# Water vapor effect on the physico-geometrical reaction pathway and kinetics of the multistep thermal dehydration of calcium chloride dihydrate 

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## S1. Water vapor effect on the reaction pathway

Weibull function

$$
\begin{equation*}
F(t)=a_{0}\left(\frac{a_{3}-1}{a_{3}}\right)^{\frac{1-a_{3}}{a_{3}}}\left\{\frac{t-a_{1}}{a_{2}}+\left(\frac{a_{3}-1}{a_{3}}\right)^{\frac{1}{a_{3}}}\right\}^{a_{3}-1} \exp \left[-\left\{\frac{t-a_{1}}{a_{2}}+\left(\frac{a_{3}-1}{a_{3}}\right)^{\frac{1}{a_{3}}}\right\}^{a_{3}}+\frac{a_{3}-1}{a_{3}}\right] \tag{S1}
\end{equation*}
$$

where $a_{0}$ is the amplitude, $a_{1}$ is the center, $a_{2}$ is the width, and $a_{3}$ is the shape parameters.


Figure S1. MDA results for the thermal dehydration process of CC-DH ( $m_{0}=3.01 \pm 0.04 \mathrm{mg}$ ) to form CC-AH under linear nonisothermal conditions at various $\beta$ values in a stream of wet $\mathrm{N}_{2}$ with $p\left(\mathrm{H}_{2} \mathrm{O}\right)=0.8 \mathrm{kPa}$.


Figure S2. MDA results for the thermal dehydration process of CC-DH ( $m_{0}=3.02 \pm 0.06 \mathrm{mg}$ ) to form CC-AH under linear nonisothermal conditions at various $\beta$ values in a stream of wet $\mathrm{N}_{2}$ with $p\left(\mathrm{H}_{2} \mathrm{O}\right)=1.8 \mathrm{kPa}$.


Figure S3. MDA results for the thermal dehydration process of CC-DH ( $m_{0}=3.03 \pm 0.05 \mathrm{mg}$ ) to form CC-AH under linear nonisothermal conditions at various $\beta$ values in a stream of wet $\mathrm{N}_{2}$ with $p\left(\mathrm{H}_{2} \mathrm{O}\right)=4.2 \mathrm{kPa}$.


Figure S4. MDA results for the thermal dehydration process of CC-DH ( $m_{0}=3.02 \pm 0.04 \mathrm{mg}$ ) to form CC-AH under linear nonisothermal conditions at various $\beta$ values in a stream of wet $\mathrm{N}_{2}$ with $p\left(\mathrm{H}_{2} \mathrm{O}\right)=7.5 \mathrm{kPa}$.

(b)


Figure S5. TG curves for hydration process of CC-AH under linear cooling at $1 \mathrm{~K} \mathrm{~min}^{-1}$ in a stream of wet $\mathrm{N}_{2}\left(q_{\mathrm{v}}\right.$ $=200 \mathrm{~cm}^{3} \mathrm{~min}^{-1}$ ): (a) typical measurement scheme for the rehydration process and (b) TG curves at various $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values. Measurements were performed using a humidity-controlled TG system constructed by coupling TG-DTA (TG8122, Rigaku) and a humidity controller (me-40DP-2PHW, Micro Equipment Co.). Initially, the CC-DH sample (300-500 $\mu \mathrm{m}, m_{0}$ : approximately 3.0 mg ) was heated to 473 K at a $\beta$ of $5 \mathrm{~K} \mathrm{~min}^{-1}$ in a stream of dry $\mathrm{N}_{2}$ and subsequently cooled to a temperature of $423-408 \mathrm{~K}$ at a cooling rate of $5 \mathrm{~K} \mathrm{~min}{ }^{-1}$.

## S2. Kinetics of the component reaction steps at different $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values



Figure S6. An example of TG-DTG measurement conducted for the two-step thermal dehydration process of CCDH to form CC-AH via CC-MH recorded by heating the sample ( $m_{0}=3.084 \mathrm{mg}$ ) according to two-step isothermal heating program in a stream of wet $\mathrm{N}_{2}$ with $p\left(\mathrm{H}_{2} \mathrm{O}\right)=1.8 \mathrm{kPa}$.


Figure S7. Kinetic curves for the first reaction step of the two-step thermal dehydration of CC-DH to form CC-AH via CC-MH (thermal dehydration of CC-DH to form CC-MH) under linear nonisothermal conditions at various $\beta$ values in a stream of wet $\mathrm{N}_{2}$ with different $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values, extracted from the overall two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH using MDA: (a) 0.8 , (b) 1.8 , (c) 4.2 , and (d) 7.5 kPa .


Figure S8. Kinetic curves for the second reaction step of the two-step thermal dehydration of CC-DH to form CCAH via CC-MH (thermal dehydration of CC-MH to form CC-AH) under linear nonisothermal conditions at different $\beta$ values in a stream of wet $\mathrm{N}_{2}$ with different $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values, extracted from the overall two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH using MDA: (a) 0.8 , (b) 1.8 , (c) 4.2 , and (d) 7.5 kPa .


Figure S9. Kinetic curves for the first reaction step of the two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH (thermal dehydration of CC-DH to form CC-MH) under isothermal and linear nonisothermal conditions at various $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values, represented in the 3D kinetic coordinate of $T^{-1}, \alpha_{1}$, and $\ln \left(\mathrm{d} \alpha_{1} / \mathrm{d} t\right)$ : (a) 0.8 , (b) 1.8 , (c) 4.2 , and (d) 7.5 kPa .


Figure S10. Kinetic curves for the second reaction step of the two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH (thermal dehydration of CC-MH to form CC-AH) under isothermal and linear nonisothermal conditions at various $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values, represented in the 3 D kinetic coordinate of $T^{-1}$, $\alpha_{2}$, and $\ln \left(\mathrm{d} \alpha_{2} / \mathrm{d} t\right)$ : (a) 0.8 , (b) 1.8 , (c) 4.2 , and (d) 7.5 kPa .


Figure S11. Friedman plots at different $\alpha_{1}$ for the first reaction step of the two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH (thermal dehydration of CC-DH to form CC-MH) at various $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values: (a) 0.8 , (b) 1.8 , (c) 4.2 , and (d) 7.5 kPa .


Figure S12. Friedman plots at different $\alpha_{2}$ for the second reaction step of the two-step thermal dehydration of CCDH to form CC-AH via CC-MH (thermal dehydration of CC-MH to form $\mathrm{CC}-\mathrm{AH}$ ) at various $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values: (a) 0.8 , (b) 1.8 , (c) 4.2 , and (d) 7.5 kPa .


Figure S13. Apparent linear correlations observed between $\ln A_{i}$ and $E_{\mathrm{a}, i}$ values established for the first and second reaction steps of the thermal dehydration process of $\mathrm{CC}-\mathrm{DH}$ to form $\mathrm{CC}-\mathrm{AH}$ via $\mathrm{CC}-\mathrm{MH}$ using the conventional Friedman plot and master plot methods.

## S3. Kinetic modeling based on IP-SR-PBR( $n$ ) models

Table S1. Differential kinetic equations of IP-SR-PBR( $n$ ) models
$n \quad \frac{\mathrm{~d} \alpha}{\mathrm{~d} t}=$
$1 \quad$ a) $t-1 / k_{\mathrm{IP}} \leq 1 / k_{\operatorname{PBR}(1)}$ :

$$
k_{\mathrm{PBR}(1)}\left[1-\exp \left(-k_{\mathrm{SR}}\left(t-\frac{1}{k_{\mathrm{IP}}}\right)\right)\right]
$$

b) $t-1 / k_{\mathrm{IP}} \geq 1 / k_{\mathrm{PBR}(1)}$ :

$$
k_{\mathrm{PBR}(1)} \exp \left(-k_{\mathrm{SR}}\left(t-\frac{1}{k_{\mathrm{IP}}}\right)\right)\left[\exp \left(\frac{k_{\mathrm{SR}}}{k_{\mathrm{PBR}(1)}}\right)-1\right]
$$

2 a) $t-1 / k_{\mathrm{IP}} \leq 1 / k_{\operatorname{PBR}(2)}$ :

$$
-2 k_{\mathrm{PBR}(2)}\left[\left(1+\frac{k_{\mathrm{PBR}(2)}}{k_{\mathrm{SR}}}\right) \exp \left(-k_{\mathrm{SR}}\left(t-\frac{1}{k_{\mathrm{IP}}}\right)\right)+k_{\mathrm{PBR}(2)}\left(t-\frac{1}{k_{\mathrm{IP}}}\right)-\left(1+\frac{k_{\mathrm{PBR}(2)}}{k_{\mathrm{SR}}}\right)\right]
$$

b) $t-1 / k_{\mathrm{IP}} \geq 1 / k_{\mathrm{PBR}(2)}$ :

$$
-2 k_{\mathrm{PBR}(2)} \exp \left(-k_{\mathrm{SR}}\left(t-\frac{1}{k_{\mathrm{IP}}}\right)\right)\left[1+\frac{k_{\mathrm{PBR}(2)}}{k_{\mathrm{SR}}}-\frac{k_{\mathrm{PBR}(2)}}{k_{\mathrm{SR}}} \exp \left(\frac{k_{\mathrm{SR}}}{k_{\mathrm{PBR}(2)}}\right)\right]
$$

$3 \quad$ a) $t-1 / k_{\mathrm{IP}} \leq 1 / k_{\mathrm{PBR}(3)}$ :

$$
\begin{aligned}
-3 k_{\mathrm{PBR}(3)}[(1+ & \left.2 \frac{k_{\mathrm{PBR}(3)}}{k_{\mathrm{SR}}}+2\left(\frac{k_{\mathrm{PBR}(3)}}{k_{\mathrm{SR}}}\right)^{2}\right) \exp \left(-k_{\mathrm{SR}}\left(t-\frac{1}{k_{\mathrm{IP}}}\right)\right)-\left(-k_{\mathrm{PBR}(3)}\left(t-\frac{1}{k_{\mathrm{IP}}}\right)\right)^{2} \\
+ & \left.2 k_{\mathrm{PBR}(3)}\left(\frac{k_{\mathrm{PBR}(3)}}{k_{\mathrm{SR}}}+1\right)\left(t-\frac{1}{k_{\mathrm{IP}}}\right)-\left(1+2 \frac{k_{\mathrm{PBR}(3)}}{k_{\mathrm{SR}}}+2\left(\frac{k_{\mathrm{PBR}(3)}}{k_{\mathrm{SR}}}\right)^{2}\right)\right]
\end{aligned}
$$

b) $t-1 / k_{\mathrm{IP}} \geq 1 / k_{\mathrm{PBR}(3)}$ :

$$
3 k_{\mathrm{PBR}(3)} \exp \left(-k_{\mathrm{SR}}\left(t-\frac{1}{k_{\mathrm{IP}}}\right)\right)\left[2\left(\frac{k_{\mathrm{PBR}(3)}}{k_{\mathrm{SR}}}\right)^{2}\left(\exp \left(\frac{k_{\mathrm{SR}}}{k_{\mathrm{PBR}(3)}}\right)-1\right)-\left(1+2 \frac{k_{\mathrm{PBR}(3)}}{k_{\mathrm{SR}}}\right)\right]
$$



Figure S14. Typical fitting results using SR-PBR(2) model for the first reaction step of the two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH (thermal dehydration of CC-DH to form CC-MH) under isothermal conditions at various $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values: (a) 0.8 , (b) 1.8 , (c) 4.2 , and (d) 7.5 kPa .


Figure S15. Typical fitting results using IP-SR-PBR(2) model for the second reaction step of the two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH (thermal dehydration of CC-MH to form CC-AH) under isothermal conditions at various $p\left(\mathrm{H}_{2} \mathrm{O}\right.$ ) values: (a) 0.8 , (b) 1.8 , (c) 4.2 , and (d) 7.5 kPa .

## Supplementary Information

Table S2. Optimized rate constants of the $\operatorname{SR}-\operatorname{PBR}(n)$ models for the first reaction step of the two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH (thermal dehydration of CC-DH to form CC-MH) at various temperatures and $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values

| model | $p\left(\mathrm{H}_{2} \mathrm{O}\right) / \mathrm{kPa}$ | T/K | Rate constant |  |  | $\mathrm{R}^{2, a}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\boldsymbol{k}_{\text {IP, } / 1 / \mathbf{s}^{-1}}$ | $\boldsymbol{k}_{\text {SR, }, 1 / \mathbf{s}^{-1}}$ | $\boldsymbol{k}_{\operatorname{PBR}(n), 1 / \mathbf{s}^{\mathbf{- 1}}}$ |  |
| SR-PBR(3) | 0.8 | 356.7 | ------ | $3.75 \times 10^{-3}$ | $3.67 \times 10^{-4}$ | 0.9922 |
|  |  | 354.6 | ------ | $3.05 \times 10^{-3}$ | $2.90 \times 10^{-4}$ | 0.9948 |
|  |  | 352.5 | ------ | $1.86 \times 10^{-3}$ | $1.82 \times 10^{-4}$ | 0.9946 |
|  |  | 350.3 | ------ | $1.51 \times 10^{-3}$ | $1.30 \times 10^{-4}$ | 0.9848 |
|  |  | 347.8 | ------ | $9.65 \times 10^{-4}$ | $6.24 \times 10^{-5}$ | 0.9822 |
|  |  | 345.3 | ------ | $7.39 \times 10^{-4}$ | $3.70 \times 10^{-5}$ | 0.9789 |
|  | 1.7 | 368.8 | ------ | $3.62 \times 10^{-3}$ | $5.68 \times 10^{-4}$ | 0.9965 |
|  |  | 366.5 | ------ | $1.74 \times 10^{-3}$ | $4.02 \times 10^{-4}$ | 0.9910 |
|  |  | 362.4 | ------ | $6.02 \times 10^{-4}$ | $1.50 \times 10^{-4}$ | 0.9741 |
|  |  | 361.4 | ------ | $5.88 \times 10^{-4}$ | $1.41 \times 10^{-4}$ | 0.9903 |
|  |  | 359.4 | ------ | $3.68 \times 10^{-4}$ | $7.12 \times 10^{-5}$ | 0.9726 |
|  | 4.1 | 387.8 | ------ | $5.83 \times 10^{-3}$ | $1.48 \times 10^{-3}$ | 0.9353 |
|  |  | 382.4 | ------ | $2.22 \times 10^{-3}$ | $5.65 \times 10^{-4}$ | 0.9690 |
|  |  | 378.5 | ------ | $7.26 \times 10^{-4}$ | $1.91 \times 10^{-4}$ | 0.9211 |
|  | 7.4 | 402.3 | ------ | $8.44 \times 10^{-3}$ | $2.05 \times 10^{-3}$ | 0.9427 |
|  |  | 400.3 | ------ | $4.07 \times 10^{-3}$ | $1.00 \times 10^{-3}$ | 0.9860 |
|  |  | 398.0 | ------ | $2.19 \times 10^{-3}$ | $5.94 \times 10^{-4}$ | 0.9960 |
|  |  | 395.5 | ------ | $2.21 \times 10^{-3}$ | $3.57 \times 10^{-4}$ | 0.9955 |
|  |  | 392.7 | -- | $7.54 \times 10^{-4}$ | $1.51 \times 10^{-4}$ | 0.9957 |
| SR-PBR(2) | 0.8 | 356.7 | ------ | $4.55 \times 10^{-3}$ | $4.98 \times 10^{-4}$ | 0.9921 |
|  |  | 354.6 | ------ | $4.32 \times 10^{-3}$ | $3.63 \times 10^{-4}$ | 0.9963 |
|  |  | 352.5 | ------ | $2.61 \times 10^{-3}$ | $2.28 \times 10^{-4}$ | 0.9964 |
|  |  | 350.3 | ------ | $2.34 \times 10^{-3}$ | $1.74 \times 10^{-4}$ | 0.9941 |
|  |  | 347.8 | ------ | $1.61 \times 10^{-3}$ | $8.00 \times 10^{-5}$ | 0.9753 |
|  |  | 345.3 | ------ | $1.23 \times 10^{-3}$ | $4.77 \times 10^{-5}$ | 0.9876 |
|  | 1.7 | 368.8 | ------ | $3.59 \times 10^{-3}$ | $7.72 \times 10^{-4}$ | 0.9944 |
|  |  | 366.5 | ------ | $1.99 \times 10^{-3}$ | $5.01 \times 10^{-4}$ | 0.9975 |
|  |  | 362.4 | ------ | $6.65 \times 10^{-4}$ | $1.91 \times 10^{-4}$ | 0.9864 |
|  |  | 361.4 | ------ | $7.18 \times 10^{-4}$ | $1.70 \times 10^{-4}$ | 0.9943 |
|  |  | 359.4 | ------ | $3.30 \times 10^{-4}$ | $1.03 \times 10^{-4}$ | 0.9867 |
|  | 4.1 | 387.8 | ------ | $6.82 \times 10^{-3}$ | $1.83 \times 10^{-3}$ | 0.9869 |
|  |  | 382.4 | ------ | $2.39 \times 10^{-3}$ | $7.32 \times 10^{-4}$ | 0.9831 |
|  |  | 378.5 | ------ | $7.80 \times 10^{-4}$ | $2.51 \times 10^{-4}$ | 0.9423 |
|  | 7.4 | 402.3 | ------ | $9.93 \times 10^{-3}$ | $2.64 \times 10^{-3}$ | 0.9632 |
|  |  | 400.3 | ------ | $5.43 \times 10^{-3}$ | $1.17 \times 10^{-3}$ | 0.9930 |
|  |  | 398.0 | ------ | $3.26 \times 10^{-3}$ | $7.84 \times 10^{-4}$ | 0.9711 |
|  |  | 395.5 | ------ | $2.53 \times 10^{-3}$ | $4.55 \times 10^{-4}$ | 0.9964 |
|  |  | 392.7 | ------ | $1.00 \times 10^{-3}$ | $1.78 \times 10^{-4}$ | 0.9959 |
| ${ }^{\text {a }}$ Determination coefficient of the nonlinear least-squares analysis. |  |  |  |  |  |  |

## Supplementary Information

Table S3. Optimized rate constants of the $\operatorname{IP}-\operatorname{SR}-\operatorname{PBR}(n)$ models for the second reaction step of the two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH (thermal dehydration of CC-MH to form CC$\mathrm{AH})$ at various temperatures and $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values

| model | $p\left(\mathrm{H}_{2} \mathrm{O}\right) / \mathrm{kPa}$ | T/K | Rate constant |  |  | $\mathbf{R}^{2, a}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\boldsymbol{k}_{\mathbf{I P}, 2} / \mathbf{s}^{-1}$ | $k_{\text {SR, } 2 / \mathbf{s}^{-1}}$ | $k_{\operatorname{PBR}(n), 2} / \mathbf{s}^{-1}$ |  |
| IP-SR-PBR(3) | 0.8 | 386.7 | ------ | $6.30 \times 10^{-3}$ | $1.29 \times 10^{-3}$ | 0.9792 |
|  |  | 384.7 | ------ | $3.89 \times 10^{-3}$ | $8.37 \times 10^{-4}$ | 0.9948 |
|  |  | 382.8 | $9.43 \times 10^{-3}$ | $2.38 \times 10^{-3}$ | $4.30 \times 10^{-4}$ | 0.9942 |
|  |  | 380.8 | $5.00 \times 10^{-3}$ | $1.47 \times 10^{-3}$ | $3.05 \times 10^{-4}$ | 0.9916 |
|  |  | 378.9 | $2.75 \times 10^{-3}$ | $8.09 \times 10^{-4}$ | $9.88 \times 10^{-5}$ | 0.9961 |
|  | 1.7 | 394.8 | $1.06 \times 10^{-2}$ | $3.25 \times 10^{-3}$ | $7.43 \times 10^{-4}$ | 0.9903 |
|  |  | 392.4 | $5.00 \times 10^{-3}$ | $2.19 \times 10^{-3}$ | $4.57 \times 10^{-4}$ | 0.9989 |
|  |  | 390.6 | $1.25 \times 10^{-3}$ | $8.93 \times 10^{-4}$ | $1.04 \times 10^{-4}$ | 0.9476 |
|  |  | 390.0 | $7.89 \times 10^{-4}$ | $6.49 \times 10^{-4}$ | $6.37 \times 10^{-5}$ | 0.9250 |
|  | 4.2 | 408.2 | $1.69 \times 10^{-2}$ | $9.19 \times 10^{-3}$ | $1.55 \times 10^{-3}$ | 0.9686 |
|  |  | 406.5 | $7.35 \times 10^{-3}$ | $3.59 \times 10^{-3}$ | $5.85 \times 10^{-4}$ | 0.9941 |
|  |  | 404.5 | $2.85 \times 10^{-3}$ | $1.75 \times 10^{-3}$ | $2.52 \times 10^{-4}$ | 0.9746 |
|  |  | 402.7 | $7.98 \times 10^{-4}$ | --- | ----- | ------ |
|  | 7.5 | 419.6 | $1.11 \times 10^{-2}$ | $9.78 \times 10^{-3}$ | $1.79 \times 10^{-3}$ | 0.9462 |
|  |  | 415.3 | $1.43 \times 10^{-3}$ | $2.26 \times 10^{-3}$ | $5.69 \times 10^{-4}$ | 0.9779 |
|  |  | 413.5 | $9.09 \times 10^{-4}$ | $8.02 \times 10^{-4}$ | $2.76 \times 10^{-4}$ | 0.9811 |
| IP-SR-PBR(2) | 0.8 | 386.7 | ------ | $7.68 \times 10^{-3}$ | $1.60 \times 10^{-3}$ | 0.9872 |
|  |  | 384.7 | ------ | $5.07 \times 10^{-3}$ | $9.84 \times 10^{-4}$ | 0.9989 |
|  |  | 382.8 | $9.43 \times 10^{-3}$ | $3.35 \times 10^{-3}$ | $5.00 \times 10^{-4}$ | 0.9984 |
|  |  | 380.8 | $5.95 \times 10^{-3}$ | $2.32 \times 10^{-3}$ | $3.54 \times 10^{-4}$ | 0.9993 |
|  |  | 378.9 | $2.75 \times 10^{-3}$ | $1.12 \times 10^{-3}$ | $1.16 \times 10^{-4}$ | 0.9940 |
|  | 1.7 | 394.8 | $1.14 \times 10^{-2}$ | $4.53 \times 10^{-3}$ | $8.91 \times 10^{-4}$ | 0.9935 |
|  |  | 392.4 | $5.00 \times 10^{-3}$ | $1.78 \times 10^{-3}$ | $7.04 \times 10^{-4}$ | 0.9959 |
|  |  | 390.6 | $1.25 \times 10^{-3}$ | $1.27 \times 10^{-3}$ | $1.48 \times 10^{-4}$ | 0.9734 |
|  |  | 390.0 | $7.89 \times 10^{-4}$ | $6.49 \times 10^{-4}$ | $6.82 \times 10^{-5}$ | 0.9806 |
|  | 4.2 | 408.2 | $1.69 \times 10^{-2}$ | $7.76 \times 10^{-3}$ | $1.89 \times 10^{-3}$ | 0.9872 |
|  |  | 406.5 | $7.35 \times 10^{-3}$ | $3.77 \times 10^{-3}$ | $7.72 \times 10^{-4}$ | 0.9819 |
|  |  | 404.5 | $3.40 \times 10^{-3}$ | $1.75 \times 10^{-3}$ | $3.67 \times 10^{-4}$ | 0.9799 |
|  |  | 402.7 | $7.98 \times 10^{-4}$ | ------ | ------ | ------ |
|  | 7.5 | 419.6 | $1.11 \times 10^{-2}$ | $9.79 \times 10^{-3}$ | $3.23 \times 10^{-3}$ | 0.9823 |
|  |  | 415.3 | $1.43 \times 10^{-3}$ | $2.47 \times 10^{-3}$ | $7.30 \times 10^{-4}$ | 0.9895 |
|  |  | 413.5 | $9.09 \times 10^{-4}$ | $9.95 \times 10^{-4}$ | $3.38 \times 10^{-4}$ | 0.9851 |

${ }^{\text {a }}$ Determination coefficient of the nonlinear least-squares analysis.


Figure S16. Arrhenius plots of the individual physicogeometrical reaction steps for the first reaction step of the two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH (thermal dehydration of CCDH to form $\mathrm{CC}-\mathrm{MH})$ at varying $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values: (a) SR and (b) PBR(2).


Figure S17. Arrhenius plots of the individual physicogeometrical reaction steps for the second reaction step of the two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH (thermal dehydration of CC-MH to form CC-AH) at varying $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values: (a) IP, (b) SR, and (c) $\operatorname{PBR}(2)$.

## Supplementary Information

Table S4. Apparent Arrhenius parameters of the component physico-geometrical processes involved in the two-step thermal dehydration process of CC-DH to form CC-AH via CC-MH at different $p\left(\mathrm{H}_{2} \mathrm{O}\right)$ values, as determined based on the $\mathrm{SR}-\mathrm{PBR}(2)$ and IP-SR-PBR(2) models

| Reaction step $i$ | Process | $p\left(\mathrm{H}_{2} \mathrm{O}\right) / \mathrm{kPa}$ | $E_{\mathrm{a}, i} / \mathrm{kJ} \mathrm{mol}^{-1}$ | $\ln \left(A_{i} / \mathrm{s}^{-1}\right)$ | $-\gamma^{\text {a }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | SR | 0.8 | $123.4 \pm 10.5$ | $36.3 \pm 3.6$ | 0.9858 |
|  |  | 1.7 | $269.3 \pm 20.1$ | $82.2 \pm 6.6$ | 0.9918 |
|  |  | 4.1 | $283.2 \pm 28.9$ | $82.9 \pm 9.1$ | 0.9948 |
|  |  | 7.4 | $291.7 \pm 26.9$ | $82.5 \pm 8.1$ | 0.9875 |
|  | PBR(2) | 0.8 | $213.6 \pm 12.2$ | $64.5 \pm 4.2$ | 0.9935 |
|  |  | 1.7 | $236.8 \pm 5.9$ | $70.1 \pm 1.9$ | 0.9991 |
|  |  | 4.1 | $258.9 \pm 33.4$ | $74.1 \pm 10.5$ | 0.9918 |
|  |  | 7.4 | $345.2 \pm 25.9$ | $97.1 \pm 7.8$ | 0.9916 |
| 2 | IP | 0.8 | $384.9 \pm 64.6$ | $116.3 \pm 20.4$ | 0.9862 |
|  |  | 1.7 | $724.9 \pm 96.4$ | $216.5 \pm 29.6$ | 0.9828 |
|  |  | 4.2 | $733.3 \pm 152.4$ | $227.0 \pm 45.3$ | 0.9890 |
|  |  | 7.5 | $607.9 \pm 73.2$ | $169.7 \pm 21.2$ | 0.9928 |
|  | SR | 0.8 | $290.6 \pm 24.1$ | $85.6 \pm 7.6$ | 0.9898 |
|  |  | 1.7 | $469.3 \pm 84.9$ | $137.6 \pm 26.1$ | 0.9688 |
|  |  | 4.2 | $558.4 \pm 19.7$ | $159.7 \pm 5.8$ | 0.9994 |
|  |  | 7.5 | $525.0 \pm 60.7$ | $145.9 \pm 17.5$ | 0.9934 |
|  | PBR(2) | 0.8 | $393.3 \pm 43.4$ | $116.0 \pm 13.6$ | 0.9822 |
|  |  | 1.7 | $681.3 \pm 205.4$ | $200.9 \pm 63.0$ | 0.9199 |
|  |  | 4.2 | $611.7 \pm 65.2$ | $173.9 \pm 19.3$ | 0.9944 |
|  |  | 7.5 | $526.0 \pm 27.7$ | $145.1 \pm 8.0$ | 0.9986 |



Figure S18. Apparent linear correlations observed between $\ln A_{i}$ and $E_{\mathrm{a}, i}$ values determined for the individual physico-geometrical reaction processes of the first and second reaction steps of the thermal dehydration process of CC-DH to form CC-AH via CC-MH based on SR-PBR(3) and IP-SR-PBR(3) models, respectively: (a) first and (b) second reaction steps.


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