Supporting Information

A Metal–Organic Framework Based Propylene Nano-trap with Dual Functionalities for Highly Efficient Propylene/Propane Separation

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Supplementary Experimental section

1. General procedures and materials

All starting reagents and solvents were purchased from commercial companies and used without further purification. Nickel hexafluorosilicate (NiSiF₆, CAS: 26043-11-8) was purchased from Energy Chemical, and 2-mercaptopyrazine (pyz-SH, CAS: 38521-06-1) was purchased from Macklin. Powder X–ray diffraction (PXRD) patterns were measured by a Rigaku Ultima IV diffractometer operated at 40 kV and 44 mA with a scan rate of 2 deg min⁻¹. Thermogravimetric analysis (TGA) was performed on a Netzsch TG209F3 instrument and the sample was heated under N₂ atmosphere with a heating rate of 5 K min⁻¹.

 CO_2 (99.995%), C_3H_6 (99.5%), C_3H_8 (99.9%), He (99.999%) and mixed gases of $C_3H_6/C_3H_8 = 50/50$ (v/v) and $C_3H_6/C_3H_8 = 10/90$ (v/v) were purchased from JinGong Company (China).

2. Synthesis of [Ni(pyz-SH)₂(SiF₆)]_n (ZJUT-2)

The powder samples of ZJUT-2 were synthesized using the same methods reported in the corresponding literature.¹ [Ni(pyz-SH)₂(SiF₆)]_n (ZJUT-2) was synthesized by the solvothermal reaction of nickel hexafluorosilicate (NiSiF₆, 0.67 mmol) with 2mercaptopyrazine (pyz-SH, 0.67 mmol) in 20 mL methanol at 85 °C. Light-yellow powder was obtained after 48 h, collected by filtration and then washed with methanol. Bulk purity of the sample was verified by PXRD.

3. Gas sorption measurements

Gas adsorption isotherms were measured by Micromeritics ASAP 2020 surface area analyzer. To remove all the guest solvents in the framework, the fresh powder sample was first solvent-exchanged with dry methanol at least 8 times within three days. The solvent-exchanged sample was evacuated at room temperature (298 K) for 24 h, and then at 323 K for additional 12 h until the outgas rate was 5 μ mHg min⁻¹ prior to measurements. The sorption measurement was maintained at 77 K with liquid nitrogen. An ice-water bath (slush) and water bath were used for adsorption isotherms at 273 and 296 K, respectively.

4. Fitting of pure component isotherms

The pure component isotherm data for C_3H_6 and C_3H_8 in ZJUT-2a at 296 K were fitted with the single-site Langmuir-Freundlich isotherm model

$$q = q_{sat} \frac{bp^{\nu}}{1 + bp^{\nu}} \tag{1}$$

with T-dependent parameter b

$$b = b_0 \exp\left(\frac{E}{RT}\right) \tag{2}$$

The fitted parameters are provided in Table S1.

5. Virial Graph Analysis

Estimation of the isosteric heats of gas adsorption (Q_{st})

A virial-type expression of comprising the temperature-independent parameters a_i and b_j was employed to calculate the enthalpies of adsorption for C₃H₆ and C₃H₈ (at 273 K, 296 K) on ZJUT-2a. In each case, the data were fitted with equation:

$$\ln P = \ln N + 1/T \sum_{i=0}^{m} a_i N_i + \sum_{j=0}^{n} b_j N_j$$
(3)

Here, *P* is the pressure expressed in mmHg, *N* is the amount absorbed in mmol g⁻¹, *T* is the temperature in K, a_i and b_j are virial coefficients, and *m*, *n* represent the number of coefficients required to adequately describe the isotherms (*m* and *n* were gradually increased till the contribution of extra added *a* and *b* coefficients were deemed to be statistically insignificant towards the overall fit. And the average value of the squared deviations from the experimental values was minimized). The values of the virial coefficients a_0 to a_m were then used to calculate the isosteric heat of absorption using the following expression:

$$Q_{st} = -R \sum_{i=0}^{m} a_i N_i \tag{4}$$

 Q_{st} is the coverage-dependent isosteric heat of adsorption and *R* is the universal gas constant. The heat enthalpies of C₃H₆ and C₃H₈ sorption for complex ZJUT-2a in this manuscript are determined by using the sorption data measured in the pressure range from 0-1 bar (at 273 K, 296 K).

6. IAST calculations

The adsorption selectivity was predicted by using the Ideal Adsorbed Solution Theory (IAST) of Myers and Prausnitz.² The adsorption selectivity is defined by

$$S_{ads} = \frac{q_1/q_2}{p_1/p_2}$$
(5)

In equation (5), q_1 and q_2 are the molar loadings of the adsorbed phase in equilibrium with the bulk gas phase with partial pressures p_1 and p_2 . The IAST calculation results of the adsorption selectivity of 50/50 (v/v) C₃H₆/C₃H₈ and 10/90 (v/v) C₃H₆/C₃H₈ for ZJUT-2a at 296 K are shown in Figure 2e.

7. Computational results and details

In order to obtain the reasonable binding sites of gas molecules in ZJUT-2a for subsequent modeling, Grand Canonical Monte Carlo (GCMC) simulations were performed in the MS modeling. The crystal structures of ZJUT-2a were chosen for related simulations without further geometry optimization. The framework and the individual C_3H_6 and C_3H_8 molecules were considered to be rigid during the simulation. Partial charges for atoms of guest-free ZJUT-2a were derived from QEq method and QEq_neutral1.0 parameter. The simulations were carried out at 296 K, adopting the locate task, Metropolis method in Sorption module and the universal force field (UFF). The partial charges on the atoms of C_3H_6 (C1: -0.276e, C2: -0.141e, C6: -0.401; H3: 0.146e, H4: 0.124e, H5: 0.142e, H7: 0.124e, H8: 0.141e, H9: 0.141e, where e = 1.6022 × 10⁻¹⁹ C is the elementary charge) and C_3H_8 (C1: -0.430e, C2: -0.295e, C7: -0.430;

H3: 0.147e, H4: 0.147e, H5: 0.128e, H6: 0.157e, H8: 0.157e, H9: 0.128e, H10: 0.147e, H11: 0.147e) were also derived from QEq method. The interaction energy between hydrocarbon molecules and framework were computed through the Coulomb and Lennard-Jones 6-12 (LJ) potentials. The cutoff radius was chosen as 12.5 Å for the LJ potential and the long-range electrostatic interactions were handled using the Ewald & Group summation method. The loading steps and the equilibration steps were 1×10^5 , the production steps were 1×10^6 .

8. Breakthrough experiments

The breakthrough experiments were performed in dynamic gas breakthrough equipment using two stainless steel columns (4.0 mm inner diameter \times 150 mm for 50/50 C₃H₆/C₃H₈ mixture and 4.0 mm inner diameter \times 120 mm for 10/90 C₃H₆/C₃H₈ mixture). The weights of sample packed in the columns were 1.2535 g and 0.6258 g, respectively. The columns were activated under reduced pressure at 323 K overnight. The experimental set-up consisted of two fixed-bed stainless steel reactors. One reactor was loaded with the adsorbent, while the other reactor was used as a blank control group to stabilize the gas flow. The gas flows were controlled at the inlet by a mass flow meter as 2 mL min⁻¹, and a gas chromatograph (TCD-Thermal Conductivity Detector, detection limit 0.1 ppm) continuously monitored the effluent gas from the adsorption bed. Prior to every breakthrough experiment, we activated the sample by flushing the adsorption bed with helium gas for 2 hours at 373 K. Subsequently, the column was allowed to equilibrate at the measurement rate before we switched the gas flow.

9. Gas equilibrium adsorption capacity and separation factor

The complete breakthrough of C_3H_6 was indicated by the downstream gas composition reaching that of the feed gas. On the basis of the mass balance, the gas adsorption capacities can be determined as follows:

$$q_i = \frac{c_i V}{22.4 \times m} \times \int_0^t \left(1 - \frac{F}{F_0}\right) dt \tag{6}$$

Where q_i is the equilibrium adsorption capacity of gas *i* (mmol g⁻¹), C_i is the feed gas concentration, *V* is the volumetric feed flow rate (cm³ min⁻¹), *t* is the adsorption time (min), F_0 and *F* are the inlet and outlet gas molar flow rates, respectively, and *m* is the mass of the adsorbent (g). The separation factor (α) of the breakthrough experiment is determined as:

$$\alpha = \frac{q_A y_B}{q_B y_A} \tag{7}$$

in which y_i is the molar fraction of gas i (i = A, B) in the gas mixture.

Notation

- q_i component molar loading of species *i*, mol kg⁻¹
- $q_{\rm sat}$ saturation loading, mol kg⁻¹
- *b* Langmuir-Freundlich constant, kPa^{- ν}
- p_i partial pressure of species *i* in mixture, kPa
- $p_{\rm t}$ total system pressure, kPa
- *T* absolute temperature, K

Greek letters

v Freundlich exponent, dimensionless

Supplementary Tables

Table S1. Single-site Langmuir-Freundlich parameter fits for C_3H_6 and C_3H_8 in ZJUT-2a. The fits are based on experimental isotherm data at 296 K.

	$q_{ m sat}$	b_0	V
	mol kg ⁻¹	kPa ^{-vA}	dimensionless
C ₃ H ₆	4.55284	0.25785	0.49151
C_3H_8	3.08133	0.00164	1.73149

MOE	T(K) -	C_3H_6 Uptake ^[a] (cm ³ cm ⁻³)		50/50 C ₃ H ₆ /C ₃ H ₈	$Q_{\rm st}$ of		
MOFS		1 bar	0.5 bar	0.1 bar	IAST selectivity ^[b]	$C_3H_6^{[t]}$ (kJ mol ⁻¹)	KeI.
ZJUT-2a	296	138.9	123.5	72.3	17.2	45	This work
$Co_2(m-dobdc)$	298	201.9	196.6	183.0	38	56	3
Co-MOF-74	298	191.4	185.9	136.9	45	[d]	4
GeFSIX-2-Cu-i	298	88.4	76.2	37.8	4	32.1	5
SIFSIX-2-Cu-i	298	74.6	61.9	28.2	4.5	35.8	5
Co-gallate	298	66.6	50.1	12	333	41.0	6
HIAM-301	298	93.0	87.2	71.5	150	27	7
Y-abtc	298	63.5	62.7	53.7	[d]	50.0	8
Co(AIP)(BPY) _{0.5}	298	63.8	58.0	26.2	21	42.4	9
KAUST-7	298	56.8	46.0	9.41	[d]	57.4	10
MAF-23-O	298	45.1	44.1	36.3	8.8	54	11
UTSA-400	298	92.1	85.5	46.3	107	60.5	12
JNU-3a	303	79.2	69.3	17.3	513	29.3	13
MFM-520	298	78	74.6	67.4	17	48.5	14
ZJU-75a	296	104.3	90.5	71.2	54.2	65.9	15

Table S2. Comparison of the C_3H_6 uptake, IAST selectivity and Q_{st} of C_3H_6 for ZJUT-2a and some top-performing MOFs reported for C_3H_6/C_3H_8 separation.

[a] Adsorption capacity is obtained from single-component gas adsorption isotherms.

[b] Selectivity is calculated by the IAST method for an equimolar mixture at 1 bar.

[c] $Q_{\rm st}$ values at near-zero coverage.

[d] The value was not reported in the literature, which shows molecular sieving effect.

MOFs	C ₃ H ₆ dynamic uptake (mmol g ⁻¹) ^[a]	C ₃ H ₆ /C ₃ H ₈ dynamic selectivity ^[b]	Ref.
ZJUT-2a	2.6	10	This work
MAF-23-0	1.3	15	11
KAUST-7 ^[c]	1.16	12	10
Co-MOF-74 ^[c]	6.50	6.48	4
Y-abtc ^[c]	1.26	8.3	8
JNU-3a	2.45	2.9	13
Ni-NP	2.30	9.6	16
SIFSIX-3-Ni	1.25	1.8	17
TIFSIX-3-Ni	0.8	2.0	17
ZU-36-Co	0.86	2.5	17
ZU-36-Ni	1.35	19	17
SIFSIX-2-Cu-i	2.00	_	5
GeFSIX-2-Cu-i	2.20	_	5

Table S3. Comparison of the C_3H_6 dynamic uptake and selectivity based on 50/50 C_3H_6/C_3H_8 breakthrough curves for ZJUT-2a and other reported materials.

[a] Dynamic C₃H₆ uptake was obtained from breakthrough experiments.

[b] Dynamic C_3H_6/C_3H_8 selectivity was calculated from breakthrough curve.

[c] Dynamic uptake and selectivity were reported in ref. 16.

Supplementary Figures



Figure S1. PXRD patterns of as-synthesized ZJUT-2 (red) and activated ZJUT-2a (blue) compared with the simulated PXRD pattern from the crystal structure of ZJUT-2 (black), which are consistent well with the PXRD patterns reported in our previous work.¹



Figure S2. (a) 196 K CO_2 adsorption isotherms of ZJUT-2a. (b) BET calculation based on CO_2 adsorption isotherm of ZJUT-2a at 196 K.



Figure S3. Adsorption isotherms of C_3H_6 (red) and C_3H_8 (black) for ZJUT-2a at 296 K up to 1 bar. Filled/empty circles represent adsorption/desorption.



Figure S4. Adsorption isotherms of C_3H_6 (red) and C_3H_8 (blue) for ZJUT-2a at 273 K up to 1 bar. Filled/empty circles represent adsorption/desorption.



Figure S5. PXRD patterns of as-synthesized SIFSIX-3-Ni (red) compared with the simulated PXRD pattern from the crystal structure of SIFSIX-3-Ni (black).



Figure S6. Adsorption isotherms of C_3H_6 (ball) and C_3H_8 (triangle) for SIFSIX-3-Ni at (a) 296 K and (b) 273 K up to 1 bar.



Figure S7. Virial fitting of the C₃H₆ adsorption isotherms for ZJUT-2a.



Figure S8. Virial fitting of the C₃H₈ adsorption isotherms for ZJUT-2a.



Figure S9. Heats of adsorption (Q_{st}) of C_3H_6 (red) and C_3H_8 (black) for ZJUT-2a.



Figure S10. Comparison of heats of adsorption (Q_{st}) of C₃H₆ for ZJUT-2a and other reported materials.



Figure S11. Heats of adsorption (Q_{st}) of C_3H_6 (red) and C_3H_8 (black) for SIFSIX-3-Ni.



Figure S12. Comparison of heats of adsorption (Q_{st}) of C₃H₆ and 0.1 bar C₃H₆ uptake for ZJUT-2a and other reported materials.



Figure S13. Comparison of C_3H_6/C_3H_8 IAST selectivity and 0.1 bar C_3H_6 uptake for ZJUT-2a and other reported materials.



Figure S14. Illustration of C_3H_8 adsorption site in the nano-trap of ZJUT-2a, revealed by theoretical calculations.



Figure S15. Illustration of C_3H_8 adsorption site in the nano-trap of ZJUT-2a, revealed by theoretical calculations.



Breakthrough experiments apparatus

Figure S16. Schematic illustration of the apparatus for the breakthrough experiments.



Figure S17. Experimental column breakthrough curves (circle) and C_3H_8 dynamic uptake calculation (square) for a 50/50 C_3H_6/C_3H_8 mixture in ZJUT-2a. The calculation of dynamic uptake is based on equation (6). Dashed blue lines: C_3H_8 gas adsorbed from t_0 to t_1 (62 min) when the C_3H_6 breakthrough occurred.



Figure S18. Experimental column breakthrough curves (circle) and C_3H_6 dynamic uptake calculation (square) for a 50/50 C_3H_6/C_3H_8 mixture in ZJUT-2a. The calculation of dynamic uptake is based on equation (6) and the dynamic selectivity is calculated based on equation (7). Dashed blue lines: C_3H_6 gas adsorbed from t₀ to t₂ (106 min) when the C_3H_6 breakthrough was completed.



Figure S19. Experimental column breakthrough curves (circle) and C_3H_6 dynamic uptake calculation (square) for a 10/90 C_3H_6/C_3H_8 mixture in ZJUT-2a. The calculation of dynamic uptake is based on equation (6). Dashed blue lines: C_3H_6 gas adsorbed from t_0 to t_2 (133 min) when the C_3H_6 breakthrough was completed.



Figure S20. Cycling column breakthrough curves for C_3H_6/C_3H_8 separation (10/90, v/v) with ZJUT-2a at 296 K and 1.0 bar.



Figure S21. PXRD patterns of as-synthesized ZJUT-2 (black), activated ZJUT-2a (red), and ZJUT-2 samples exposed to air for three days (purple), one week (blue) and one month (wine), indicating its great air stability.



Figure S22. PXRD patterns of as-synthesized ZJUT-2 (black) and ZJUT-2 samples after multiple breakthrough tests (red).



Figure S23. TGA curves of synthesized (black) and activated (red) ZJUT-2 samples under a flow of N_2 at a rate of 5 °C min⁻¹.

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