 0.001$ |
| 95 | 5   |                   |                |                   | 70                | 25             | 5                 |
| 90 | 10  | $0.848 \pm 0.001$ | $45.8 \pm 0.4$ | $2.519 \pm 0.001$ |                   |                |                   |
| 75 | 25  | $0.859 \pm 0.001$ | $41.0 \pm 0.0$ | $2.220 \pm 0.001$ |                   |                |                   |
| 50 | 50  | $0.879 \pm 0.001$ | $41.7 \pm 1.0$ | $1.888 \pm 0.001$ |                   |                |                   |
| 30 | 70  | $0.895 \pm 0.001$ | $40.1 \pm 0.7$ | $1.685 \pm 0.001$ |                   |                |                   |
| 20 | 80  | $0.902 \pm 0.001$ | $38.0 \pm 0.0$ | $1.605 \pm 0.001$ |                   |                |                   |
| 0  | 100 | $0.918 \pm 0.001$ | $41.3 \pm 0.6$ | $1.455 \pm 0.001$ |                   |                |                   |
| 95 | 5   | 70                | 5              | 25                |                   |                |                   |
| 90 | 10  |                   |                |                   | $0.848 \pm 0.001$ | $55.7 \pm 1.2$ | $2.471 \pm 0.001$ |
| 75 | 25  |                   |                |                   | $0.860 \pm 0.001$ | $51.4 \pm 0.5$ | $2.235 \pm 0.001$ |
| 50 | 50  |                   |                |                   | $0.882 \pm 0.001$ | $46.7 \pm 0.6$ | $1.988 \pm 0.001$ |
| 30 | 70  |                   |                |                   | $0.899 \pm 0.001$ | $42.7 \pm 0.6$ | $1.825 \pm 0.001$ |
| 20 | 80  |                   |                |                   | $0.910 \pm 0.001$ | $38.0 \pm 0.0$ | $1.760 \pm 0.001$ |
| 0  | 100 |                   |                |                   | $0.926 \pm 0.001$ | $37.3 \pm 1.0$ | $1.636 \pm 0.001$ |

|    |     |                   |                |                   |                   |                |                   |
|----|-----|-------------------|----------------|-------------------|-------------------|----------------|-------------------|
| 95 | 5   | 80                | 15             | 5                 | $0.845 \pm 0.001$ | $58.7 \pm 0.6$ | $2.604 \pm 0.001$ |
| 90 | 10  |                   |                |                   | $0.850 \pm 0.001$ | $57.0 \pm 0.0$ | $2.489 \pm 0.001$ |
| 75 | 25  |                   |                |                   | $0.865 \pm 0.001$ | $54.3 \pm 0.6$ | $2.244 \pm 0.001$ |
| 50 | 50  |                   |                |                   | $0.889 \pm 0.001$ | $51.3 \pm 0.6$ | $1.995 \pm 0.002$ |
| 30 | 70  |                   |                |                   | $0.908 \pm 0.001$ | $49.0 \pm 0.0$ | $1.814 \pm 0.001$ |
| 20 | 80  |                   |                |                   | $0.921 \pm 0.001$ | $46.7 \pm 0.6$ | $1.765 \pm 0.001$ |
| 0  | 100 |                   |                |                   | $0.938 \pm 0.001$ | $44.5 \pm 0.7$ | $1.627 \pm 0.001$ |
| 95 | 5   |                   |                |                   | 80                | 5              | 15                |
| 90 | 10  | $0.850 \pm 0.001$ | $53.3 \pm 0.6$ | $2.481 \pm 0.001$ |                   |                |                   |
| 75 | 25  | $0.865 \pm 0.001$ | $48.7 \pm 0.6$ | $2.278 \pm 0.001$ |                   |                |                   |
| 50 | 50  | $0.890 \pm 0.001$ | $47.3 \pm 0.6$ | $2.043 \pm 0.001$ |                   |                |                   |
| 30 | 70  | $0.913 \pm 0.001$ | $46.7 \pm 0.6$ | $1.893 \pm 0.001$ |                   |                |                   |
| 20 | 80  | $0.923 \pm 0.001$ | $43.7 \pm 0.6$ | $1.829 \pm 0.001$ |                   |                |                   |
| 0  | 100 | $0.941 \pm 0.001$ | $45.0 \pm 0.0$ | $1.697 \pm 0.001$ |                   |                |                   |
| 95 | 5   | 90                | 5              | 5                 |                   |                |                   |
| 90 | 10  |                   |                |                   | $0.851 \pm 0.001$ | $59.3 \pm 0.6$ | $2.516 \pm 0.002$ |
| 75 | 25  |                   |                |                   | $0.869 \pm 0.001$ | $58.3 \pm 0.6$ | $2.309 \pm 0.002$ |
| 50 | 50  |                   |                |                   | $0.899 \pm 0.001$ | $57.0 \pm 0.0$ | $2.114 \pm 0.001$ |
| 30 | 70  |                   |                |                   | $0.923 \pm 0.001$ | $57.0 \pm 0.0$ | $1.985 \pm 0.001$ |
| 20 | 80  |                   |                |                   | $0.935 \pm 0.001$ | $56.7 \pm 0.6$ | $1.938 \pm 0.001$ |
| 0  | 100 |                   |                |                   | $0.957 \pm 0.001$ | $55.3 \pm 0.4$ | $1.804 \pm 0.001$ |

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