

## Curvature screening in draped mechanical metamaterial sheets Supporting Information

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### 1 Boundary layer analysis

#### 1.1 Dilational metamaterial

For dilational metamaterial sheets, the governing equations of motion in the Föppl-Von Kármán limit are

$$\Delta(\chi/Y) = (\kappa_0/Y)A - (\kappa_1/Y)\Delta A, \quad (1)$$

$$\Delta^2(\chi/Y) = -G - \Delta A \quad (2)$$

where  $\kappa_1/YL^2$  is assumed to be a small, dimensionless number, where  $L$  is the dimension of the sheet. Here  $Y = 4\mu$  as per the main text. And The boundary conditions are

$$\hat{\mathbf{n}} \cdot \nabla A|_B = 0, \quad (3)$$

$$\boldsymbol{\sigma} \cdot \hat{\mathbf{n}}|_B = 0, \quad (4)$$

where  $\boldsymbol{\sigma}$  is the stress tensor,  $|_B$  denotes the restriction of the functions to the boundary,  $\hat{\mathbf{n}}$  is the unit vector normal to the boundary but tangent to the metamaterial sheet, and repeated indices are summed.

The presence of a small parameter  $\kappa_1/YL^2$  multiplying the highest derivative of  $A$  suggests the solution will take the form of a slowly varying bulk term and a rapidly varying boundary layer. An approximate solution may be obtained as described in the next sections.

##### 1.1.1 Outside the boundary layer

Since  $\varepsilon = \frac{\kappa_1}{YL^2}$  is small, we look for a solution in the bulk of the sheet of the form,

$$A = A_0 + \varepsilon A_1 + O(\varepsilon^2) \quad (5)$$

$$\chi = \chi_0 + \varepsilon \chi_1 + O(\varepsilon^2). \quad (6)$$

Substituting into Eqs. (1) and (2), we obtain

$$\Delta \chi_0 = \kappa_0 A_0 \quad (7)$$

$$\Delta A_0 = -\frac{Y}{Y + \kappa_0} G \quad (8)$$

to lowest order in  $\varepsilon$ . Assuming axisymmetry and setting  $Y = 4\mu$  we therefore obtain  $a_2 = -\frac{\mu G}{(4\mu + \kappa_0)}$ , thus giving

$$A_0 = -\frac{\mu G}{4\mu + \kappa_0} r^2 + a_0, \quad (9)$$

,where  $a_0$  is a constant.

##### 1.1.2 Inside the boundary layer

To obtain the solution near the boundary, assume the boundary layer has thickness  $\delta$  and make the coordinate substitution  $\eta = (R - r)/\delta$ . From the equations of motion, we obtain the following effective equation in  $A$

$$\frac{\kappa_1/4\mu}{\delta^2} \Delta^2 A_{in} = \left(1 + \frac{\kappa_0}{4\mu}\right) \Delta A_{in}. \quad (10)$$

Setting the boundary layer thickness  $\delta = \sqrt{\frac{\kappa_1}{4\mu + \kappa_0}} = l_{sc}$ , we obtain

$$A(\eta)_{in} = c_1 (I_0(\eta) - 1) + c_2 Y_0(-i\eta) \quad (11)$$

### 1.1.3 Full solution

Imposing the boundary condition  $A'(R) = 0$  on the boundary layer solution, in the limit  $\delta \rightarrow 0$  that we can evaluate A

$$A = a_0 - \frac{4\mu G}{4\mu + \kappa_0} \left( \frac{r^2}{4} - l_{sc} \frac{R}{2} \frac{I_0\left(\frac{r}{l_{sc}}\right)}{I_1\left(\frac{R}{l_{sc}}\right)} \right) \quad (12)$$

The coefficient  $a_0$  can be obtained by minimizing the energy for A we have obtained. Therefore, up to leading order in the screening length we have

$$A = \frac{\mu G(R^2 - 12l_{sc}^2)}{3(\kappa_0 + 4\mu)} - \frac{4\mu G}{4\mu + \kappa_0} \left( \frac{r^2}{4} - l_{sc} \frac{R}{2} \frac{I_0\left(\frac{r}{l_{sc}}\right)}{I_1\left(\frac{R}{l_{sc}}\right)} \right) \quad (13)$$

Similarly to ensure vanishing normal and shear stresses on the boundary, i.e.,  $\chi'(R) = 0$ , we get  $\chi$  up to appropriate order in  $\delta$

$$\chi = d_0 + \frac{G\mu\kappa_0 R^2}{12(\kappa_0 + 4\mu)} r^2 - \frac{G\mu\kappa_0}{16(\kappa_0 + 4\mu)} r^4 + l_{sc}^2 \frac{\mu G}{4\mu + \kappa_0} \left( 4\mu r^2 - \frac{R}{2} \frac{I_0\left(\frac{r}{l_{sc}}\right)}{I_1\left(\frac{R}{l_{sc}}\right)} \right) \quad (14)$$

Note that the harmonic function in  $\chi$  in the main text with the choice of boundary conditions reduces to the constant  $d_0$ .

## 1.2 Simple shear metamaterial

For simple shear sheets, in Cartesian coordinates, the equilibrium equations are

$$\partial_1 \partial_2 \chi = -\kappa_0 A + \kappa_1 \Delta A \quad (15)$$

$$\frac{1}{Y} \Delta^2 \chi - \frac{1}{\mu} \partial_1^2 \partial_2^2 \chi = -G + \partial_1 \partial_2 A \quad (16)$$

### 1.2.1 Outside the boundary layer

Outside the boundary layer,

$$A = A_0 + \varepsilon A_1 + O(\varepsilon^2), \quad (17)$$

$$\chi = \chi_0 + \varepsilon \chi_1 + O(\varepsilon^2) \quad (18)$$

and so

$$\partial_1 \partial_2 \chi_0 = -\kappa_0 A_0, \quad (19)$$

$$\frac{1}{Y} \Delta^2 \chi_0 - \frac{1}{\mu} \partial_1^2 \partial_2^2 \chi_0 = -G + \partial_1 \partial_2 A_0. \quad (20)$$

We obtain the following working equation in  $\chi_0$ ,

$$\frac{1}{Y} \left( \partial_1^4 + \partial_2^4 \right) \chi_0 + \left( \frac{1}{\kappa_0} + 2\frac{1}{Y} - \frac{1}{\mu} \right) \partial_1^2 \partial_2^2 \chi_0 = -G. \quad (21)$$

We can guess the form of the simplest solution for the limit  $\kappa_1 \rightarrow 0$  and  $\kappa_0 \ll Y$  to be

$$\chi_0 = \frac{-\kappa_0 \mu Y G / 4}{\mu Y + 2\kappa_0 \mu - \kappa_0 Y} x^2 y^2 + P(x) + Q(y) \quad (22)$$

$$A_0 = \frac{\mu Y G}{\mu Y + 2\kappa_0 \mu - \kappa_0 Y} xy \quad (23)$$

These functions do not satisfy the boundary conditions and are corrected by an additional exponentially growing term inside the boundary layer whose thickness scales with  $\kappa_1$ .

### 1.2.2 Inside the boundary layer

The working equations are the following

$$\partial_1 \partial_2 \chi = -\kappa_0 A + \kappa_1 \Delta A \quad (24)$$

$$\frac{1}{Y} \Delta^2 \chi - \frac{1}{\mu} \partial_1^2 \partial_2^2 \chi = -G + \partial_1 \partial_2 A \quad (25)$$

Near boundary  $x = L$ , the  $y$  derivatives are small and  $x$  derivatives are large. Introducing an internal variable,  $\eta = (L - x)/\delta$ , the equations become,

$$-\delta \partial_\eta \partial_2 \chi = -\delta^2 \kappa_0 A + \kappa_1 \left( \partial_\eta^2 + \delta^2 \partial_2^2 \right) A \quad (26)$$

$$-\delta^3 \partial_\eta \partial_2 A = \frac{1}{Y} \left( \partial_\eta^4 + \delta^4 \partial_2^4 + 2\delta^2 \partial_\eta^2 \partial_2^2 \right) \chi \quad (27)$$

$$- \frac{1}{\mu} \delta^2 \partial_\eta^2 \partial_2^2 \chi \quad (28)$$

If the  $\chi$  and  $A$  are sufficiently slowly varying in  $y$  near  $x = L$ , then

$$\delta^2 \kappa_0 / \kappa_1 A = \partial_\eta^2 A \quad (29)$$

$$-Y \delta^3 \partial_\eta \partial_2 A = \partial_\eta^4 \chi \quad (30)$$

the solutions are of the following form

$$\begin{aligned} A(x, y) &= \frac{\mu Y G}{\mu Y + 2\kappa_0 \mu - \kappa_0 Y} xy + f(y) \left( e^{-(L-x)/l_{shear}} - e^{-(L+x)/l_{shear}} \right) \\ &+ g(x) \left( e^{-(L-y)/l_{shear}} - e^{-(L+y)/l_{shear}} \right) \end{aligned} \quad (31)$$

where  $\delta = l_{shear} = \sqrt{\kappa_1 / \kappa_0}$ . Correspondingly,  $\chi$  is

$$\begin{aligned} \chi(x, y) &= \frac{-\kappa_0 \mu Y G / 4}{\mu Y + 2\kappa_0 \mu - \kappa_0 Y} x^2 y^2 + p(x^2 + y^2) \\ &- Y l_{shear}^3 \left( f'(y) \left( e^{-(L-x)/l_{shear}} + e^{-(L+x)/l_{shear}} \right) \right. \\ &\left. + g'(x) \left( e^{-(L-y)/l_{shear}} + e^{-(L+y)/l_{shear}} \right) \right) \end{aligned} \quad (32)$$

For 31 and 32, to satisfy 24 and ??, the forms of  $f(x)$  and  $g(y)$  are

$$\begin{aligned} f(y) &= a_1 y \\ g(x) &= a_1 x \end{aligned}$$

We determine the constants  $a_1$  and  $p$  by satisfying the boundary condition in the limit  $\kappa_1 \rightarrow 0$  and  $\kappa_0 G \rightarrow 0$ . Thus,

$$\begin{aligned} a_1 &= \frac{\mu Y G l_{shear} \left( 1 + \tanh \left( L \sqrt{\frac{\kappa_0}{\kappa_1}} \right) \right)}{2(\mu Y + 2\kappa_0 \mu - \kappa_0 Y)} \\ p &= \frac{\kappa_0 \mu Y G}{4(\mu Y + 2\kappa_0 \mu - \kappa_0 Y)} L^2 \end{aligned}$$

Hence, the fields simplify to the following final expressions

$$\begin{aligned} A(x, y) &= \frac{\mu Y G}{\mu Y + 2\kappa_0 \mu - \kappa_0 Y} \left( xy + l_{shear} \frac{x \sinh(y/l_{shear}) + y \sinh(x/l_{shear})}{\cosh(L/l_{shear})} \right) \\ \chi(x, y) &= \frac{\mu Y G / 4}{\mu Y + 2\kappa_0 \mu - \kappa_0 Y} \left( L^2(x^2 + y^2) - x^2 y^2 \right. \\ &\left. - 4Y l_{shear}^4 \frac{\cosh(x/l_{shear}) + \cosh(y/l_{shear})}{\cosh(L/l_{shear})} \right) \end{aligned}$$

where, we have small parameters  $\kappa_1$  and  $\kappa_0$  satisfying  $l_{shear} \ll L$  and  $GL^2 \kappa_0 / Y \rightarrow 0$ . Thus  $l_{shear} \ll \sqrt{Y/G \kappa_0}$ , which gives  $\kappa_1 / Y \ll 1/G$  or  $G \ll Y / \kappa_1$ . Hence, this solution is valid in this limit of sufficiently weakly curved substrate.

## 2 Numerics

The metamaterials are modeled as linear and torsional spring networks with each spring having energy

$$E_{lin} = \frac{k}{2} \left( \frac{l^2 - \bar{l}^2}{2\bar{l}^2} \right)^2, \quad (33)$$

where  $l$  is the spring length,  $\bar{l}$  the equilibrium length, and  $k$  the spring constant. For small strains,  $l \approx \bar{l} + \delta l$  and the energy reduces to

$$E_{lin} \approx \frac{k}{2} \left( \frac{l}{\bar{l}} \right) \quad (34)$$

Torsional springs are modeled as

$$E_{tor} = \frac{K}{2} (\theta - \bar{\theta})^2, \quad (35)$$

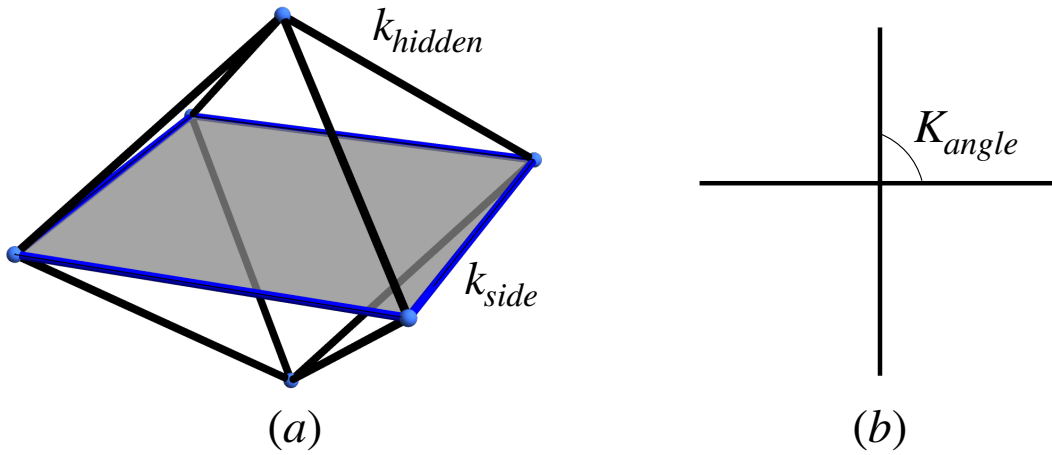
where  $\theta$  is the angle between a pair of edges and  $\bar{\theta}$  is their equilibrium angle, and  $K$  is the torsional spring constant.

Finally, each geometrically-confined vertex is modeled with energy

$$E_{con} = \frac{k_{con}}{2} (z - h(x, y))^2, \quad (36)$$

where  $h(x, y)$  is the height function of a surface and  $(x, y, z)$  are the coordinates of the vertex. The constraint  $k_{con}$  is set to 100 times the largest modulus and we have confirmed that  $k_{con}$  is always sufficiently large so as to not change the numerical results.

The total energy was minimized with the standard L-BFGS algorithm and conjugate gradient algorithm as implemented by Mathematica version 12.



**Figure 1** (a) One unit of the dilational metamaterial. (b) A vertex of the shear metamaterial.

## 2.1 Dilational metamaterial

The dilational metamaterial is constructed as a system of counter-rotating squares. Each square is actually modeled according to Fig. 1, with hidden edges leading to a vertex above and below the centroid of the square. The sides of the square have spring constant  $k_{side} = 1$  and  $k_{hidden} = 10^{-3}$  sets the bending rigidity of the square. Torsional springs are placed at the vertices where squares meet.

## 2.2 Shear metamaterial

The shear metamaterial is built from a square lattice of springs with spring constant  $k = 1$ . There is a torsional spring with spring constant  $K_{bend}$  preventing the bending of each rod through the vertex and an additional torsional spring with spring constant  $K_{angle}$  at one corner of each square of the metamaterial.