

## Supporting Information

### **High thermoelectric performance in *p*-type ZnSb upon Zn vacancies: An experimental and theoretical study**

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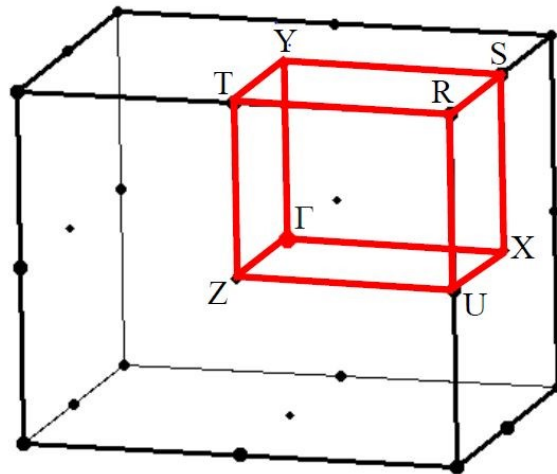


Figure S1. The Brillouin zone of pure ZnSb

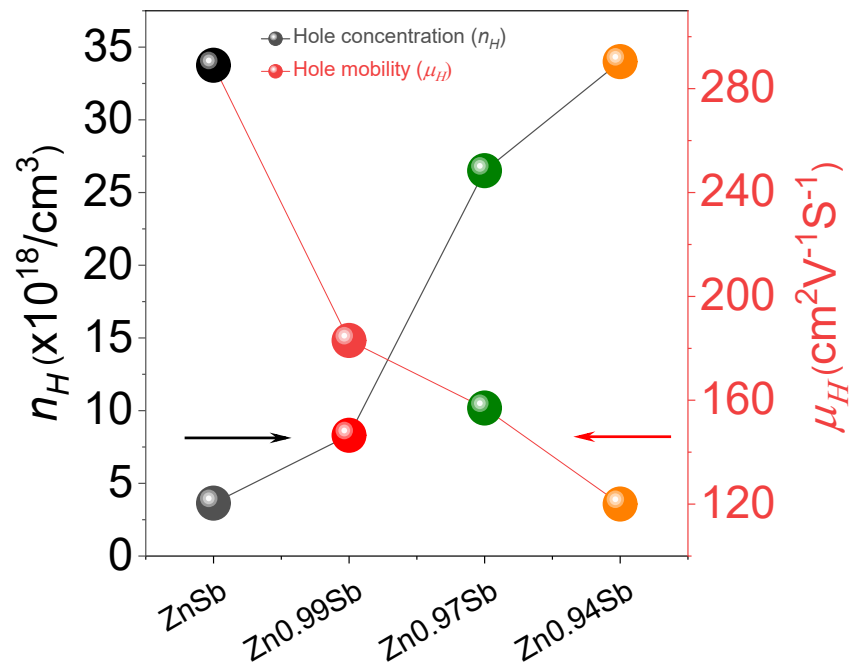


Figure S2. Hall plot of Zn<sub>1-x</sub>Sb (x = 0, 0.01, 0.03, 0.06) vs.  $n_H$  and  $\mu_H$ .

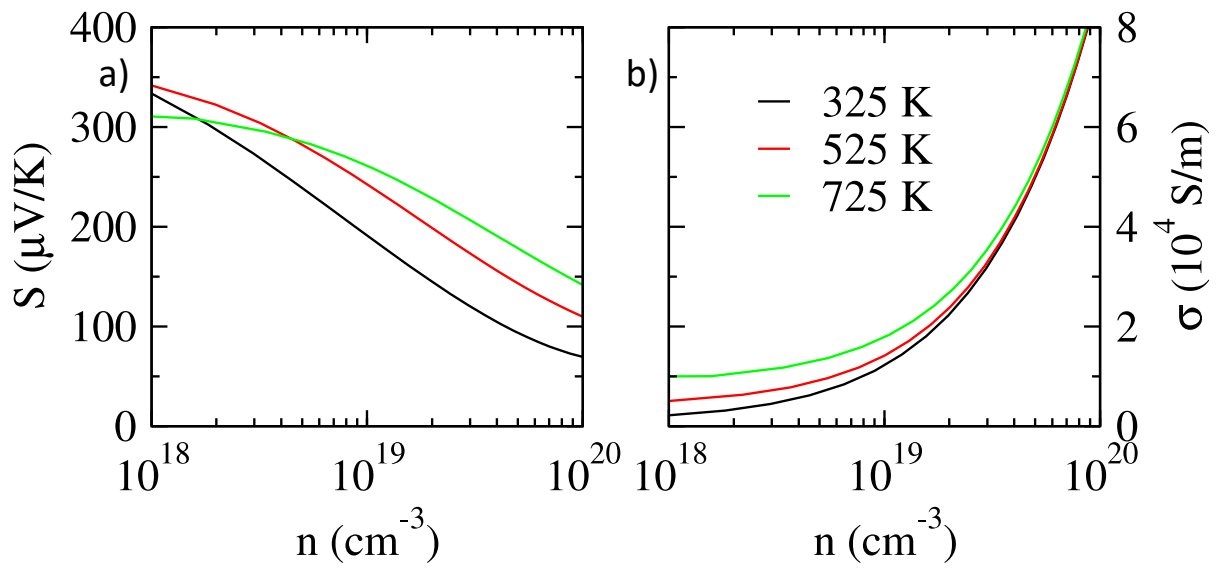


Figure S3. Theoretical DFT studies of (a)  $S$  vs.  $n$  and (b)  $\sigma$  vs.  $n$ .

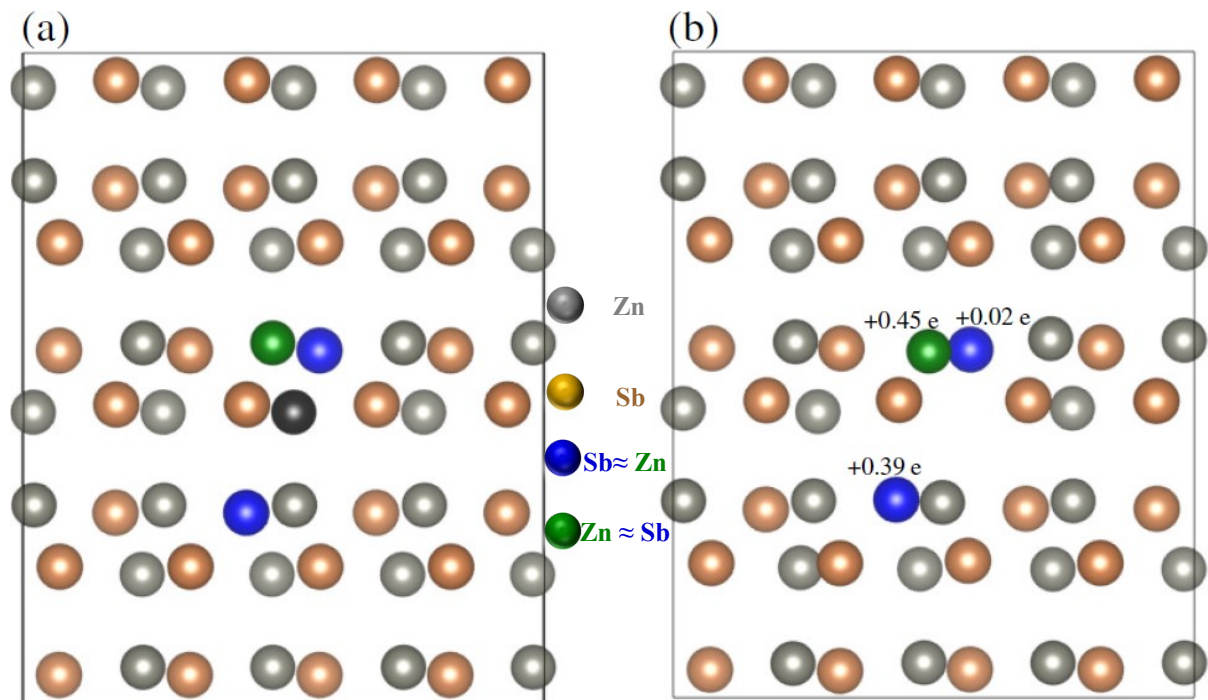


Figure S4. The supercell of  $2 \times 2 \times 1$  for (a) ZnSb and (b)  $\text{Zn}_{0.94}\text{Sb}$ . Here, plus sign stands for the charge gain. Blue atoms represent the nearest Sb atoms and green is the nearest Zn atom to the vacancy.

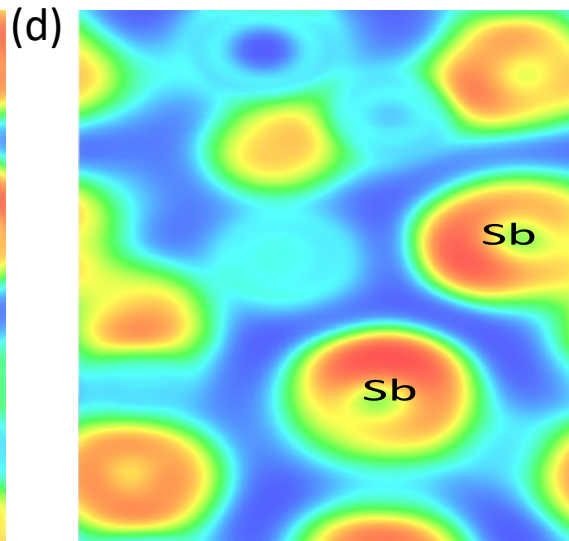
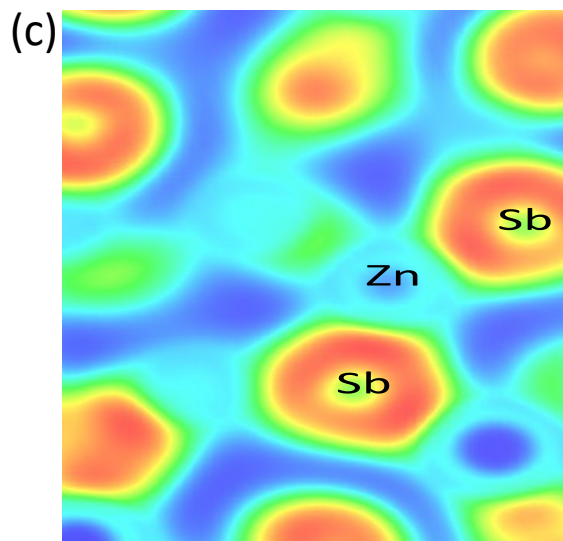
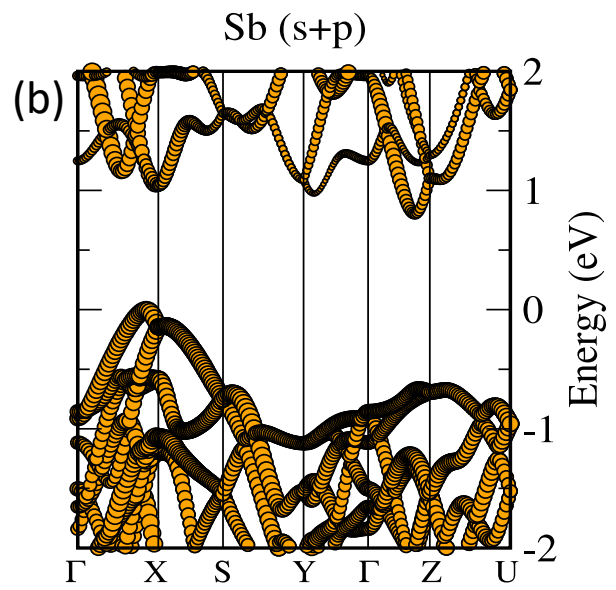
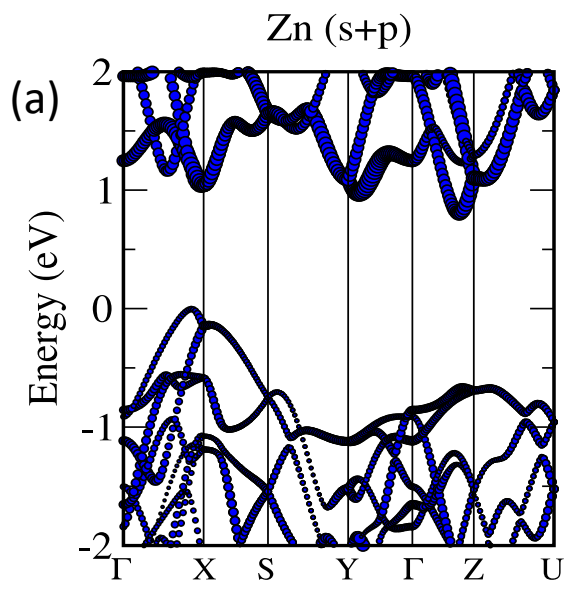


Figure S5 (a) & (b) Electronic structure of Zn (s+p) and Sb (s+p) orbitals shown in E vs.  $k$  diagram, (c) Hole density mapping of orthorhombic ZnSb and (d) Hole density map of  $\text{Zn}_{0.94}\text{Sb}$

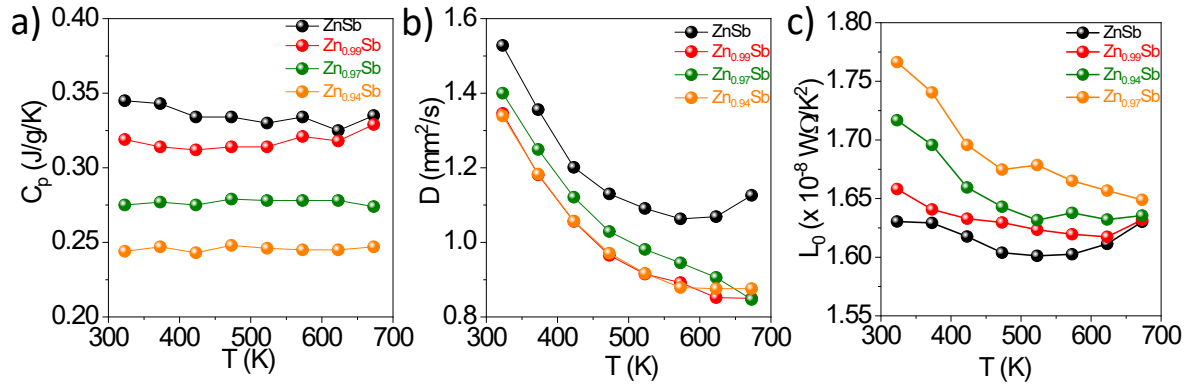


Figure S6. Temperature-dependent (a) Specific heat capacity; (b) Thermal diffusivity and (c) Lorentz number for  $\text{Zn}_{1-x}\text{Sb}$  ( $x = 0, 0.01, 0.03$  and  $0.06$ ).

The Lorenz number was calculated using simple parabolic band model with function temperature using following relation,

$$L = \left(\frac{k_B}{e}\right)^2 \cdot \left\{ \frac{3F_0(\eta)F_2(\eta) - 4F_1(\eta)^2}{F_0(\eta)^2} \right\}$$

Here,  $k_B$ ,  $\eta$  and  $e$  for Boltzmann constant, the reduced chemical potential and charge of an electron respectively. Specifically this model assumes that the carriers are scattered by acoustic phonons. The L values can be measured using the Seebeck coefficient values and the relation between the reduced chemical potential and S is given below

$$S = \left(\frac{k_B}{e}\right) \left\{ \frac{2F_1(\eta)}{F_0(\eta)} - \eta \right\}$$

$$F_i(\eta) = \int_0^{\infty} \frac{\xi^i d\xi}{1 + e^{\xi - \eta}}$$

Where  $F_i(\eta)$  fermi integrals of  $i^{\text{th}}$  order and  $\xi$  denotes the reduced carrier energy. Here Figure S6 (c) , depicts the Lorentz number as a function of temperature as calculated from  $\kappa_{\text{ele}}$  values.

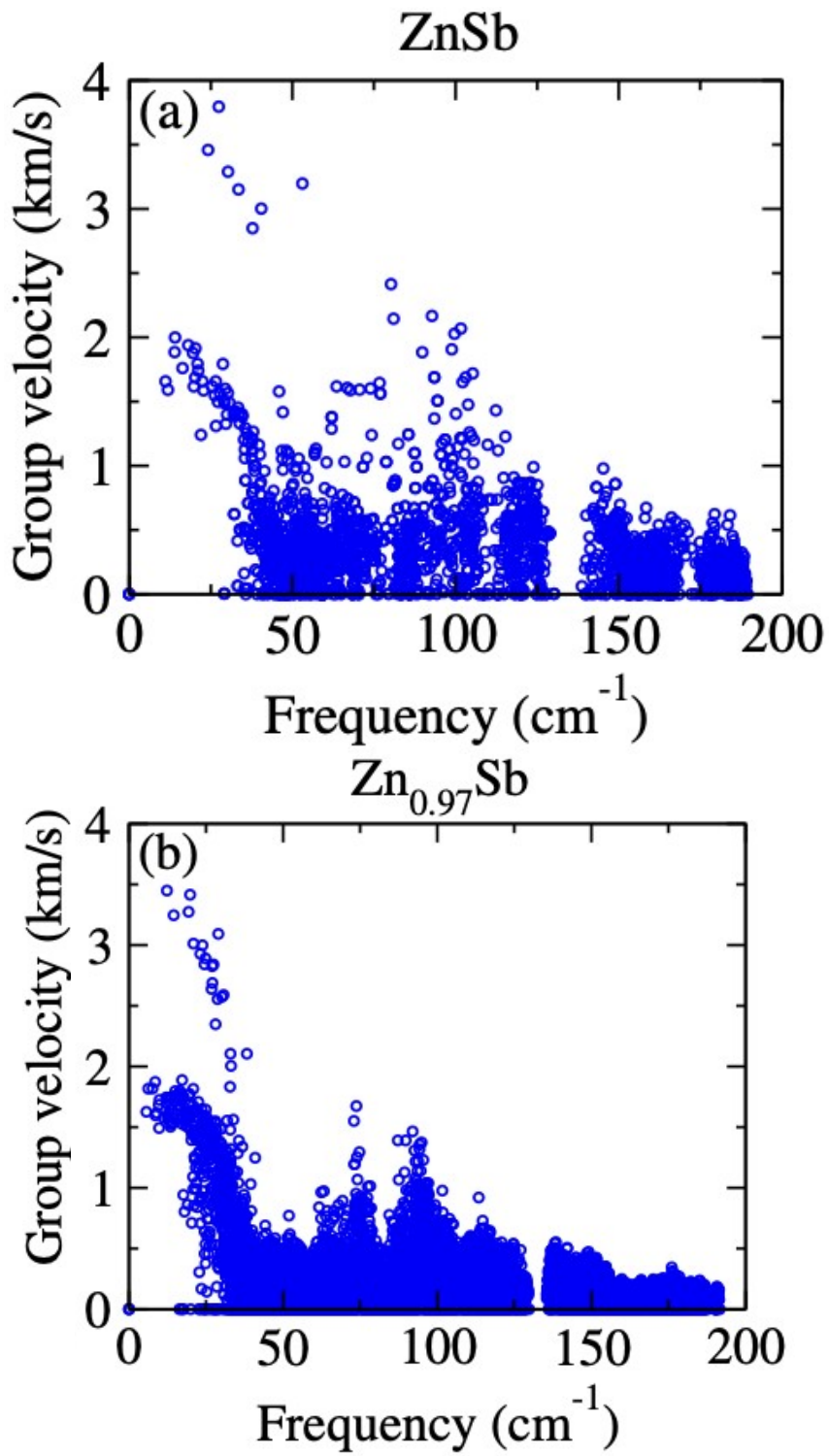


Figure S7. The calculated phonon group velocities (a) ZnSb and (b) Zn<sub>0.94</sub>Sb as a function of phonon frequency.

### The calculation for $ZT_{eng}$ , $PF_{eng}$ , $P_d$ , and $\eta_{max}$

The figure of merit,  $zT$ , of thermoelectric material is an indefinite indicator for determining the conventional thermoelectric conversion efficiency ( $\eta_{max}$ ) because it assumes temperature-independent behavior of  $S$ ,  $\rho = 1/\sigma$ , and  $\kappa_{total}$  in the calculations. H. S. Kim et al.<sup>1</sup> recently proposed the term  $ZT_{eng}$ , a quantitative measure that assesses the effectiveness of thermoelectric (TE) conversion.  $ZT_{eng}$  takes into account the temperature-dependent properties of TE materials. This metric is especially valuable for precisely evaluating the thermoelectric efficiency of material when there is a substantial temperature difference between the cold and hot side of the thermoelectric legs. Here,  $(PF)_{eng}$ ,  $(ZT)_{eng}$ ,  $P_d$ , and  $\eta_{max}$  are calculated using the following relations,

$$(i) \quad zT_{avg} = \frac{S^2(T)}{\rho(T)} * T$$

$$(ii) \quad ((PF))_{eng} = \frac{\left( \int_{T_C}^{T_H} S(T) dT \right)^2}{T_H \int_{T_C}^{T_H} \rho(T) dT} \Delta T \quad \text{in W/mK}^2$$

Where  $\rho(T)$  represents the resistivity,  $S(T)$  represents the Seebeck coefficient,  $\kappa(T)$  represents the total thermal conductivity,  $\eta_C$  represents the Carnot efficiency, and  $\alpha$  represents a dimensionless intensity component of the Thomson coefficient.

$$(iii) \quad (ZT)_{eng} = \frac{((PF))_{eng}}{\int_{T_C}^{T_H} \kappa(T) dT}$$

$$(iv) \quad P_d = \frac{(PF)_{eng} \Delta T}{L} \frac{m_{opt}}{(1 + m_{opt})^2} \text{ in W/cm}^2; \quad m_{opt} = \sqrt{1 + (ZT)_{eng} \left( \alpha / \eta_C - 1/2 \right)}$$

Where  $(PF)_{eng}$  and  $m_{opt}$  are the engineering power factor and optimum ratio of external electrical load ( $R_L$ ) and internal resistance ( $R_{int}$ ).

$$(iv) \quad \eta_{max} = \eta_C \frac{\sqrt{1 + (ZT)_{eng} \left( \alpha / \eta_C - 1/2 \right)} - 1}{\alpha \sqrt{1 + (ZT)_{eng} \left( \alpha / \eta_C - 1/2 \right)} - \eta_C}; \quad \eta_C = \frac{\Delta T}{T_H} \quad \text{and} \quad \alpha = \frac{S(T_H) \Delta T}{\int_{T_C}^{T_H} S(T) dT}$$

References:

(1) H. S. Kim, W. Liu, G. Chen, C.-W. Chu, and Z. Ren, Relationship between



thermoelectric figure of merit and energy conversion efficiency, Proceedings of the National Academy of Sciences, 2015, 112, 8205–8210.