Supplementary Materials

Biomimetic hierarchical porous high entropy alloy for significantly enhancing overall seawater splitting

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Experimental section

Preparation of BHP-HEA cathodes: We chose the spherical AlCoCrFeNi_{2.1} powder prepared by aerosolization by Beijing Yanbang New Materials Technology Co., Ltd as the raw material. The particle size range of the powder is 15-53 μ m, and the particle size distribution is uniform without the satellite particles powder (Fig. S1). In addition, the energy-dispersive spectrometry (EDS) results indicate the distribution of various elements is relatively uniform. Specimens with 10×10×1 mm and porous AlCoCrFeNi_{2.1} HEA are prepared using an SLM machine equipped with a 500 W laser device (FF-M180D). During the printing process, the spot diameter is 120 μ m, the scanning interval is 100 μ m, the laser power is 200 W, and the scanning speed is 600 mm/s. To reduce internal stress and macroscopic porosity, the laser scanning directions of two successive layers differed by 66.7°.To obtain a nanoporous high entropy alloy, the printed precursor alloy is immersed in 0.5 M H₂SO₄ solution for selective phase dissolution. After 48 hours of free corrosion, a nanoporous structure with a dual continuous porous structure is formed on the surface of the precursor.

Microstructure characterization: The X-ray diffraction (XRD, Empyrean) with Cu Ka radiation is used to analyze the phase composition of the electrodes. The scanning electron microscopy (SEM, Zeiss Ultra 55) and transmission electron microscopy (TEM, JSM 2100F) are used to characterize the microstructure of the electrodes, and the chemical composition is analyzed using EDS equipped with them. An X-ray photoelectron spectrometer (XPS, Thermo Scientific ESCALAB 250 XI) is used to determine the types of elements and chemical states on the electrode surface.

Electrochemical measurements: The electrochemical measurements are performed in a conventional three-electrode setup(CHI 660E, Shanghai). The BHP-HEA electrode is used as the working electrode, the Pt sheet is used as the counter electrode, and the Ag/AgCl is used as the reference electrode. To ensure the accuracy of the experiment, all potentials are iR-corrected according to the equation $E_{\text{RHE}}=E_{\text{Ag/AgCl}}+0.198+0.059$ pH. The polarization curve measurements are conducted at a scanning speed of 5 mV s⁻¹. In addition, EIS analysis is measured in a frequency ranging from 10 MHz to 100 kHz frequency with an AC signal amplitude of 5 mV. The overall seawater splitting performance is measured using a two-electrode system, and stability tests are conducted under constant current density at 100 mA cm⁻².

Electrochemical active surface area (ECSA) measurements and calculation: The ECSA is calculated through performing the capacitive current associated with doublelayer charging from the scan-rate dependence of CV. The CV of all samples is conducted with different scan rate in non-faradic potential window. The ECSA is evaluated in terms of double layer capacitance (C_{dl} in mF): ECSA = C_{dl}/C_s . The ECSA is determined assuming a C_{dl} capacitance of 40 µF cm⁻².

Specific activity and Turnover frequency (TOF):

The specific activity is obtained by normalizing the apparent current to ECSA. Specific activity is calculated as follows:¹ Specific activity = $j \times A/ECSA$. Where j is the current density, A is the surface area, ECSA is the electrochemical surface area of the catalyst. The turnover frequency (TOF) are calculated using the following formula:

$$TOF_{HER} = \frac{I}{2 \times F \times n}$$
$$TOF_{OER} = \frac{I}{4 \times F \times n}$$

Where *I* is the current, F is the Faraday's constant (96485.3 C/mol), *n* is the number of active sites.

Faraday efficiency (FE): The Faraday efficiency of water splitting refers to the ratio of the gas produced during the electrolysis process to the theoretical yield. It is an important indicator for measuring the efficiency and purity of the electrolysis process. The faradaic yield is calculated from the ratio of $V_{\text{experimental}}$ to $V_{\text{theoretical}}$ during the charge transport process.²

$$FE_{\text{HER}} = \frac{V_{\text{experimental}}}{V_{\text{theoretical}}} = \frac{V_{\text{experimental}}}{\frac{1}{2} \times \frac{Q}{F} \times V_{m}}$$

$$FE_{\text{OER}} = \frac{V_{\text{experimental}}}{V_{\text{theoretical}}} = \frac{V_{\text{experimental}}}{\frac{1}{4} \times \frac{Q}{F} \times V_{m}}$$

where Q is the charge passed through the electrode, F is Faraday constant (96485 C/mol), V_m is the molar volume of gas (24.5 L/mol, 298 K, 101 KPa).



Fig. S1 (a)SEM morphologies of AlCoCrFeNi $_{2.1}$ powders. (b) Corresponding EDS mapping.



Fig. S2 (a)The microscopic morphology of porous AlCoCrFeNi $_{2.1}$ HEA. (b)The microscopic morphology of BHP-HEA



Fig. S3 TEM image and corresponding EDS elemental mappings of the AlCoCrFeNi_{2.1} HEA.



Fig. S4 (a-c) CV curves at scan rates of 20, 40, 60, 80, 100, and 120 mV s⁻¹ for Precursor alloy (a), NP-HEA (b), BHP-HEA (c). (d-f) Double layer capacitance for Precursor alloy (d), NP-HEA (e), and BHP-HEA (f).



Fig. S5 (a, b) LSV curves and corresponding Tafel plots for OER in 1 M KOH. (c, d) LSV curves and corresponding Tafel plots for HER in 1 M KOH.



Fig. S6 Overpotential of electrodes in seawater and KOH at the same current density.



Fig. S7 (a) LSV curves for OER before and after 2000 cyclic voltammograms. (b) LSV curves for HER before and after 2000 cyclic voltammograms. (c) The CA curves recorded at 50 mA cm⁻² of BHP-HEA electrode for 20 h. (d) The CA curves recorded at 10 mA cm⁻² of BHP-HEA electrode for 20 h.



Fig. S8 (a) XRD characterization for electrode after 20 h for OER test in seawater. (b) XRD characterization for electrode after 20 h for HER test in seawater.



Fig. S9 The stability test results of overall seawater splitting.



Fig. S10 Faradaic efficiency of the BHP-HEA electrolyze.

| | or as princed, for the | i, and bin mentered | |
|------------|-------------------------|---------------------|---------------------|
| Catalysts | ECSA (cm ²) | $TOF_{OER}(s^{-1})$ | $TOF_{HER}(s^{-1})$ |
| As-printed | 160.5 | 0.08 | 0.02 |
| NP-HEA | 407.5 | 0.317 | 0.158 |
| BHP-HEA | 487.5 | 0.375 | 0.187 |

Table S1. ECSA and TOF of as-printed , NP-HEA, and BHP-HEA electrode.

| Element/at.% | Al | Co | Cr | Fe | Ni |
|--------------|-------|-------|-------|-------|-------|
| As-printed | 16.23 | 17.64 | 16.40 | 17.26 | 32.47 |
| After SPD | 12.64 | 17.85 | 17.29 | 18.59 | 33.63 |
| After OER | 12.45 | 17.40 | 18.63 | 17.80 | 33.36 |
| After HER | 12.27 | 17.43 | 19.03 | 17.83 | 33.44 |

 Table S2. Different metal contents in the HEA electrode before and after stability tests.

| compared with those previously reported educitysis. | | | | | | | |
|---|-----------------------------|--------------------|-----------|--|--|--|--|
| Catalysts | Electrolyte | Voltage (V @ mA | Ref | | | | |
| | | cm ⁻²) | | | | | |
| BHP HEA | Seawater | 1.53@100 | This work | | | | |
| NiTe@FeOOH | Seawater | 1.79@100 | [3] | | | | |
| NiFeP-NW-OER | simulated seawater | 1.57@100 | [4] | | | | |
| C@CoP-FeP/FF | simulated alkaline seawater | 1.73@100 | [5] | | | | |
| NiMoO4@NiFeP | 1 M KOH + seawater | 1.71@100 | [6] | | | | |
| MoN-Co ₂ N/NF | 1 M KOH + seawater | 1.70@100 | [7] | | | | |
| Pd _{0.2} Ni ₅₈ Fe ₃₀ O _{11.8} | alkaline seawater | 1.76@100 | [8] | | | | |
| Mo-CoP _x /NF | 1 M KO+0.5 M NaCl | 2.01@100 | [9] | | | | |
| (NiFeCoV)S ₂ /NF | 1 M KOH + seawater | 1.77@100 | [10] | | | | |
| S-NiMoO4@NiFe-LDH | 1 M KOH + seawater | 1.73@100 | [11] | | | | |
| Co-Fe ₂ P | simulated alkaline seawater | 1.84@100 | [12] | | | | |
| NiFe-PBA-gel-cal | alkaline freshwater | 1.66@100 | [13] | | | | |
| Ru SAs-MoO _{3-x} /NF | alkaline seawater | 1.76@100 | [14] | | | | |
| NiS@FeNiP/NF | 1 M KOH + seawater | 1.64@100 | [15] | | | | |
| RuO ₂ -Ti ₃ C ₂ /NF | 1 M KOH + seawater | 1.84@100 | [16] | | | | |

Table S3. The cell voltages to achieve 100 mA cm^{-2} for the GHP-HEA electrode, compared with those previously reported catalysts.

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